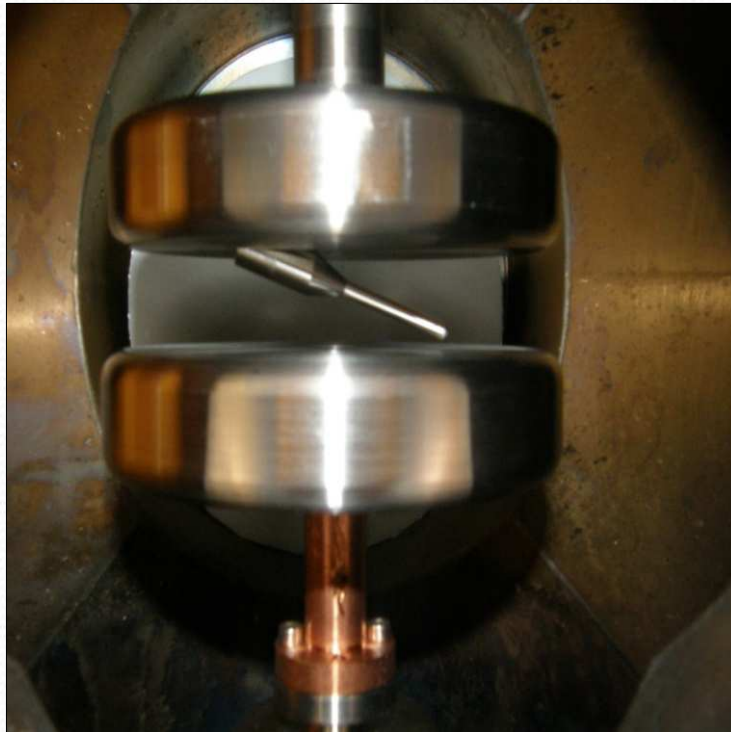


# Impact of electro-chemical cleaning on the dielectric strength in sealed vacuum interrupters



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## Abstract :

- Vacuum interrupters (VI's) are used in medium voltage circuit breakers to protect electrical distribution systems. Today the world wide annual production exceeds 2 million units.
- Size reduction of VI's and application in solid insulated systems tend to increase the dielectric stresses inside these VI's. Cleaning is a key parameter to obtain reproducible dielectric results.
- Here the impact of electro-chemical cleaning will be discussed. Considerable progress is obtained in the dielectric strength over the last 5 years.
- A great difference persists to exist with respect to Cern published results.

# What is a vacuum interrupter

In MV network Circuit breakers to protect the network against short circuits

Vacuum interrupters contain the main contacts of the circuit breaker under a pressure of  $10^{-5}$ Pa to 2 Pa

Typical size

Diameter 90 mm

Length 180 mm



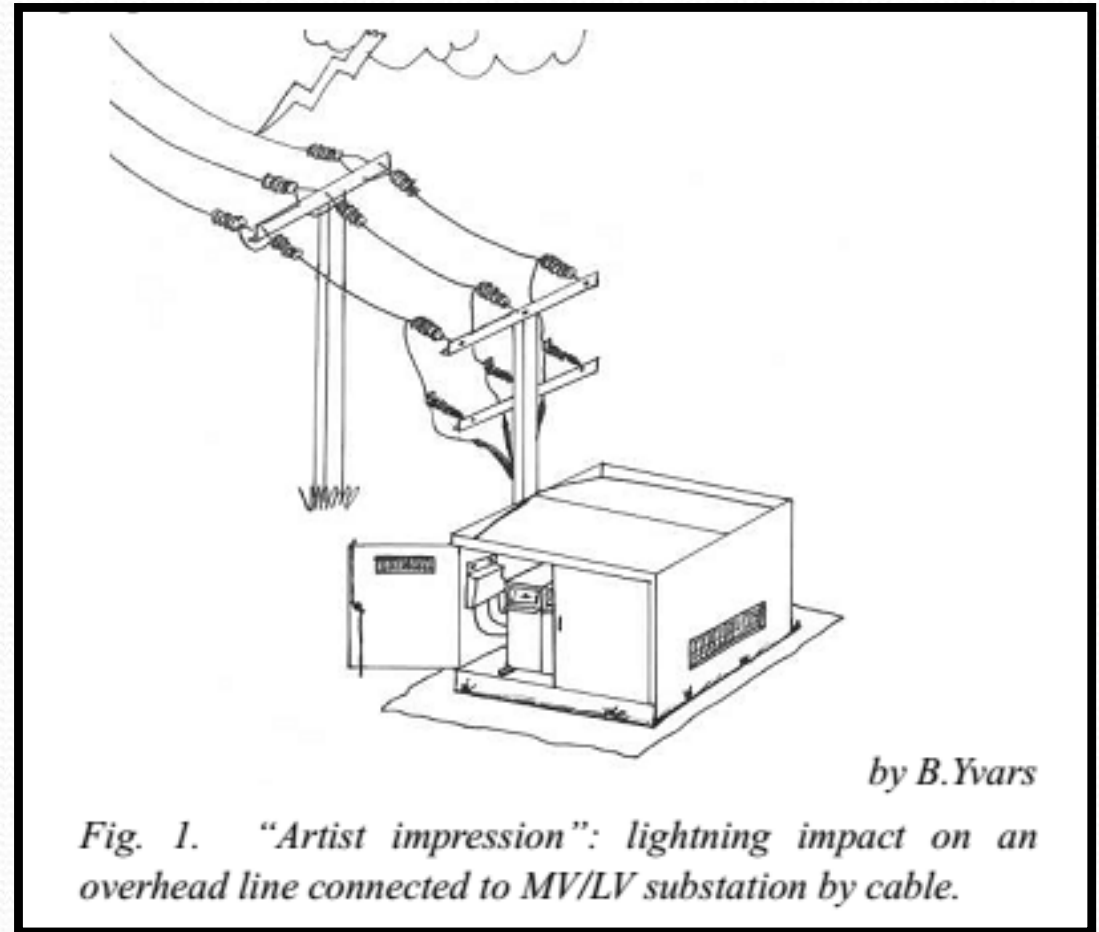
# What is the dielectric challenge

In OPEN position VI must withstand lightning stroke to protect circuit.

