



ICEC/ICMC

25th International Cryogenic Engineering Conference & International Cryogenic Materials Conference 2014

July 7-11, 2014

University of Twente, Enschede, The Netherlands



Performance Evaluation of Heat Transfer Enhancement in Plate-fin Heat Exchangers with Offset Strip Fins

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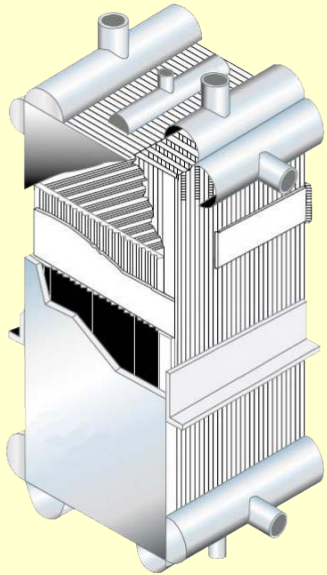
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Outline

- **Background**
- **Physical model and entropy generation**
- **A new evaluation method**
- **Effects of the geometrical parameters**
- **Conclusions**

Plate-fin heat exchanger



Aerospace



Gases



Automobile

Application

Plate-fin surface

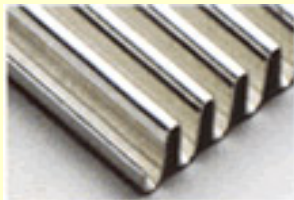
Plain fin

Perforated fin

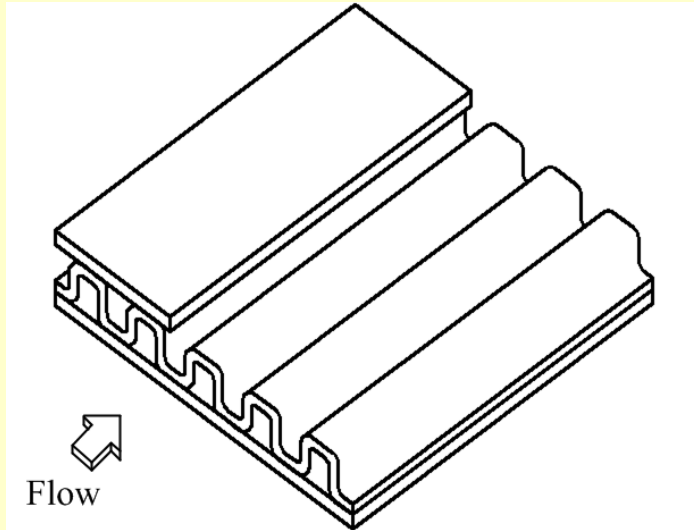
Offset strip fin

Wavy fin

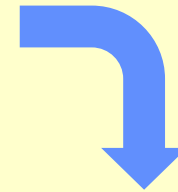
Louvered fin



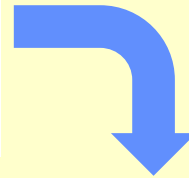
Offset Strip Fin (OSF)



Heat transfer
Pressure drop



Enhanced heat transfer
Increased pressure drop

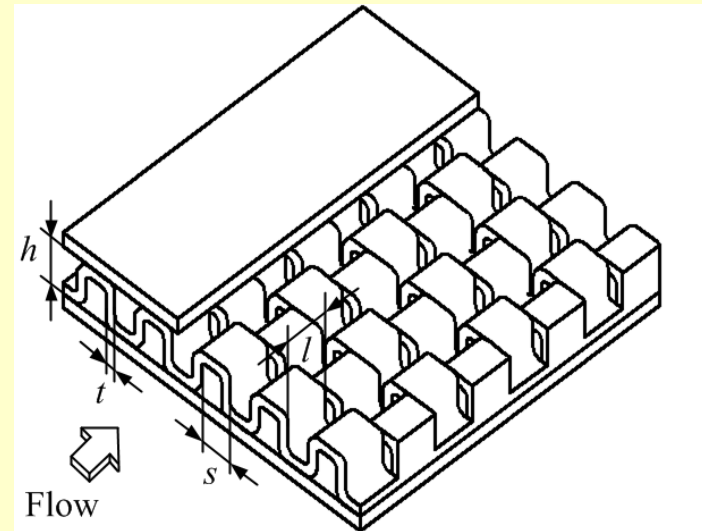


Non-dimensional parameters:

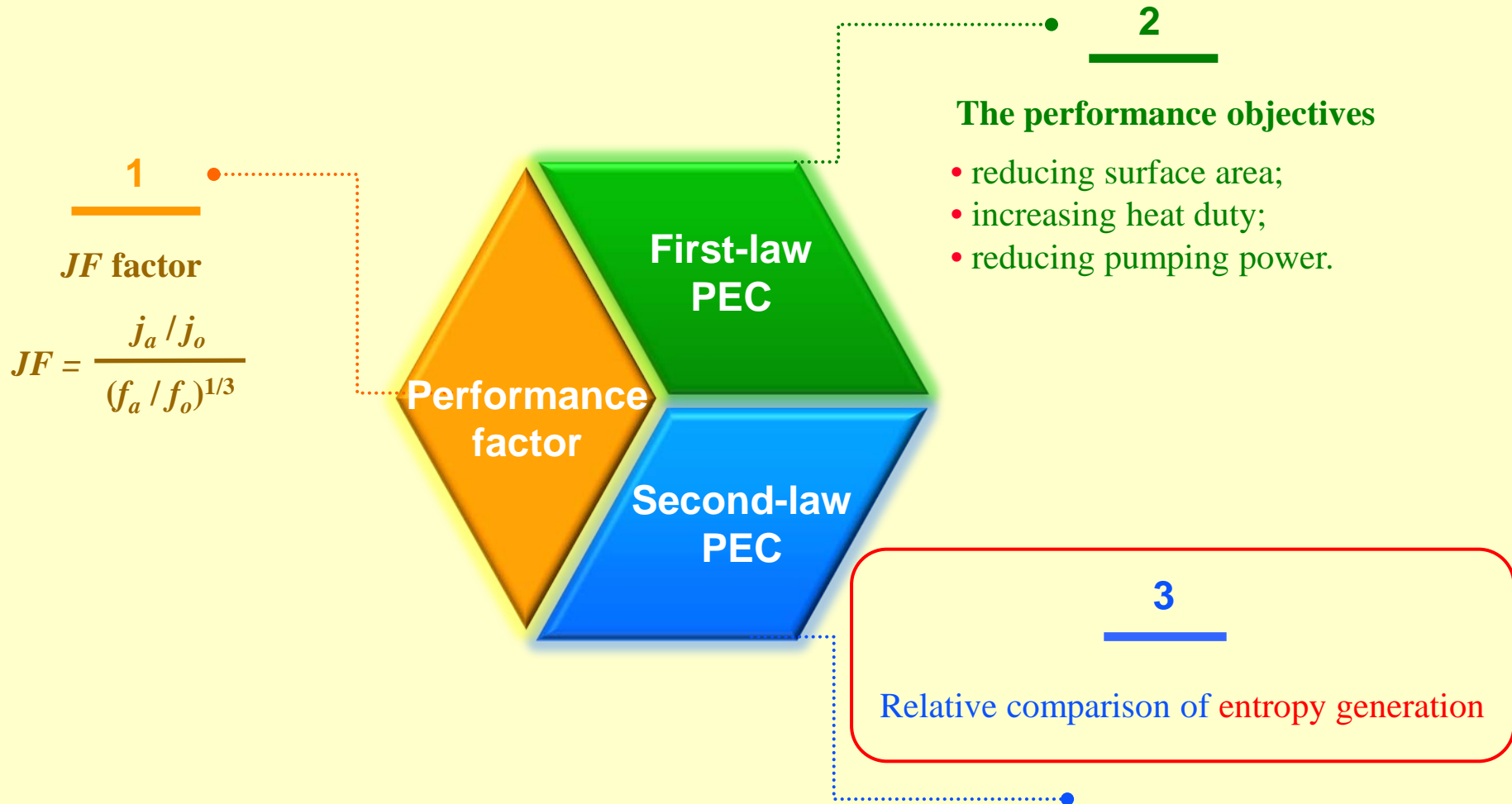
The fin thickness-to-height ratio $\alpha = (t/h)$

Fin density $\gamma = (t/s)$

The fin thickness-to-length ratio $\delta = (t/l)$



Performance evaluation criteria (PEC)



Physical model and entropy generation

Boundary condition:

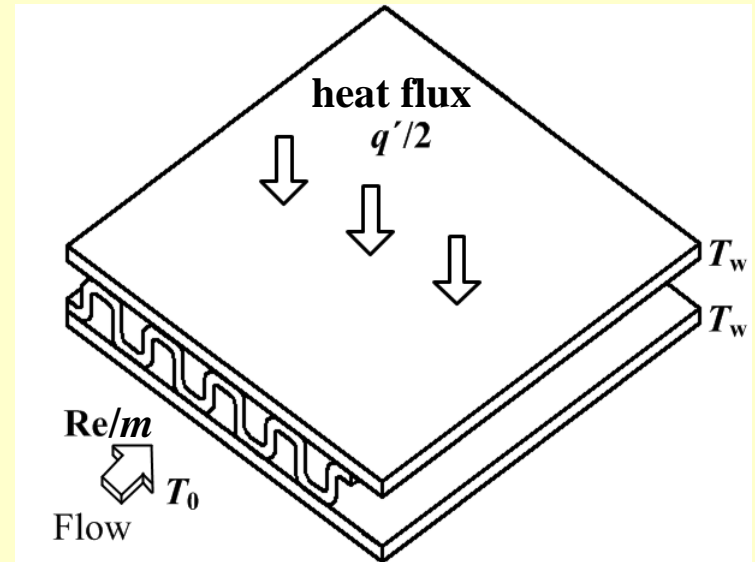
Constant wall temperature

Assumptions:

The thermo-physical properties of the fluid are constant.

Entropy Generation:

$$\left. \begin{aligned} \frac{dS_{gen}}{dx} &= -mC_p \frac{T - T_w}{TT_w} \frac{dT}{dx} + \frac{m}{\rho T} \left(-\frac{dp}{dx} \right) \\ \theta &= \theta_0 \exp\left(-\frac{h}{\rho u C_p} \frac{4x}{D_h} \right) \end{aligned} \right\} \rightarrow S_{gen} = mC_p \left\{ \tau_0 \varepsilon + \ln \left[\frac{1 + \tau_0 (1 - \varepsilon)}{1 + \tau_0} \right] \right\} + \frac{f}{2j} \frac{m^3 \text{Pr}^{2/3}}{\rho^2 A_c^2 T_w} \ln \left[\frac{1 + \tau_0 (1 - \varepsilon)}{(1 + \tau_0)(1 - \varepsilon)} \right]$$



Important parameters:

Relative temperature difference $\tau_0 = \frac{T_0 - T_w}{T_w}$

Reynolds number $Re_a = \frac{D_{h,a}}{D_{h,o}} Re_o$

The second-law PEC

Augmentation entropy generation number

$N_{s,a}$ ($N_{s,a} < 1$ is desirable)

$$N_{s,a} = \frac{S_{gen,a}}{S_{gen,o}} = \frac{S_{gen,a,\Delta T} + S_{gen,a,\Delta p}}{S_{gen,o,\Delta T} + S_{gen,o,\Delta p}}$$

Entropy generation distribution factor

ψ ($\psi > 1$ is desirable)

$$\psi = \frac{S_{gen,o,\Delta T} - S_{gen,a,\Delta T}}{S_{gen,a,\Delta p} - S_{gen,o,\Delta p}}$$

The second-law PEC

The dimensionless entropy generation

$$S_{gen} \rightarrow N_{s1} = \frac{T_w \cdot S_{gen}}{Q}$$

The irreversibility distribution ratio

$$\phi_0 = \frac{N_{s1,o,\Delta p}}{N_{s1,o,\Delta T}}$$

$$N_{s,a} = \frac{S_{gen,a}}{S_{gen,o}} = \frac{S_{gen,a,\Delta T} + S_{gen,a,\Delta p}}{S_{gen,o,\Delta T} + S_{gen,o,\Delta p}}$$



$$N_{s1}^* = \frac{N_{s1,a}}{N_{s1,o}} = \frac{N_{s1,a,\Delta T} + N_{s1,a,\Delta p}}{N_{s1,o,\Delta T} + N_{s1,o,\Delta p}} = \frac{N_{s1,\Delta T}^* + \phi_0 N_{s1,\Delta p}^*}{1 + \phi_0}$$

$N_{s1}^* < 1$ is desirable

$$\psi = \frac{S_{gen,o,\Delta T} - S_{gen,a,\Delta T}}{S_{gen,a,\Delta p} - S_{gen,o,\Delta p}}$$



$$\Psi = \frac{N_{s1,o,\Delta T} - N_{s1,a,\Delta T}}{N_{s1,a,\Delta p} - N_{s1,o,\Delta p}} = \frac{1}{\phi_0} \frac{1 - N_{s1,\Delta T}^*}{N_{s1,\Delta p}^* - 1}$$

