

# Simulation of liquid level, temperature and pressure inside a 2000 liter liquid hydrogen tank during a truck transportation

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# OUTLINES

- 1. INTRODUCTION**
- 2. GOVERNING EQUATIONS**
- 3. ANALYTICAL MODEL**
- 4. TERMAL ANALYSIS**
- 5. OSCILLATION AND TERMAL ANALYSES**
- 6. SAMMARY**

# 1. INTRODUCTION

Sustainable/renewable energy such as solar energy, wind energy and tidal energy is greatly attractive as an alternative energy source.

Using electrolysis technique, sustainable energy can be changed to hydrogen, which is an ultimate energy source because of chemical reaction with only water.

➡ Liquid Hydrogen (20.3 K, high density)



Production of H<sub>2</sub>



Transport of H<sub>2</sub>



Use of H<sub>2</sub>

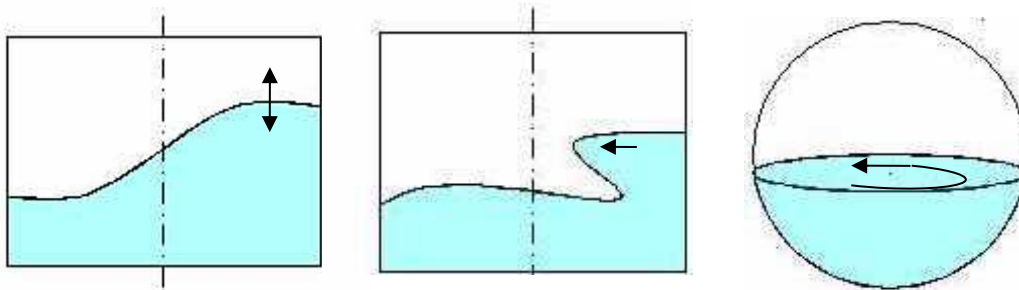
# Background

Liquid hydrogen (LH<sub>2</sub>) is expected to be the ultimate energy medium for the worldwide storage and transport of large amounts of H<sub>2</sub>.

To establish LH<sub>2</sub> worldwide storage and land/marine transport, it is important to develop LH<sub>2</sub> tanks/carriers.



The complex sloshing conditions inside an LH<sub>2</sub> tank during transportation have been estimated:



**LH<sub>2</sub>/LNG:**

**Density; ca. 1/6**

**Viscosity; ca. 1/8**

# Objectives

**Synchronous measurements of LH<sub>2</sub> level, temperature and pressure inside a 2000 liter tank were carried out during a truck transportation:**

**an LH<sub>2</sub> level exceeding 1200 mm**

**average period of oscillation of 2 s**

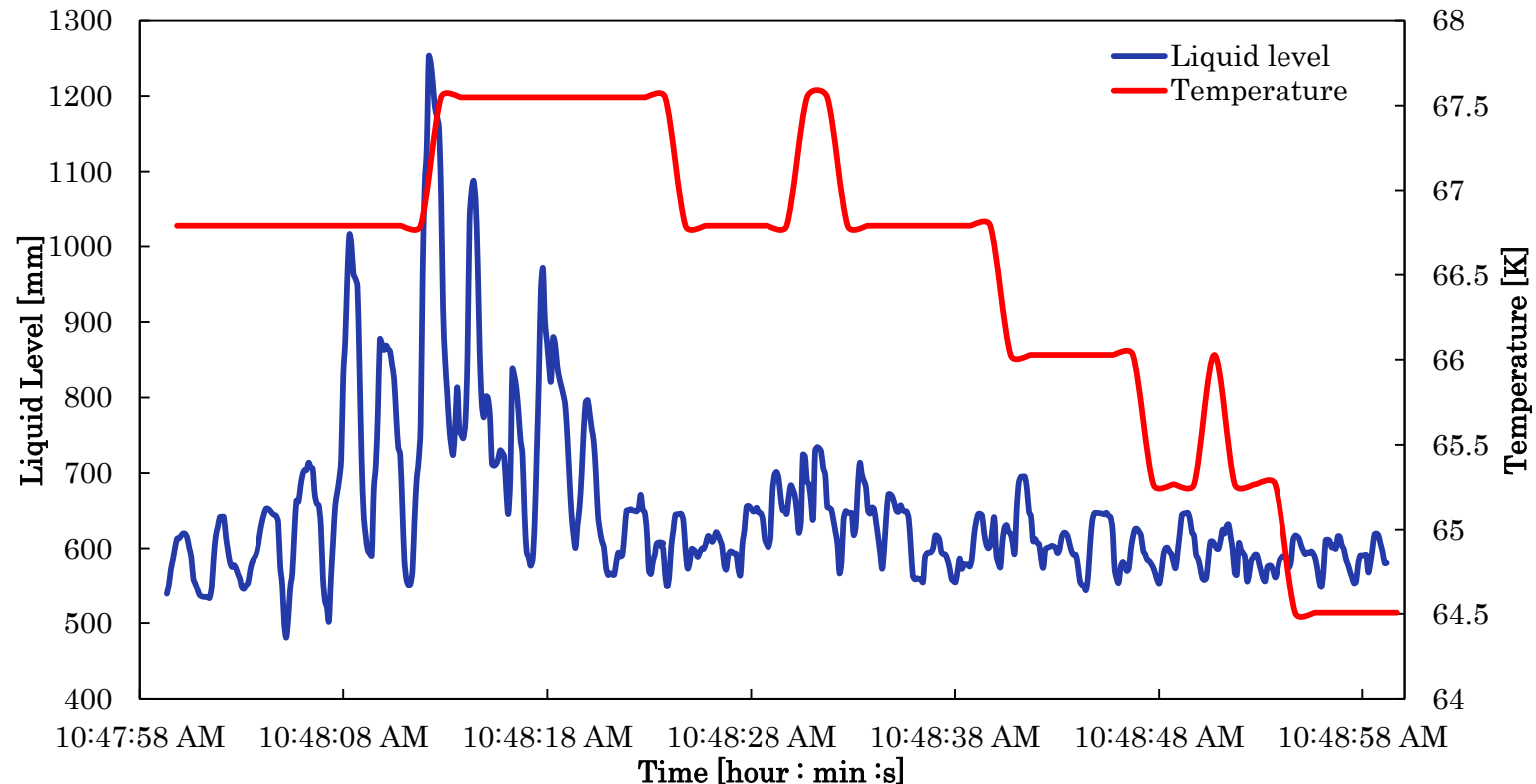
**decreasing temperature and pressure after truck started**