Lightning impulse of 110kV  
Duration 1.2 $\mu$ s/50 $\mu$ s

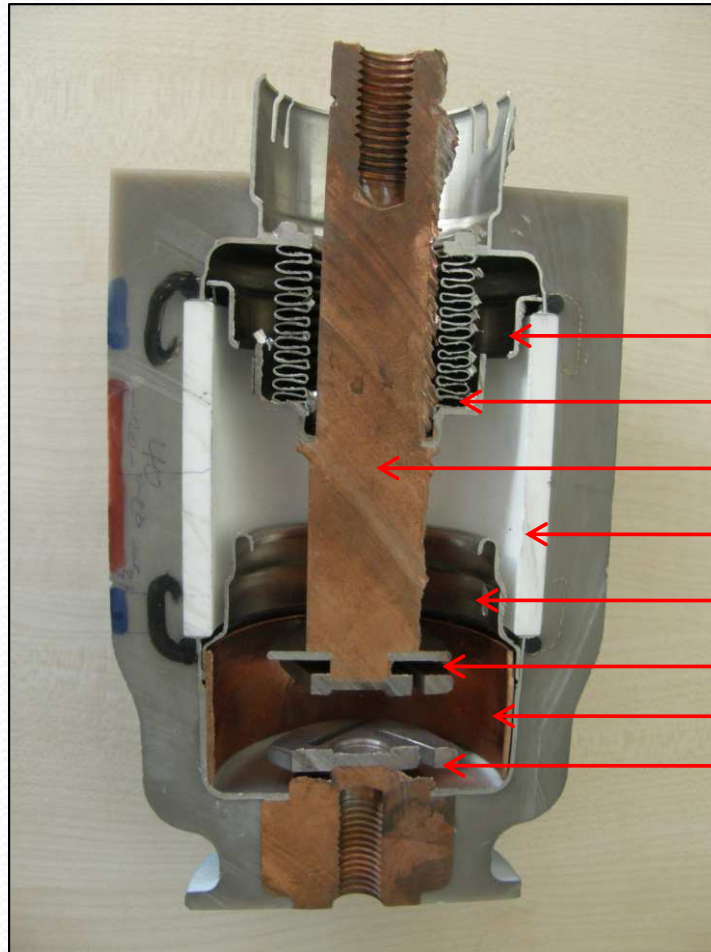
In case of breakdown :  
Power : 40MW 50 $\mu$ s  
(Line impedance 300 Ohm)

Consequence :  
Metallisation of isolator



# Vacuum interrupter with solid insulation and earth screen

- Introduction
- **Le projet**
- Fonctionnement
- L'étude
- Perspective
- Conclusion



- ← Ecran inox
- ← Soufflet
- ← Electrode
- ← Céramique
- ← Ecran inox
- ← Contact mobile
- ← Ecran cuivre
- ← Contact fixe

# Design : Optimisation – 1

## Application

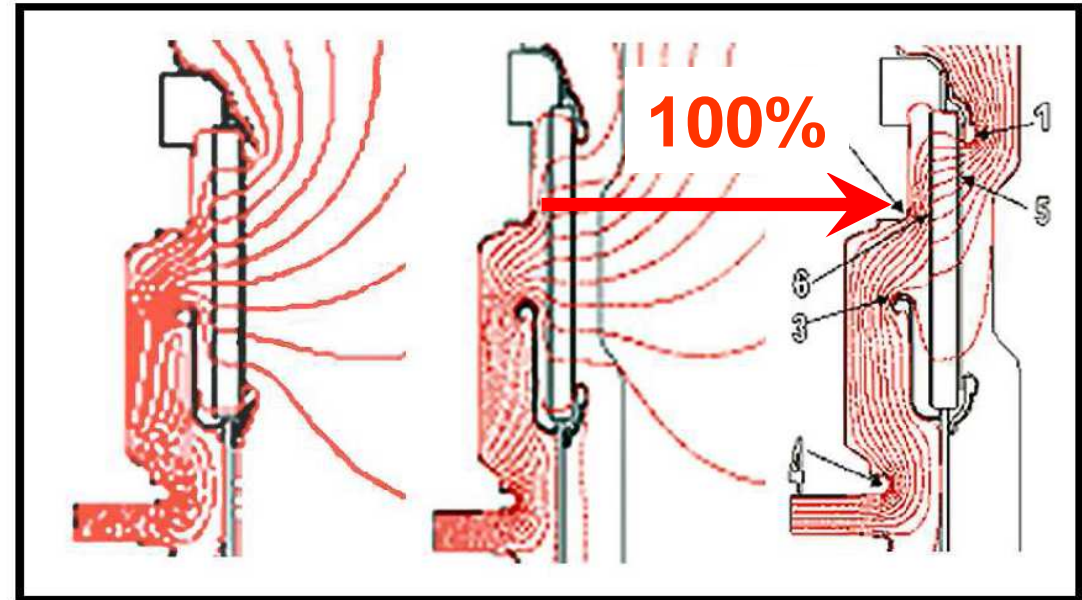
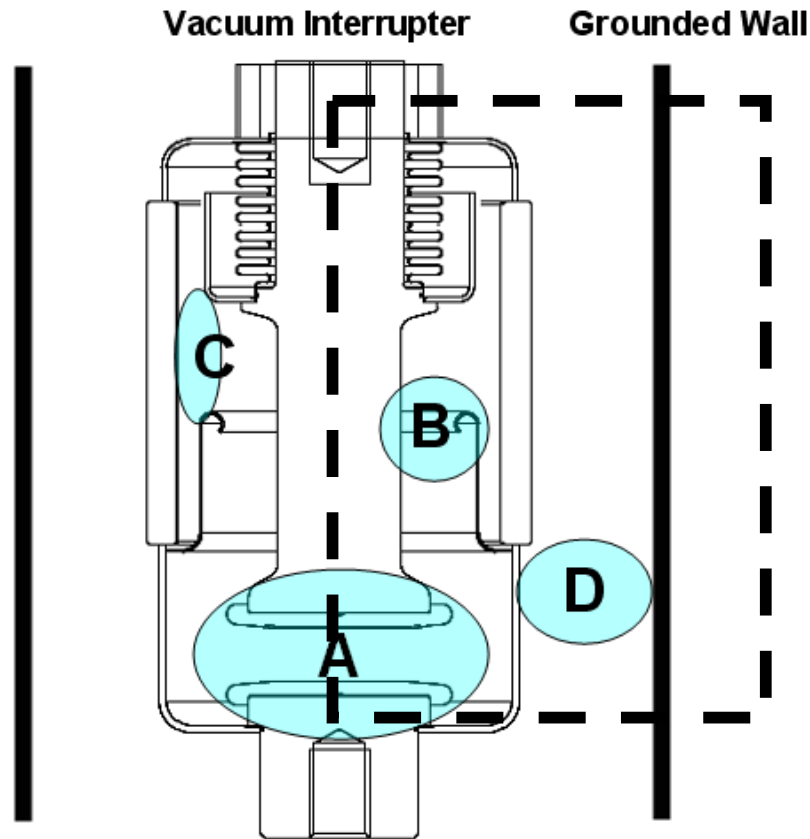