$\Psi > 1$ is desirable

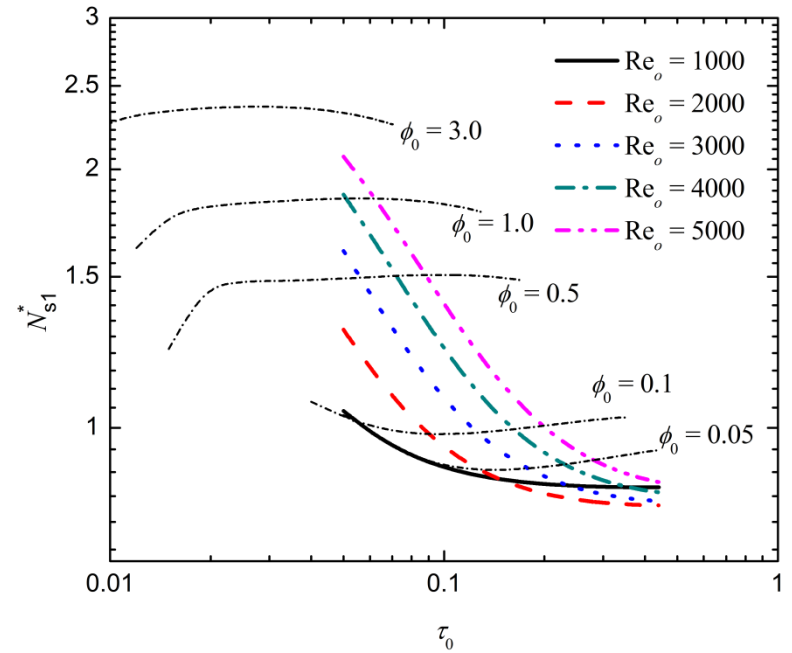
The second-law PEC

Relative temperature difference $\tau_0 = \frac{T_0 - T_w}{T_w}$

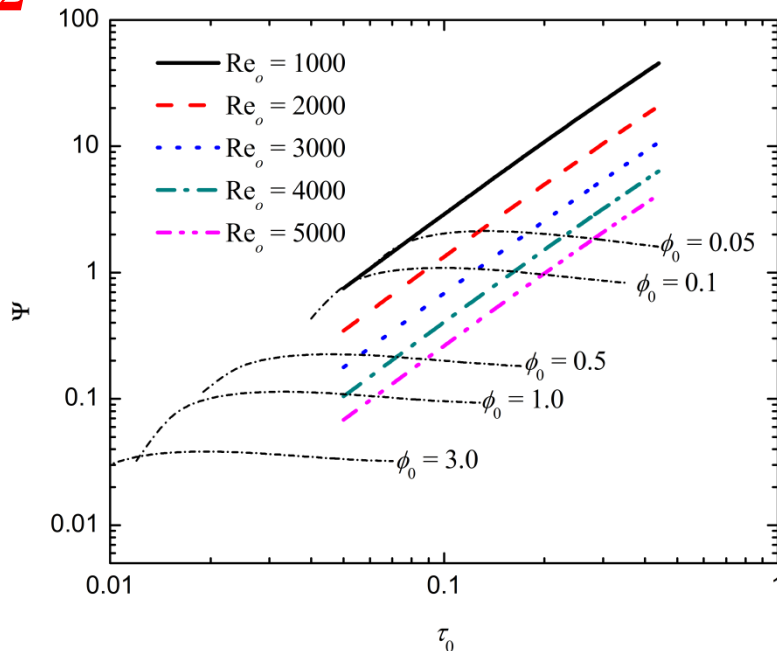
The irreversibility distribution ratio $\phi_0 = \frac{N_{s1,o,\Delta p}}{N_{s1,o,\Delta T}}$

- **Fig. 1** N_{s1}^* vs. τ_0
- It is more advantageous to use OSFs under larger temperature difference.

1



2



- **Fig. 2** Ψ vs. τ_0
- The conditions with high irreversibility of heat transfer are desirable.

