

First Experience with the New Coupling-Loss Induced Quench System



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H. H. J. ten Kate^{1,2}, and A. P. Verweij¹

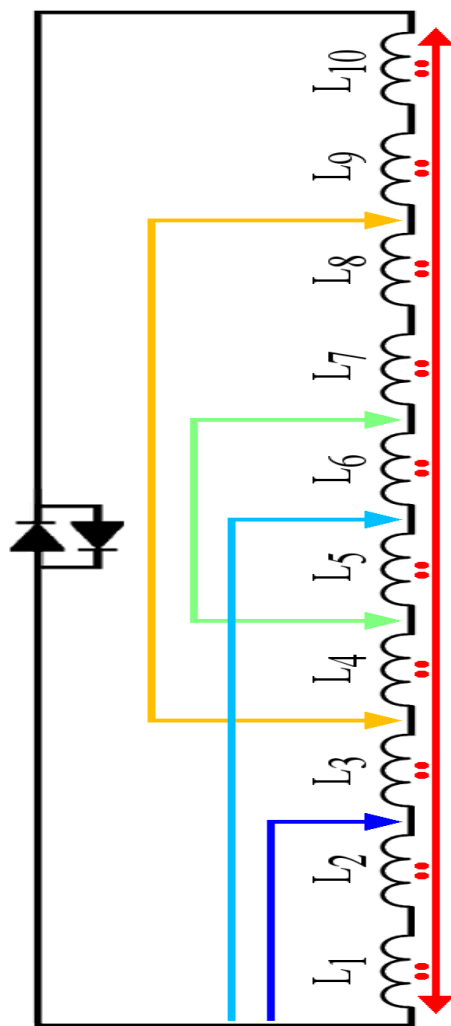
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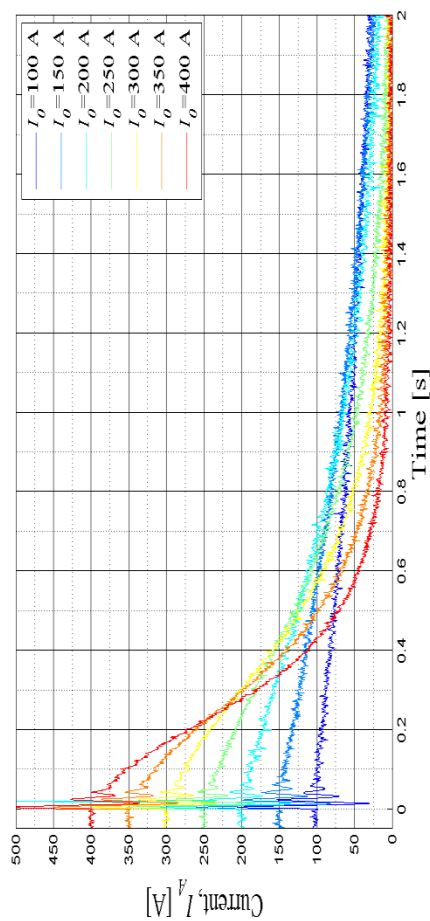
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OF TWENTE.

First Experience with the New Coupling-Loss Induced Quench System

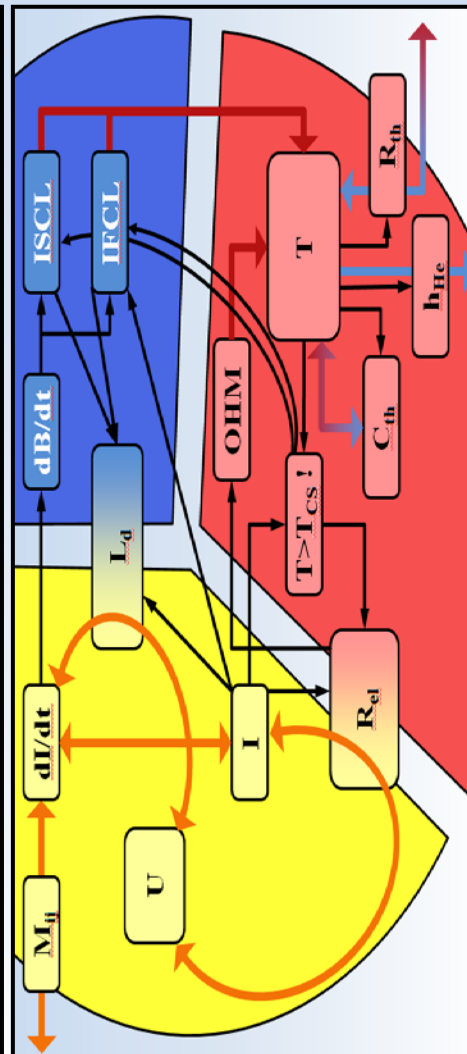
Theory



Test Results



Modeling



Outlook

| CLIQ - Conclusion... | | ... and Future Steps | |
|----------------------|---|----------------------|--|
| Design | <ul style="list-style-type: none"> Heat deposited in the copper matrix Not relying on thermal diffusion Quick and global quench initiation Robust system | | <ul style="list-style-type: none"> Multiple CLIQ Systems Effect of a delay in the triggering Redundancy |
| Tests | <ul style="list-style-type: none"> 30+ tests on a 2 m long NbTi quadrupole magnet (MOXC2) 1000+ tests on a small-size solenoid magnet Key parameters studied and optimized | | <ul style="list-style-type: none"> CERN, NbTi quadrupole magnet (MOXC2) ENAL, Nb3Sn quadrupole magnet (HQ2 → MOXF) Oxford Instruments, Nb3Sn solenoid magnet CERN, NbTi Individually-Powered Quadrupole (IPO) CERN, NbTi solenoid magnet (Multi-CLIQ) |
| Modeling | <ul style="list-style-type: none"> 2D Lumped-Elements Electro-Thermal Dynamic behaviour | | <ul style="list-style-type: none"> Validation of the model on a wide variety of practical cases More flexibility, modularity, GUI Migration from PSpice to Simulink? 3D? |

First Experience with the New Coupling-Loss Induced Quench System

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Theory

Quench in a Superconducting Magnet

High Current Density

$$J \approx \text{kA/cm}^2$$

High Magnetic Field

$$B = 5\text{-}10 \text{ T (15 T?)}$$

High Energy Density

$$e = B^2/(2 \mu_0) \approx 10\text{-}40 \text{ MJ/m}^3$$

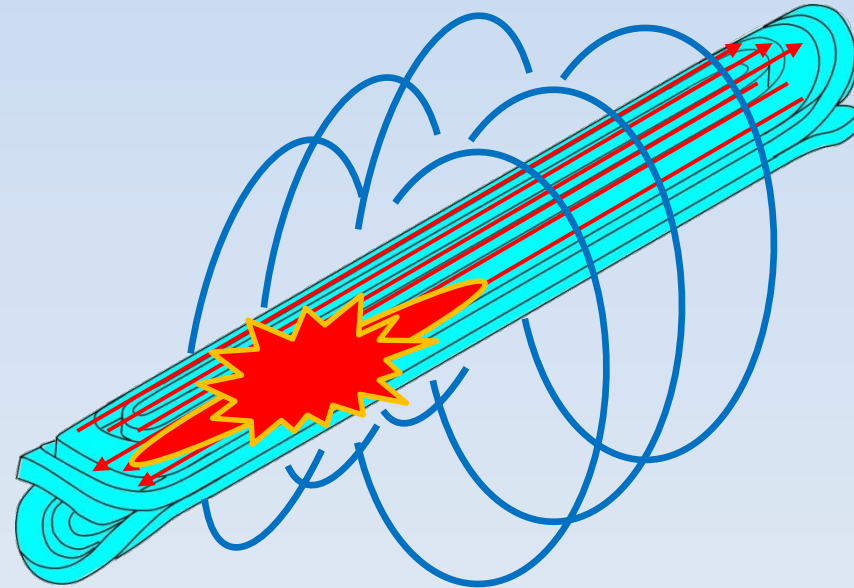
Quench

If a portion of cable suddenly becomes non-superconducting, it starts heating up

Quench Propagation

The heat mainly propagates through the Copper matrix around the sc filaments

The energy stored in the magnet is usually sufficient to melt kilos of Copper and destroy the magnet!

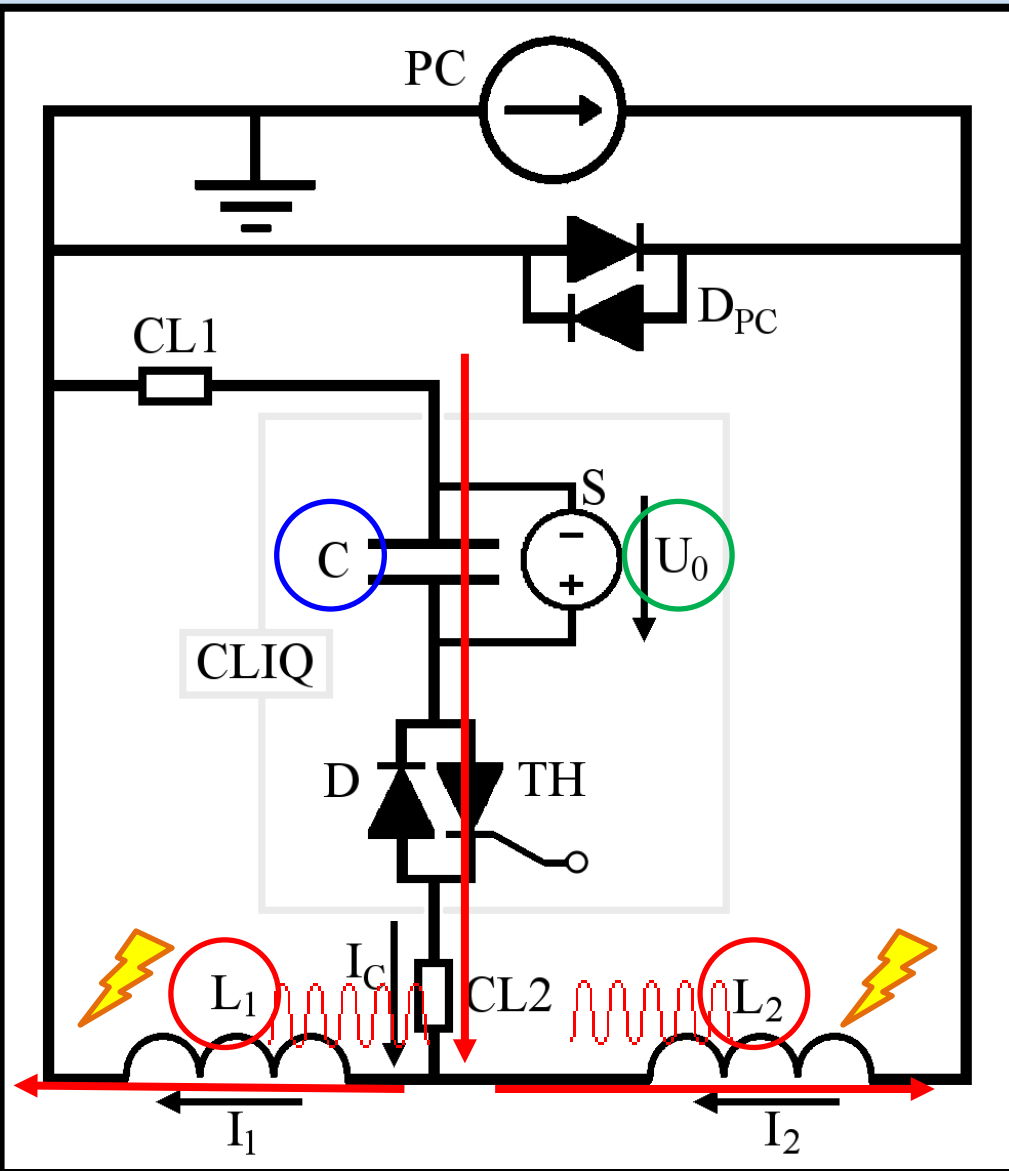


How to keep the hot-spot temperature low and protect the magnet?

Quick extraction of the energy (i.e. the current) stored in the magnet

Fast propagation of the quench to reduce the discharge time

Concept of CLIQ – Coupling-Loss Induced Quench



Current
Change

$$I_c(t) \approx -U_0 \sqrt{\frac{C}{L}} \cdot \sin\left(\frac{t}{\sqrt{LC}}\right)$$

$$\frac{dI_c(t)}{dt} \approx \frac{U_0}{L} \cdot \cos\left(\frac{t}{\sqrt{LC}}\right)$$

Magnetic
Field
Change

$$\frac{dB_t(t)}{dt} = f_m \frac{dI_c(t)}{dt} \left[1 - \exp\left(-\frac{t}{\tau_{IF}}\right) \right]$$

Coupling-
Losses
(Heat)

$$\frac{P_{IF}}{vol} = \beta_{IF} \left[\frac{dB_t(t)}{dt} \right]^2 \propto \left(\frac{U_0}{L} \right)^2$$

Temperature
Rise

$$\tau_{IF} = \frac{\mu_0}{2} \left(\frac{l_p}{2\pi} \right)^2 \frac{1}{\rho_{eff}(B)}$$

$$\beta_{IF} = \left(\frac{l_p}{2\pi} \right)^2 \frac{1}{\rho_{eff}(B)}$$

QUENCH

E. Ravaioli et al., MT23, 2013.

E. Ravaioli et al., EUCAS11, 2013.

EU Patent EP13174323.9, June 2013.