Fig. 2 : Electric field distribution inside and outside the VI for : a - air insulation, b – epoxy insulation, c – earth screened epoxy

Table 1. Dielectric stress in kV/mm for geometries in fig. 2  
2a – Air insulation, 2b – Epoxy insulation,  
2c – Earth screened epoxy insulation

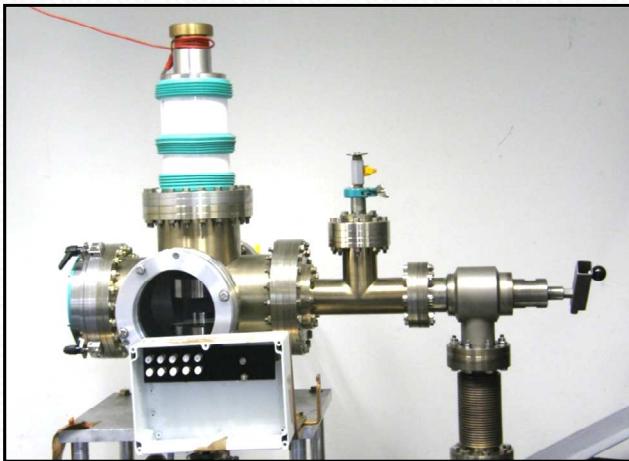
Location	Geometry			Breakdown Strength
	2a	2b	2c	
A : 4 (*)	23.3	23.3	23.3	22 – 25 (CuCr)
B : 2 – 3	9.7	9.3	18.7	~ 11 (StSt – Ceramic)
C : 6	2.8	2.8	3.6	No data available
D : 1 – 5	7.6	4.8	21.6	SF <sub>6</sub> 1bar : 8 Epoxy : 24

# Fonctionnement

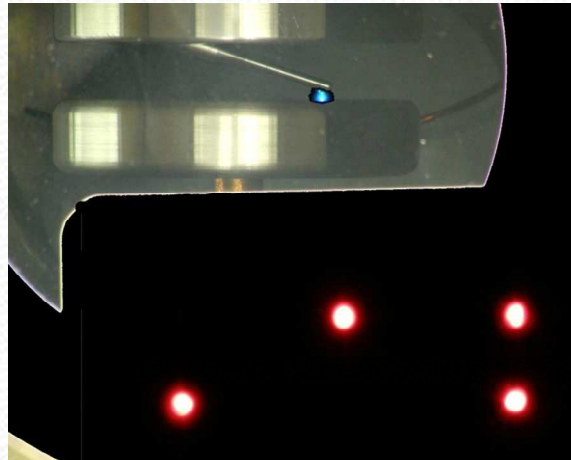
## La machine

- Introduction
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### Test setup



### Typical measurement



### Comparison

Table 1. Comparison of test setups used in this study and in [1,2].

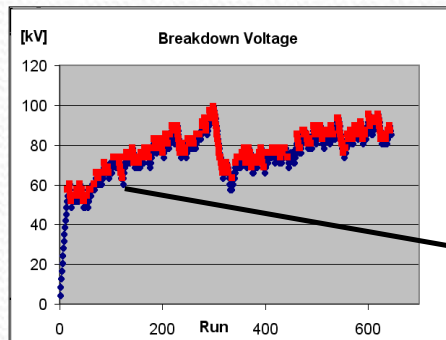
	Ref. [1]	This study	Ref. [2]
<b>Pulse Generator</b>			
Voltage [kV]	400	150	15
Pulse Duration	1.2 – 50 $\mu$ s	1 – 5 ms	
Current [A]	100	15	1
Discharge Time	50 $\mu$ s	10 $\mu$ s	
Method	Up - Down		
<b>Vacuum Chamber</b>			
Contact distance	5 mm	1 mm	20 $\mu$ m
Contact position	Vertical	Inclined	Vertical
Polarity Needle	Negative	Negative	Positive
<b>Additional Analysis</b>			
	Camera	Camera	Non

# Fonctionnement

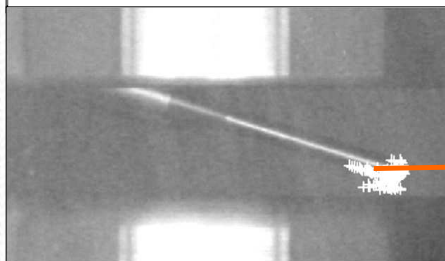
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## Characterisation of electrode "cleanliness" $\beta_m^1$

