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Design of the Helium Purifier for IHEP-ADS Helium Purification System

Zhang Jianqin, Li Shaopeng *, Zhang Zhuo, Ge Rui, Bian Lin

Department of Accelerators, Institute of High Energy Physics, Chinese Academy of Science, 19B Yuquan Lu, Shijingshan District, Beijing, China

Abstract

Helium Purification System is an important sub-system in the Accelerator Driven Sub-critical System of the Institute of High Energy Physics (IHEP-ADS). The purifier is designed to work at the temperature of 77K. The oil and moisture are removed by coalescing filters and a dryer, while nitrogen and oxygen are condensed by a phase separator and then adsorbed in several activated carbon absorption cylinders. The purifier will work in a flow rate of 5.2g/s at 20MPa in continuous operation of 12 hours. After purification, the purified helium has an impurity content of less than 5ppm.

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Keywords: Helium purifier; heat transfer; numerical; activated carbon, absorption

1. Introduction

There are a lot of superconducting facilities in the Accelerator Driven Sub-critical System of the Institute of High Energy Physics (IHEP-ADS), which need an enlarged cryogenic system to supply more liquid helium. Since helium is rare and expensive, the helium purification system is under construction to meet the high purity standard of the cryogenic system. The impure helium is mainly from the tests of superconducting cavities and the failures of the cryogenic system. The impurities of the impure helium can solidify at low temperature, which will choke the tubes and damage the turbo expanders. The helium purification system can keep the purity of helium for 99.9995% and has a storage capacity of 20000Nm³ (including impure helium and pure helium) at 20MPa. The simplified process scheme of the purification system is in Fig.1, which includes gas bag, compressor, coalescing filters, dryer, helium

* Corresponding author. Tel.: +86 10 88236468; fax: +86 10 88236033

E-mail address: lisp@ihep.ac.cn (Li Shaopeng).

up. The liquid nitrogen in the dewar is emptied to the buffer tank when the pressure of the dewar increases. The absorbent cylinders are heat to 100°C with an evacuation . The regeneration is completed by pressurization with pure helium. The purifier is equipped with an automatically process control system and a local operator panel. So the purification and the regeneration process can be controlled automatically and manually.

3. Design of helium purifier

The purifier includes dewar, outer heat exchanger, high pressure heat exchanger, condenser, liquid air separator and absorption cylinders. The dewar is fitted with a quantity of liquid nitrogen, in which condenser, liquid air separator and absorbent cylinders are submerged. The height of the purifier is 3050mm, and the diameter of dewar is 600mm with a thickness of 5mm. The outer heat exchanger acts as dryer which brings down the water dew point to approximately 1°C. The helically coiled tube-in-tube heat exchanger is selected as the high pressure heat exchanger, which is compact and high efficient. The outside diameter of the inner tube is 8mm with a wall thickness of 1.5mm, while the outside diameter of the outer tube is 16mm with a wall thickness of 3mm. The diameter of the coil is 270mm. In order to decrease the drop pressure of the tube, the heat exchanger is divided into five layers. The result of the high pressure heat exchanger is shown in table 2 and the tube length is 11.84m. The liquid air separator (vol. 18.3l) collects the liquid air at the bottom of the separator. After the liquid air separator, the impurities of the gas are less than 0.32%. There are 6 absorption cylinders (vol. 18.3l) which are divided into two ways and connected in series. The absorbent in the absorber is coconut shell activated carbon with a good performance at 77K.

Table 2. Parameters of the helically coiled tube-in-tube heat exchanger

	Input temperature K	Input Pressure MPa	Flow rate g/s	Output temperature K	Pressure drop Pa
Input gas	300	20	5.2	93.5	5140
Output gas	78	19.8	4.9	295	2360

3.1. Numerical studies of high pressure heat exchanger

The designed helically coiled tube-in-tube heat exchanger is model with CFD methods [3, 4]. The input gas is in the annulus and the output gas is in the inner tube. These two fluids are counter-flow. Fluent 14.0 in ANSYS is used to analysis the heat transfer and fluid flow in the heat exchanger. The transport and thermal properties of helium is dependent on the temperature. The RNG k-ε model with standard wall functions is used in the analysis. The boundary condition of inlet is velocity, as the outlet is pressure. The convergence residual is 1.0e-05. The results show that the difference of the outlet temperature between the calculated and the numerical is less than 0.5% and the difference of the pressure drop is less than 20%. The temperature distribution of the whole heat exchanger is shown in Fig.2. And the sectional views of the outlet temperature in the inner tube and the annulus are shown in Fig.3. The secondary flow caused by the centrifugal forces can enhance the heat transfer in the inner tube and the annulus.

