



An approximate electromagnetic model for superconducting helically wound cables and cable-in-conduit conductors

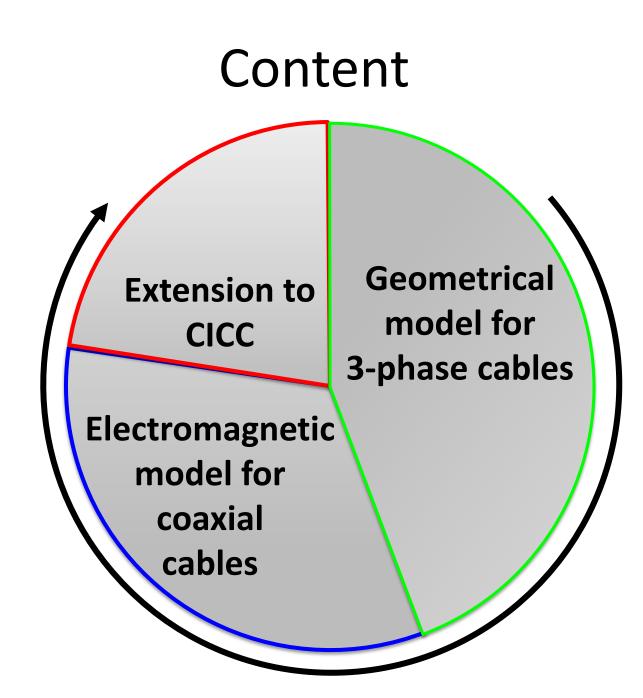
V. Zermeno, F. Grilli

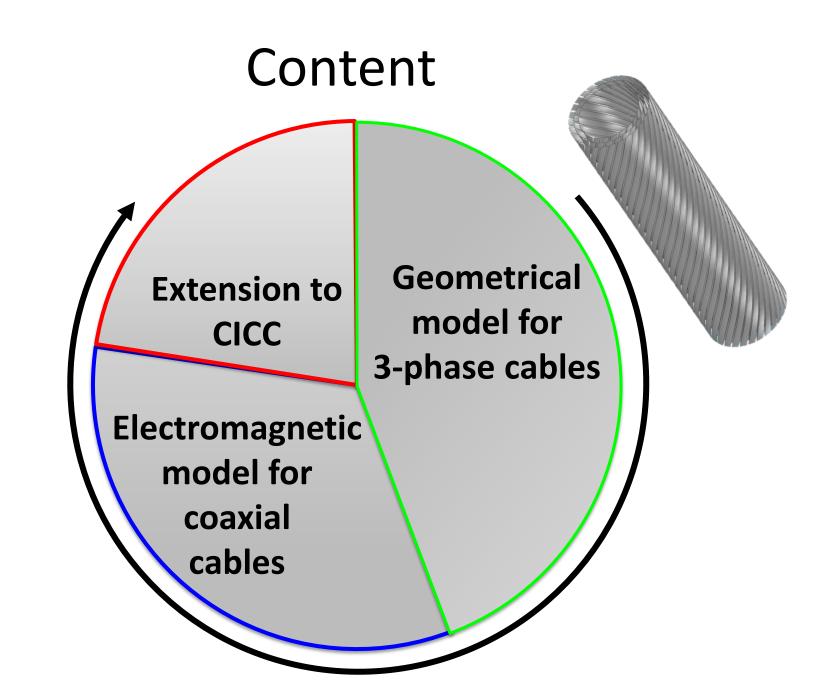
Karlsruhe Institute of Technology

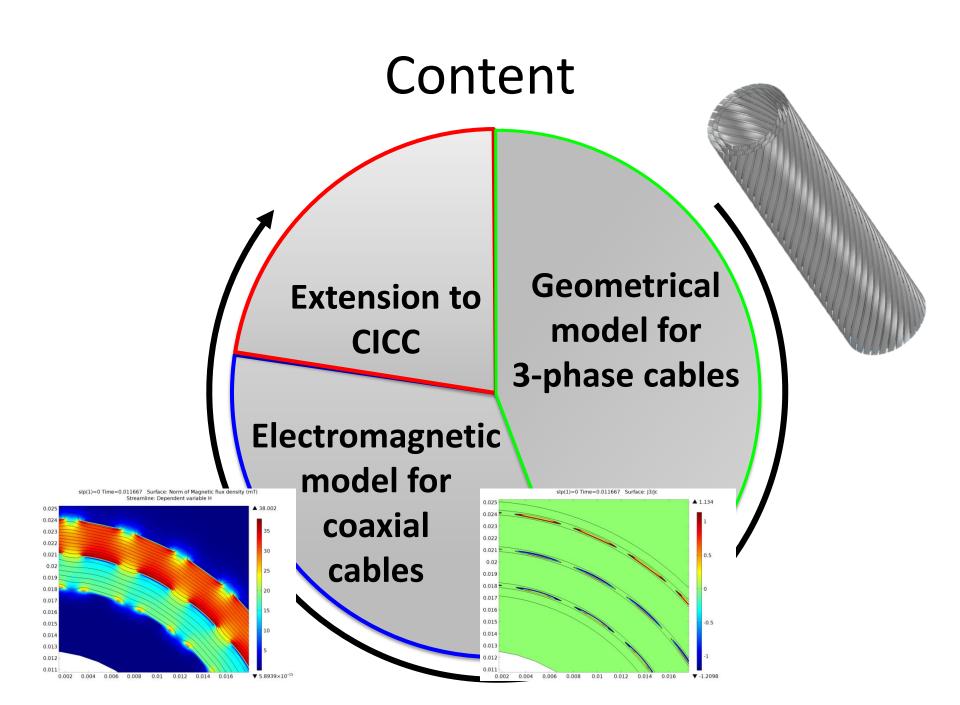
victor.zermeno@kit.edu

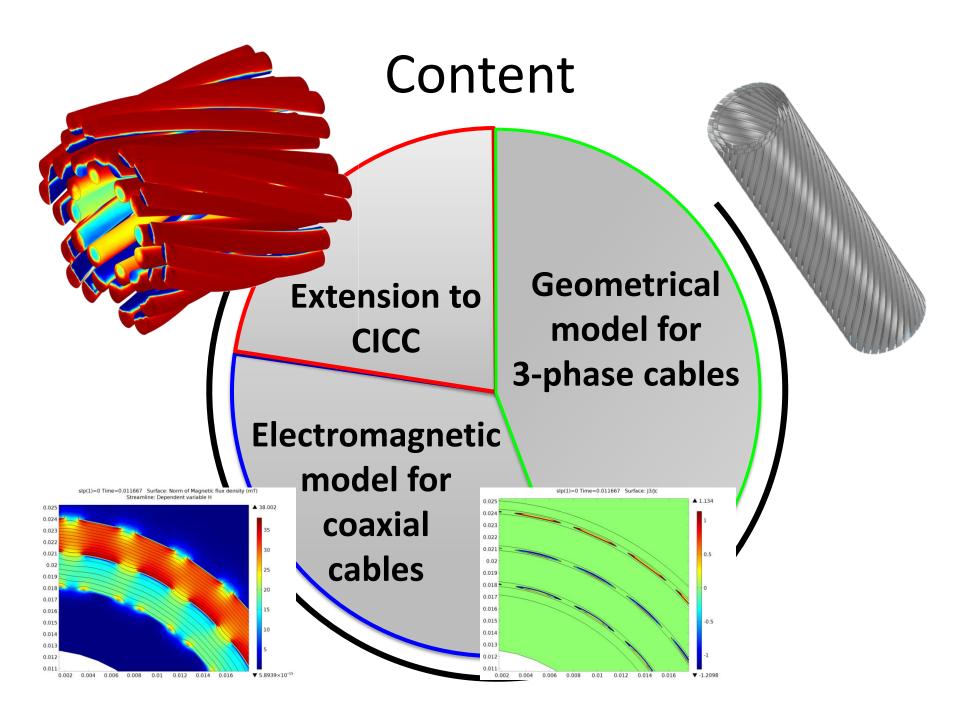
KIT – University of the State of Baden-Wuerttemberg and National Laboratory of the Helmholtz Association

www.kit.edu







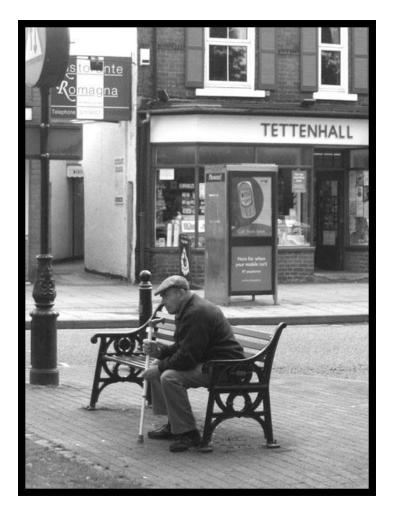


The modeler's dilemma

Real

VS.

Possible Feasible Practical



What is a model?



Analytic Approximation





Numeric Approximation 1





Numeric Approximation 2

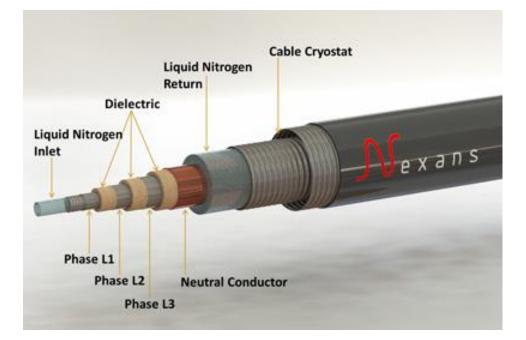




Numeric Approximation 3



Ampacity project





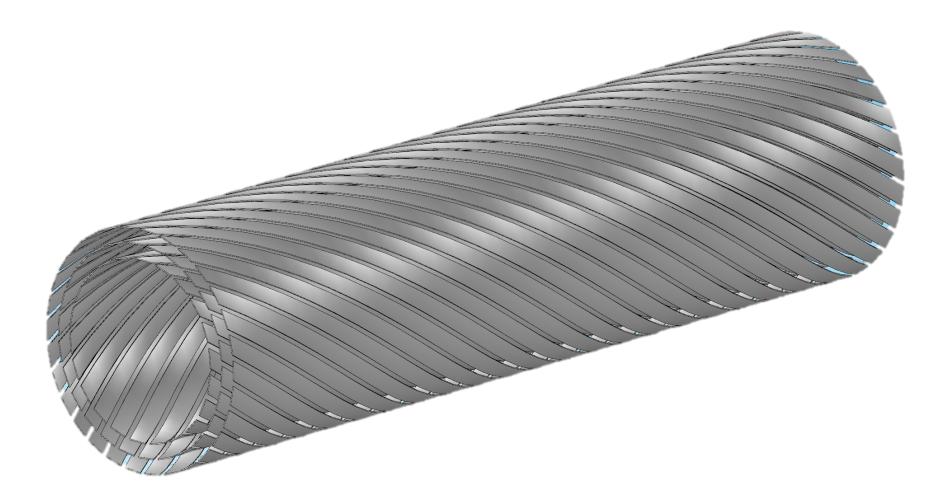
Karlsruher Institut für Technologie



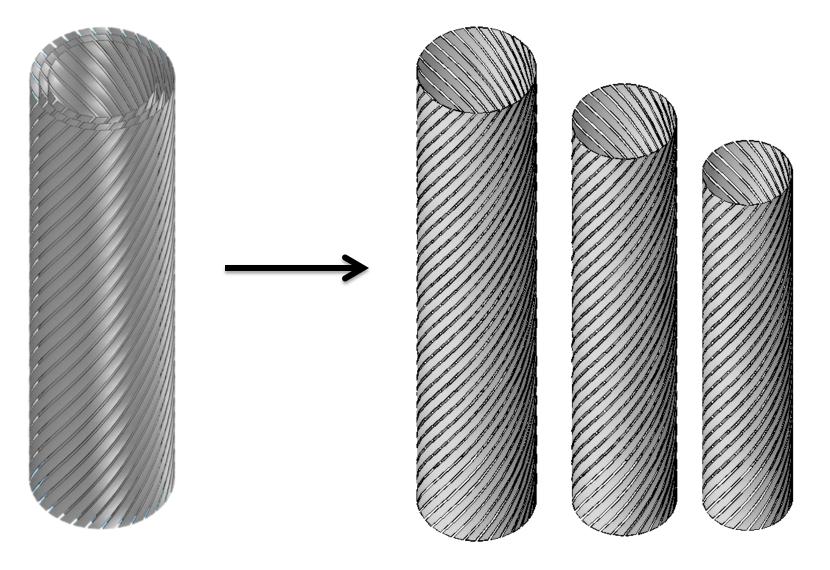
Phase	# of tapes	radius	Pitch angle
А	22	36.1 mm	17.44°
В	26	42.1 mm	17.44°
С	30	48.2 mm	17.44°

How to model a 3-phase helically wound cable?