A New evaluation method

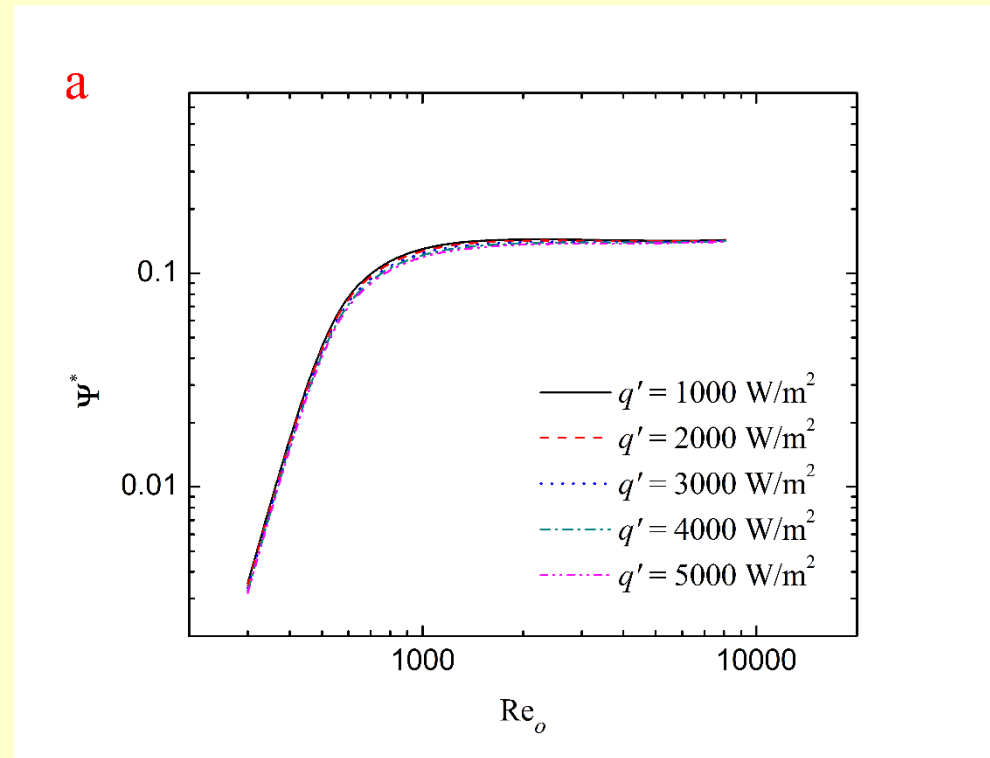
Relative entropy generation distribution factor, Ψ^*

$$\Psi^* = \frac{(N_{s1,o,\Delta T} - N_{s1,a,\Delta T}) / N_{s1,o,\Delta T}}{(N_{s1,a,\Delta p} - N_{s1,o,\Delta p}) / N_{s1,o,\Delta p}} = \frac{1 - N_{s1,\Delta T}^*}{N_{s1,\Delta p}^* - 1}$$

The higher the Ψ^* value, the higher the degree of the heat transfer enhancement.

The evaluation results of Ψ^*

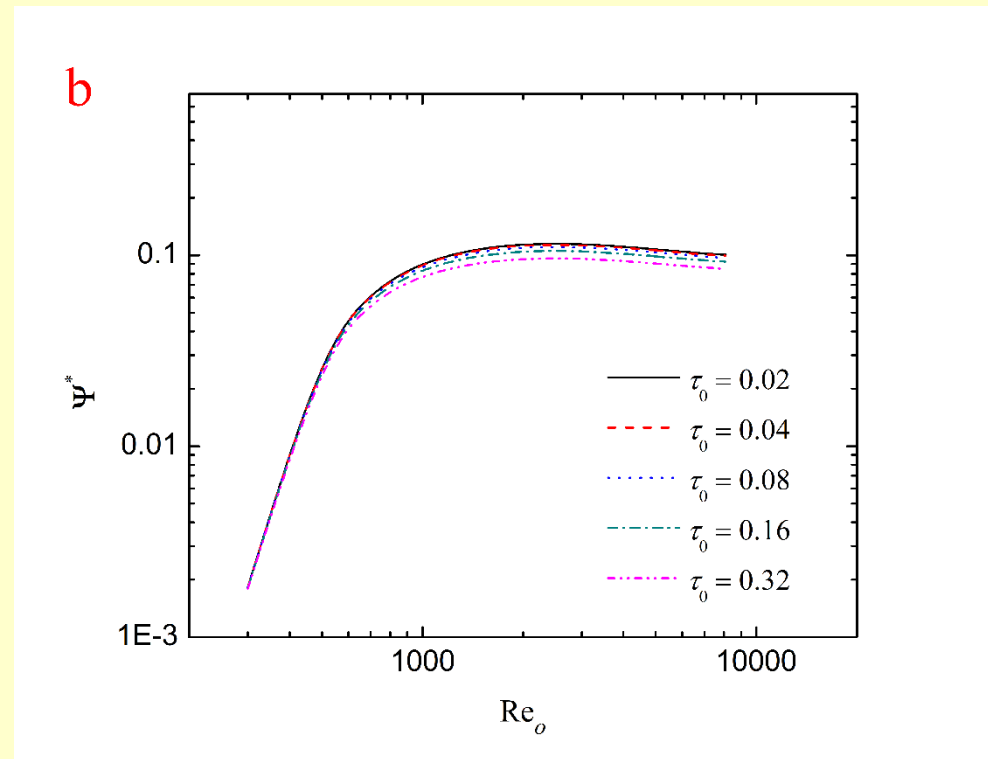
- Fig. a Ψ^* vs. Re_o with heat flux q' as a parameter
- The q' has little influence on Ψ^*
- Ψ^* is a strong function of Re_o