CLIQ – Main Advantages

Heat generated exactly where we need it: directly in the copper matrix of the strand, without relying on thermal diffusion

Very fast quench mechanism

Global quench initiation
→ More homogenous temperature distribution

Cheap and robust system

First Experience with the New Coupling-Loss Induced Quench System

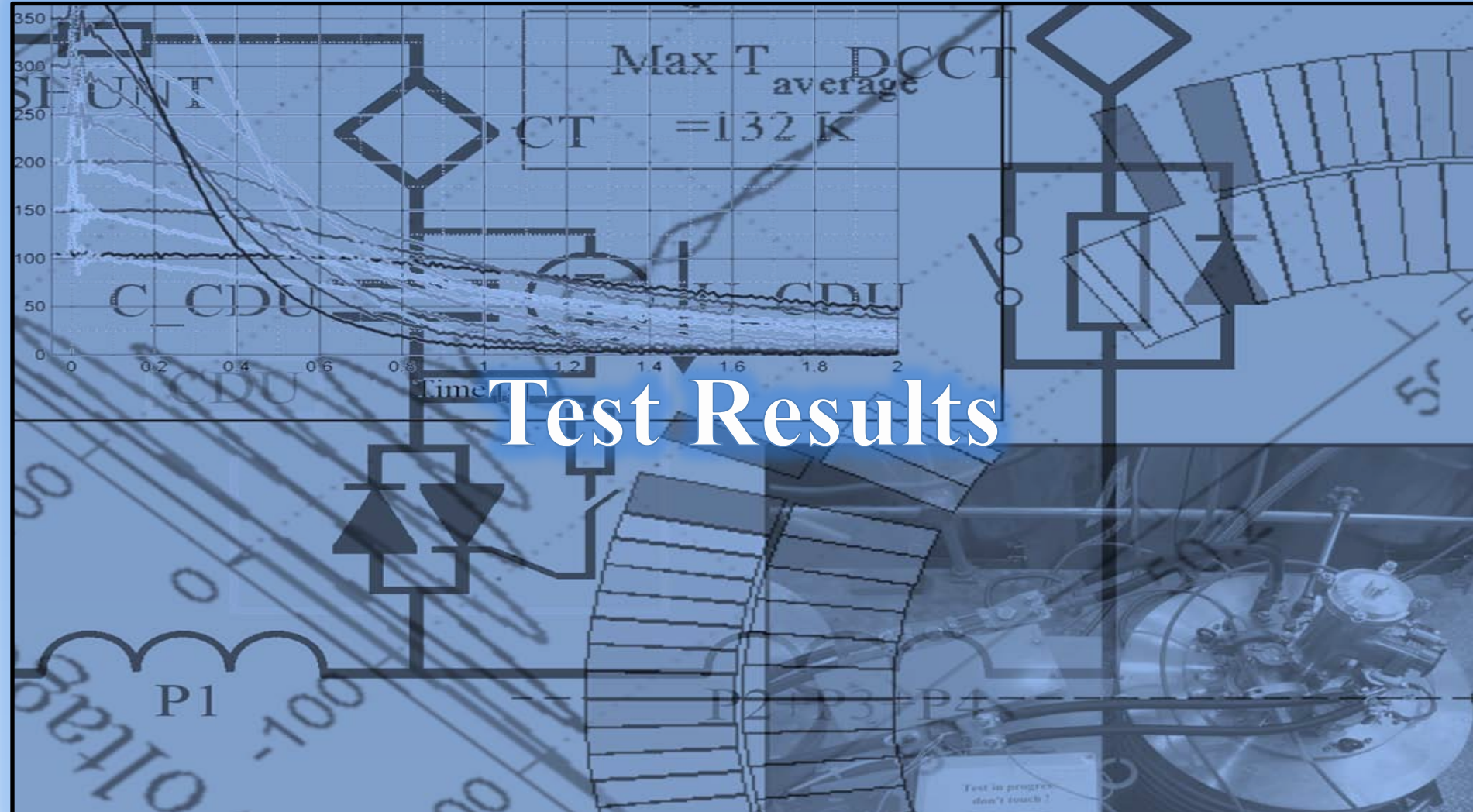
Theory

Test Results

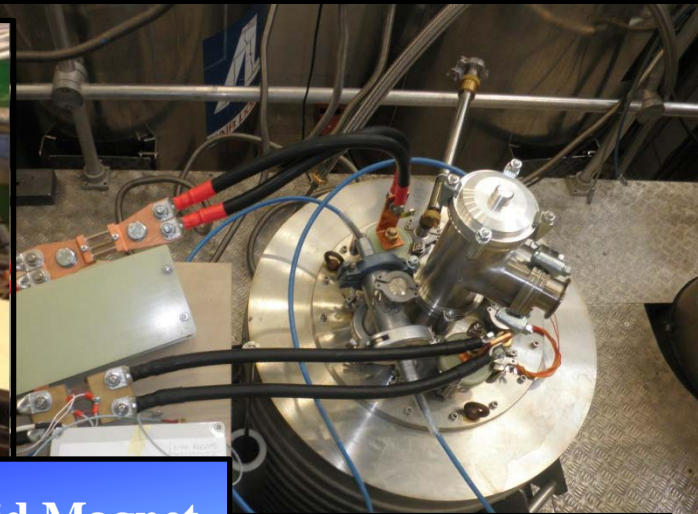
Modeling

Outlook

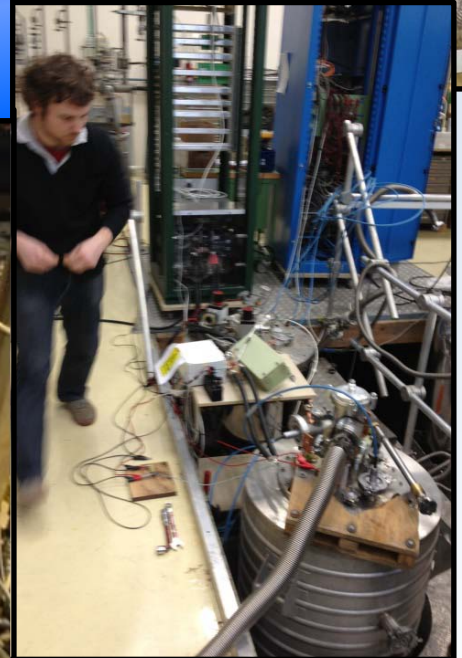
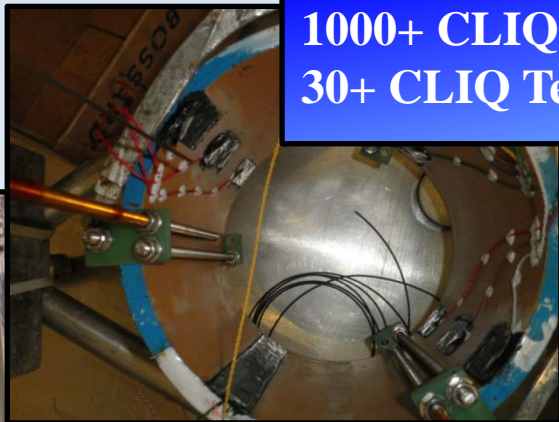
Test Results



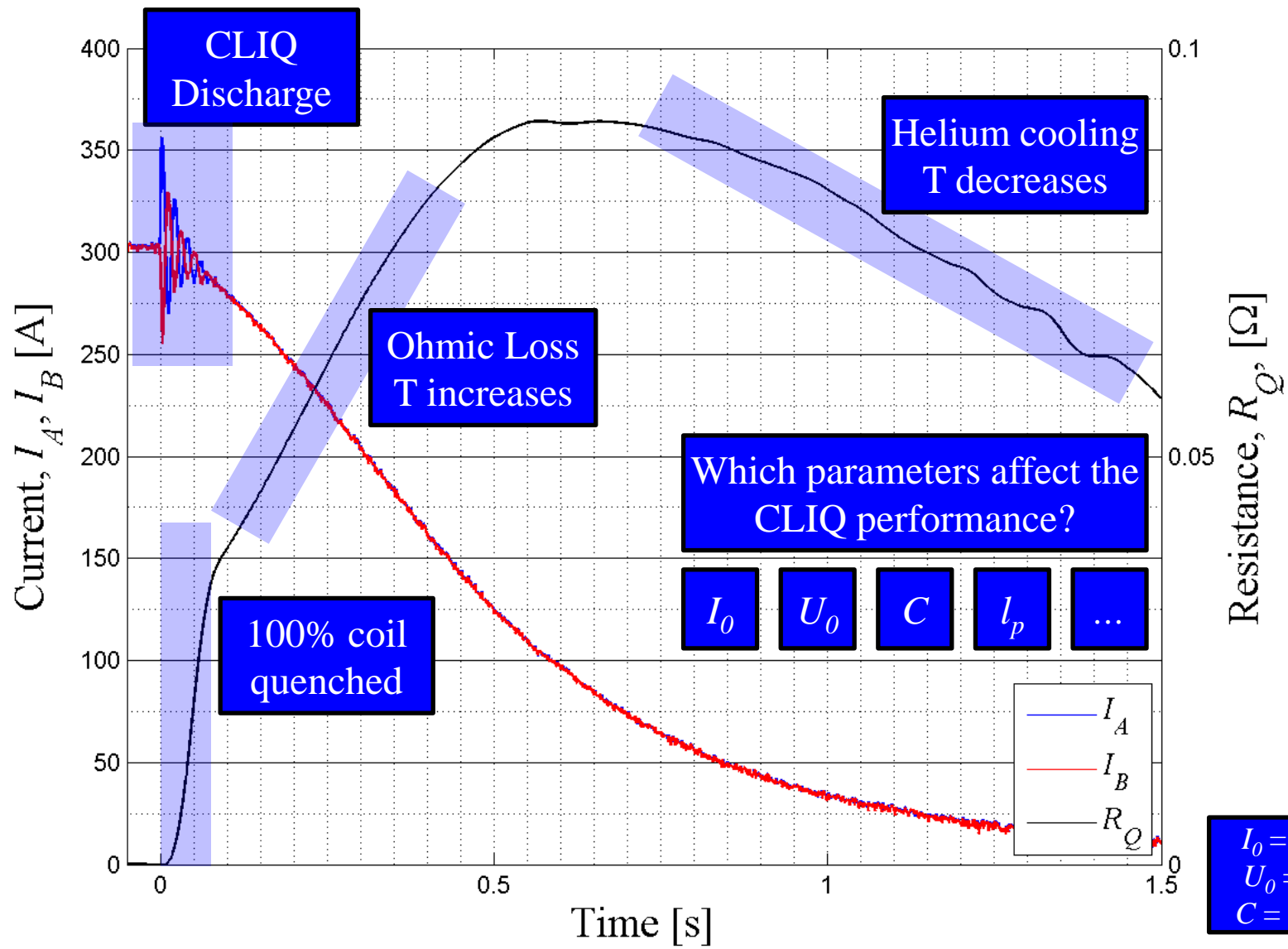
Test Setup – CERN Cryogenic Laboratory & Magnet Test Facility



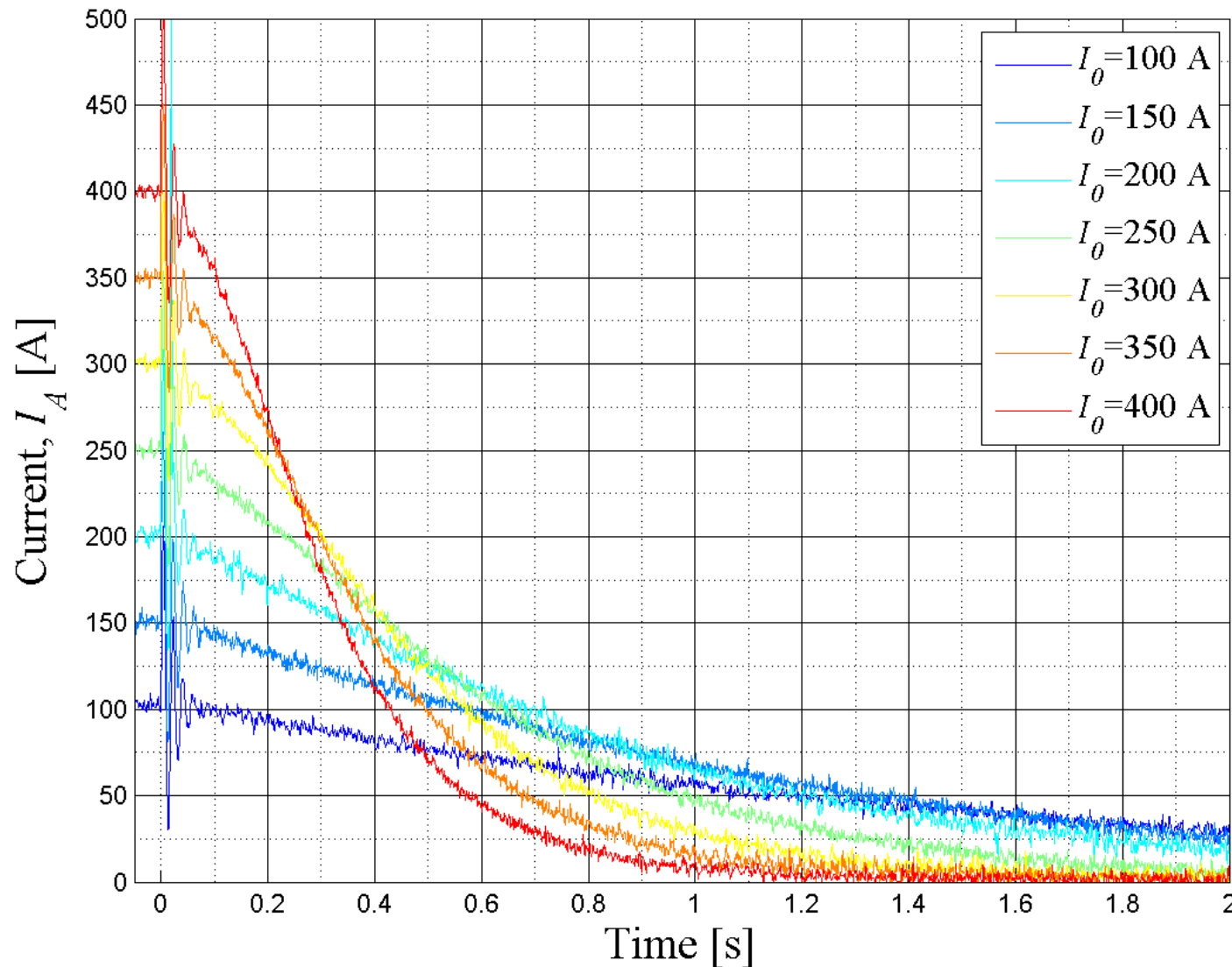
1000+ CLIQ Tests on a small-size Solenoid Magnet
30+ CLIQ Tests on a 2 meter Quadrupole Magnet