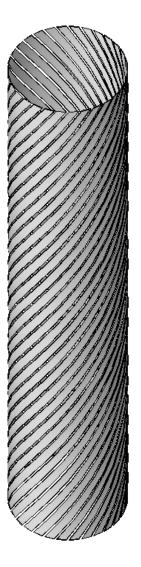
How to model a 3-phase helically wound cable?



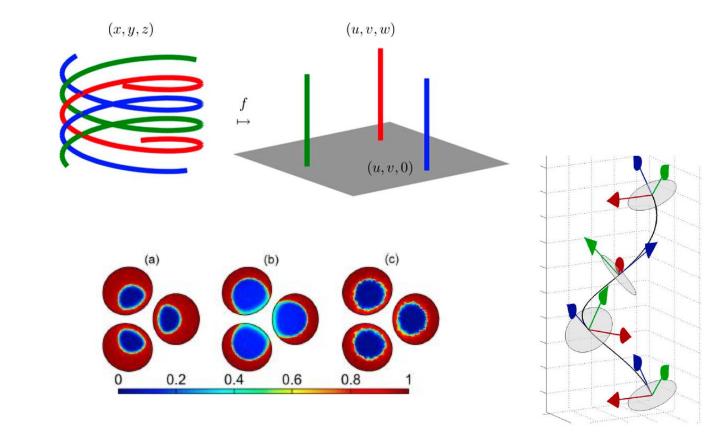
Original model design dissected



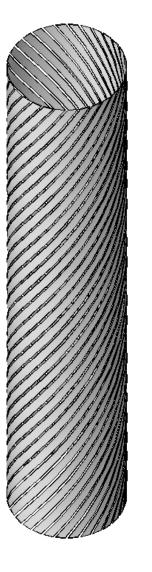
1 pitch length of each phase

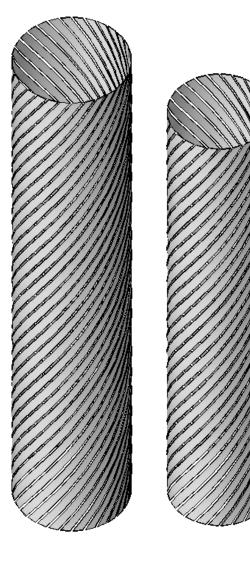


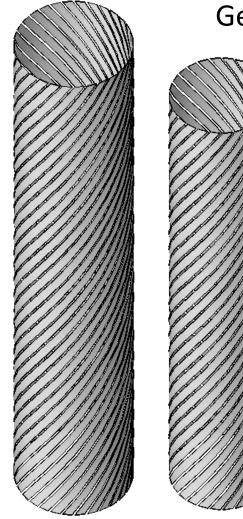
Geometry can be modelled in 2D using helical coordinates



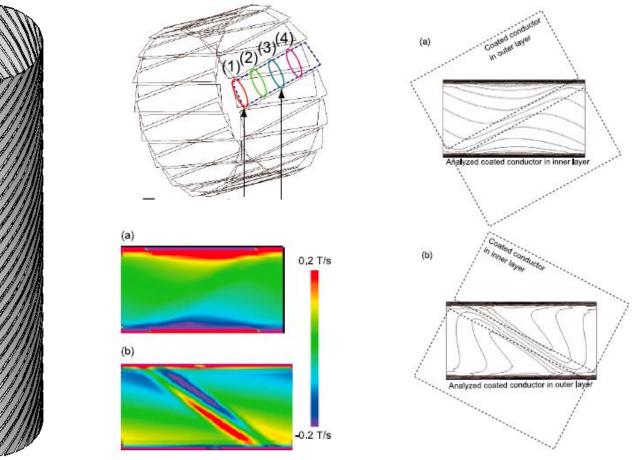
Stenvall, A. et al. IEEE TAS 23 -3 2013



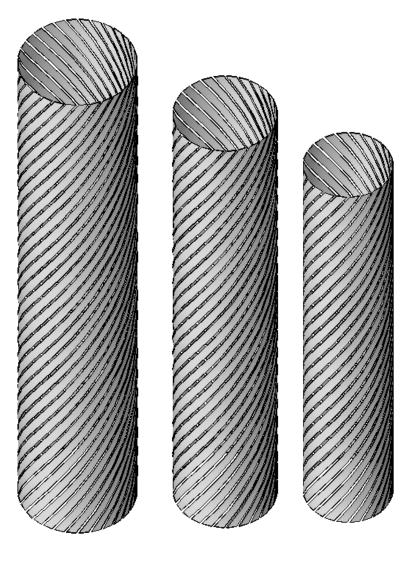




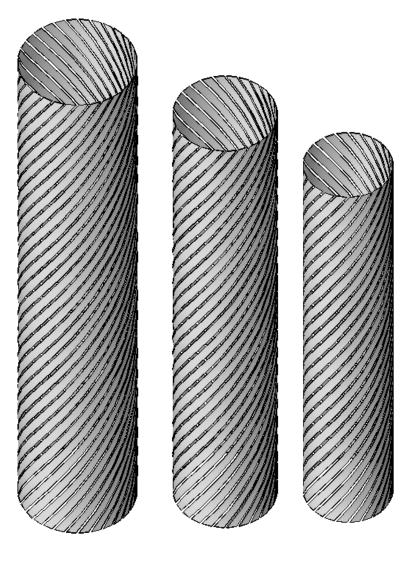
Geometry must be modelled in a small 3D section



K Takeuchi et al Supercond. Sci. Technol. 24 (2011) 085014



Geometry must be modelled in a large 3D section



Geometry must be modelled in a large 3D section?

Model size

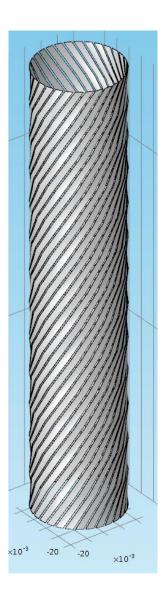
- With constant pitch angle (17.44 deg), there are different pitch lengths for each phase:
 - Phase 1 -> 361.013100007 mm
 - Phase 2 -> **421**.015277294 mm
 - Phase 3 -> 482.017490868 mm

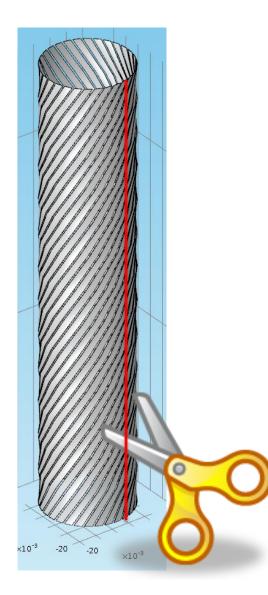
Model size

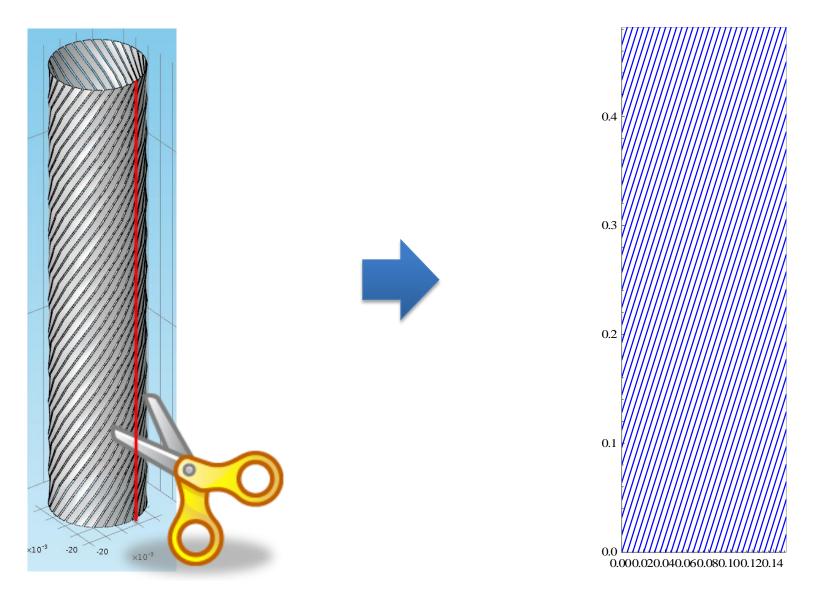
- With constant pitch angle (17.44 deg), there are different pitch lengths for each phase:
 - Phase 1 -> 361.013100007 mm
 - Phase 2 -> 421.015277294 mm
 - Phase 3 -> **482**.017490868 mm
- Lmc(361,421,482)=73254842... so, the spatial period is >73km ^(S)

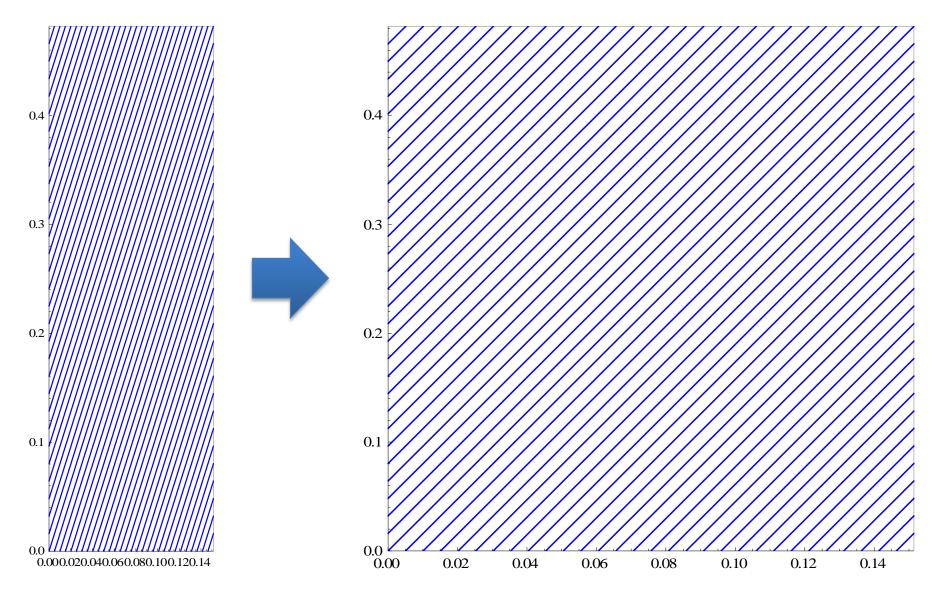
Model size

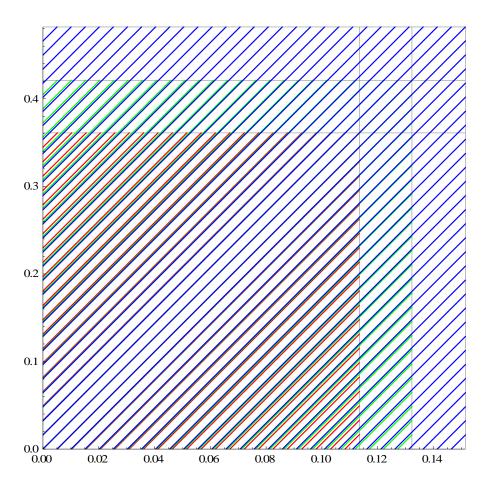
- With constant pitch angle (17.44 deg), there are different pitch lengths for each phase:
 - Phase 1 -> 361.013100007 mm
 - Phase 2 -> 421.015277294 mm
 - Phase 3 -> **482**.017490868 mm
- Assume the tolerance is on our side and approximate the actual layout with something similar ③.