Breakdown Voltage

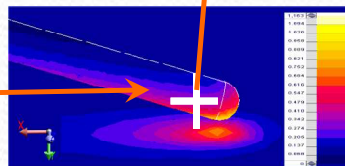


Breakdown Position

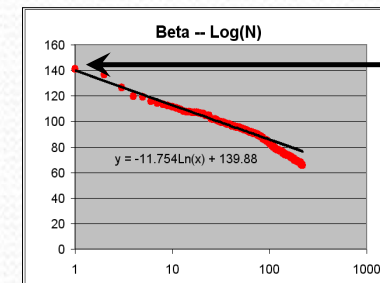
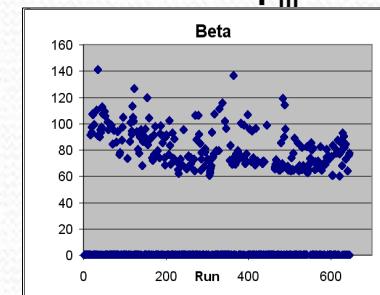


Correction for Local Field

$$\frac{1}{V_B} \times \frac{E_c d}{\beta_g} \Rightarrow \beta_m$$



Variation of  $\beta_m$



$\beta_m^1$

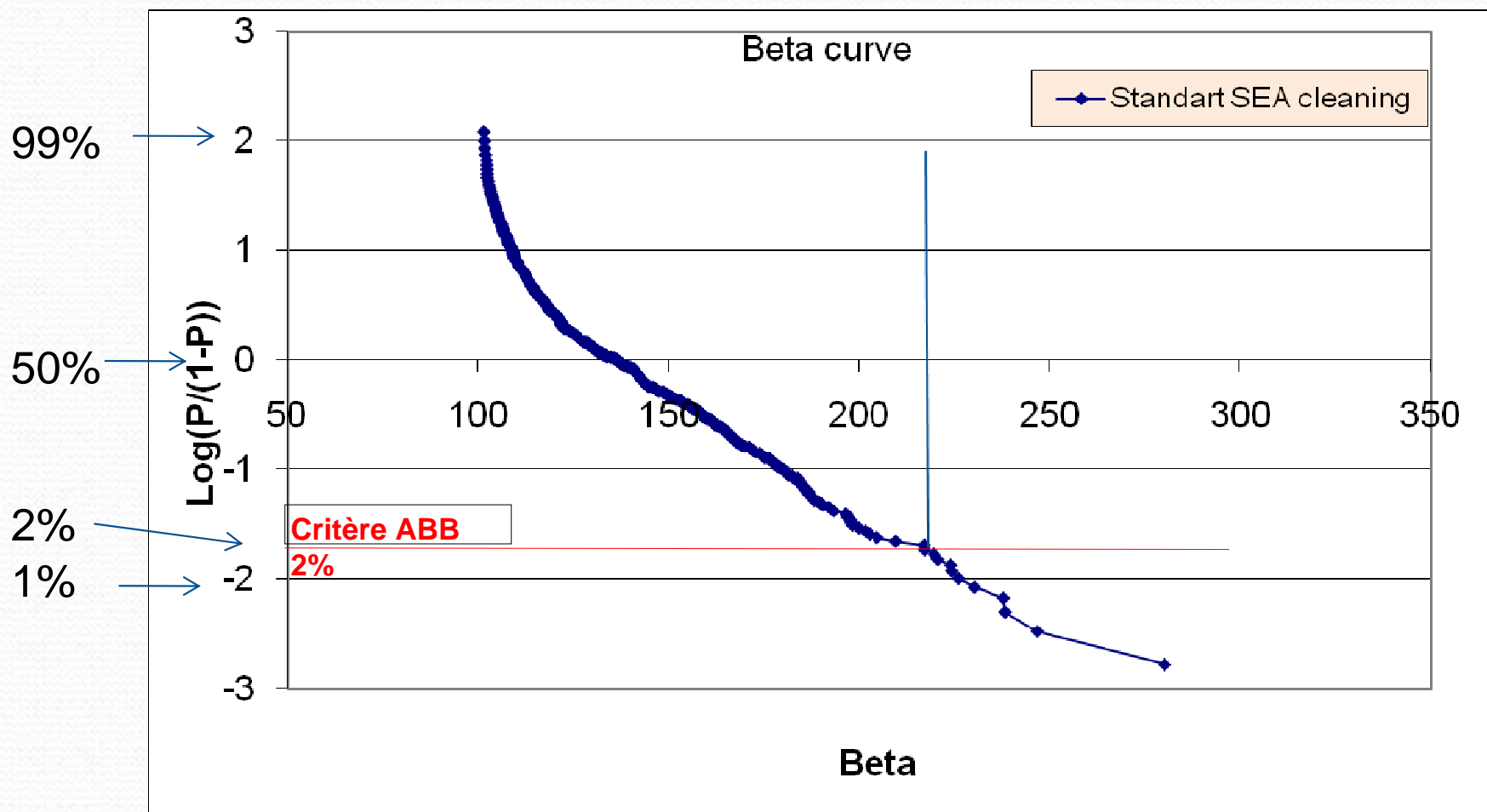


# Fonctionnement

## L'analyse du beta

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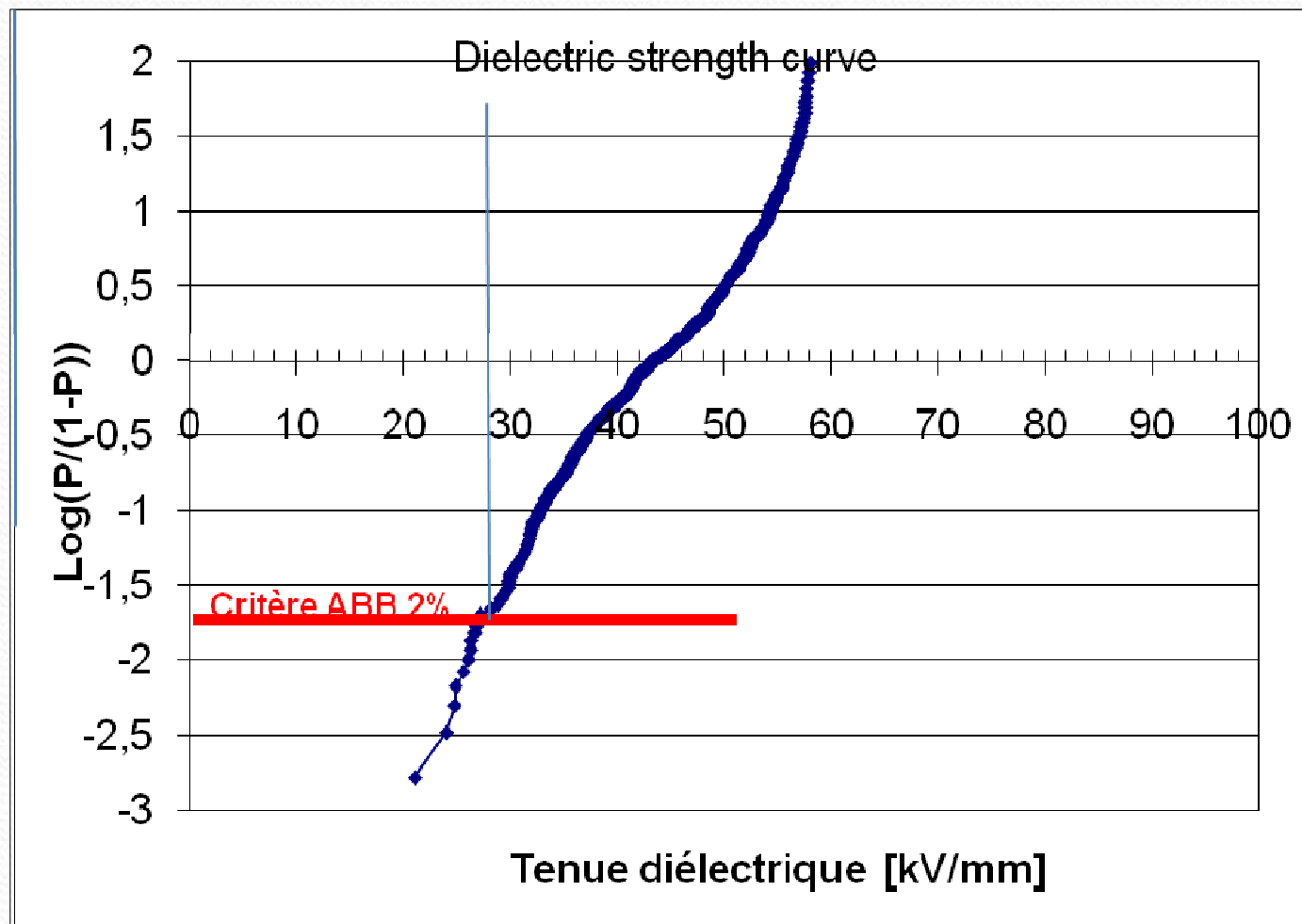
P = Probabilité



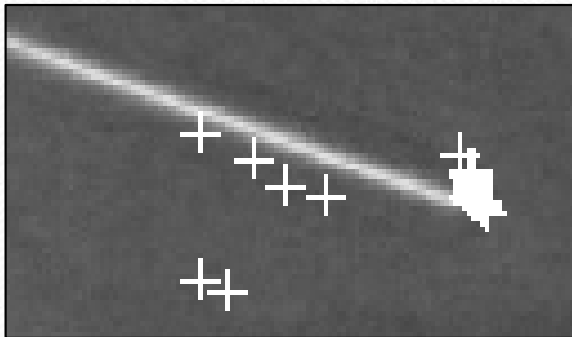