CLIQ – Coupling-Loss Induced Quench



CLIQ – Effect of the Initial Current I_0 – Magnet Current

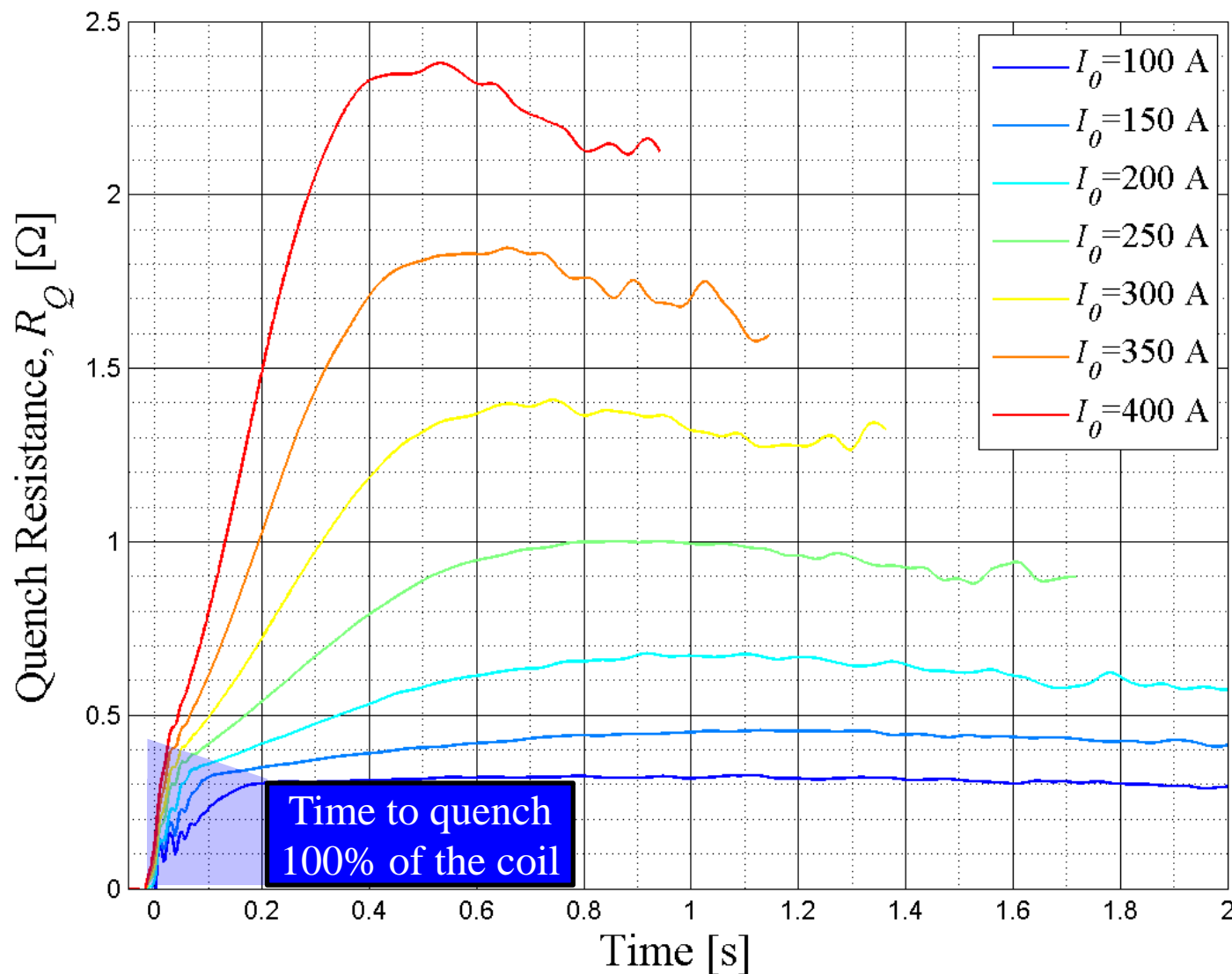


$$\frac{dI}{dt} \neq f(I_0)$$
$$\frac{P_{IF}}{vol} \neq f(I_0)$$

$$T_{cs} = f(I_0)$$
$$P_{Ohm} \propto I_0^2$$

$$U_0 = 150 \text{ V}$$
$$C = 4.7 \text{ mF}$$

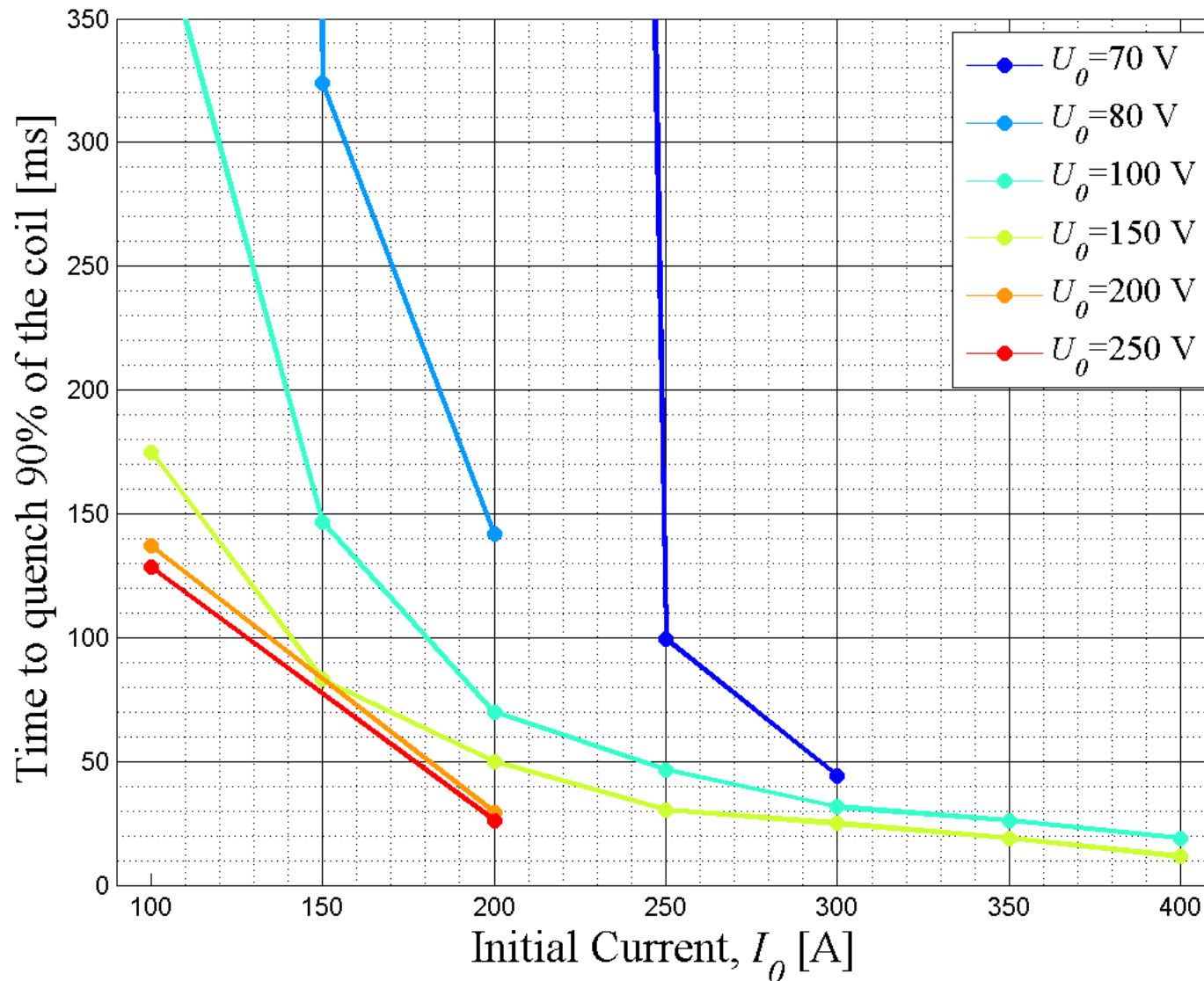
CLIQ – Effect of the Initial Current I_0 – Quench Resistance