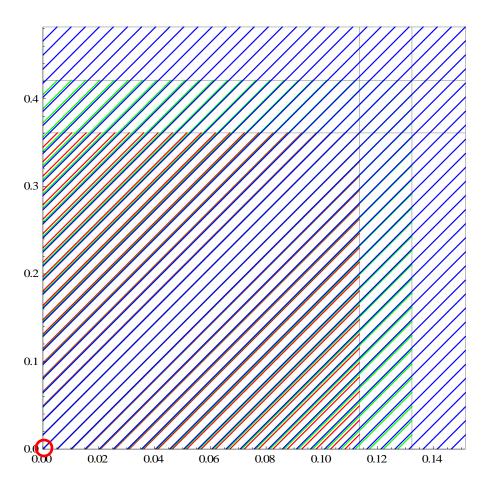




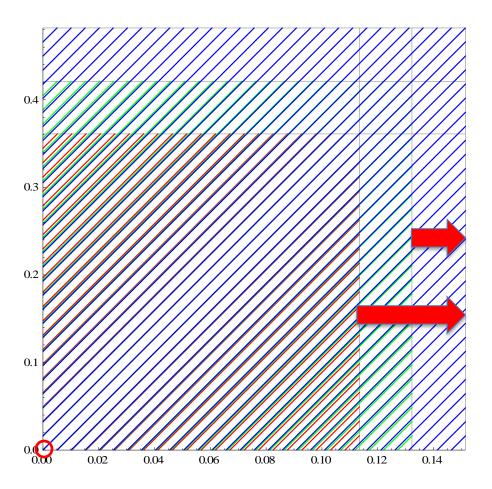




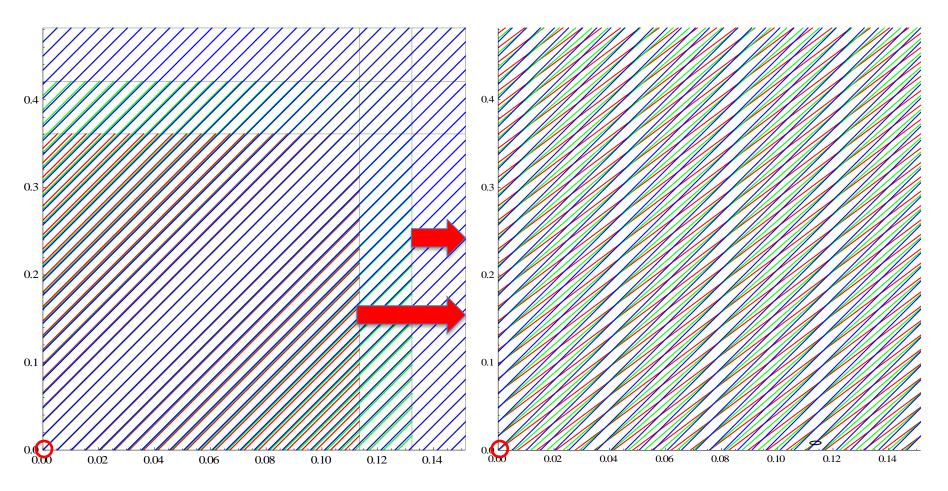




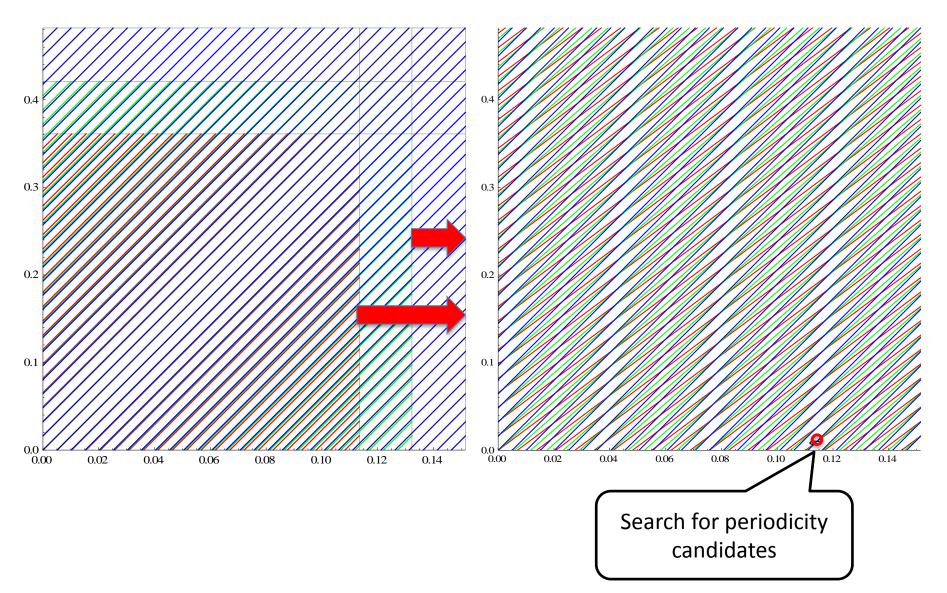
3-phase layout projected



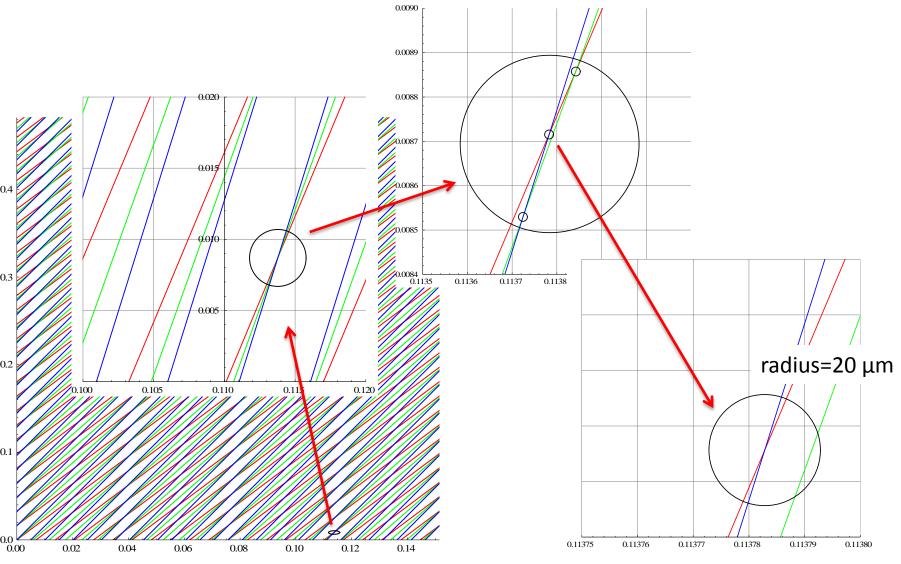
3-phase layout projected



3-phase layout projected

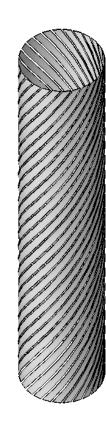


Search for periodicity candidates



Find minimum period per phase







Find minimum period per phase









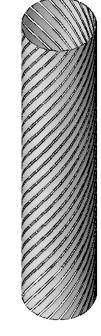




Find minimum period per phase



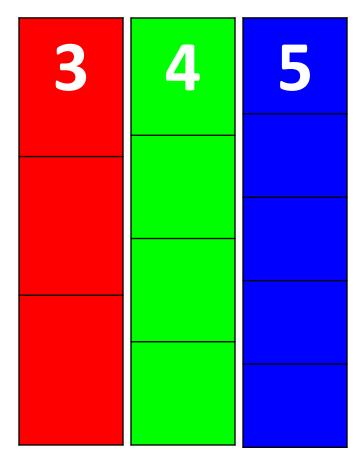






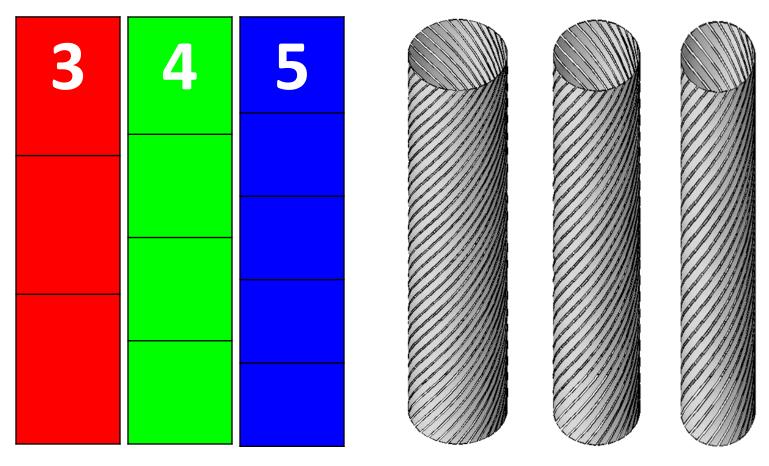
Search for candidate geometries

Use integer combinations of the minimum periods per phase



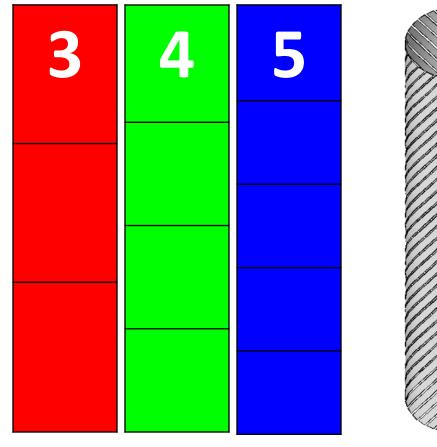
Search for candidate geometries

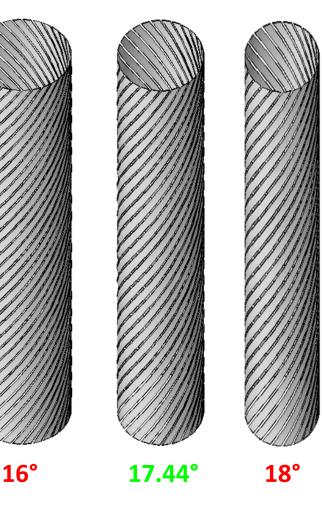
Use integer combinations of the minimum periods per phase