**Objectives of this work is to make a simulation model of sloshing of LH<sub>2</sub> inside a 2000 liter tank during a truck transportation using a multipurpose software ANSYS CFX.**

# Background

## Truck transportation test of 2000 L LH<sub>2</sub> tank\*



**Average period of oscillation: 2.0 s**

**Max liquid level: 1252 mm**

**Temperature: 67.5 K → 64.5 K**

**\*Takeda *et al.* : Proc. ICEC24-ICMC2012**

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# 2. GOVERNING EQUATIONS

## i ) Equation of continuity

$$\frac{\partial}{\partial t}(r_\alpha \rho_\alpha) + \nabla \cdot (r_\alpha \rho_\alpha \vec{U}_\alpha) = 0 \quad (1)$$

## ii ) Equation of motion

$$r_\alpha \rho_\alpha \left[ \frac{\partial \vec{U}_\alpha}{dt} + (\vec{U}_\alpha \cdot \text{grad}) \vec{U}_\alpha \right] = -\text{grad} r_\alpha p_\alpha + r_\alpha \mu_\alpha \Delta \vec{U}_\alpha + \vec{f}_\alpha \quad (2)$$

## iii ) Buoyancy

$$F_\alpha = (\rho_\alpha - \rho_{ref}) g \quad (3)$$



# 2. GOVERNING EQUATIONS

iv ) Volume fraction

$$r_{\alpha} = \frac{V_{\alpha}}{V} \quad (4)$$

v ) Equation of state (Redlich Kwong model)

$$p_{\alpha} = \frac{RT_{\alpha}}{v_{\alpha} - b} - \frac{a(T_{\alpha})}{v_{\alpha}(v_{\alpha} + b)} \left( a = a_0 \left( \frac{T_{\alpha}}{T_{\alpha c}} \right)^{-0.5}, \quad a_0 = \frac{0.42747R^2T_{\alpha c}^2}{p_{\alpha c}}, \quad b = \frac{0.08664RT_{\alpha c}}{p_{\alpha c}} \right) \quad (5)$$

vi ) Equation of specific heat at constant pressure

$$C_{\alpha,p}^0 = R_{\alpha} \left( a_{\alpha,1} + a_{\alpha,2}T_{\alpha} + a_{\alpha,3}T_{\alpha}^2 + a_{\alpha,4}T_{\alpha}^3 + a_{\alpha,5}T_{\alpha}^4 \right) \quad (6)$$

# 2. GOVERNING EQUATIONS

vii ) Equation of heat energy

$$\begin{aligned} \frac{\partial}{\partial t} (r_\alpha \rho_\alpha e_\alpha) + \nabla \cdot (r_\alpha (\rho_\alpha \vec{U}_\alpha e_\alpha)) \\ = \nabla \cdot (r_\alpha \lambda_\alpha T_\alpha) + r_\alpha \tau_\alpha (\nabla \vec{U}_\alpha)^2 + S_{E\alpha} + Q_\alpha \end{aligned} \quad (7)$$

viii) Equation of phase generation density

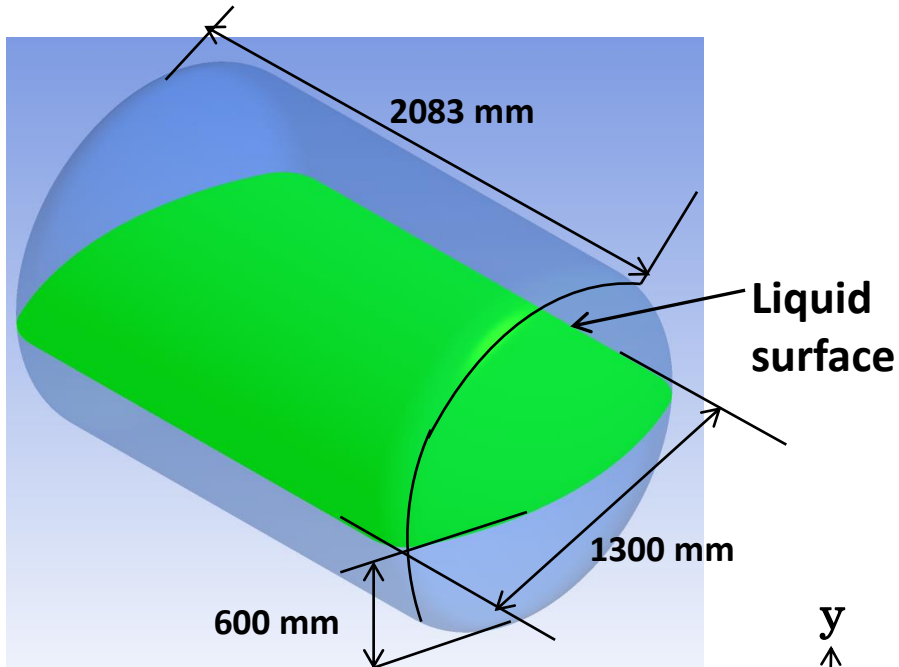
$$\dot{m}_{\alpha,\beta} = \frac{k_\alpha (T_\alpha - T_s) - k_\beta (T_s - T_\beta)}{L} \quad (8)$$