$$T_{cs} = f(I_0)$$
$$P_{Ohm} \propto I_0^2$$

$$U_0 = 150 \text{ V}$$
$$C = 4.7 \text{ mF}$$

CLIQ – Effect of the Charging Voltage U_0 – Time to Quench

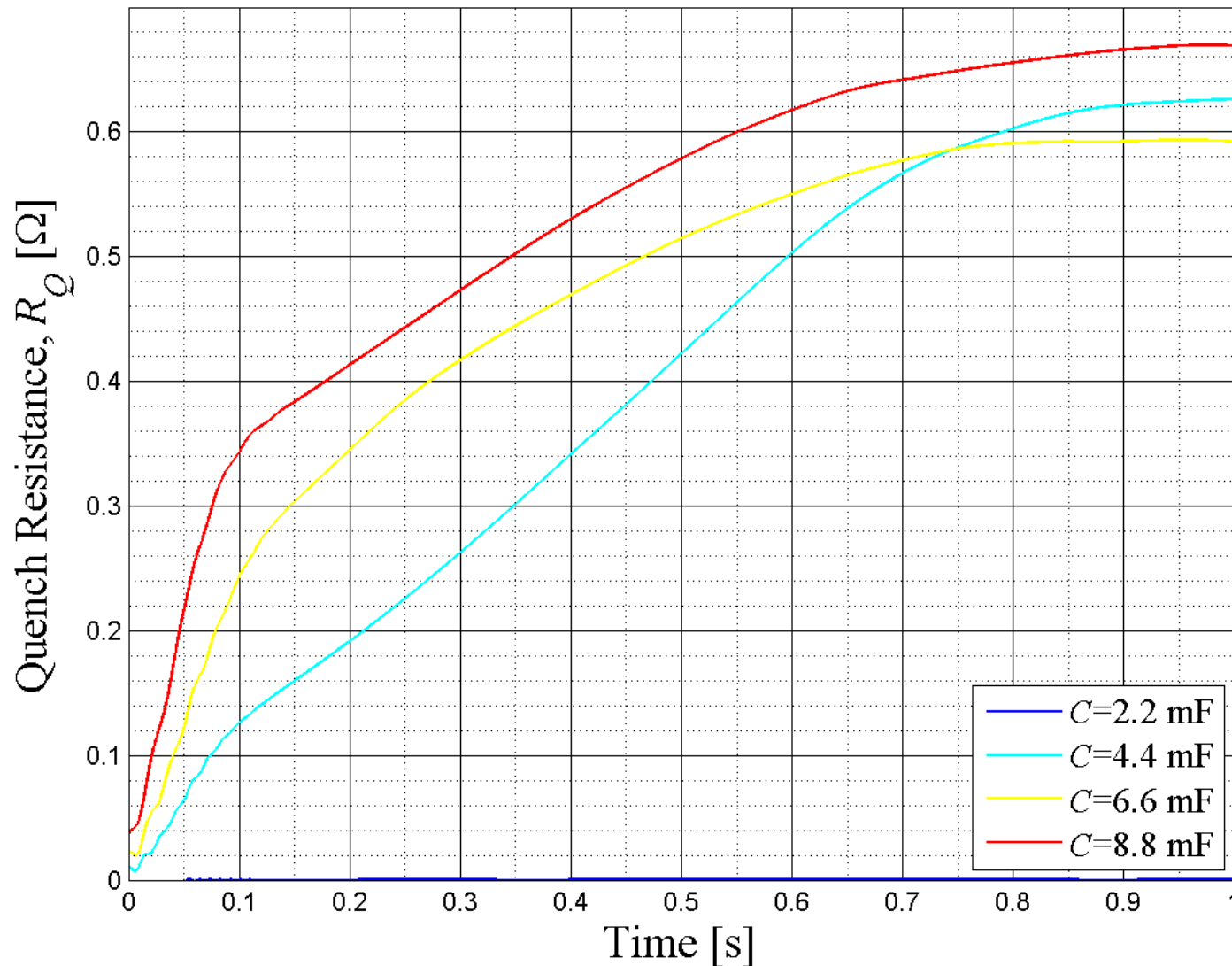


$$\frac{P_{IF}}{vol} \propto \left(\frac{U_0}{L}\right)^2$$

U_0 usually limited by safety limits

$C = 4.7$ mF

CLIQ – Effect of the Capacitance C – Quench Resistance



For the tested magnet the performance improves with larger C

$I_0 = 200$ A
 $U_0 = 75$ V

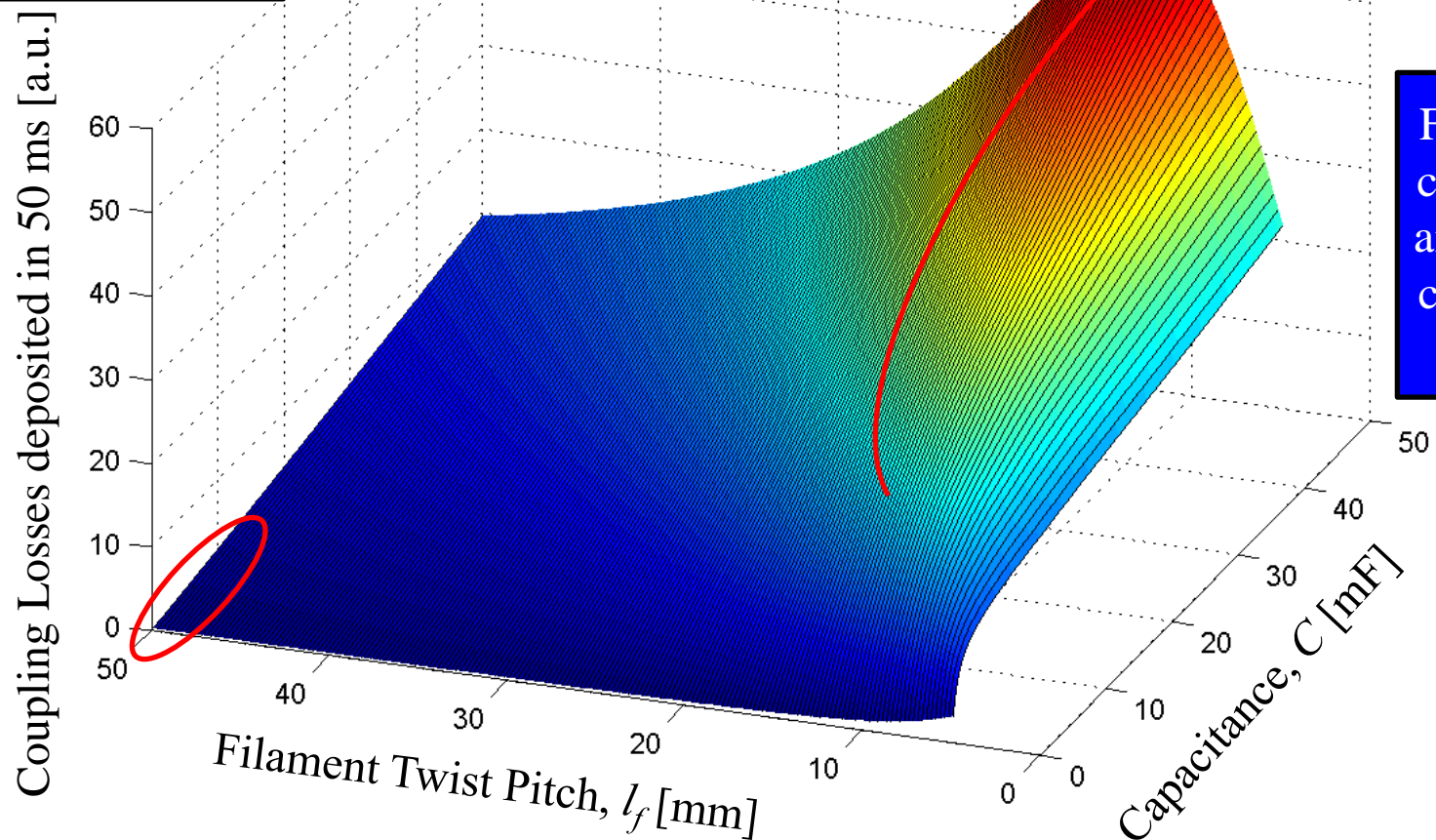
CLIQ – Effect of the Capacitance and of the Filament Twist Pitch

$$I_c(t) \approx -U_0 \sqrt{\frac{C}{L}} \cdot \sin\left(\frac{t}{\sqrt{LC}}\right)$$

$$\frac{dI_c(t)}{dt} \approx \frac{U_0}{L} \cdot \cos\left(\frac{t}{\sqrt{LC}}\right)$$

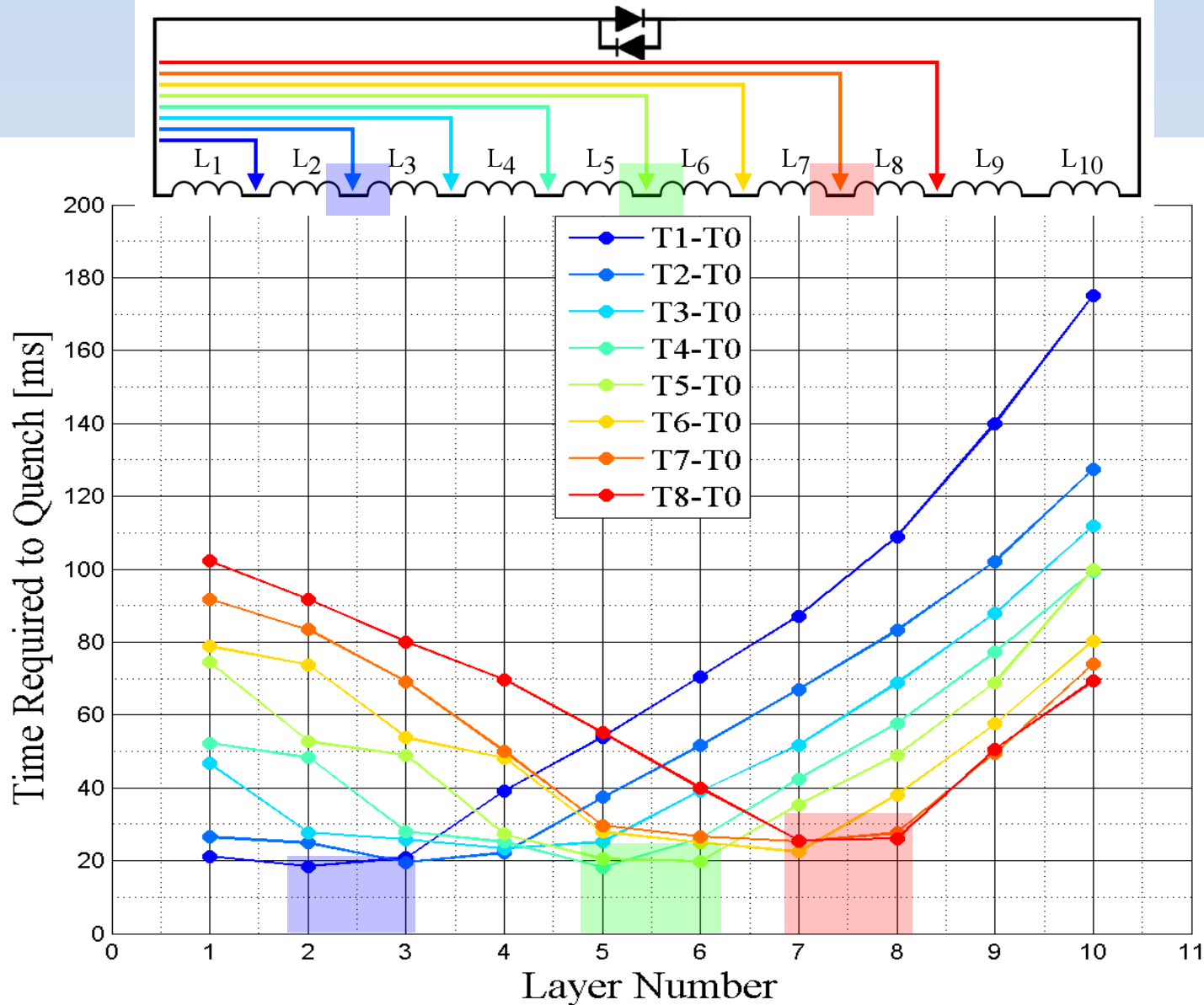
$$\tau_{IF} = \frac{\mu_0}{2} \left(\frac{l_p}{2\pi}\right)^2 \frac{1}{\rho_{eff}(B)}$$

$$\omega = \frac{1}{\sqrt{LC}}$$



For a given coil there is an optimum choice of C and l_f

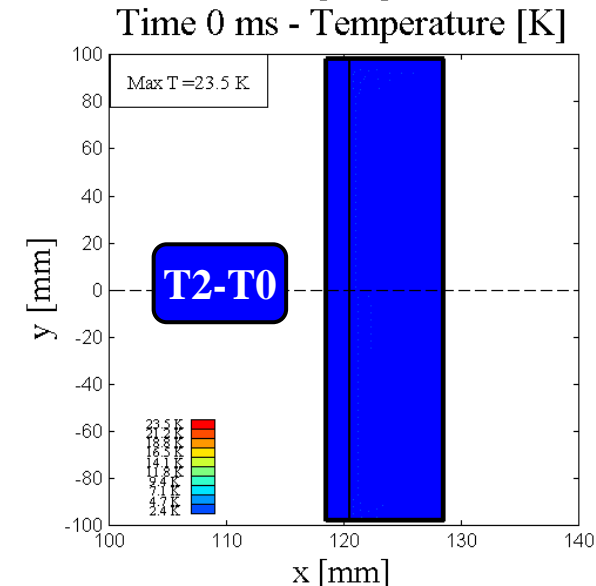
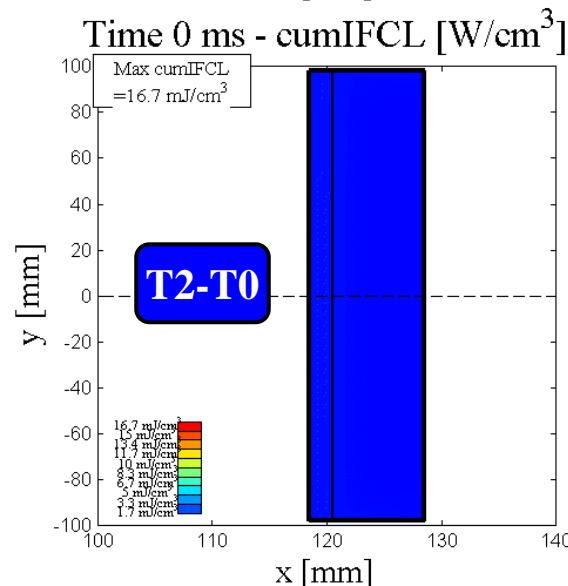
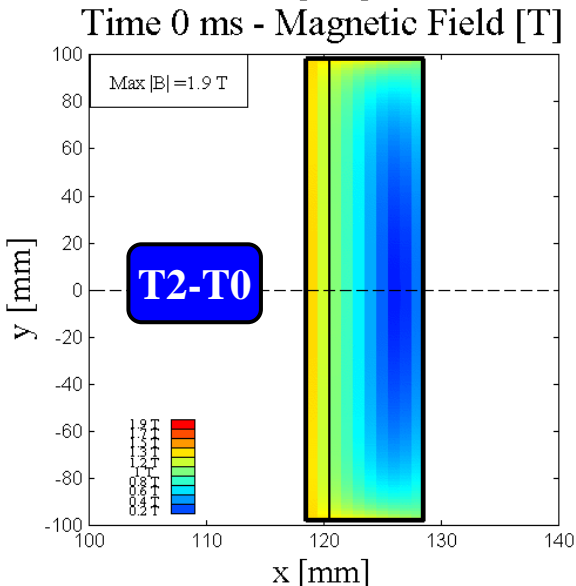
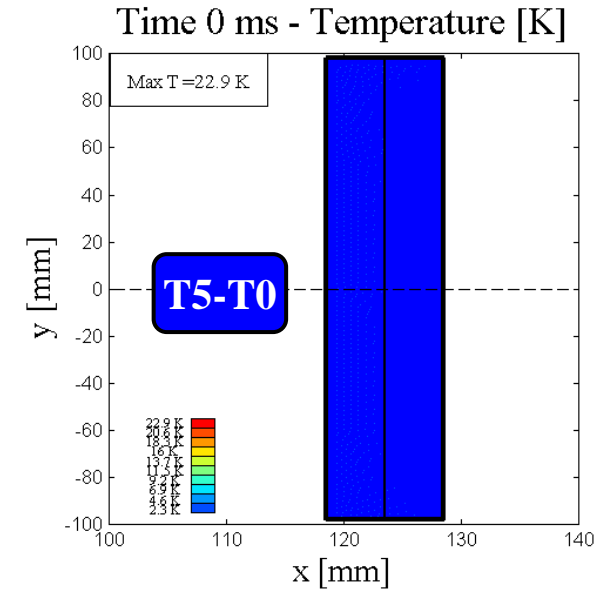
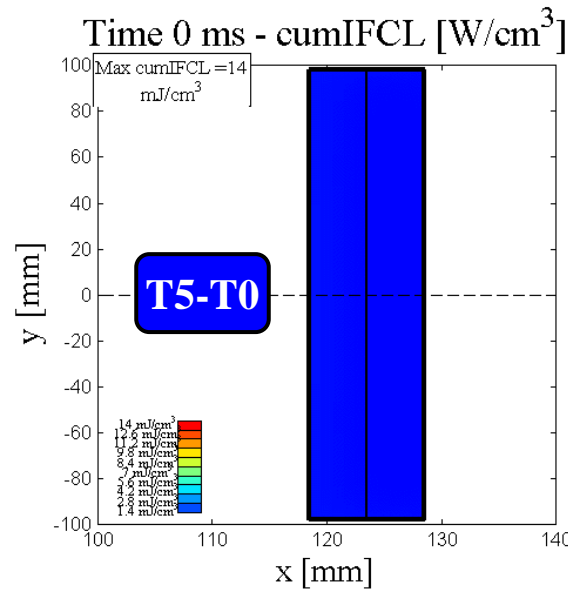
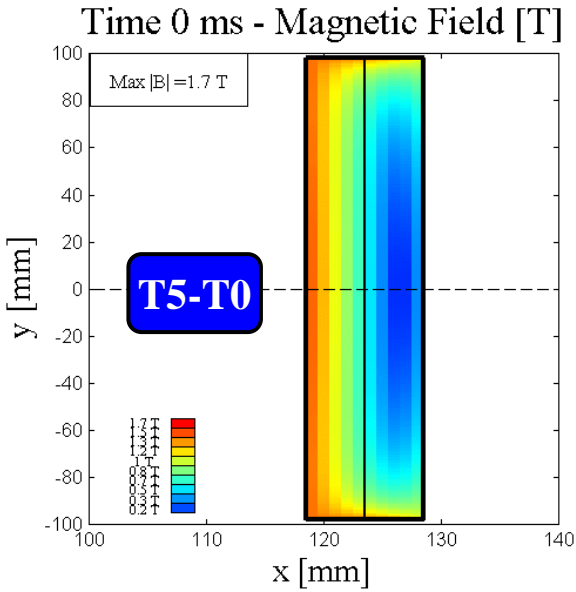
CLIQ – Effect of the Injection/Extraction Points – Time to Quench