Search for candidate geometries

Use integer combinations of the minimum periods per phase





And test for the corresponding pitch angles

Dispersion[deg]	Ma	ax error(%)	αa[deg]	αb[deg]	αc[deg]	qa	dþ	qc	<pre>Pitch length[m]</pre>	\ddagger of slices
		in pitch angle								
0.195927		1.12343	17.2441	17.44	17.3128	39	40	40	0.647716	120
0.206592		1.18459	17.2334	17.44	17.3128	38	39	39	0.631523	117
0.21782		1.24897	17.2222	17.44	17.3128	37	38	38	0.61533	114
0.219066		1.25611	17.6591	17.44	17.3128	1	1	1	0.0161929	3
0.229657		1.31684	17.2103	17.44	17.3128	36	37	37	0.599137	111
0.242153		1.38849	17.1978	17.44	17.3128	35	36	36	0.582944	108
0.255365		1.46425	17.1846	17.44	17.3128	34	35	35	0.566751	105
0.269356		1.54447	17.1706	17.44	17.3128	33	34	34	0.550558	102
0.284197		1.62957	17.1558	17.44	17.3128	32	33	33	0.534366	99
0.289227		1.65841	17.2334	17.44	17.7292	38	39	40	0.631523	120
0.289227		1.65841	17.6591	17.44	17.7292	39	39	40	0.631523	120
0.299969		1.72	17.14	17.44	17.3128	31	32	32	0.518173	96
0.30016		1.7211	17.2222	17.44	17.7402	37	38	39	0.61533	117
0.30016		1.7211	17.6591	17.44	17.7402	38	38	39	0.61533	117
0.311683		1.78717	17.2103	17.44	17.7517	36	37	38	0.599137	114
0.311683		1.78717	17.6591	17.44	17.7517	37	37	38	0.599137	114
0.316761		1.81629	17.1232	17.44	17.3128	30	31	31	0.50198	93
0.323844		1.8569	17.1978	17.44	17.7638	35	36	37	0.582944	111
0.323844		1.8569	17.6591	17.44	17.7638	36	36	37	0.582944	111
0.334675		1.91901	17.1053	17.44	17.3128	29	30	30	0.485787	90
0.336698		1.93061	17.1846	17.44	17.7767	34	35	36	0.566751	108
0.336698		1.93061	17.6591	17.44	17.7767	35	35	36	0.566751	108
0.350306		2.00863	17.1706	17.44	17.7903	33	34	35	0.550558	105
0.350306		2.00863	17.6591	17.44	17.7903	34	34	35	0.550558	105

¥									
Dispersion[deg]	Max error(%)	αa[deg]	αb[deg]	αc[deg]	qa	dþ	dc	Pitch length[m]	$\mbox{\tt \ddagger}$ of slices
	in pitch angle								
0.195927	1.12343	17.2441	17.44	17.3128	39	40	40	0.647716	120
0.206592	1.18459	17.2334	17.44	17.3128	38	39	39	0.631523	117
0.21782	1.24897	17.2222	17.44	17.3128	37	38	38	0.61533	114
0.219066	1.25611	17.6591	17.44	17.3128	1	1	1	0.0161929	3
0.229657	1.31684	17.2103	17.44	17.3128	36	37	37	0.599137	111
0.242153	1.38849	17.1978	17.44	17.3128	35	36	36	0.582944	108
0.255365	1.46425	17.1846	17.44	17.3128	34	35	35	0.566751	105
0.269356	1.54447	17.1706	17.44	17.3128	33	34	34	0.550558	102
0.284197	1.62957	17.1558	17.44	17.3128	32	33	33	0.534366	99
0.289227	1.65841	17.2334	17.44	17.7292	38	39	40	0.631523	120
0.289227	1.65841	17.6591	17.44	17.7292	39	39	40	0.631523	120
0.299969	1.72	17.14	17.44	17.3128	31	32	32	0.518173	96
0.30016	1.7211	17.2222	17.44	17.7402	37	38	39	0.61533	117
0.30016	1.7211	17.6591	17.44	17.7402	38	38	39	0.61533	117
0.311683	1.78717	17.2103	17.44	17.7517	36	37	38	0.599137	114
0.311683	1.78717	17.6591	17.44	17.7517	37	37	38	0.599137	114
0.316761	1.81629	17.1232	17.44	17.3128	30	31	31	0.50198	93
0.323844	1.8569	17.1978	17.44	17.7638	35	36	37	0.582944	111
0.323844	1.8569	17.6591	17.44	17.7638	36	36	37	0.582944	111
0.334675	1.91901	17.1053	17.44	17.3128	29	30	30	0.485787	90
0.336698	1.93061	17.1846	17.44	17.7767	34	35	36	0.566751	108
0.336698	1.93061	17.6591	17.44	17.7767	35	35	36	0.566751	108
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0									
Dispersion[deg]	Max error(%) in pitch angle	αa[deg]	αb[deg]	αc[deg]	qa	dp	qc	Pitch length[m]	♯ of slices
0.195927	1.12343	17.2441	17.44	17.3128	39	40	40	0.647716	120
0.206592	1.18459	17.2334	17.44	17.3128	38	39	39	0.631523	117
0.21782	1.24897	17.2222	17.44	17.3128	37	38	38	0.61533	114
0.219066	1.25611	17.6591	17.44	17.3128	1	1	1	0.0161929	3
0.229657	1.31684	17.2103	17.44	17.3128	36	37	37	0.599137	111
0.242153	1.38849	17.1978	17.44	17.3128	35	36	36	0.582944	108
0.255365	1.46425	17.1846	17.44	17.3128	34	35	35	0.566751	105
0.269356	1.54447	17.1706	17.44	17.3128	33	34	34	0.550558	102
0.284197	1.62957	17.1558	17.44	17.3128	32	33	33	0.534366	99
0.289227	1.65841	17.2334	17.44	17.7292	38	39	40	0.631523	120
0.289227	1.65841	17.6591	17.44	17.7292	39	39	40	0.631523	120
0.299969	1.72	17.14	17.44	17.3128	31	32	32	0.518173	96
0.30016	1.7211	17.2222	17.44	17.7402	37	38	39	0.61533	117
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0.316761	1.81629	17.1232	17.44	17.3128	30	31	31	0.50198	93
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0.323844	1.8569	17.6591	17.44	17.7638	36	36	37	0.582944	111
0.334675	1.91901	17.1053	17.44	17.3128	29	30	30	0.485787	90
0.336698	1.93061	17.1846	17.44	17.7767	34	35	36	0.566751	108
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									1
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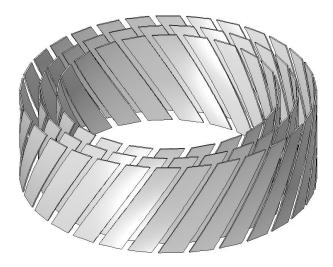
T		1	1	1		I	-		
Dispersion[deg]	Max error(%)	αa[deg]	αb[deg]	αc[deg]	qa	dþ	qc	Pitch length[m]	♯ of slices
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0.195927	1.12343	17.2441	17.44	17.3128	39	40	40	0.647716	120
0.206592	1.18459	17.2334	17.44	17.3128	38	39	39	0.631523	117
0.21782	1.24897	17.2222	17.44	17.3128	37	38	38	0.61533	114
0.219066	1.25611	17.6591	17.44	17.3128	1	1	1	0.0161929	3
0.229657	1.31684	17.2103	17.44	17.3128	36	37	37	0.599137	111
0.242153	1.38849	17.1978	17.44	17.3128	35	36	36	0.582944	108
0.255365	1.46425	17.1846	17.44	17.3128	34	35	35	0.566751	105
0.269356	1.54447	17.1706	17.44	17.3128	33	34	34	0.550558	102
0.284197	1.62957	17.1558	17.44	17.3128	32	33	33	0.534366	99
0.289227	1.65841	17.2334	17.44	17.7292	38	39	40	0.631523	120
0.289227	1.65841	17.6591	17.44	17.7292	39	39	40	0.631523	120
0.299969	1.72	17.14	17.44	17.3128	31	32	32	0.518173	96
0.30016	1.7211	17.2222	17.44	17.7402	37	38	39	0.61533	117
0.30016	1.7211	17.6591	17.44	17.7402	38	38	39	0.61533	117
0.311683	1.78717	17.2103	17.44	17.7517	36	37	38	0.599137	114
0.311683	1.78717	17.6591	17.44	17.7517	37	37	38	0.599137	114
0.316761	1.81629	17.1232	17.44	17.3128	30	31	31	0.50198	93
0.323844	1.8569	17.1978	17.44	17.7638	35	36	37	0.582944	111
0.323844	1.8569	17.6591	17.44	17.7638	36	36	37	0.582944	111
0.334675	1.91901	17.1053	17.44	17.3128	29	30	30	0.485787	90
0.336698	1.93061	17.1846	17.44	17.7767	34	35	36	0.566751	108
0.336698	1.93061	17.6591	17.44	17.7767	35	35	36	0.566751	108
0.350306	2.00863	17.1706	17.44	17.7903	33	34	35	0.550558	105
0.350306	2.00863	17.6591	17.44	17.7903	34	34	35	0.550558	105

- Dignomation [dog]	Marrie anno m (%)			a a [do a]	~~~	arla	~~	Ditch longth[m]	# of aligna
Dispersion[deg]	Max error(%)	αa[deg]	αb[deg]	αc[deg]	qa	αp	dc	Pitch length[m]	♯ of slices
	in pitch angle								
0.195927	1.12343	17.2441	17.44	17.3128	39	40	40	0.647716	120
0.206592	1.18459	17.2334	17.44	17.3128	38	39	39	0.631523	117
0.21782	1.24897	17.2222	17.44	17.3128	37	38	38	0.61533	114
0.219066	1.25611	17.6591	17.44	17.3128	1	1	1	0.0161929	3
0.229657	1.31684	17.2103	17.44	17.3128	36	37	37	0.599137	111
	and the second second second	17.1978	17.44	17.3128	35	36	36	0.582944	108
All Street and Distances	State of the local division of the local div	17.1846	17.44	17.3128	34	35	35	0.566751	105
ALC: N REAL	and the second second	17.1706	17.44	17.3128	33	34	34	0.550558	102
	and the second division of the second divisio	17.1558	17.44	17.3128	32	33	33	0.534366	99
	TITEMAL C	17.2334	17.44	17.7292	38	39	40	0.631523	120
and the second second	successive statements and	17.6591	17.44	17.7292	39	39	40	0.631523	120
	STREET, BLOCK	17.14	17.44	17.3128	31	32	32	0.518173	96
		17.2222	17.44	17.7402	37	38	39	0.61533	117
	and the local division of the local division	17.6591	17.44	17.7402	38	38	39	0.61533	117
States and States in	CONTRACTOR OF STREET, NO. 100	17.2103	17.44	17.7517	36	37	38	0.599137	114
	- Annotation of the local division of the lo	17.6591	17.44	17.7517	37	37	38	0.599137	114
100	and the second se	17.1232	17.44	17.3128	30	31	31	0.50198	93
-TWEEL		17.1978	17.44	17.7638	35	36	37	0.582944	111
- States	Contraction of the local division of the	17.6591	17.44	17.7638	36	36	37	0.582944	111
	1000	17.1053	17.44	17.3128	29	30	30	0.485787	90
And Personnel Pe		17.1846	17.44	17.7767	34	35	36	0.566751	108
Sector and Sector	State of the state	17.6591	17.44	17.7767	35	35	36	0.566751	108
The second second	and the second second	17.1706	17.44	17.7903	33	34	35	0.550558	105
0.350306	2.00863	17.6591	17.44	17.7903	34	34	35	0.550558	105