# Fonctionnement

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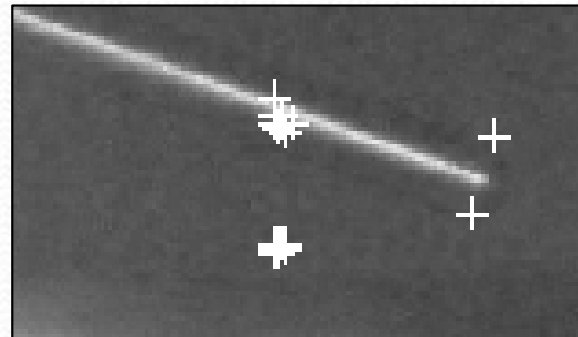
## La tenue diélectrique



## Observations

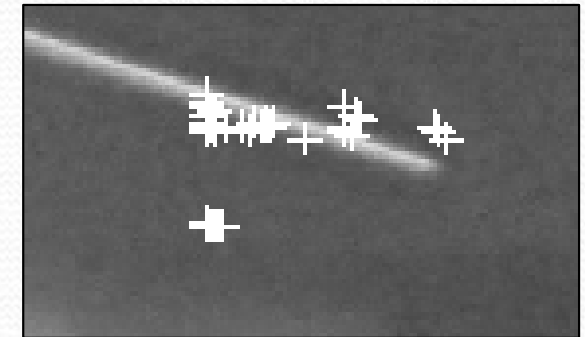


### Localisation des betas les plus élevés



### Sites d'amorçages très espacés

- $180 < \text{Beta de l'inox} < 220$
- Les sites d'amorçages sont espacés
- La tenue diélectrique est indépendante du temps de polissage



## Hypothèses de travail 2008



Référence: Phase identification of carbide and nitride precipitates in a ferritic stainless steel