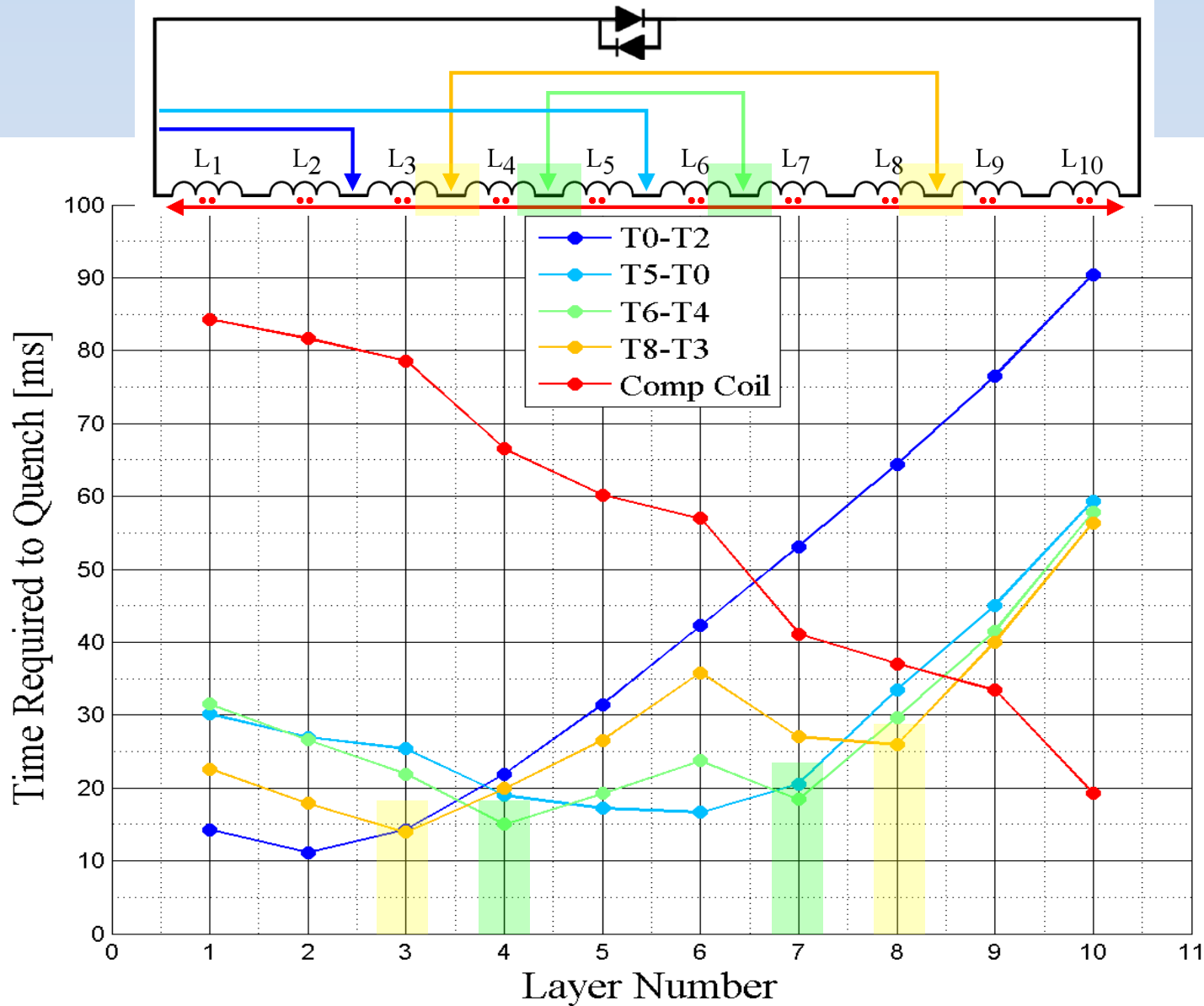
CLIQ discharge in the central region spreads the quench faster

$I_0 = 200 \text{ A}$
 $U_0 = 75 \text{ V}$
 $C = 8.8 \text{ mF}$

CLIQ – Effect of the Injection/Extraction Points – Simulation



CLIQ – Effect of the Injection/Extraction Points – Time to Quench

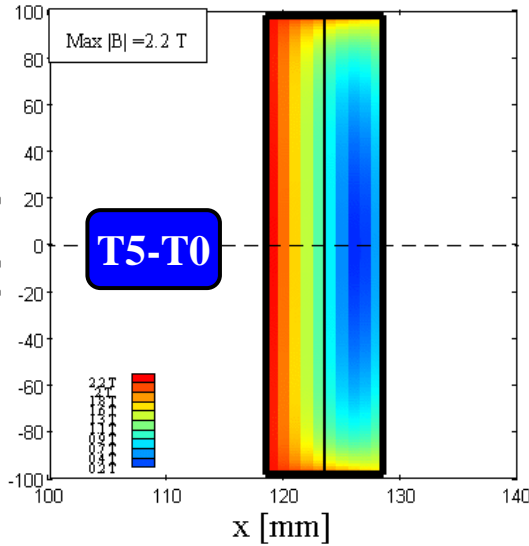


Two separate quench areas can be created

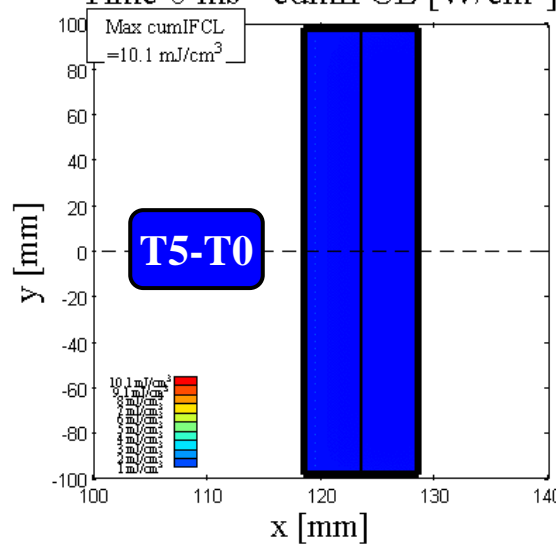
$I_0 = 300 \text{ A}$
 $U_0 = 75 \text{ V}$
 $C = 8.8 \text{ mF}$

CLIQ – Effect of the Injection/Extraction Points – Simulation

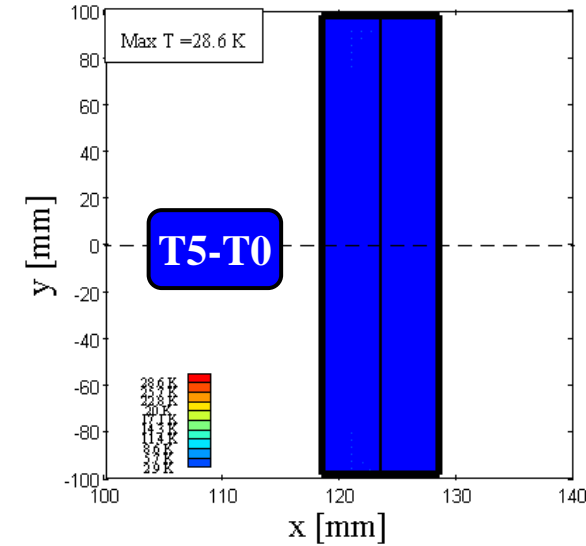
Time 0 ms - Magnetic Field [T]



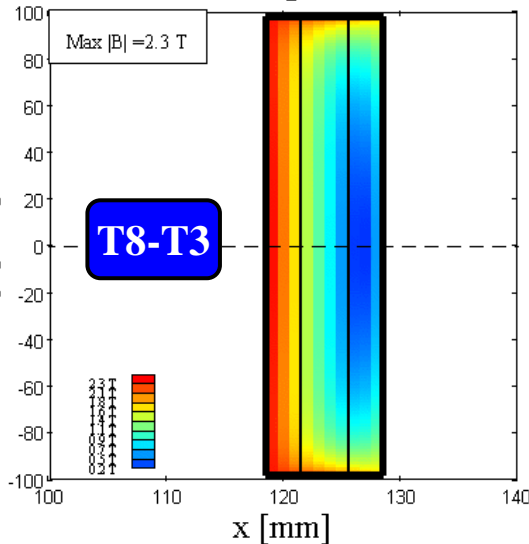
Time 0 ms - cumIFCL [W/cm^3]



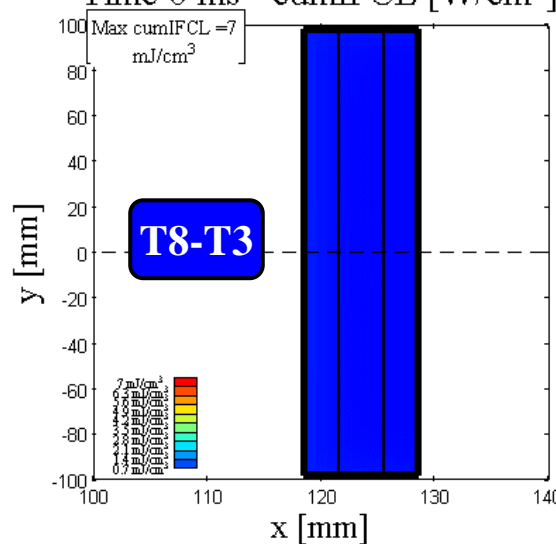
Time 0 ms - Temperature [K]



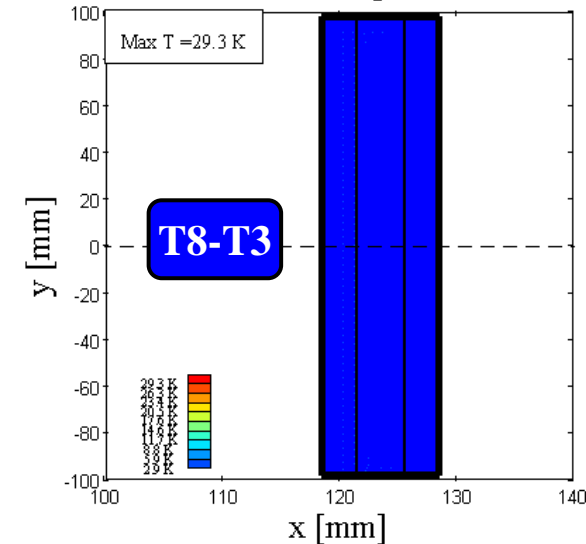
Time 0 ms - Magnetic Field [T]