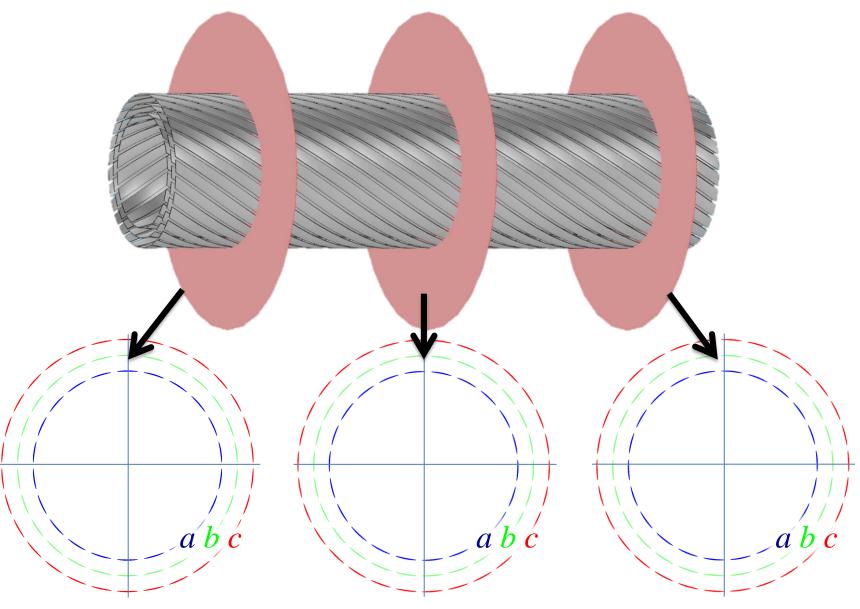
Designs under Dis m

0									
Dispersion[deg]	<pre>Max error(%) in pitch angle</pre>	αa[deg]	αb[deg]	αc[deg]	qa	dþ	dc	Pitch length[m]	$\mbox{\tt \ \ }$ of slices
0.195927	1.12343	17.2441	17.44	17.3128	39	40	40	0.647716	120
0.206592	1.18459	17.2334	17.44	17.3128	38	39	39	0.631523	117
0.21782	1.24897	17.2222	17.44	17.3128	37	38	38	0.61533	114
0.219066	1.25611	17.6591	17.44	17.3128	1	1	1	0.0161929	3
0.229657	1.31684	17.2103	17.44	17.3128	36	37	37	0.599137	111
		17.1978	17.44	17.3128	35	36	36	0.582944	108
	STA	17.1846	17.44	17.3128	34	35	35	0.566751	105
Romacoa		17.1706	17.44	17.3128	33	34	34	0.550558	102
	Real Property lies of the lies	17.1558	17.44	17.3128	32	33	33	0.534366	99
	TETTENHALL	17.2334	17.44	17.7292	38	39	40	0.631523	120
the statement		17.6591	17.44	17.7292	39	39	40	0.631523	120
	E a T	17.14	17.44	17.3128	31	32	32	0.518173	96
		17.2222	17.44	17.7402	37	38	39	0.61533	117
515	100 m 10	17.6591	17.44	17.7402	38	38	39	0.61533	117
	And	17.2103	17.44	17.7517	36	37	38	0.599137	114
	Barris Harrison	17.6591	17.44	17.7517	37	37	38	0.599137	114
		17.1232	17.44	17.3128	30	31	31	0.50198	93
TOT		17.1978	17.44	17.7638	35	36	37	0.582944	111
Nov	CITAN TO CONTRACT	17.6591	17.44	17.7638	36	36	37	0.582944	111
	NOV	17.1053	17.44	17.3128	29	30	30	0.485787	90
		17.1846	17.44	17.7767	34	35	36	0.566751	108
And the second	E State	17.6591	17.44	17.7767	35	35	36	0.566751	108
		17.1706	17.44	17.7903	33	34	35	0.550558	105
0.350306	2.00863	17.6591	17.44	17.7903	34	34	35	0.550558	105

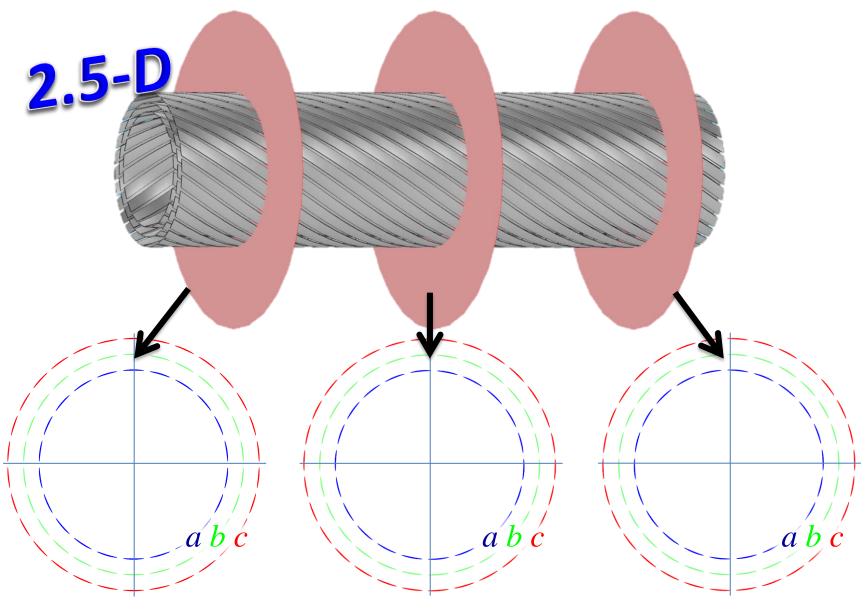
- Using an approximate pitch length of 16.193 mm for each phase:
 - Phase 1 -> 17.659 deg (0.219 deg error)
 - Phase 2 -> 17.44 deg (0 deg error)
 - Phase 3 -> 17.313 deg (0.127 deg error)



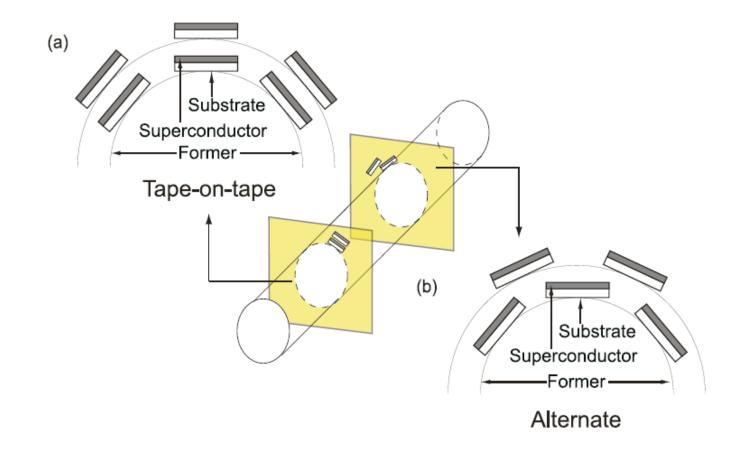
Model of cable by several 2D slices



Model of cable by several 2D slices



Model of cable by two 2-D slices



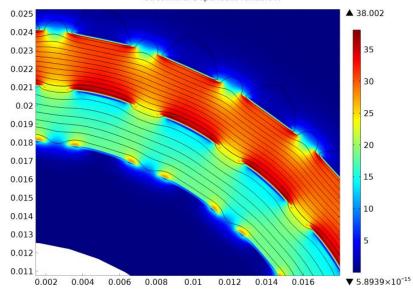
M Nakahata and N Amemiya Supercond. Sci. Technol. 21 (2008) 015007

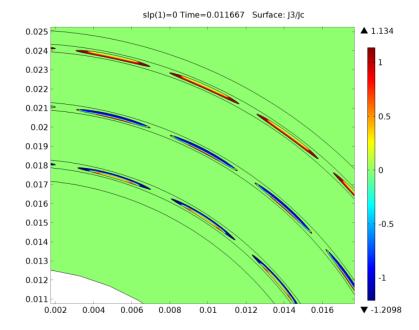
Model of cable by subsequent 2D slices

- Takes into account the different relative position of tapes along length (as a result of the pitch)
- Good results expected for low pitch angles
- Neglects axial field
- Manageable computing time (per slice)

Magnetic flux density and Normalized current density

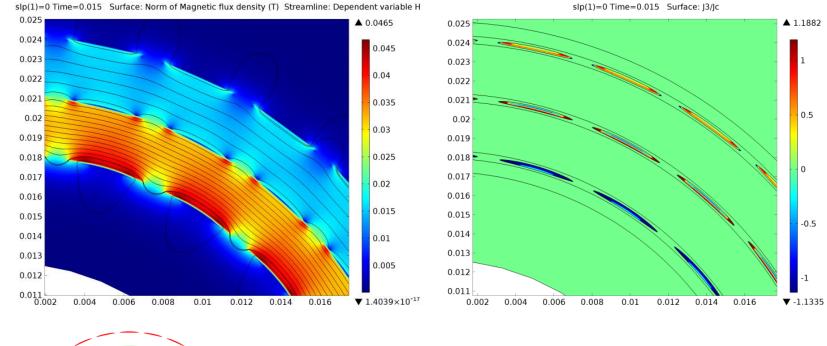
slp(1)=0 Time=0.011667 Surface: Norm of Magnetic flux density (mT) Streamline: Dependent variable H





Using H-formulation, Brambilla et al. SUST 20-1 (2007)

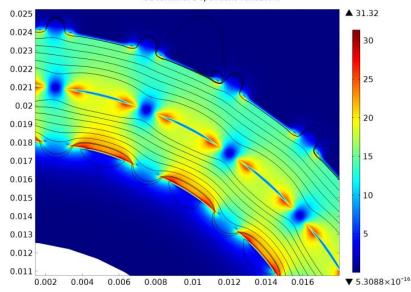
Magnetic flux density and Normalized current density

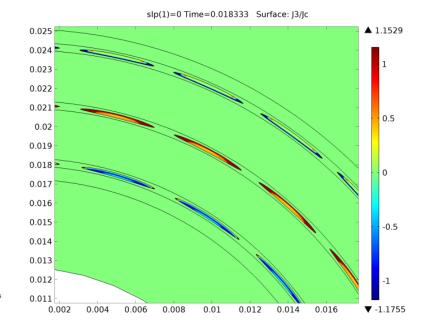


Using H-formulation, Brambilla et al. SUST 20-1 (2007)

Magnetic flux density and Normalized current density

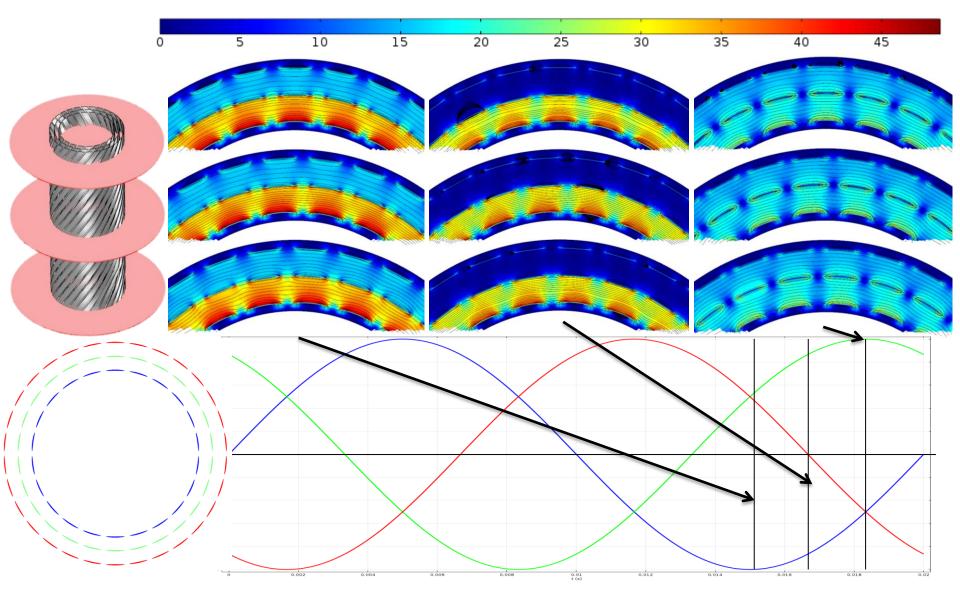
slp(1)=0 Time=0.018333 Surface: Norm of Magnetic flux density (mT) Streamline: Dependent variable H





Using H-formulation, Brambilla et al. SUST 20-1 (2007)

Magnetic field profile in different slices Surface: |B| (mT) Streamlines: (B1,B2)



Assessing the need for several slices

• Magnetic field is almost azimuthal in the interphase region:

For several time steps and several slice positions

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For several time steps and several slice positions

 Computed AC losses using several slices (3-5) provided estimates with less than 0.5% variation.