Impuretés aux joints de grain

# L'étude depuis 2008

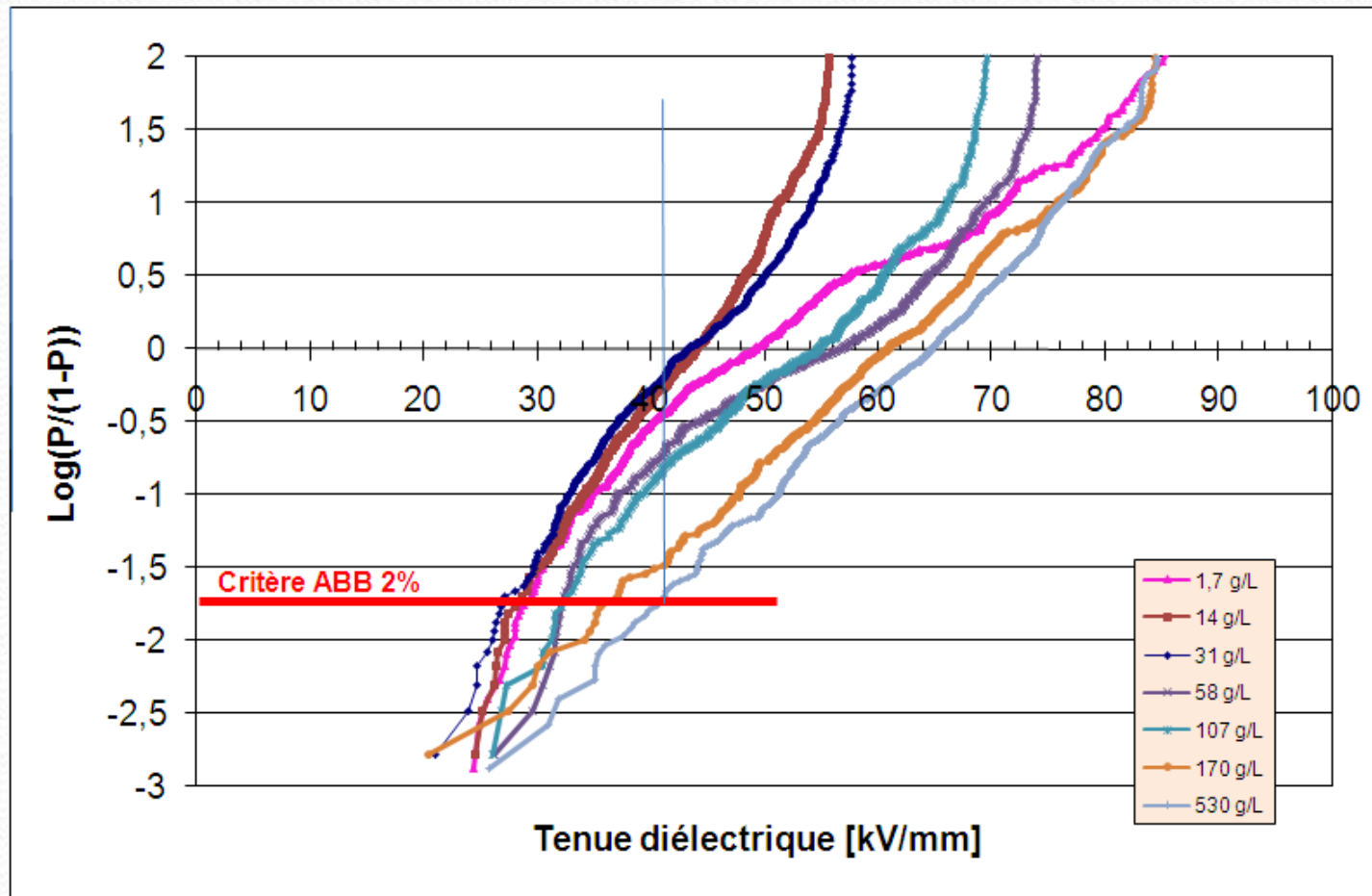
- Introduction
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## Solutions

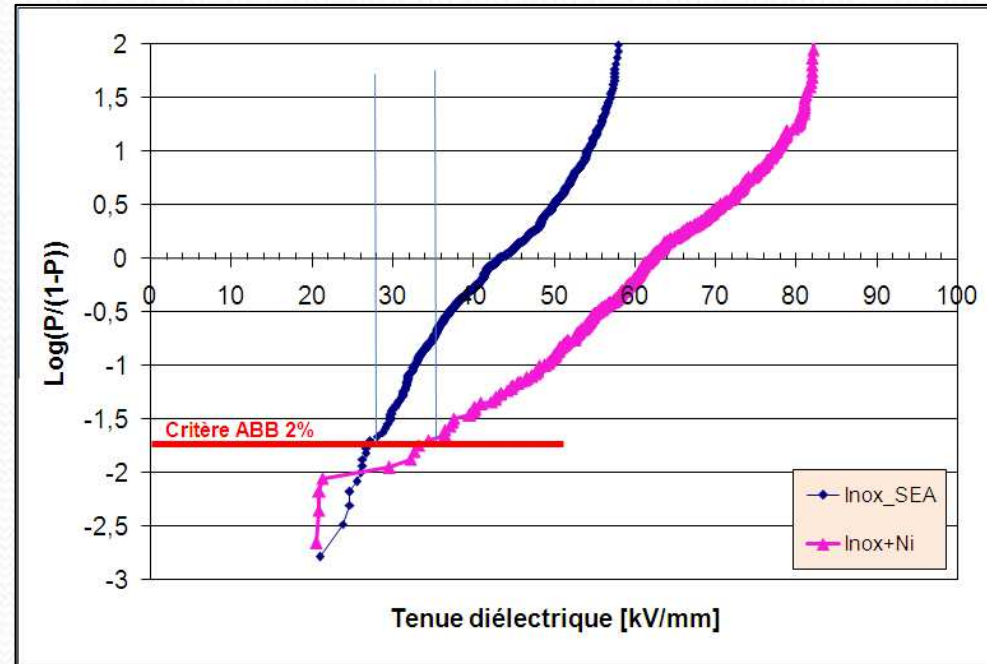
- Pour éviter la présence de carbure, 3 différentes solutions:
1. L'électrolyse selective
  2. Le dépôt Nickel
  3. Utilisation steel without chrome « maraging steel »