The evaluation results of Ψ^*

Relative temperature difference on the inlet $\tau_0 = \frac{T_0 - T_w}{T_w}$

- Fig. b Ψ^* vs. Re_o with τ_0 as a parameter.
- The performance of heat transfer enhancement of OSF fin degrades as τ_0 is increased.

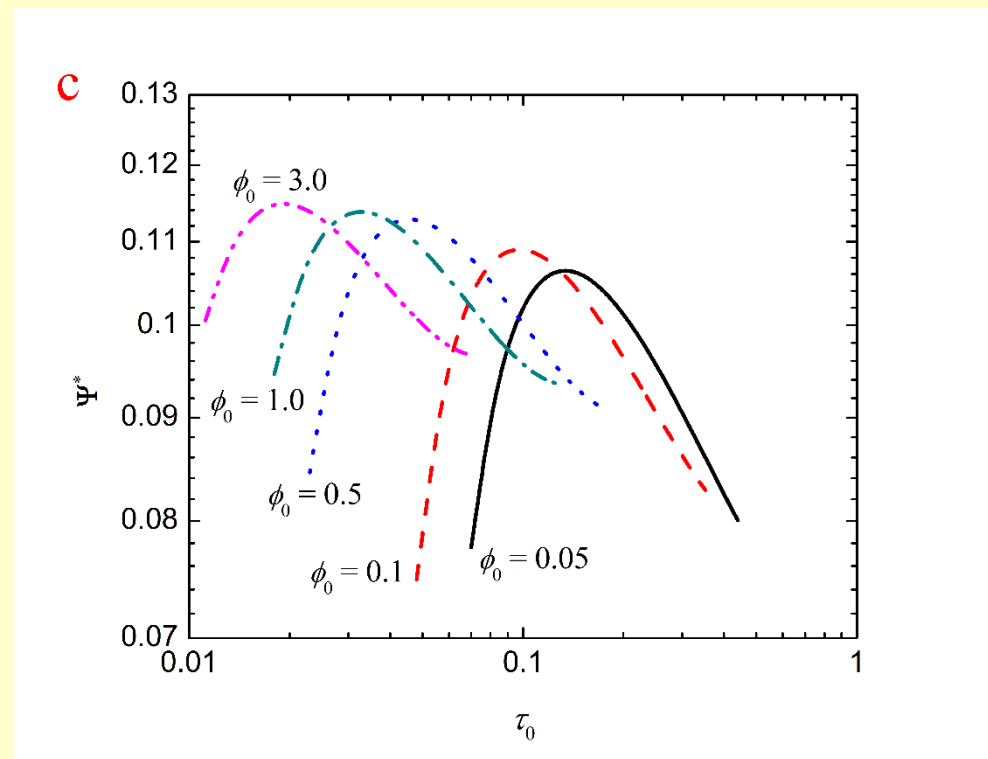


The evaluation results of Ψ^*

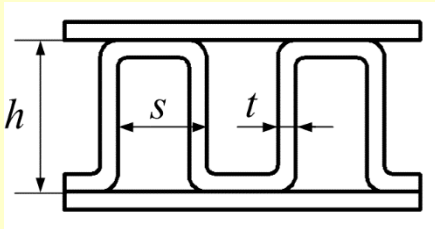
The irreversibility distribution ratio

$$\phi_0 = \frac{N_{s1,o,\Delta p}}{N_{s1,o,\Delta T}}$$

- Fig. c Ψ^* vs. τ_0 with ϕ_0 as a parameter.
- For a particular ϕ_0 , there exists optimum condition of τ_0 and Re_o which corresponds to the maximum Ψ^* .

