



# Performance study on ST/JT hybrid cryocoolers working at liquid helium temperature



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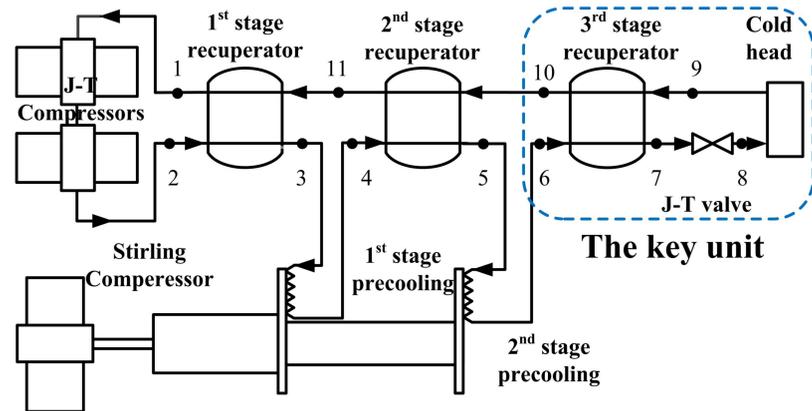
## Introduction

- The hybrid space cryocooler, which consists of a Stirling cryocooler and a J-T loop, has become the main cooling technology at liquid helium temperature (around 4 K) in the long-life space mission. It is usually used to directly cool the detectors or precool the other cryocoolers which work at lower temperature.
- There is little detail about the design and the performance analysis of the hybrid cryocoolers in the published literatures.
- For the required cooling power, better performance means less power consumption, which may reduce the weight and volume of the cryocoolers and the power equipment. It is meaningful to the space missions.

## Conclusion

- The effective ways to improve the overall COP are enhancing the performance of the J-T compressors with larger pressure ratio and the precooler at lower temperature.
- How  $P_H$ ,  $T_{pre2}$ , and  $\varepsilon$  affects the cooling power has been illustrated with P-h map and thermodynamic calculation.
- For fixed  $T_{pre2}$ ,  $P_{H,opt}$  exists; for fixed  $P_H$ , reducing  $T_{pre2}$  above the turning point has a significant positive effect on the cooling power (shown in part 3).
- The optimal  $P_H$  and  $T_{pre2}$  can be calculated out with the actual performance of the J-T compressors and the precooler.

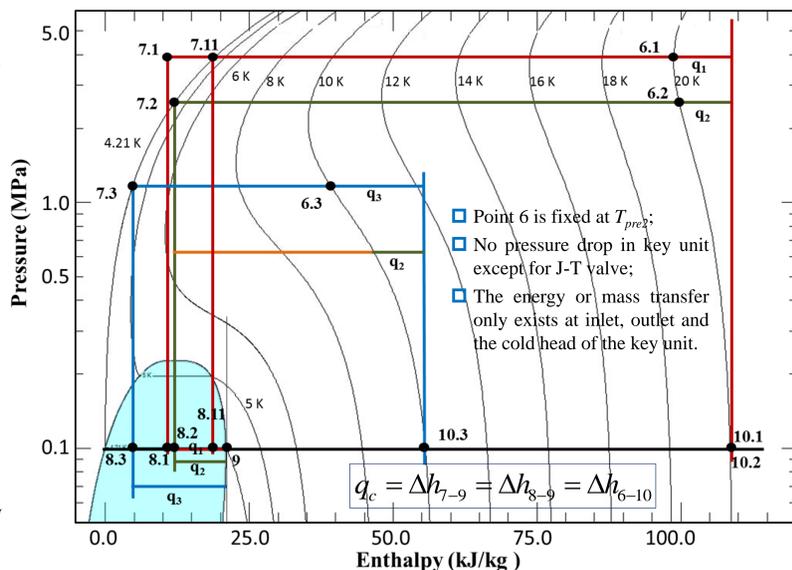
## 1. Common process and key unit



- The key unit can reach liquid helium temperature as long as the precooler is powerful enough.
- Ineffectiveness of the last (3rd) stage recuperator has no compensation provider.
- $T_{pre2}$  has great impact on the cooling power.
- The function of the upper stages is reducing the precooling load of the last stage.