## 1- Résultats: Electrolyse selective (pitting)

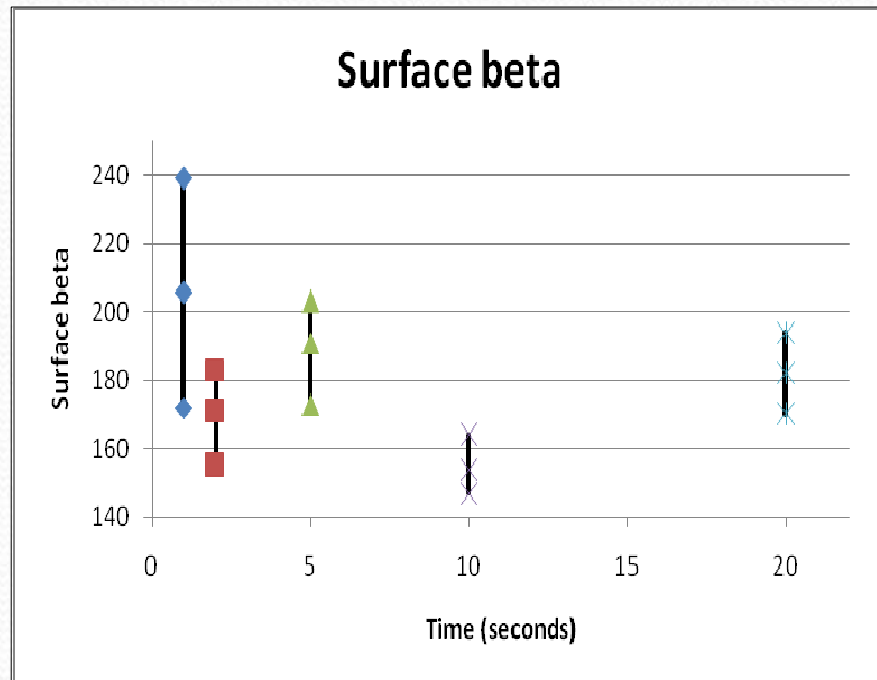


## 2- Résultats: Dépôt de nickel qq $\mu\text{m}$

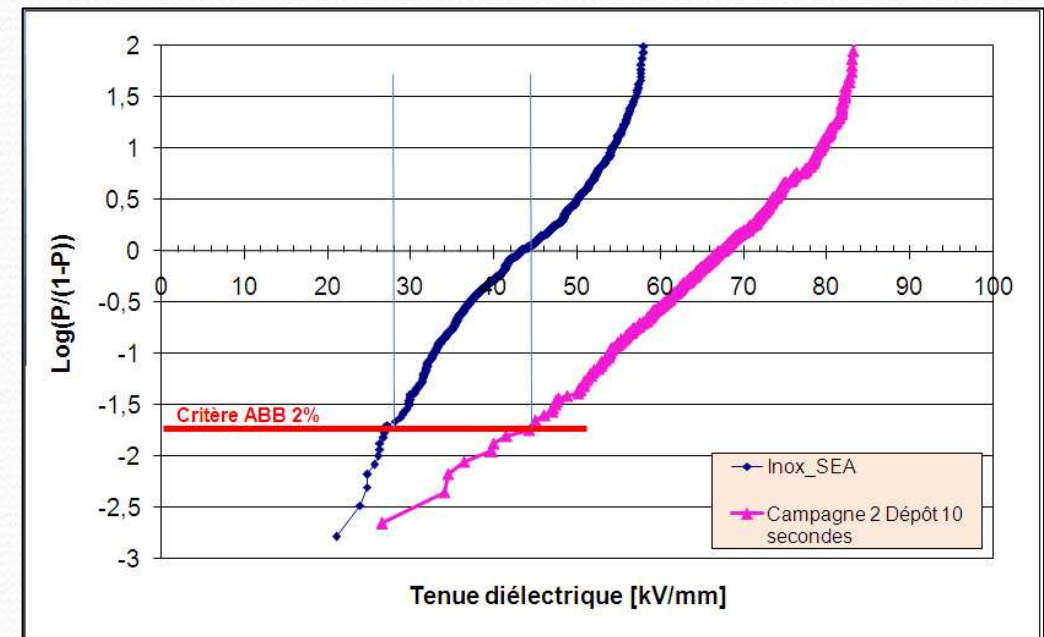


Lot	Preparation		Surface beta
1	Wood Ni - Ni 1 to 2 $\mu\text{m}$ - EDI + US Hot Air - 2H degreasing	Mean	200
		Sigma	17.7
2	Ni Wood - Ni 1 to 2 $\mu\text{m}$ EDI + US - Hot Air	Mean	191
		Sigma	44.2