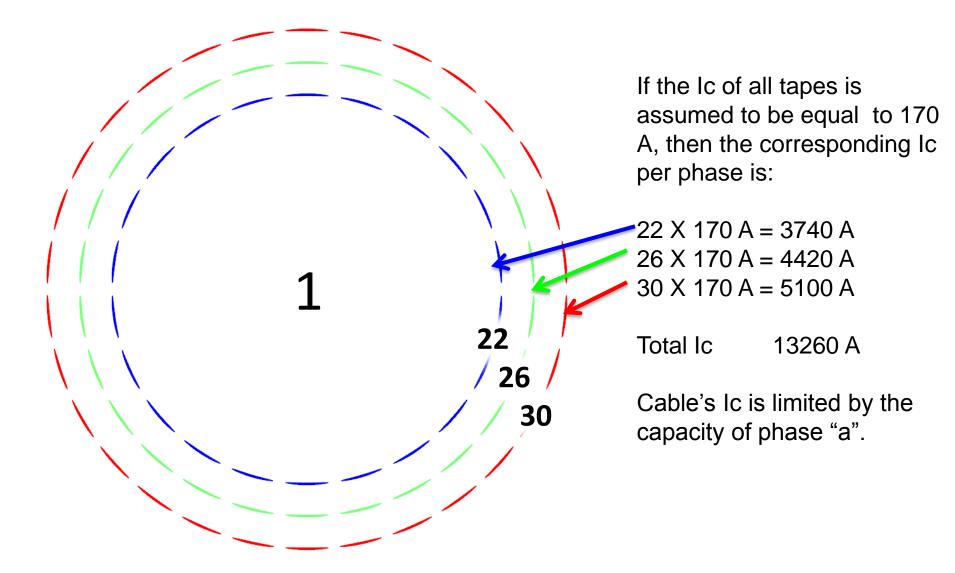
Assessing the need for several slices

• Magnetic field is almost azimuthal in the interphase region:

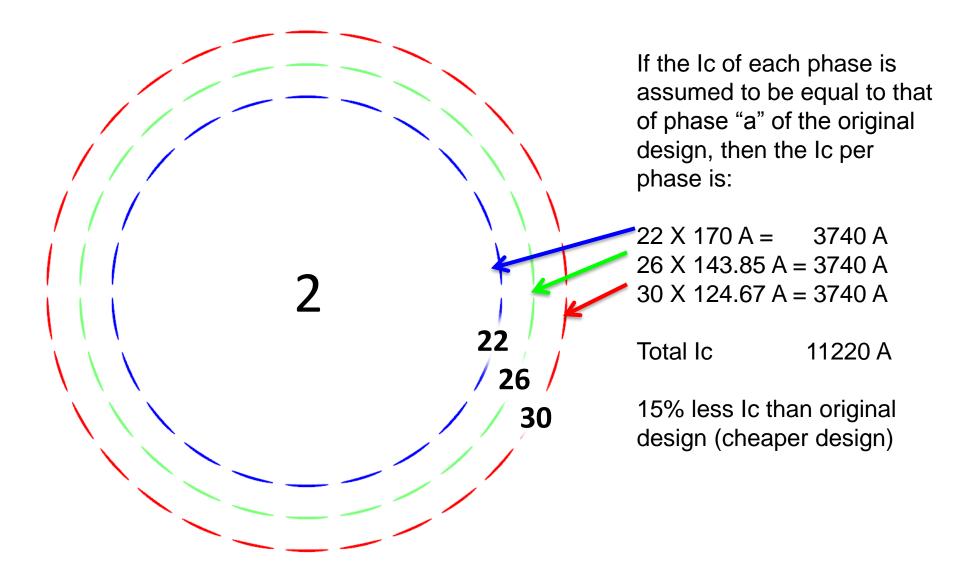
For several time steps and several slice positions

- Computed AC losses using several slices (3-5) provided estimates with less than 0.5% variation.
- One slice can provide accurate estimates.
 Fast time to solution.