## 2. Pressure-Enthalpy map analysis

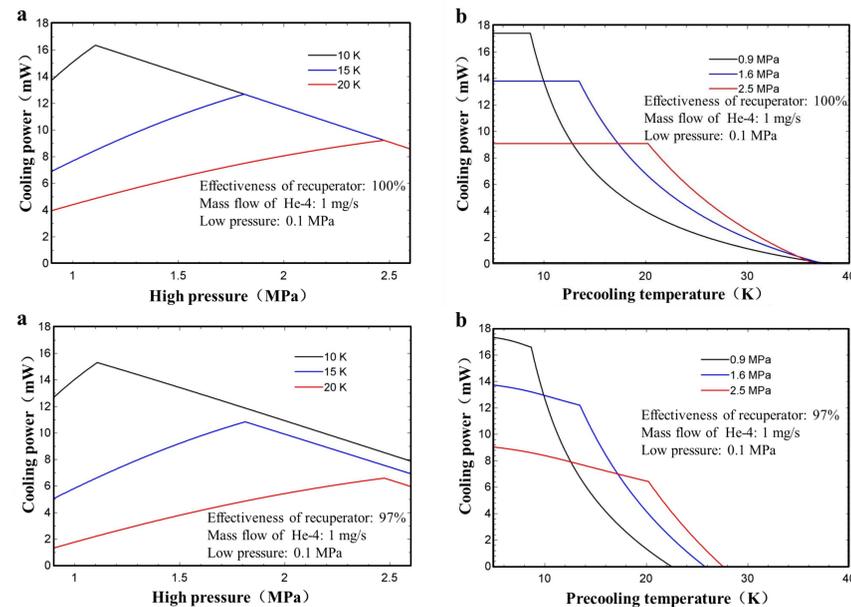
- The 1st process: 6.1-7.1-8.1-9-10.1,  $T_6=20$  K:
  - violate the 2nd law of thermodynamics
  - $q_c = \Delta h_{8.11-9} < \Delta h_{6.1-10.1}$
  - $T_{10} < T_6$
- The 2nd process: 6.2-7.2-8.2-9-10.2,  $T_6=20$  K:
  - $q_{c,max}$  with  $P_{H,opt}$  around 2.5 MPa
  - $T_{10} = T_6$
  - As  $P_H$  goes lower,  $q_c$  decrease with  $\Delta h_{6-10}$
- The 3rd process: 6.3-7.3-8.3-9-10.3,  $T_6=10$  K:
  - larger  $q_{c,max}$  with lower  $P_{H,opt}$  around 1.1 MPa
  - same  $q_c$  as  $q_{c,max}$  of the 2nd process with  $P_H$  around 0.6 MPa



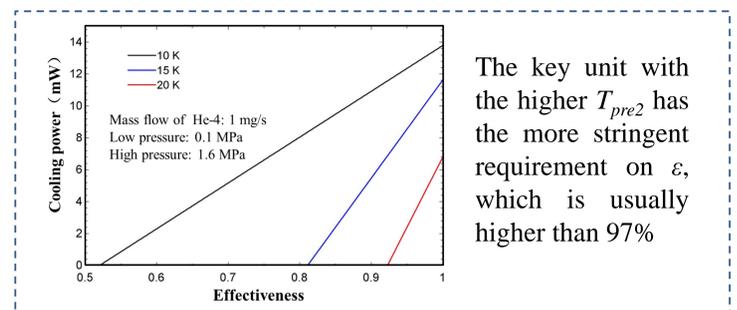
- Point 6 is fixed at  $T_{pre2}$ ;
- No pressure drop in key unit except for J-T valve;
- The energy or mass transfer only exists at inlet, outlet and the cold head of the key unit.

$$q_c = \Delta h_{7-9} = \Delta h_{8-9} = \Delta h_{6-10}$$

## 3. Thermodynamic calculation of the key unit

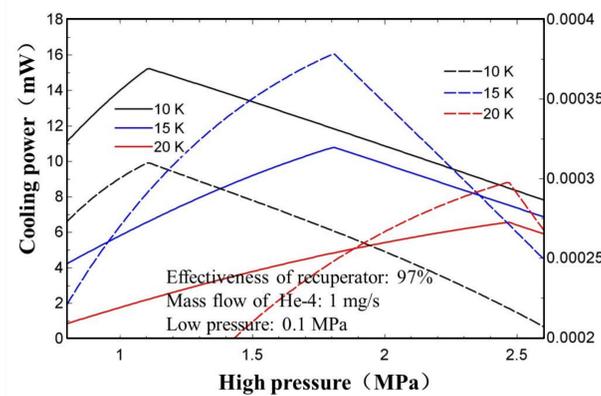


- Effectiveness of the recuperator  $\varepsilon = 100\%$ :
  - $q_c$  have the maximum value at  $P_{H,opt}$  with fixed  $T_{pre2}$
  - $P_H > P_{H,opt}$ ,  $h_7$  limited by  $T_7 = T_9$ ,  $T_{10} < T_6$
  - $P_H < P_{H,opt}$ ,  $h_7$  limited by fixed  $\Delta h_{9-10}$ ,  $T_{10} = T_6$
- Effectiveness of the recuperator  $\varepsilon = 97\%$ :
  - $\varepsilon$  does not affect the  $P_{H,opt}$
  - lower cooling power and  $T_{pre2}$  at zero  $q_c$  point



The key unit with the higher  $T_{pre2}$  has the more stringent requirement on  $\varepsilon$ , which is usually higher than 97%

## 4. COP optimization of the ST/JT hybrid cryocooler



- Dotted lines: optimized COP as the function of  $P_H$ , with the optimization parameter  $T_{pre1}$ .
- Solid lines: corresponding cooling power of the optimized COP.
- The maximum value of optimized COP ( $COP_{max}$ ) exists at the  $P_{H,opt}$  with fixed  $T_{pre2}$ .
- The corresponding cooling power behaves the same as the key unit.
- Optimal  $T_{pre2}$  can be found.

## References

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