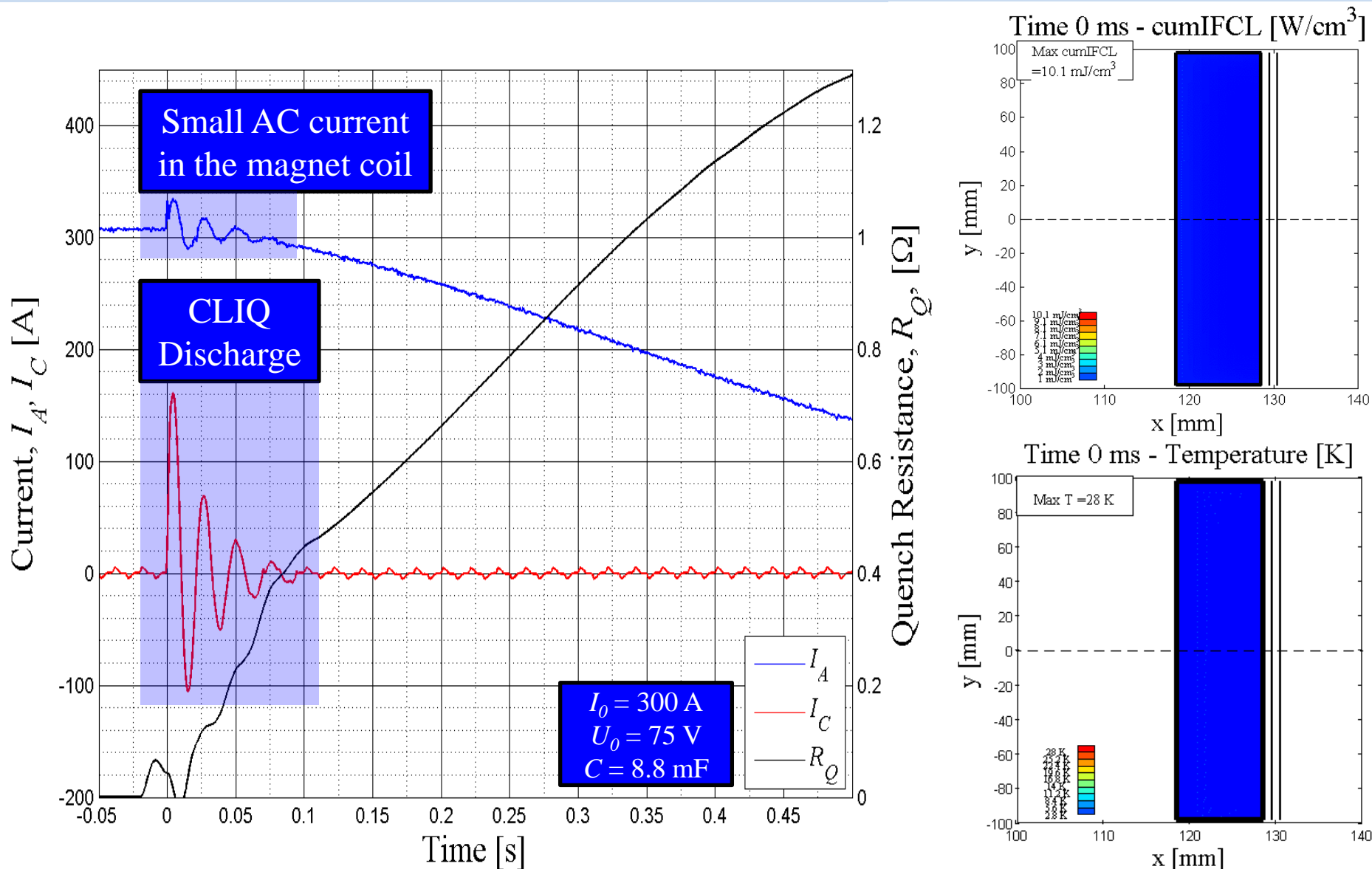
Time 0 ms - cumIFCL [W/cm^3]



Time 0 ms - Temperature [K]



CLIQ – Using the Compensation Coil – Measurements + Sims



CLIQ – Using the Compensation Coil – Pros & Cons

Pros

- The CLIQ discharging circuit is **electrically insulated** from the magnet
- Increasing the **insulation thickness** of the compensation coil does not reduce the quench efficiency because CLIQ does not rely on thermal diffusion (**higher voltage** allowed)
- The **AC current** is not directly injected in the coil, thus the change in the magnet current is limited (little increase of Ohmic loss due to CLIQ)
- A purposefully-designed, **highly-insulated, robust** compensation coil can work at high voltage and AC current without a great impact on the **safety** in the system

Cons

- For a given coil and charging voltage, it is typically **less efficient** than a standard CLIQ discharge (if the compensation coil has **less turns** than the solenoid magnet)
- How to implement this on a **dipole/quadrupole magnet?...**

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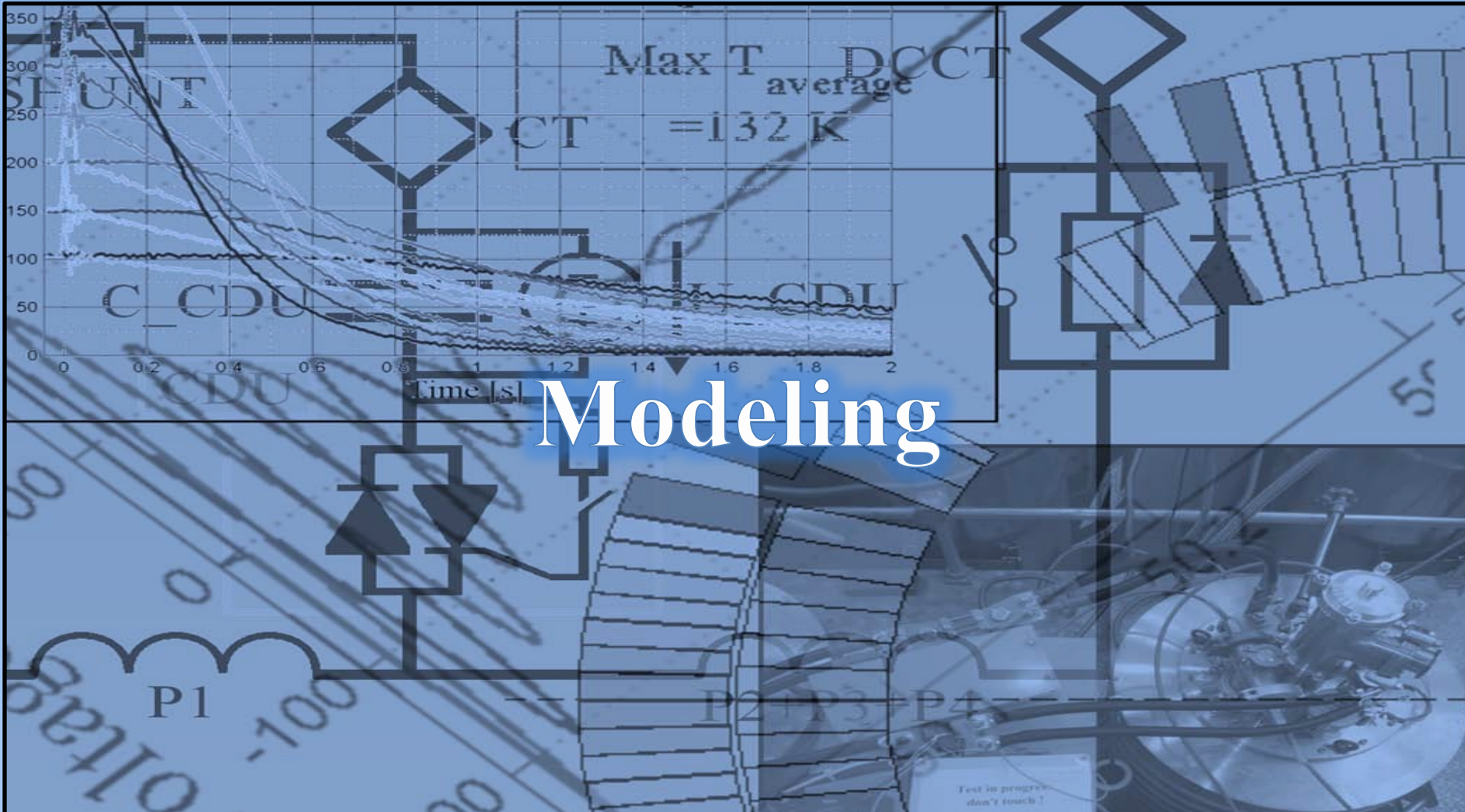
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Modeling



LEDET Lumped-Element Dynamic ElectroThermal model

2D model
No longitudinal direction

Superconducting magnet divided in blocks with homogeneous properties: magnetic field, temperature, heat capacity, resistivity, thermal conductance, etc

The electrical, thermal, and dynamic problems are described with networks of lumped-elements which are solved simultaneously with commercial software (PSpice, Simulink, Simplorer, etc)

Very fast simulations but a smart method for the choice of the lump-elements has to be found

Electrical - *Obvious*

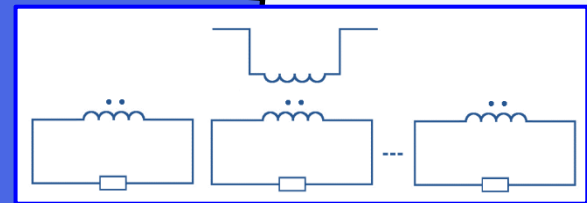
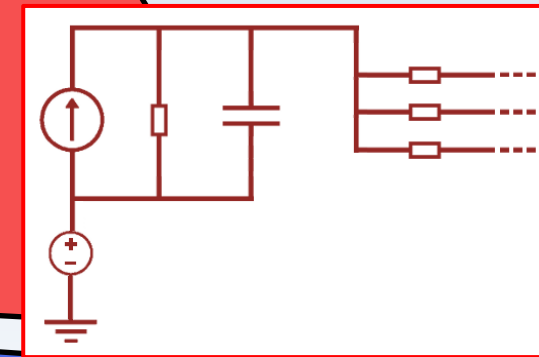
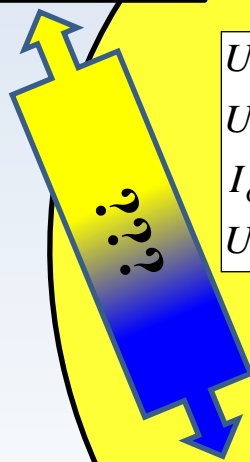
$U \equiv \Delta T, I \equiv Q$

Thermal - *Easy*

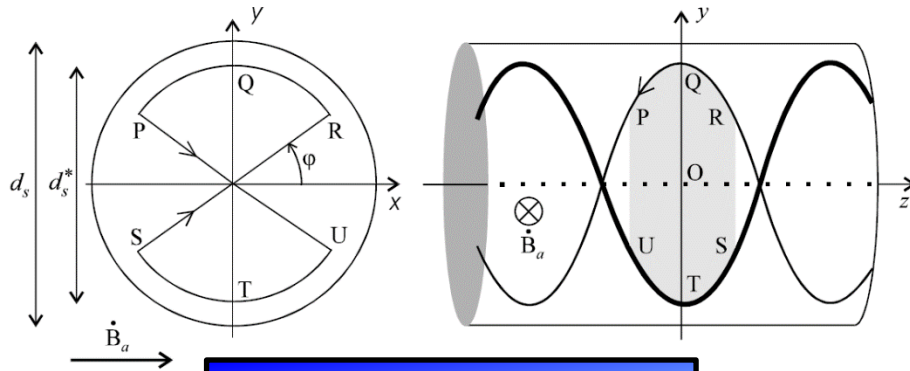
$$\begin{aligned}
 &U_{source}, I_{source} \\
 &U_R = R_{EL} I \\
 &I_C = C dU_C / dt \\
 &U_L = L dI_L / dt
 \end{aligned}$$

$$\begin{aligned}
 Q_{OHM} &= R_{EL} I^2 \\
 \Delta T &= R_{TH} Q_{ex} \\
 Q_{TH} &= C_{TH} dT / dt
 \end{aligned}$$

Dynamic - *Tricky*



Implementation of the Magnet Dynamic Behavior in the Model



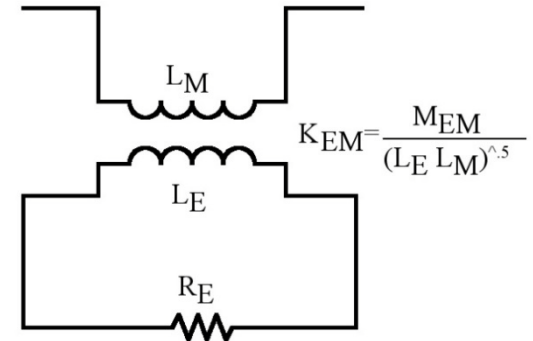
Physical Behavior

$$\begin{cases} P_{IF} = \beta V \dot{B}_t^2 \\ I_{IF} = \pm \frac{2d_s^* B_i}{\mu_0} = \pm \frac{2d_s^* \tau \dot{B}_t}{\mu_0} = \pm \beta d_s^* \dot{B}_t \end{cases}$$

$$\begin{cases} \dot{B}_t = \dot{B}_a + \dot{B}_i \\ \dot{B}_t = \pm \frac{1}{\beta d_s^*} I_{IF} \\ \dot{B}_a = f_M \dot{I}_M \\ \dot{B}_i = \frac{\mu_0}{2d_s^*} \dot{I}_{IF} \end{cases} \rightarrow \begin{cases} \pm \frac{1}{\beta d_s^*} I_{IF} = f_M \dot{I}_M + \frac{\mu_0}{2d_s^*} \dot{I}_{IF} \\ \pm \frac{V}{\beta d_s^*} I_{IF} = \frac{f_M V}{d_s^*} \dot{I}_M + \frac{\mu_0 V}{2d_s^*} \dot{I}_{IF} \end{cases}$$

$$R_E = \frac{V}{\beta d_s^*}, \quad M_{EM} = \frac{f_M V}{\beta d_s^*}, \quad L_E = \frac{\mu_0 V}{2\beta d_s^*}$$

$$\begin{aligned} P_{IF} &\equiv R_E I_E^2 \\ I_{IF} &\equiv I_E \\ \tau_{IF} &\equiv L_E / R_E \end{aligned}$$



Lumped-Element Equivalent Model

$$P_E = R_E I_E^2 \rightarrow R_E = \frac{P_E}{I_E^2} = \frac{V}{\beta d_s^*}$$

For any coupling – loss loop

$$-R_E I_E = -M_{EM} \dot{I}_M + L_E \dot{I}_E$$

A. Verweij, "Electrodynamics of Superconducting Cables in Accelerator Magnets," 1995.

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Outlook

CLIQ – Conclusion...