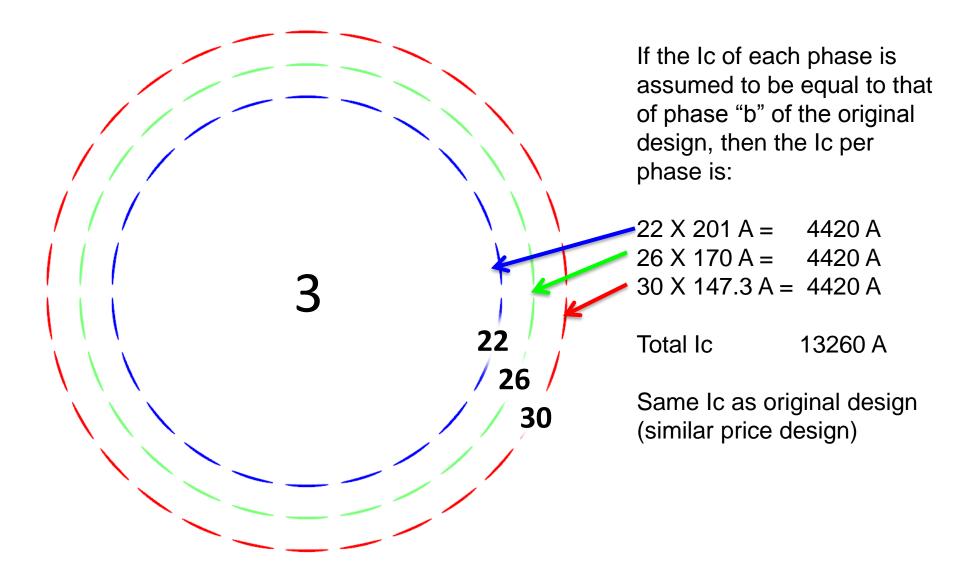
Original design: 1



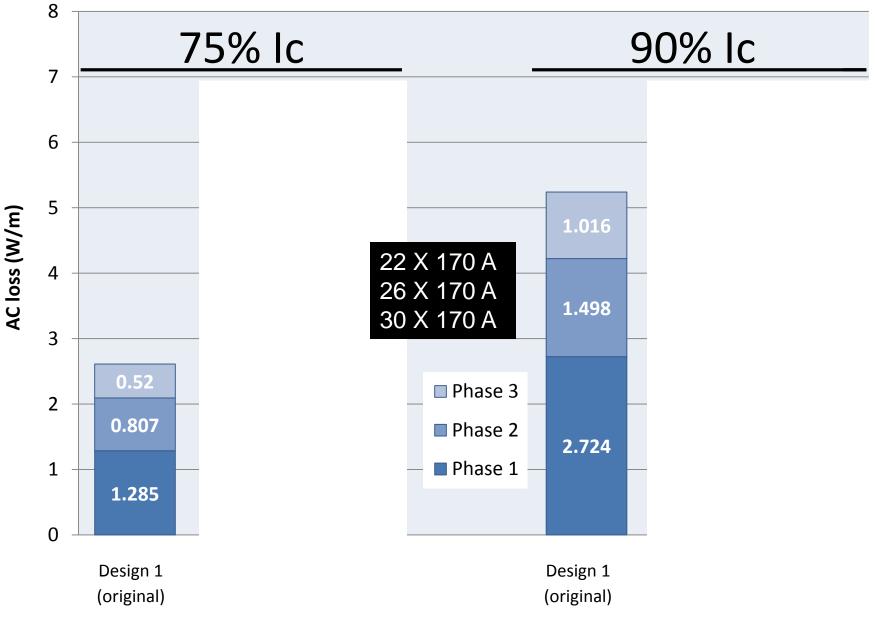
Optional design: 2



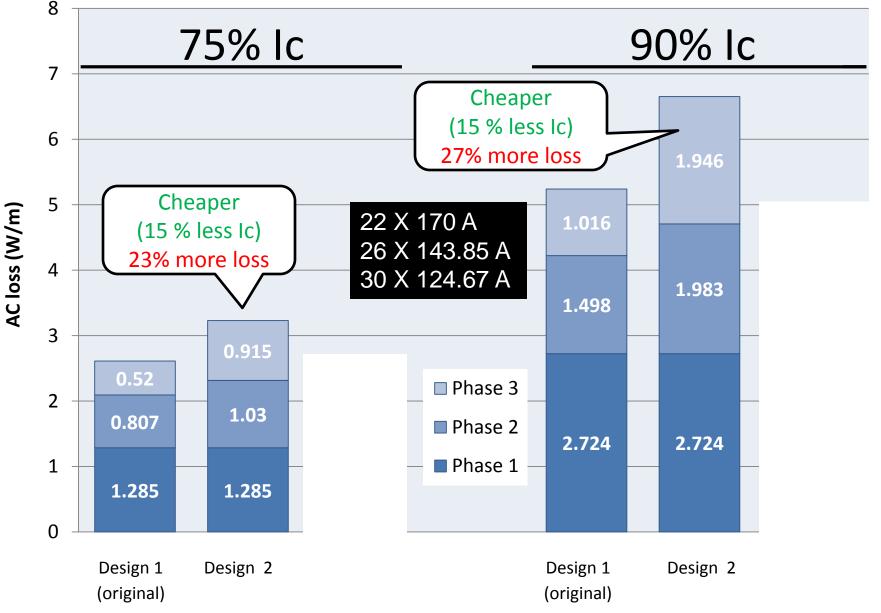
Optional design: 3



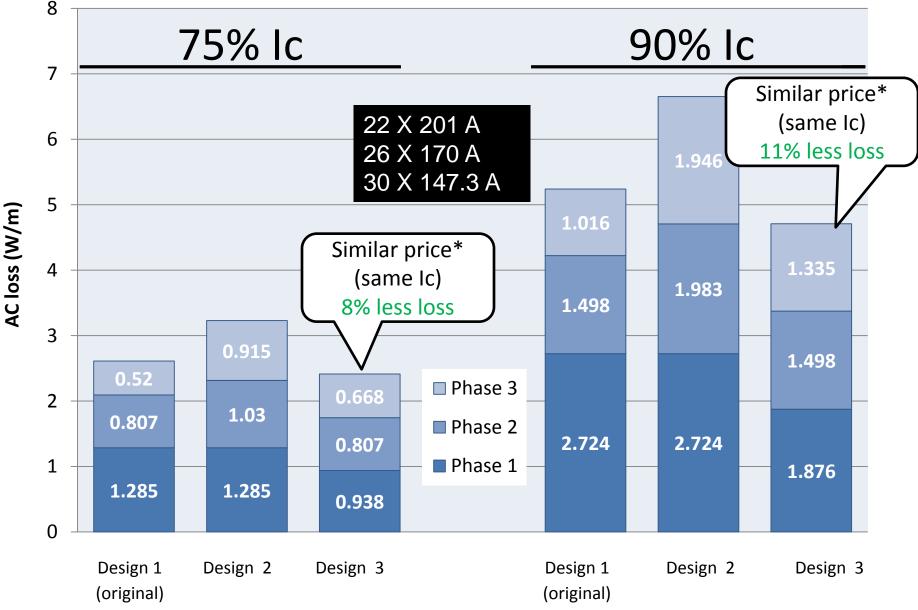
AC loss in original design



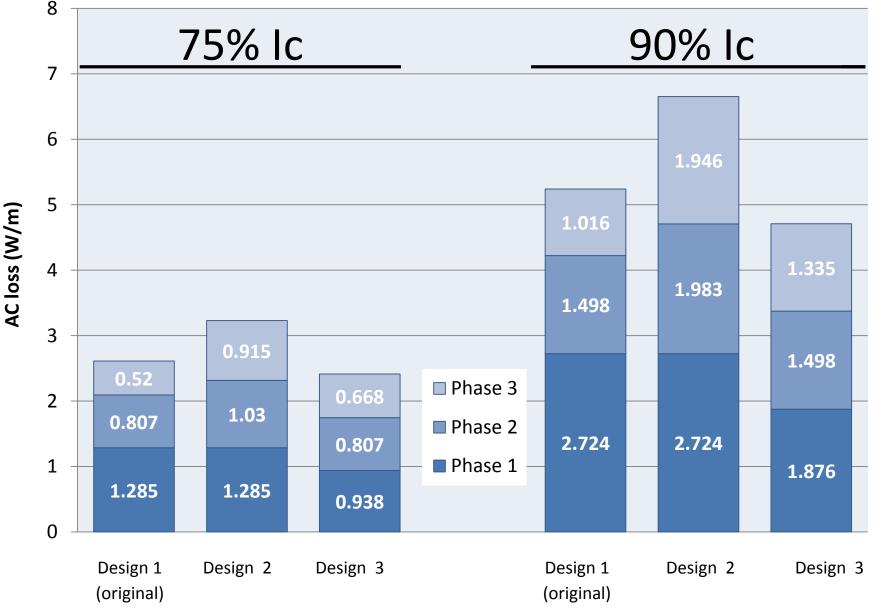
AC loss comparison for other designs



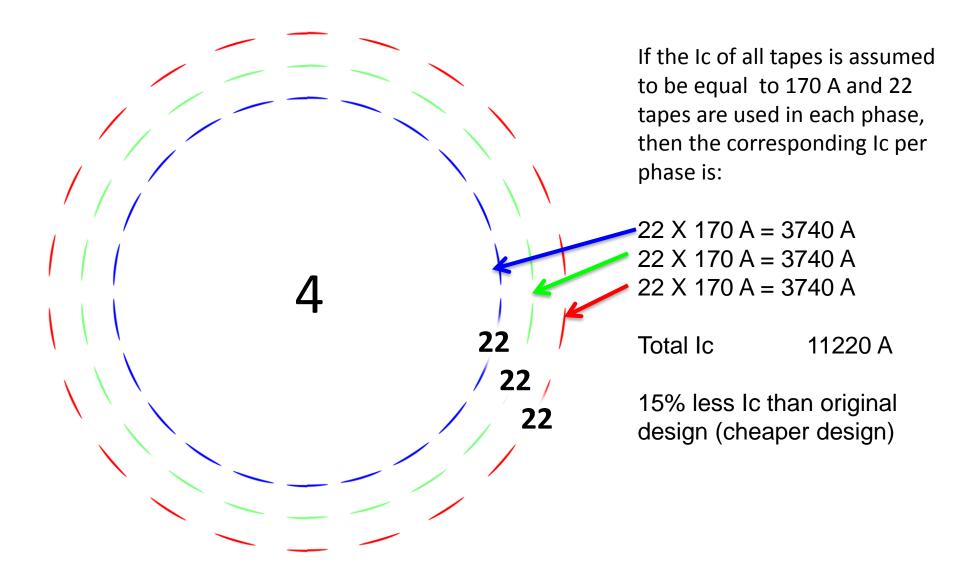
AC loss comparison for other designs



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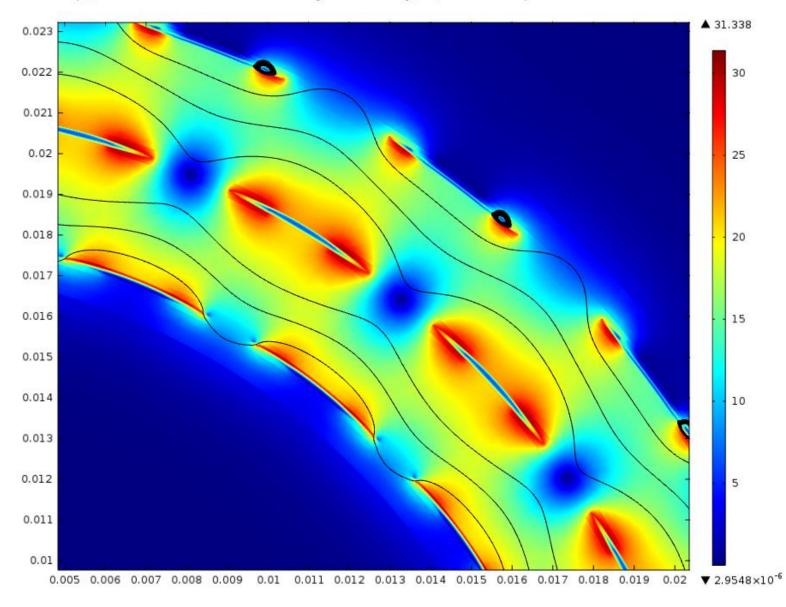


Optional design:4



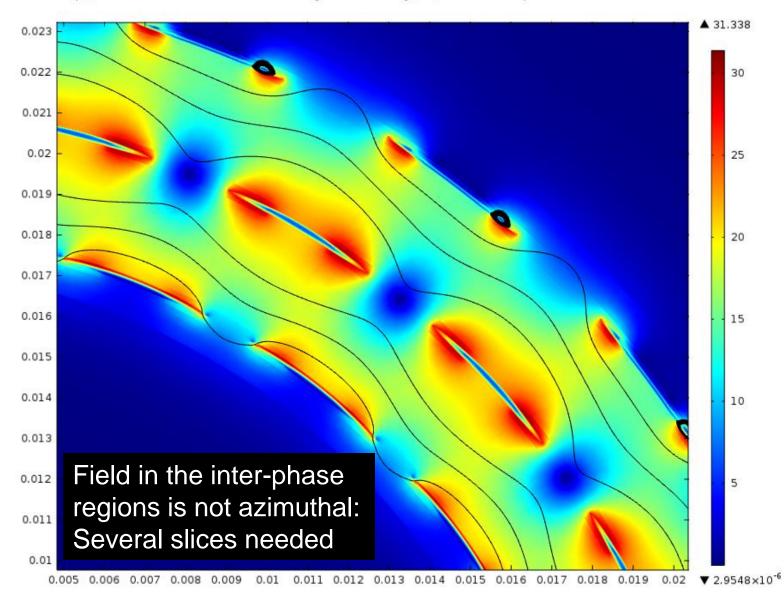
Original design:4

slp(1)=11 Time=0.0184 Surface: Norm of Magnetic flux density (mT) Streamline: Dependent variable H

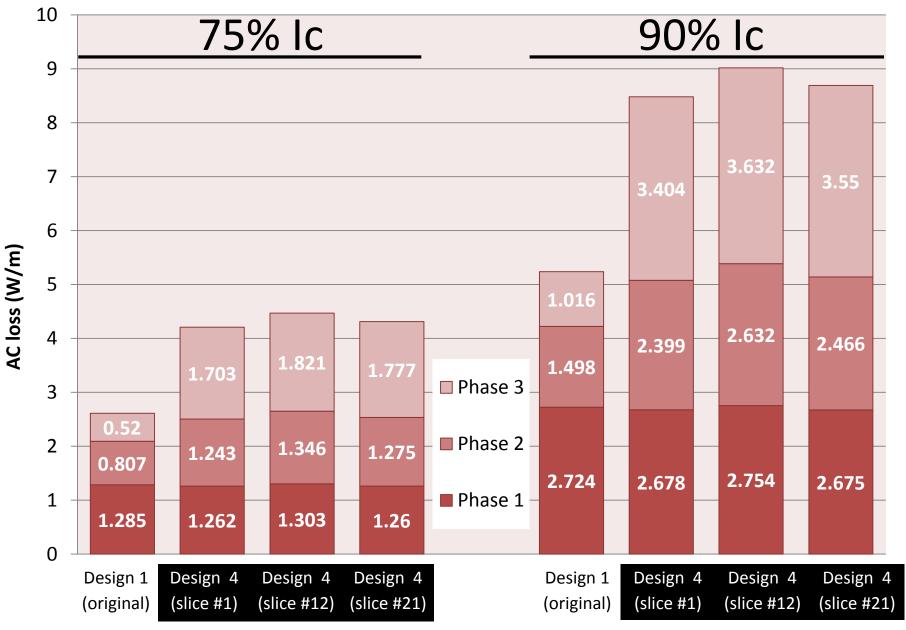


Original design:4

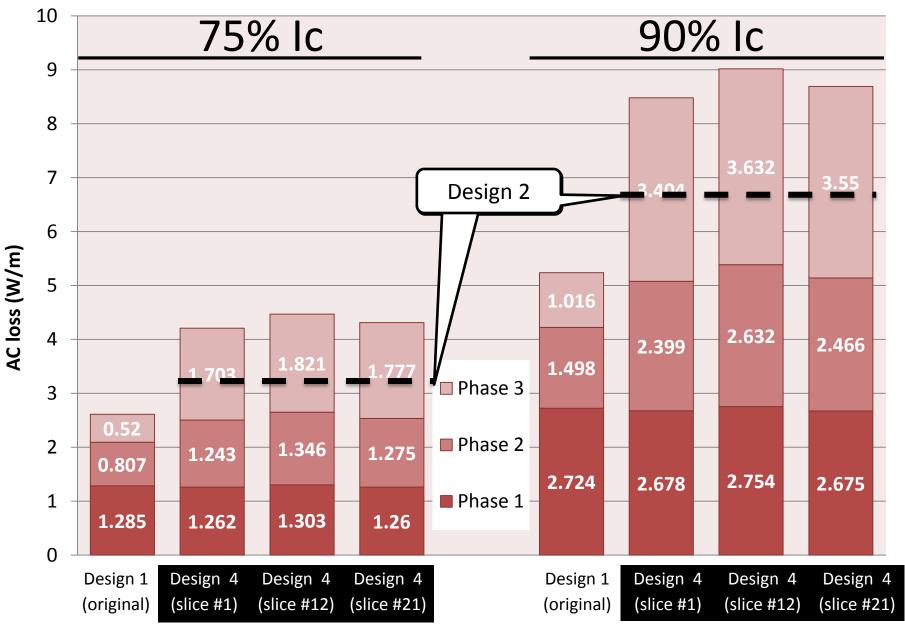
slp(1)=11 Time=0.0184 Surface: Norm of Magnetic flux density (mT) Streamline: Dependent variable H



Cable with 22 tapes per phase

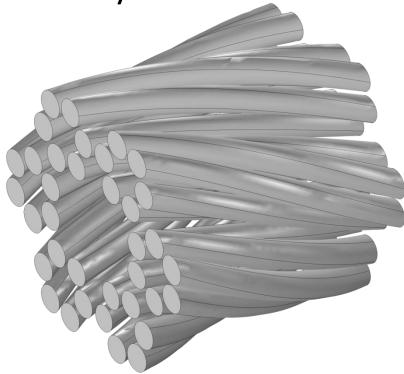


Cable with 22 tapes per phase

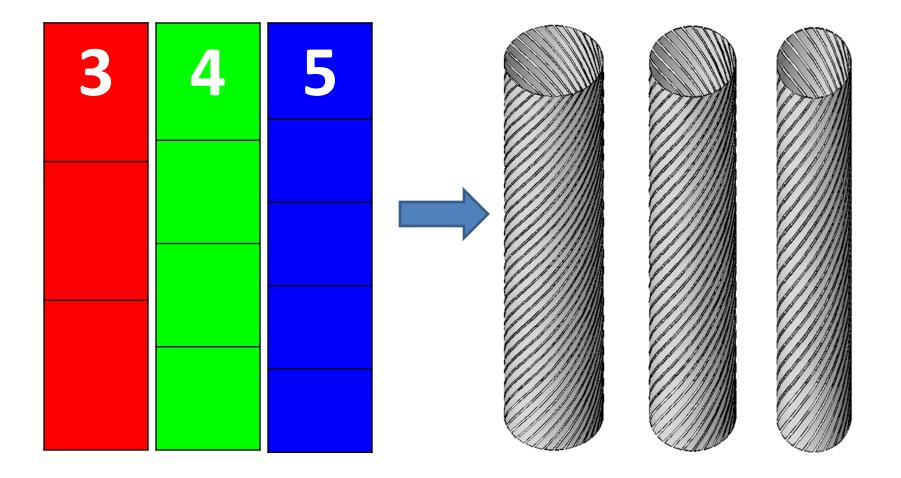


How about CICC?