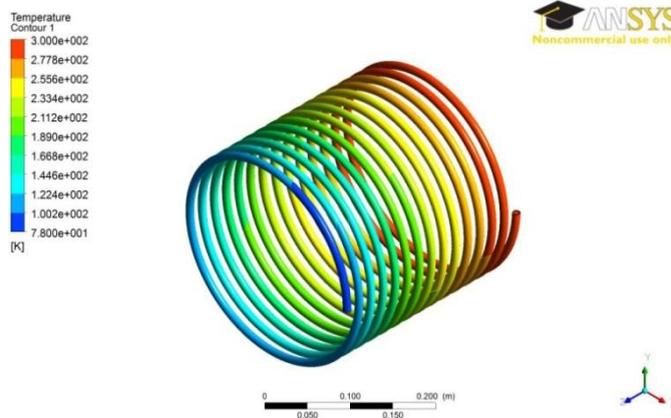


Fig.2. Temperature profiles of the helically coiled tube-in-tube heat exchanger

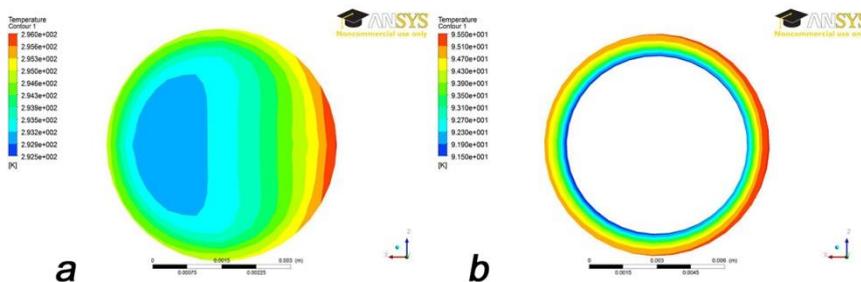


Fig.3. Temperature profiles of the outlet in (a) the inner tube and (b) the annulus

3.2. Experimental studies of the absorbents

The Linde activated carbon is widely used in the purification. The properties of the static and dynamic adsorption of Linde coconut shell activated carbon are studied experimentally. The adsorption isotherms of N₂ and O₂ (77K) are presented in Fig.4a. In the figure, it shows that the static adsorption capacity of O₂ is larger than that of N₂ and they belong to type I. The specific surface area is 999.72m²/g which is fitted with N₂ adsorption isotherm by the BET model [5]. The pore size distribution is analyzed using Density Functional Theory (DFT) method with N₂ adsorption isotherm, which is shown in Fig.4b. The total pore volume of Linde activated carbon is 0.465cm³/g and micropore occupies approximately 95% of the total volume.

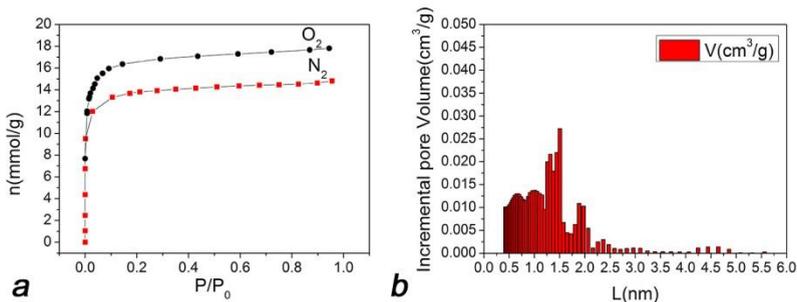


Fig.4. (a) N₂ and O₂ static adsorption isotherms (77K); (b) Pore size distribution of Linde activated carbons

The breakthrough curves of N₂ and O₂ are shown in Fig.5a, which is for the adsorption of a binary mixture of O₂ and N₂ (22:78) on the adsorbent of the Linde activated carbon. In Fig.5a, N₂ breaks through firstly. Then the concentration of N₂ in the outlet increases and reaches a maximum, which is higher than the concentration of N₂ in the entering gas stream. The concentration of O₂ leaving the bed increases, with that of N₂ decreasing. Finally, the concentrations of N₂ and O₂ in the leaving gas and the entering gas are same. The breakthrough adsorption capacity is the adsorption capacity of the component when the component breaks through. Fig.5b presents the breakthrough adsorption capacity in a binary mixture and the static adsorption capacity of N₂ at different partial pressure. When P/P₀>0.1, the N₂ breakthrough adsorption capacity has little changes. The breakthrough adsorption capacity is approximately 44% less than the static adsorption capacity. The amount of the activated carbon can be calculated by the N₂ static adsorption capacity with a factor of 1.5-2.

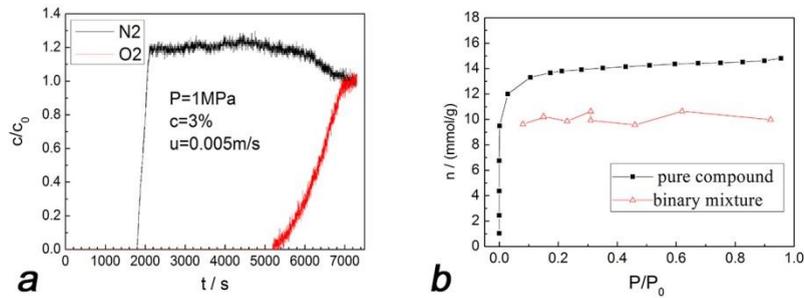


Fig.5. (a) Breakthrough curves of a binary mixture (O₂ and N₂); (b) N₂ breakthrough adsorption capacity vs. N₂ static adsorption capacity

4. Conclusion

High pressure purifier is a key equipment of the helium purification system. The working principles of the helium purification and regeneration are described. The design of the purifier is shown in details. It's known that the high pressure heat exchanger and the absorption cylinders are important parts of the purifier. The helically coiled tube-in-tube heat exchanger is numerically studied and can meet the need of heat transfer. The experiments of static and dynamic adsorption of Linde coconut shell activated carbon are carried out. The activated carbon has 95% micropore which can adsorb the impurities well at low pressure. The amount of the activated carbon can be calculated by the N₂ static adsorption capacity with a factor of 1.5~2.

Until now, the helium purification system is under construction and the purifier is being manufactured. The system will be finished in the year of 2015.

Nomenclature

n	adsorption capacity	mmol/g
P	pressure	MPa
P_0	saturation pressure at 77K	MPa
L	pore width	nm
V	the volume of a certain pore width	cm ³ /g
C	the concentration of an adsorbate	
C_0	concentration of an adsorbate in the entering gas stream	

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