Design

- Heat deposited in the copper matrix
- Not relying on thermal diffusion
- Quick and global quench initiation
- Robust system

Tests

- 30+ tests on a 2 m long NbTi quadrupole magnet (MQXC2)
- 1000+ tests on a small-size solenoid magnet
- Key parameters studied and optimized
- CLIQ with compensation coil

Modeling

- 2D
- Lumped-Elements
- Electro-Thermal
- Dynamic behaviour

... and Future Steps

- Multiple CLIQ Systems
- Effect of a delay in the triggering
- Redundancy

- CERN, NbTi quadrupole magnet (MQXC2)
- FNAL, Nb₃Sn quadrupole magnet (HQ2→MQXF)
- Oxford Instruments, Nb₃Sn solenoid magnet
- CERN, NbTi Individually-Powered Quadrupole (IPQ)
- CERN, NbTi solenoid magnet (Multi-CLIQ)

- Validation of the model on a wide variety of practical cases
- More flexibility, modularity, GUI
- Migration from PSpice to Simulink? 3D?

Thanks to

Vladimir Datskov, Alexey Dudarev, Glyn Kirby,
Kevin Sperin, Herman ten Kate, Arjan Verweij,

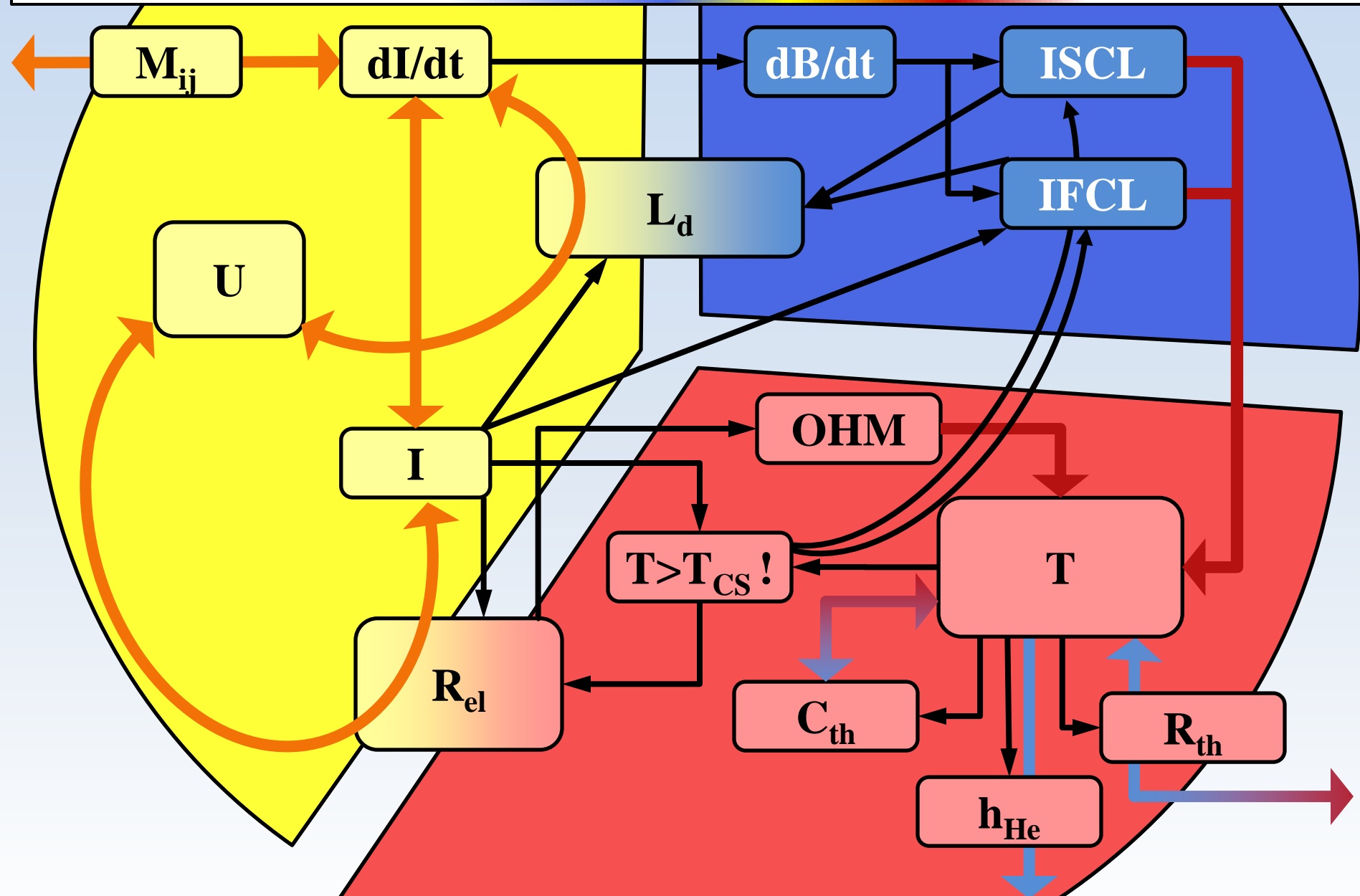
Tim Mulder, Bernhard Auchmann, Christian Giloux, Jerome
Feuvrier, Francois-Olivier Picot, Nikolay Kopeykin, Igor Titenkov,
Johan Bremer, Laetitia Dufay Chantat, Tiemo Winkler, ...

QUESTIONS?

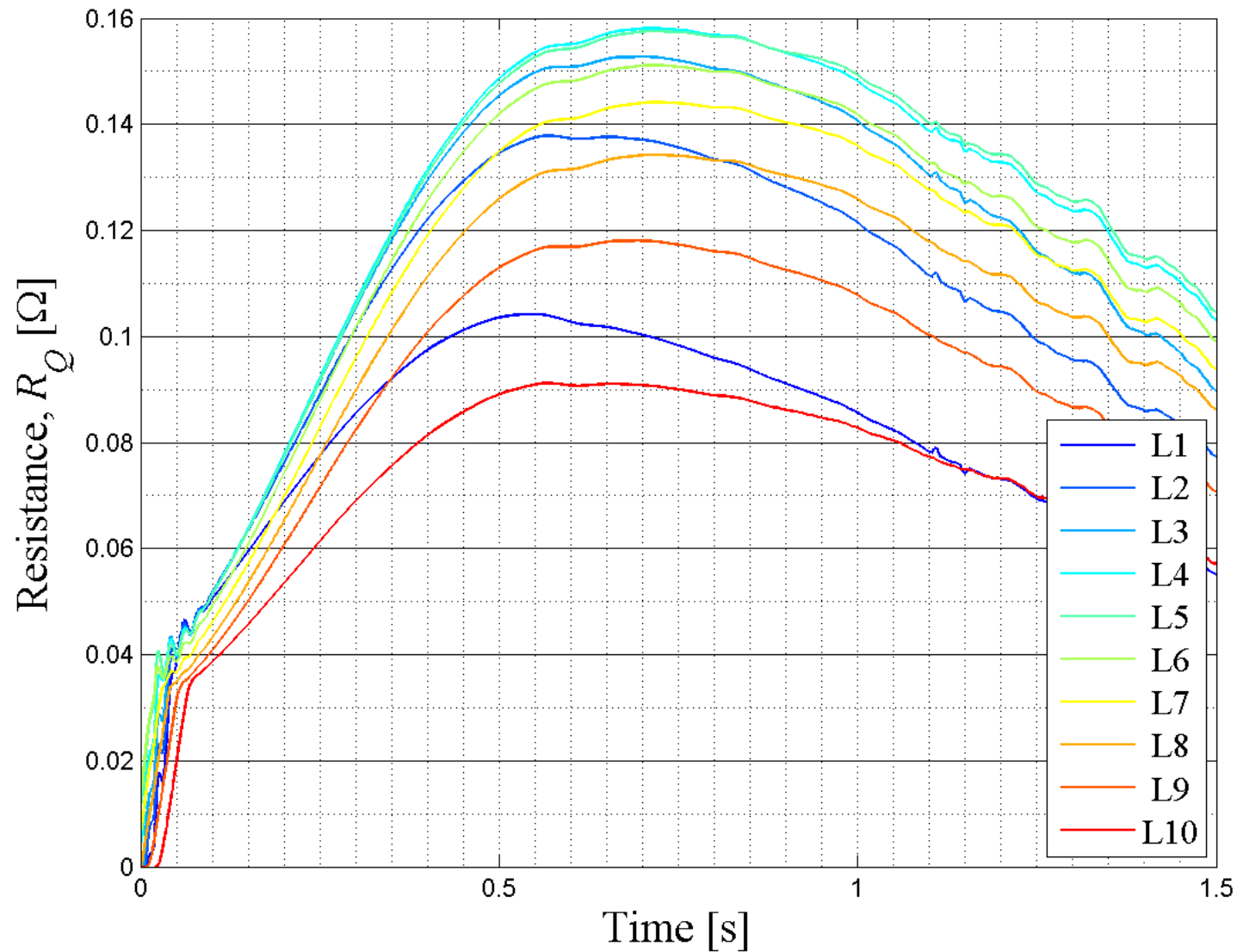
Ask me the
CLIQ
Recipe!

Emmanuele.Ravaioli@cern.ch

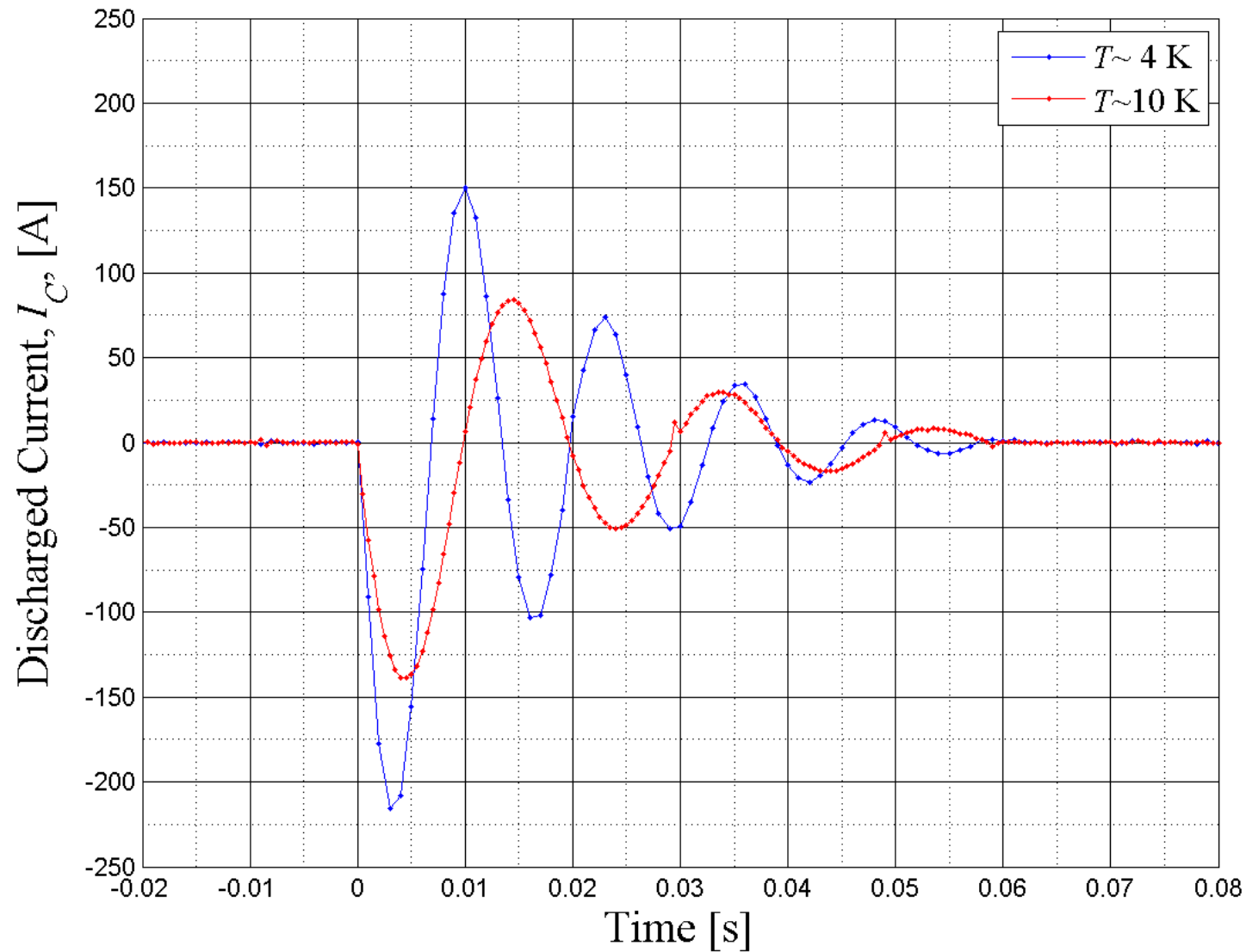
LEDET Lumped-Element Dynamic ElectroThermal model