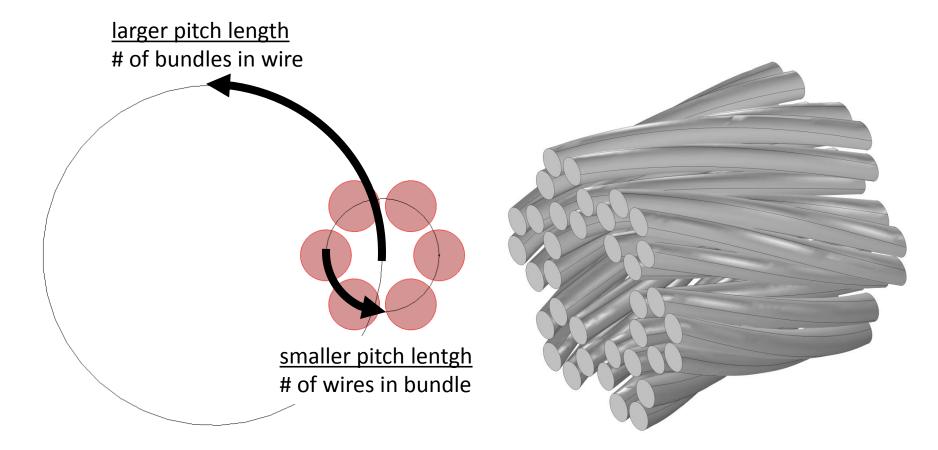
- Similar strategy can be followed:
 - Pitch length now relates to wires and filaments rather than to layers.

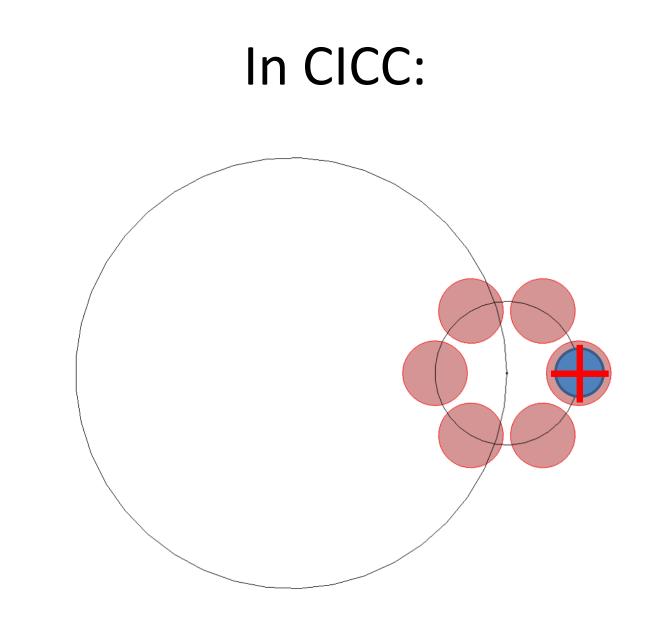


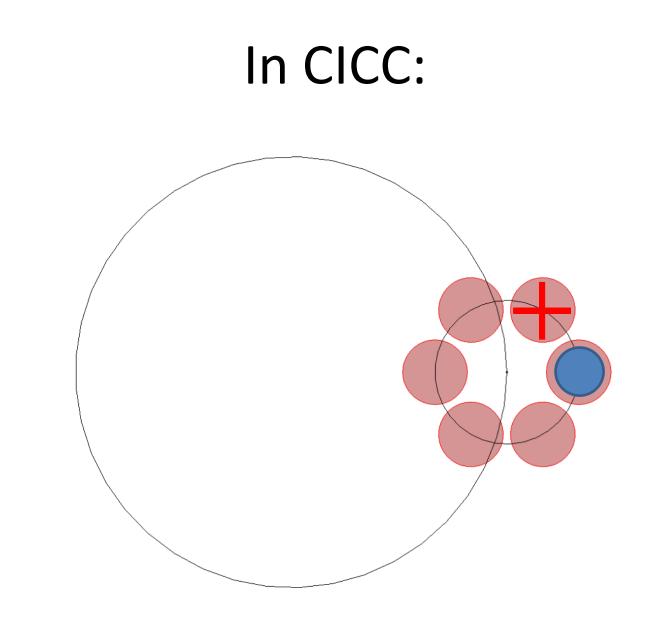
In helically wound cables:

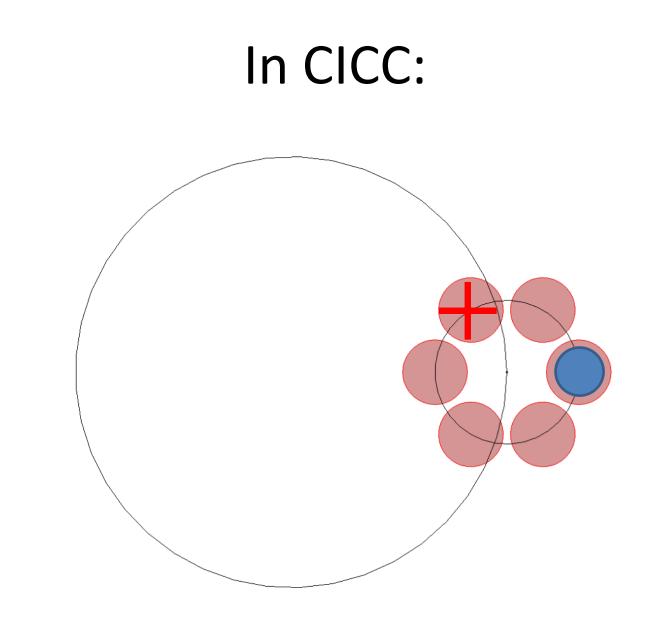


In CICC:

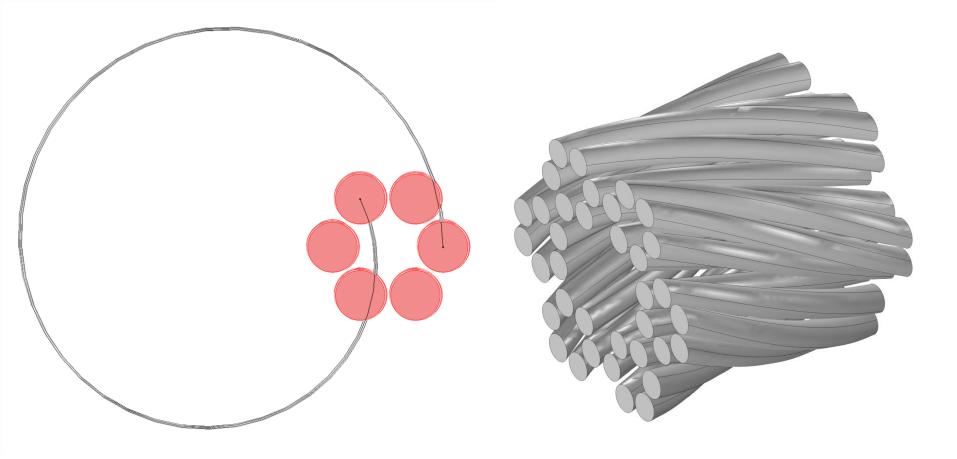






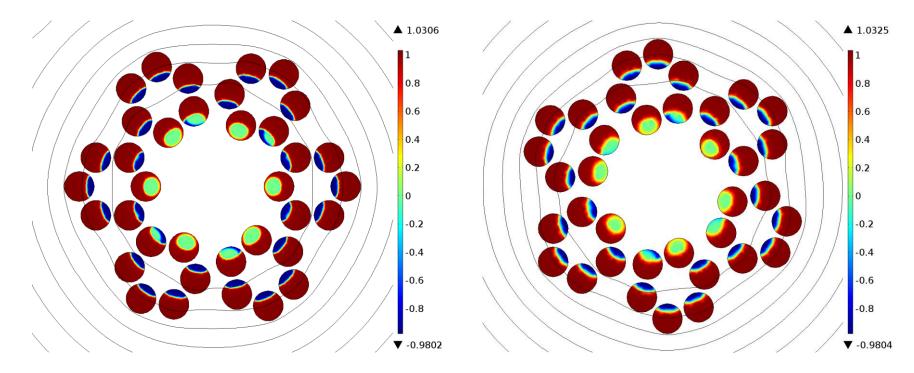


Test design



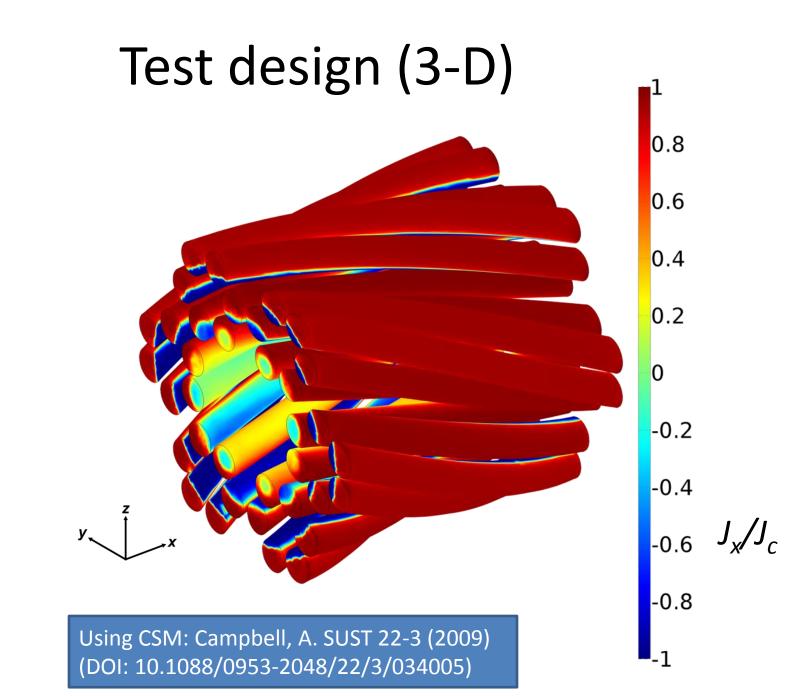
Test design (2.5-D)

Surface: |J/Jc| Streamlines: (B1,B2)



Use of several slices provided similar AC loss calculation (~1% difference)

Using H-formulation, Brambilla et al. SUST 20-1 (2007)



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- The CICC geometrical model was used for simulating the electromagnetic transient response of the cables in transport conditions by means of FEM using H-formulation.
- A 3-D model based in the CSM was implemented