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# 3. ANALYTICAL MODEL

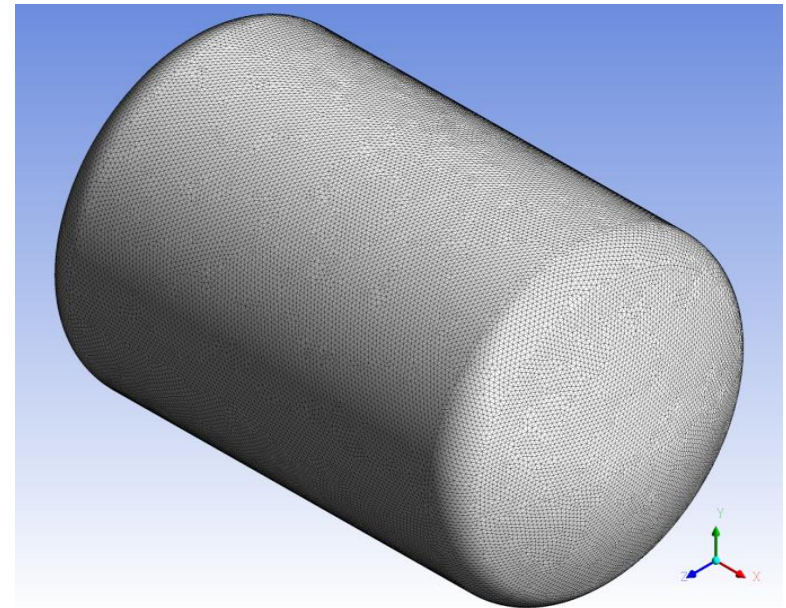
## (1) 2000 liter tank



Analytical Model

LH<sub>2</sub>: 1189 liter/600 mm

Smooth initial surface position



Mesh Configuration

Number of meshes:  $1.66 \times 10^6$

Configuration: tetrahedral

Maximum size: 16.5 mm

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# 4. THERMAL ANALYSIS

## (1) Outlines

### (a) Analysis condition

Evaporation and convection of saturated LH<sub>2</sub> (20.3 K) was negligible.

### (b) Initial condition

Temperature of GH<sub>2</sub> was set 20.3 K.

LH<sub>2</sub> level was set 600 mm.

### (c) Boundary condition

Uniform heat leak from wall of the tank was set 17 W, which was obtained through the experiment.

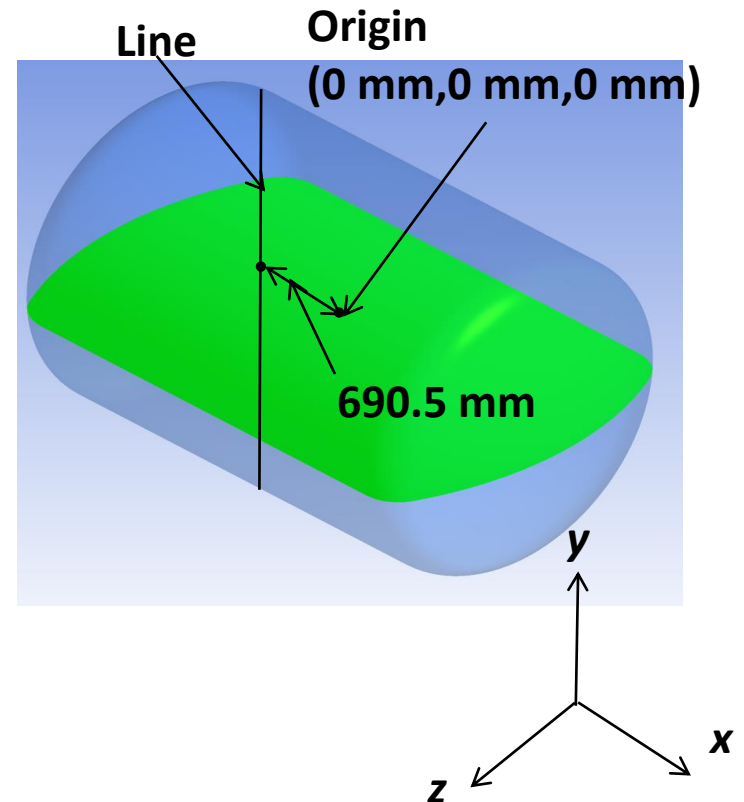
# 4. THERMAL ANALYSIS

## (1) Outlines

### (d) Indication of numerical results

1) Temperature distribution of  $\text{GH}_2$  in the tank at  $z = 0$  mm plane and  $x = -690.5$  mm plane, where the origin was defined as the center of gravity.

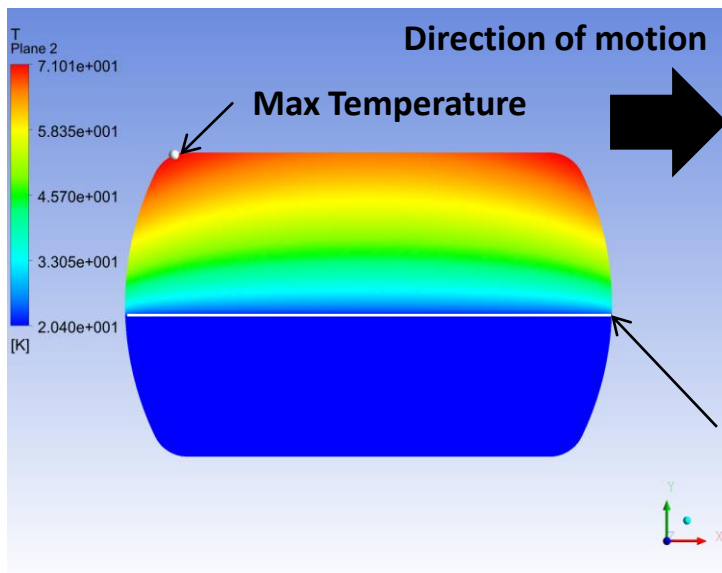
2) Temperature distribution along the line located in  $z = 0$  mm and  $x = -690.5$  mm, where the liquid level and temp. sensor was installed.