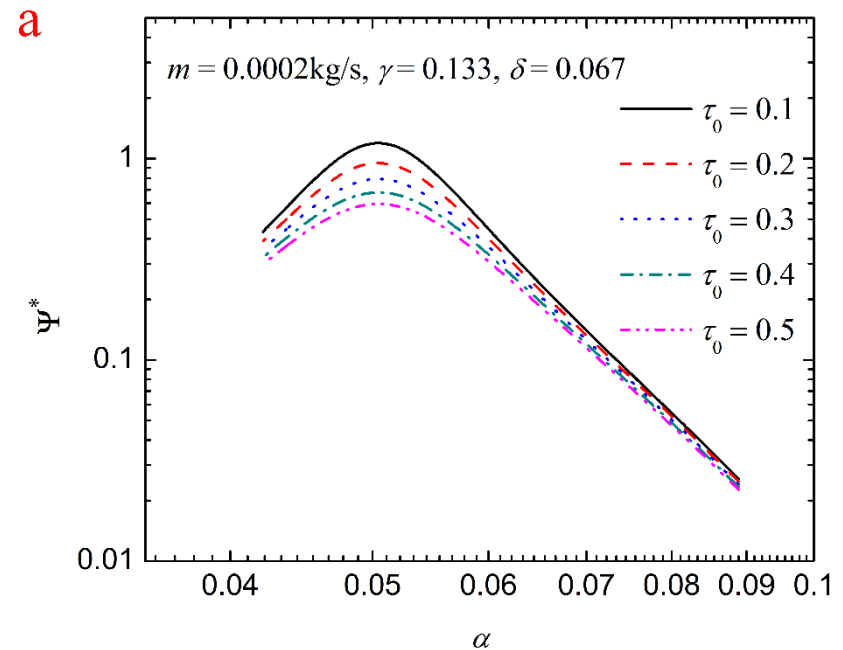


Effects of the geometric parameters

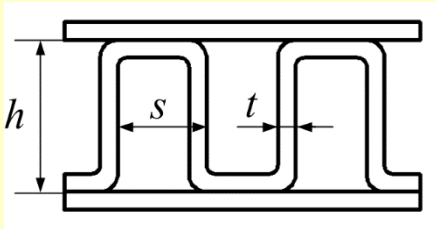


The fin thickness-to-height ratio $\alpha = (t/h)$

- **Fig. a** Ψ^* vs. α with τ_0 as a parameter.
- **Range: $\alpha = 0.042-0.089$.**
- **The optimum $\alpha = 0.051$.**