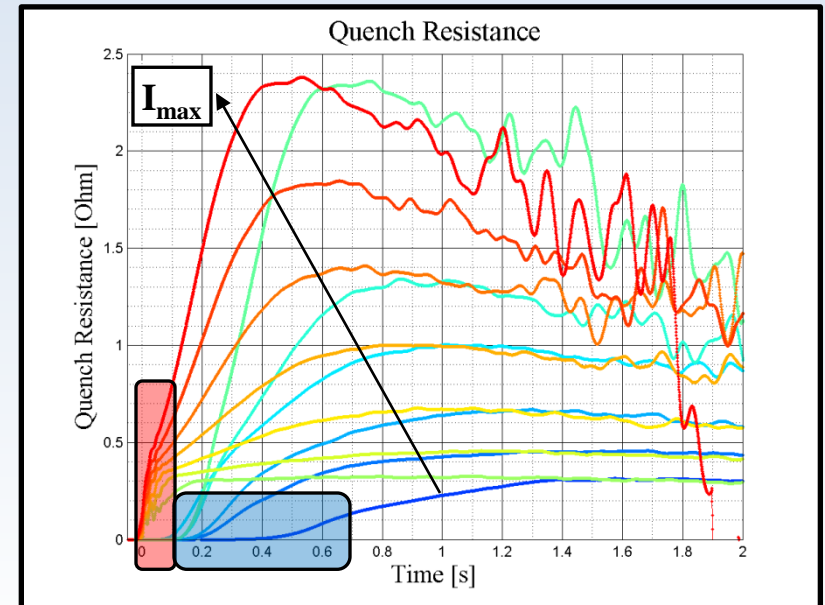
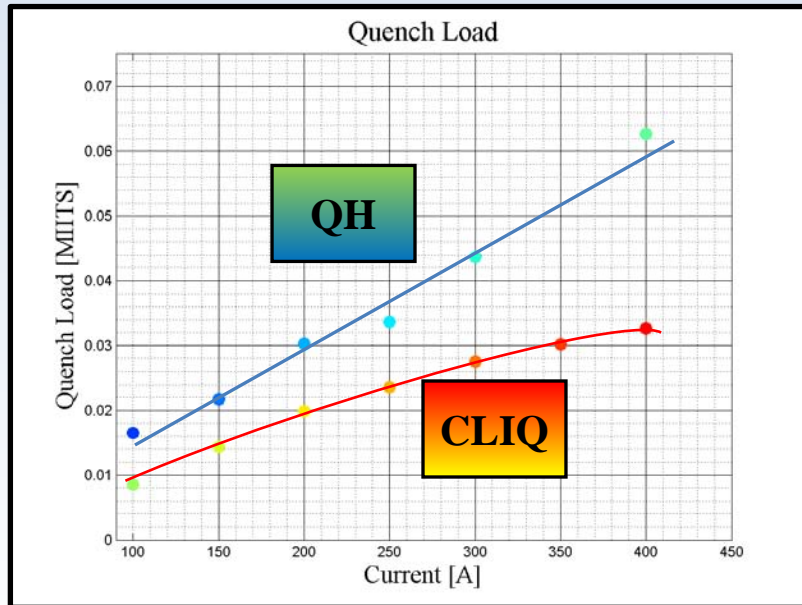
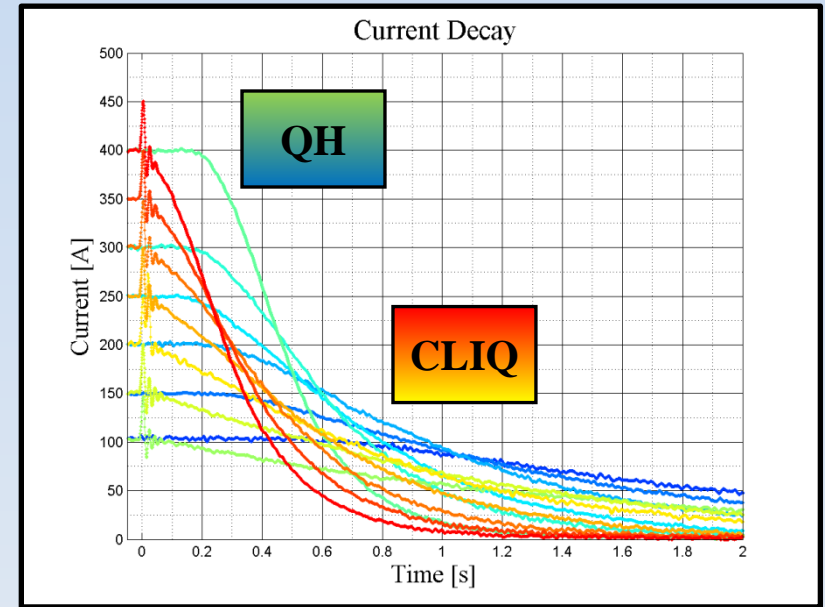
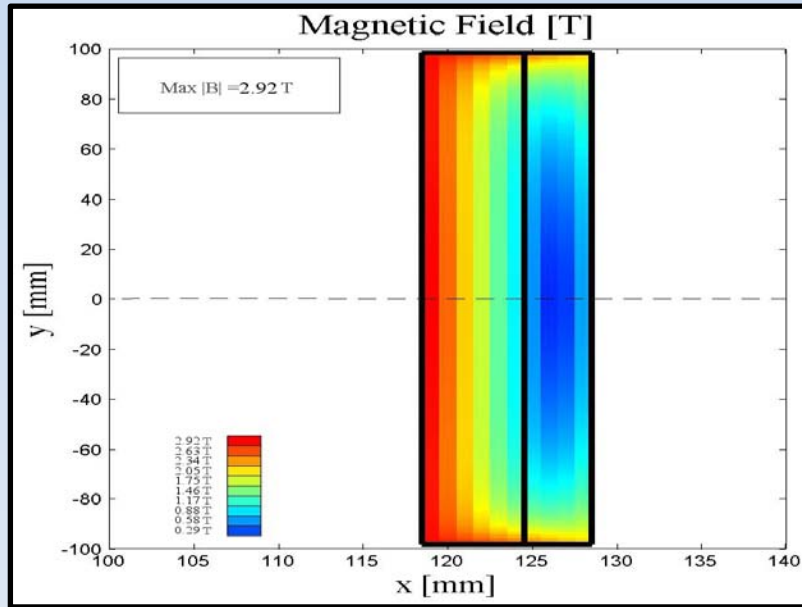
CLIQ – Coupling-Loss Induced Quench – Quench in the 10 Layers



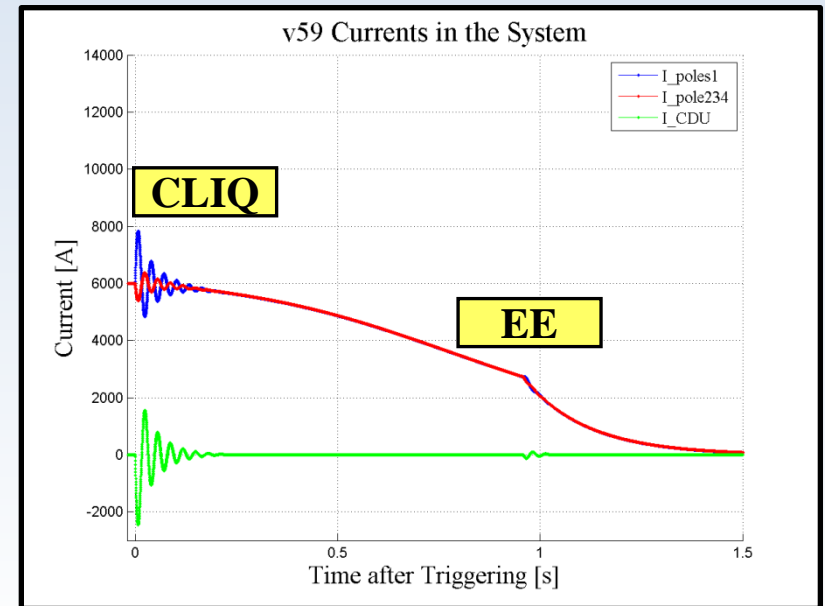
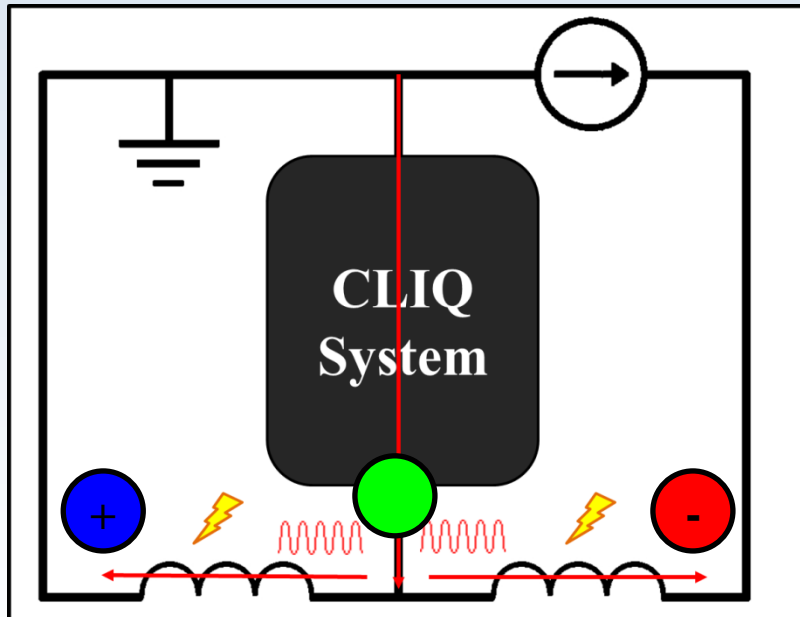
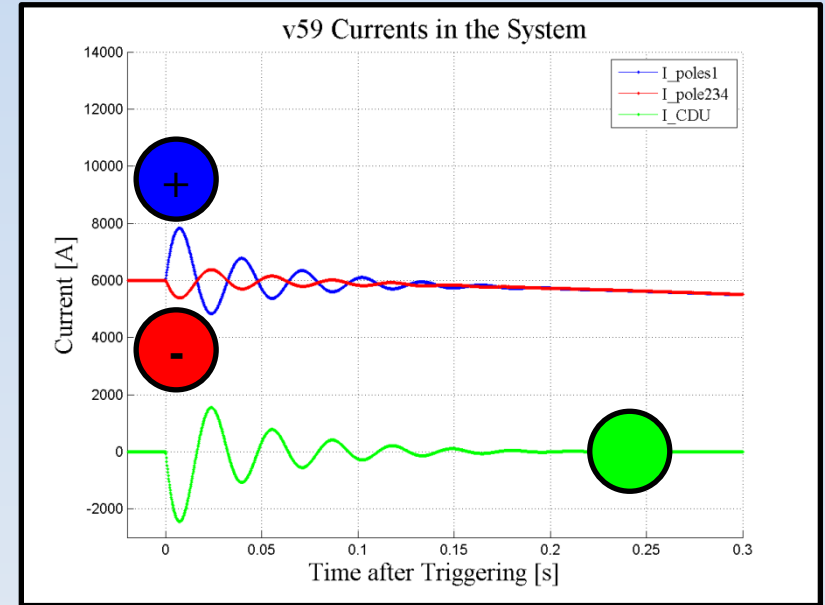
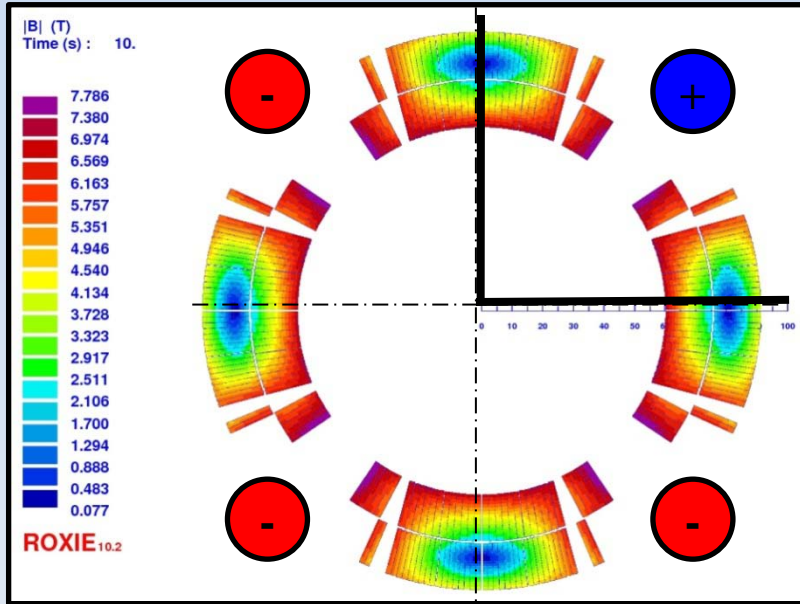
Dynamic Effects related to Inter-Filament Coupling Currents



CLIQ Tests on a Superconducting Solenoid – CLIQ vs QH



CLIQ Tests on a Superconducting Quadrupole Magnet – I=6 kA – d_EE=950 ms



CLIQ Tests on a Superconducting Quadrupole Magnet