# 4. THERMAL ANALYSIS

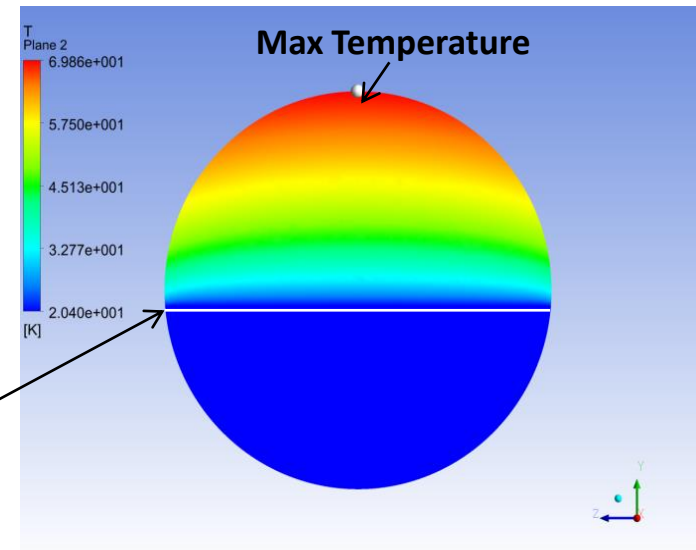
## (2) Numerical results

### (a) Temperature distribution in the tank



Side section at  $z = 0$  mm

Maximum temperature: 71.0 K



Vertical section at  $x = -690.5$  mm

Maximum temperature: 69.8 K

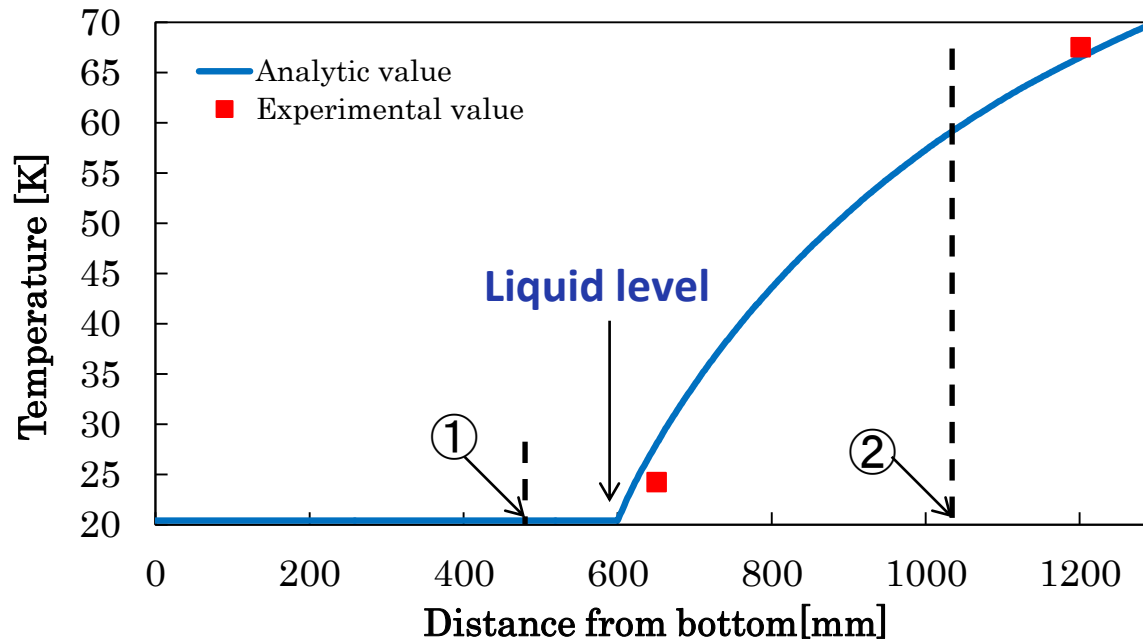
Maximum temperature in the tank: 71.0 K



# 4. THERMAL ANALYSIS

## (2) Numerical results

### (b) Temperature distribution along the line



① Temperature at 650 mm from bottom (50 mm from surface)

Experiment: 24.2 K, Analysis: 28.0 K

② Temperature at 1200 mm from bottom (600 mm from surface)

Experiment: 67.5 K, Analysis: 66.5 K

# OUTLINES

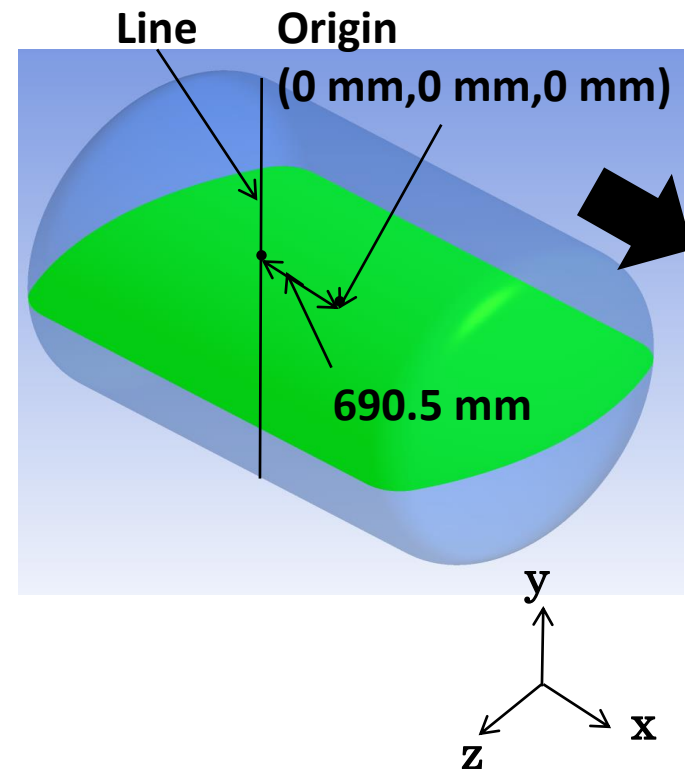
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# 5. OSCILLATION AND THERMAL ANALYSES