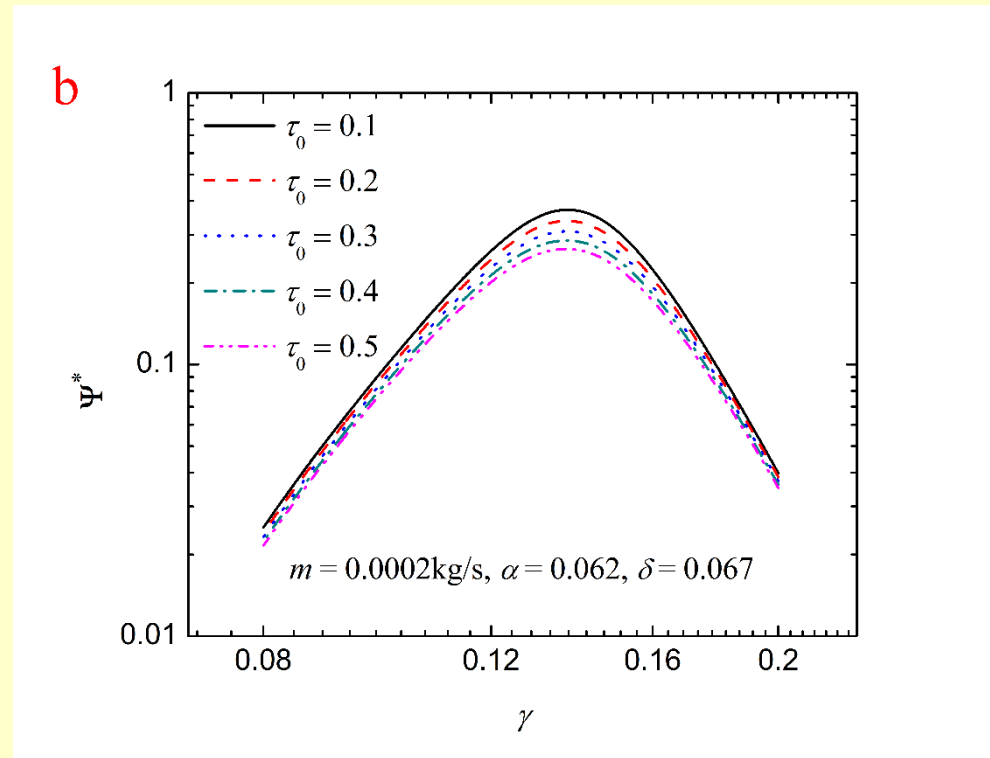


Effects of the geometric parameters



Fin density $\gamma = (t/s)$

- **Fig. b** Ψ^* vs. γ with τ_0 as a parameter.
- **Range: $\gamma = 0.08-0.2$.**
- **The optimum $\gamma = 0.138$.**

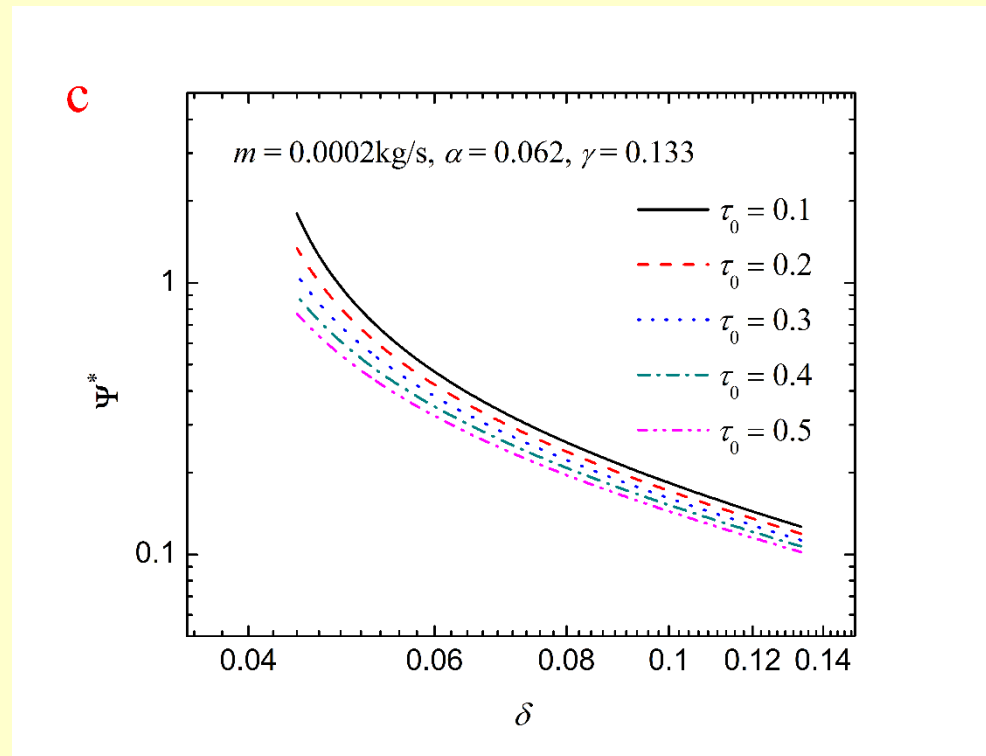


Effects of the geometric parameters



The fin thickness-to-length ratio $\delta = (t/l)$

- **Fig. c** Ψ^* vs. δ with τ_0 as a parameter
- **Range:** $\delta = 0.04-0.133$.
- **Smaller δ is desirable.**



Conclusion

- **A new evaluation method is proposed to evaluate the performance of heat transfer enhancement of OSFs.**
- **The proposed method provides rational evaluations under different operating conditions.**
- **There exist the optimum geometric parameters that maximize the degree of heat transfer enhancement of OSFs.**

Thanks for your attention !

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