## (1) Outlines

### (a) Analysis condition

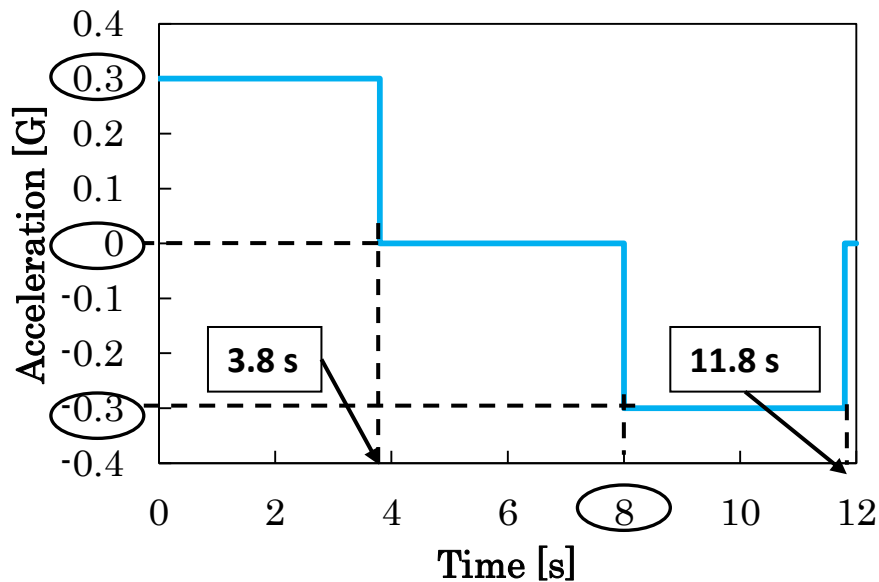
- ⊙ Temperature and pressure of  $\text{GH}_2$  can change.
- ⊙ Evaporation of  $\text{LH}_2$  and heat leak of 17 W.
- ⊙ Time step of 0.01 s and total time of 12 s.
- ⊙ Horizontal vibration: see next view graph.



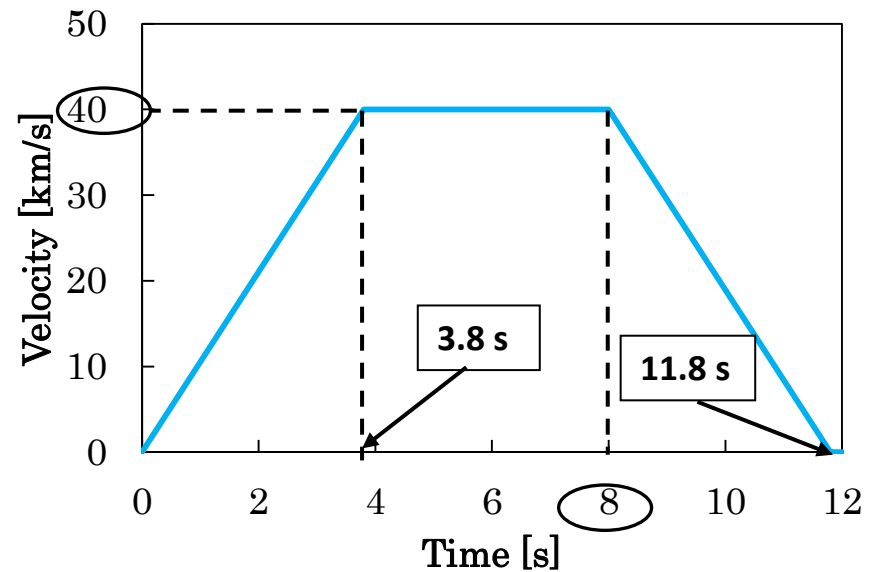
(Machine time: 15 d)

# 5. OSCILLATION AND THERMAL ANALYSES

## (1) Outlines: (a) Analysis condition



(a) Acceleration



(b) Velocity

# 5. OSCILLATION AND TERMAL ANALYSES

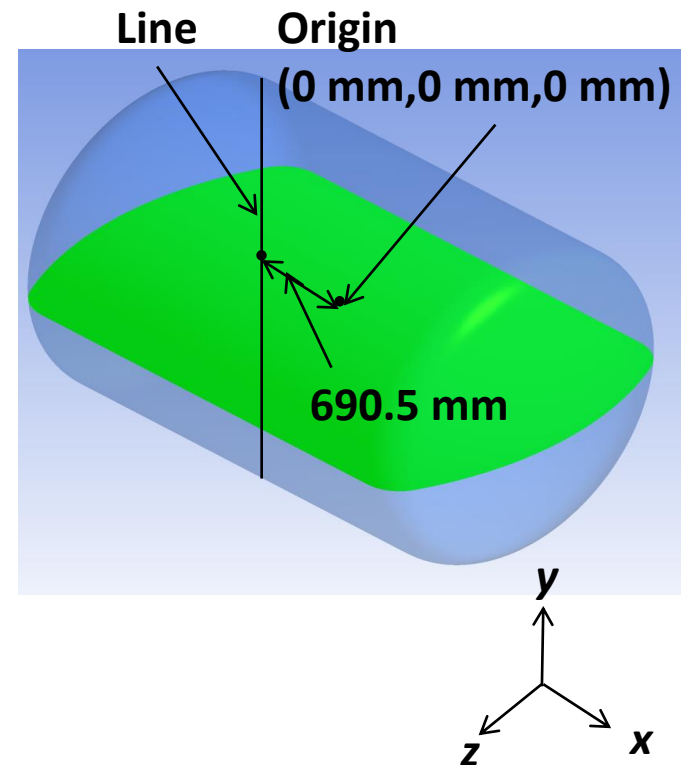
## (1) Outlines

### (b) Initial condition

- ⊙ Numerical results of thermal analysis under the static condition.

### (c) Boundary condition

- ⊙ Uniform heat leak of 17 W from wall of the tank, which was obtained through the experiment.



# 5. OSCILLATION AND THERMAL ANALYSES

## (d) Indication of numerical results

### ⊙ Simulation:

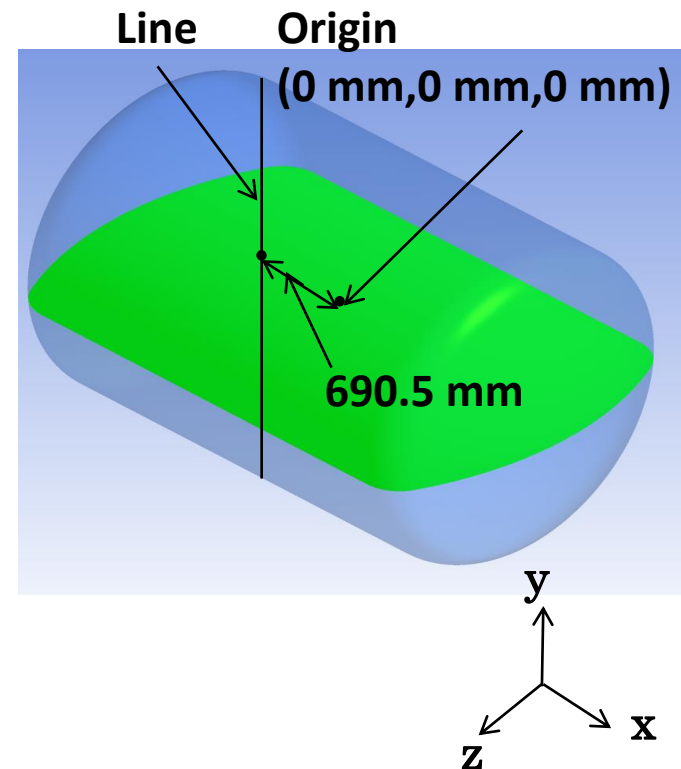
- 1) LH<sub>2</sub> surface oscillation
- 2) Temperature distribution

Side section at  $z = 0$  mm

Vertical section at  $x = -690.5$  mm

### ⊙ Numerical results:

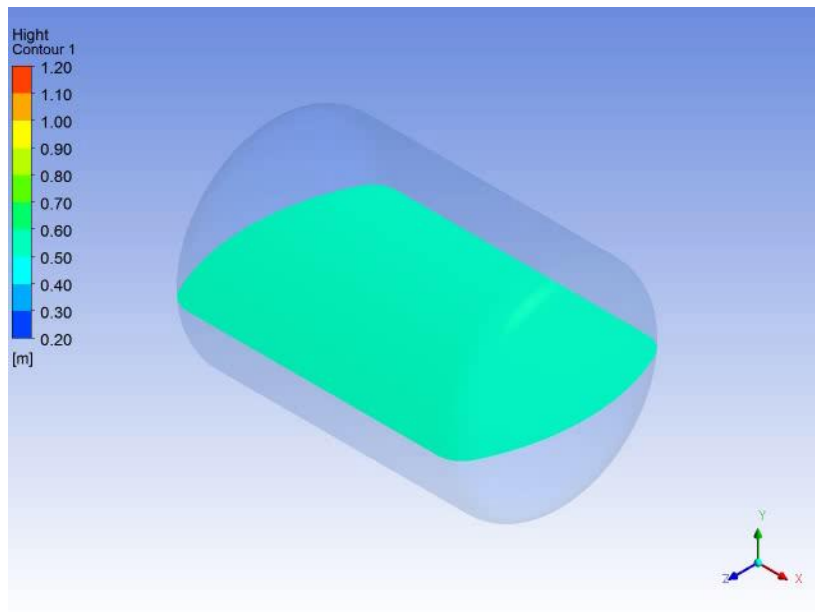
- 1) LH<sub>2</sub> Level and temperature of GH<sub>2</sub> at 1200 mm from bottom on the line.
- 2) Average temperature and pressure of GH<sub>2</sub> in the tank.



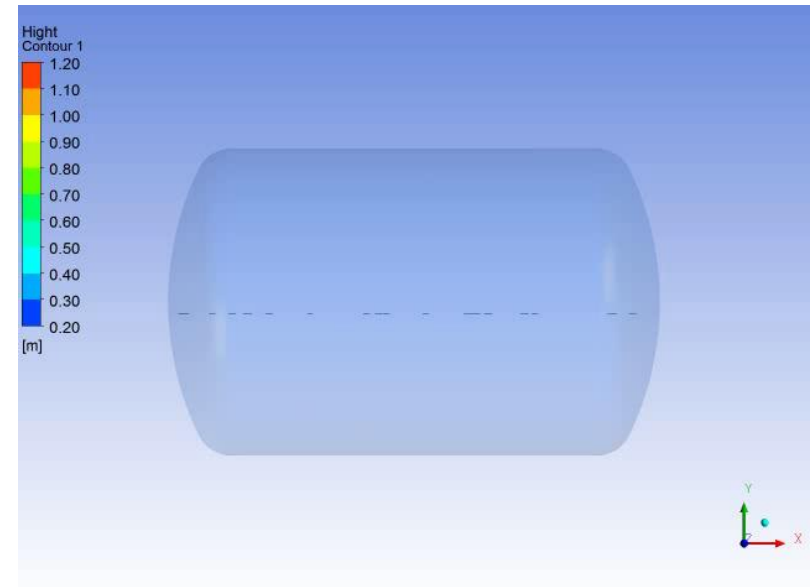
# 5. OSCILLATION AND THERMAL ANALYSES

## (2) Simulation

### (a) LH<sub>2</sub> Surface oscillation



3D model

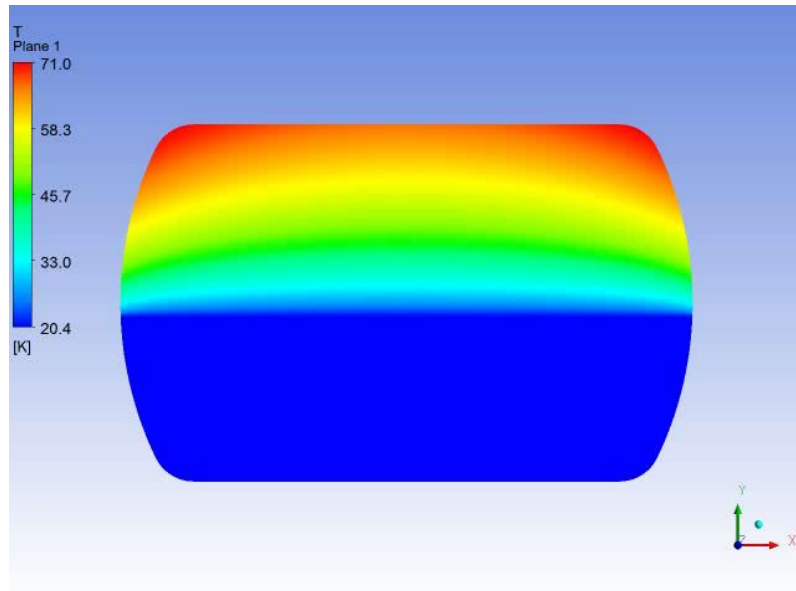


Side View

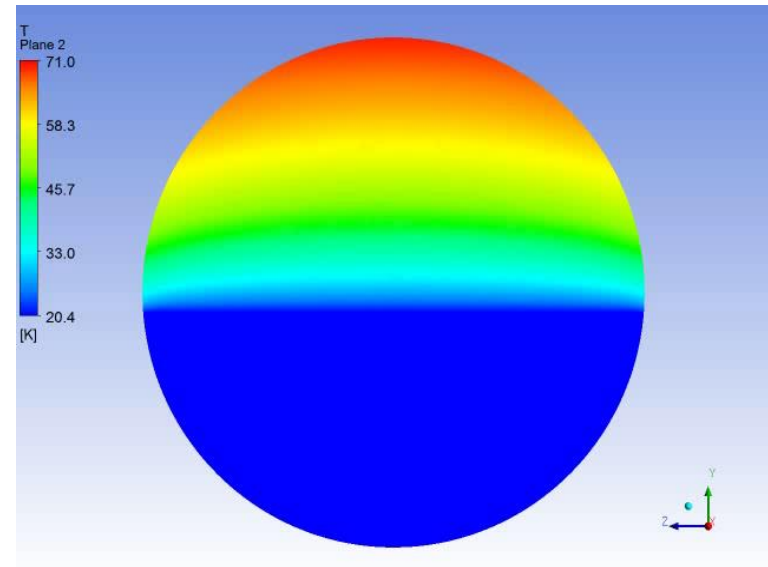
# 5. OSCILLATION AND THERMAL ANALYSES

## (2) Simulation

### (b) Temperature distribution



Side section at  $z = 0$  mm



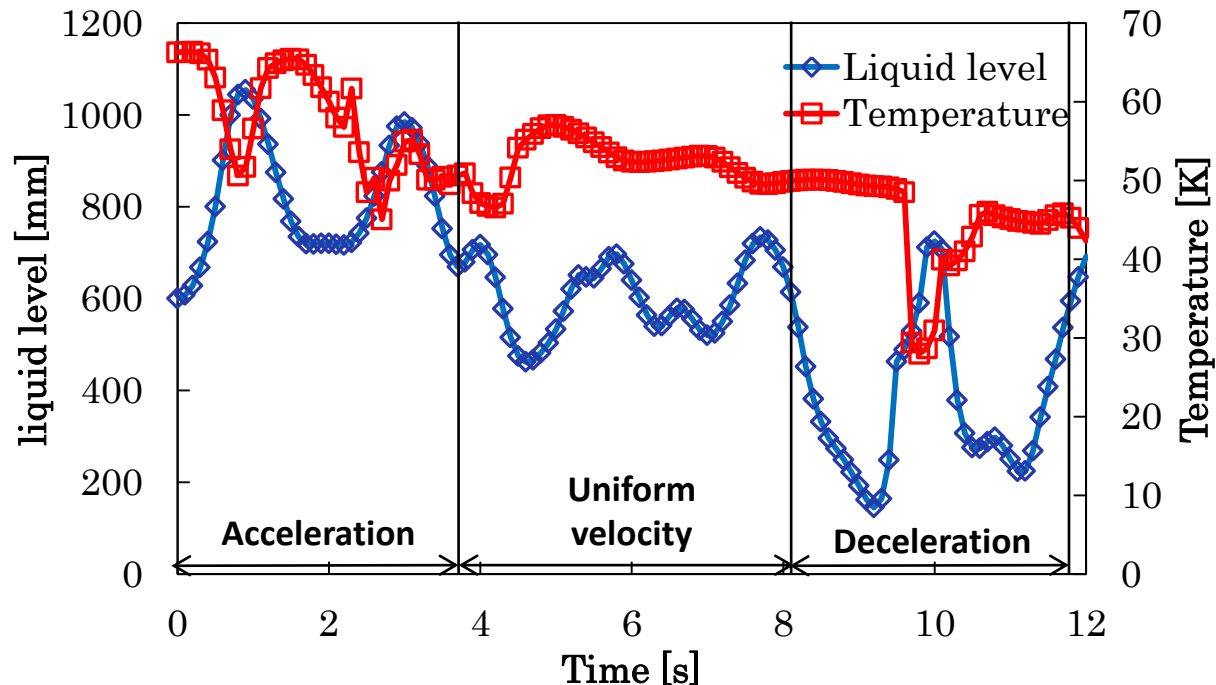
Vertical section at  $x = -690.5$  mm

Maximum temperature in the tank: 71.0 K  $\rightarrow$  47.6 K



# 5. OSCILLATION AND THERMAL ANALYSES

(3) Numerical results : (a) LH<sub>2</sub> level and temperature of GH<sub>2</sub> at 1200 mm from the bottom on the line

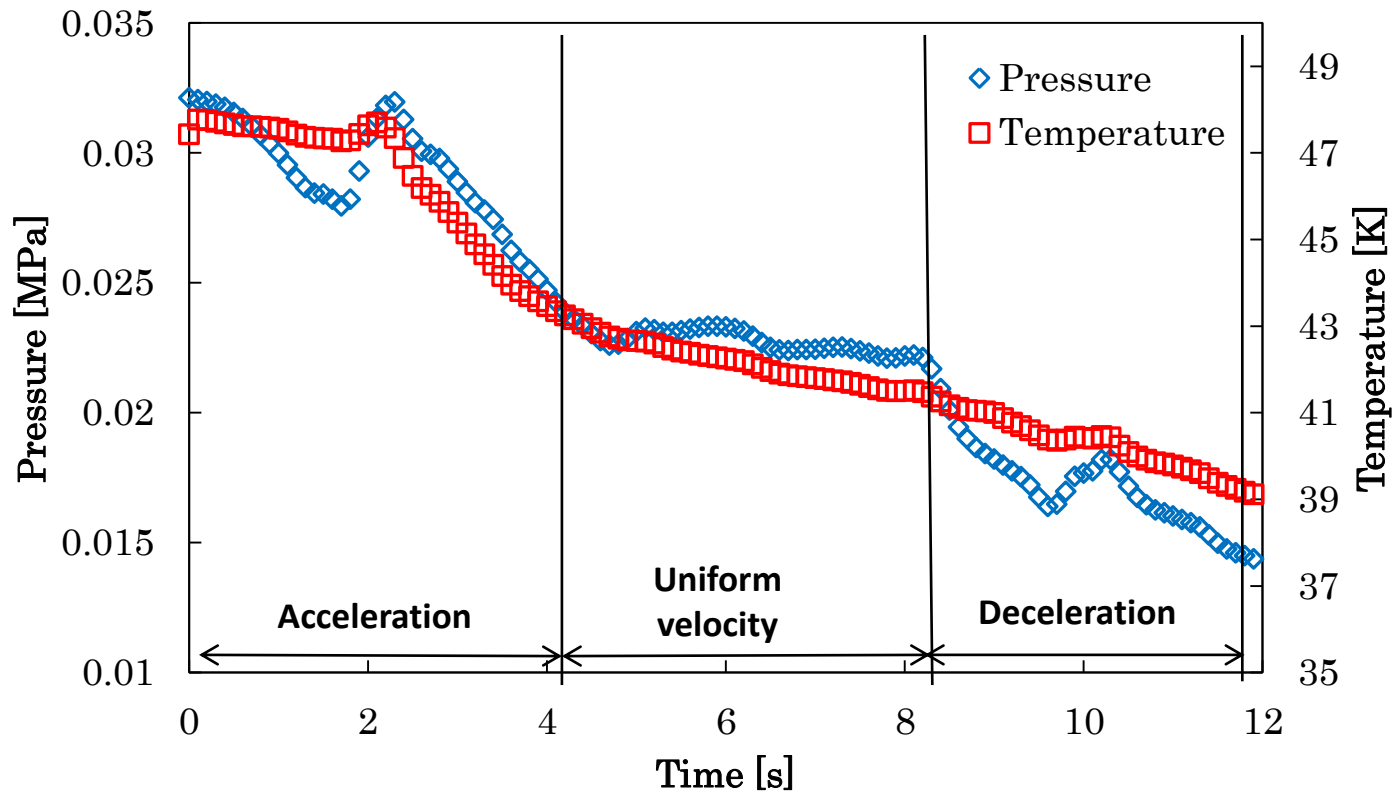


Average period of oscillation: 2 s ↔ 2.0 s (Exp.)

Max liquid level: 1054 mm ↔ 1252 mm (Exp.)

# 5. OSCILLATION AND THERMAL ANALYSES

## (3) Numerical results: (b) Average temperature and pressure of $\text{GH}_2$



Temperature: 47.8 K  $\rightarrow$  39.1 K

Pressure: 0.032 MPaG  $\rightarrow$  0.014 MPaG

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# 6. SAMMARY

- ⊙ **(1) Simulation of LH<sub>2</sub> surface oscillation, temperature and pressure inside a 2000 liter tank during truck transportation were carried out using an ANSYS CFX.**
- ⊙ **(2) Periodic oscillation of LH<sub>2</sub> level, maximum LH<sub>2</sub> level over 1000 mm and decreasing average pressure with decreasing average temperature inside the tank were demonstrated successfully.**
- ⊙ **(3) Oscillation and thermal analyses of a large LH<sub>2</sub> tank of 1250 m<sup>3</sup> for marine transportation will be carried out as a future work.**

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