## 2- Résultats: Dépôt couche mince



→ 10 secondes = Conditions optimales



→ 10 secondes dépôt Ni électrolytique = + 44 nm sur l'aiguille



## 3- Solutions: Maraging steel (proposed by Farall ~1980)

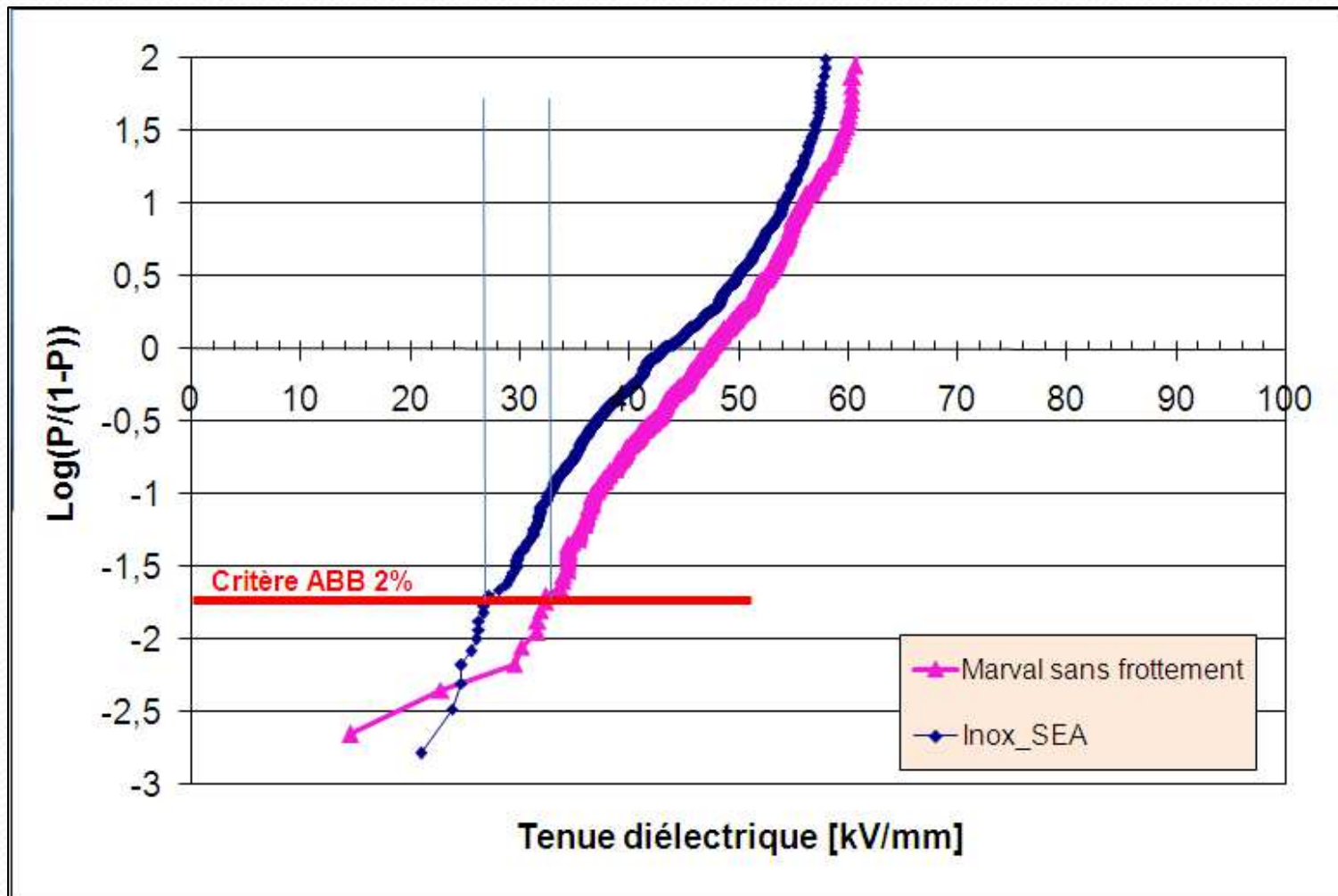
**Proposed by Farall ~1980 : No Chromium carbide**

### → Composition maraging steel:

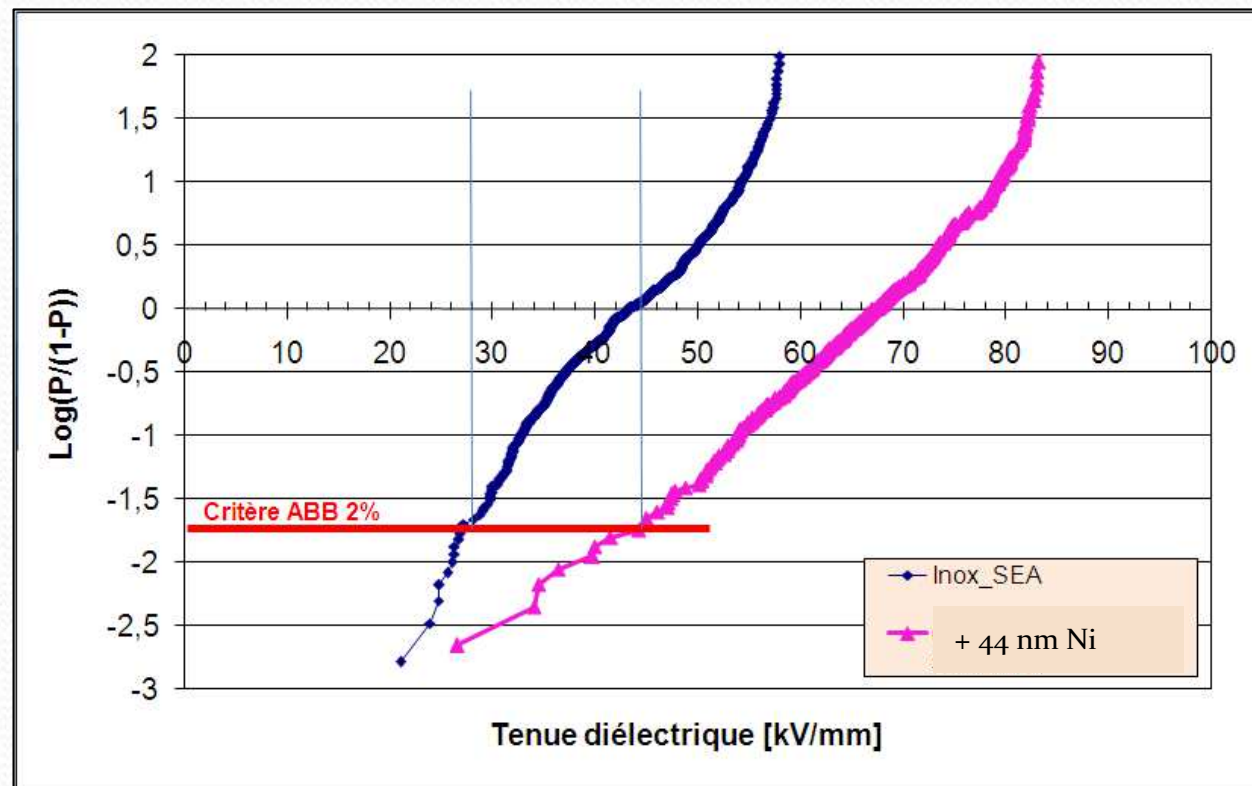
- Fer
- Nickel (18%)
- Molybdène (5%)
- Cobalt (8%)
- Carbone, aluminium et soufre (faible quantité)



## 3- Résultats: Maraging steel



Courbes de référence:

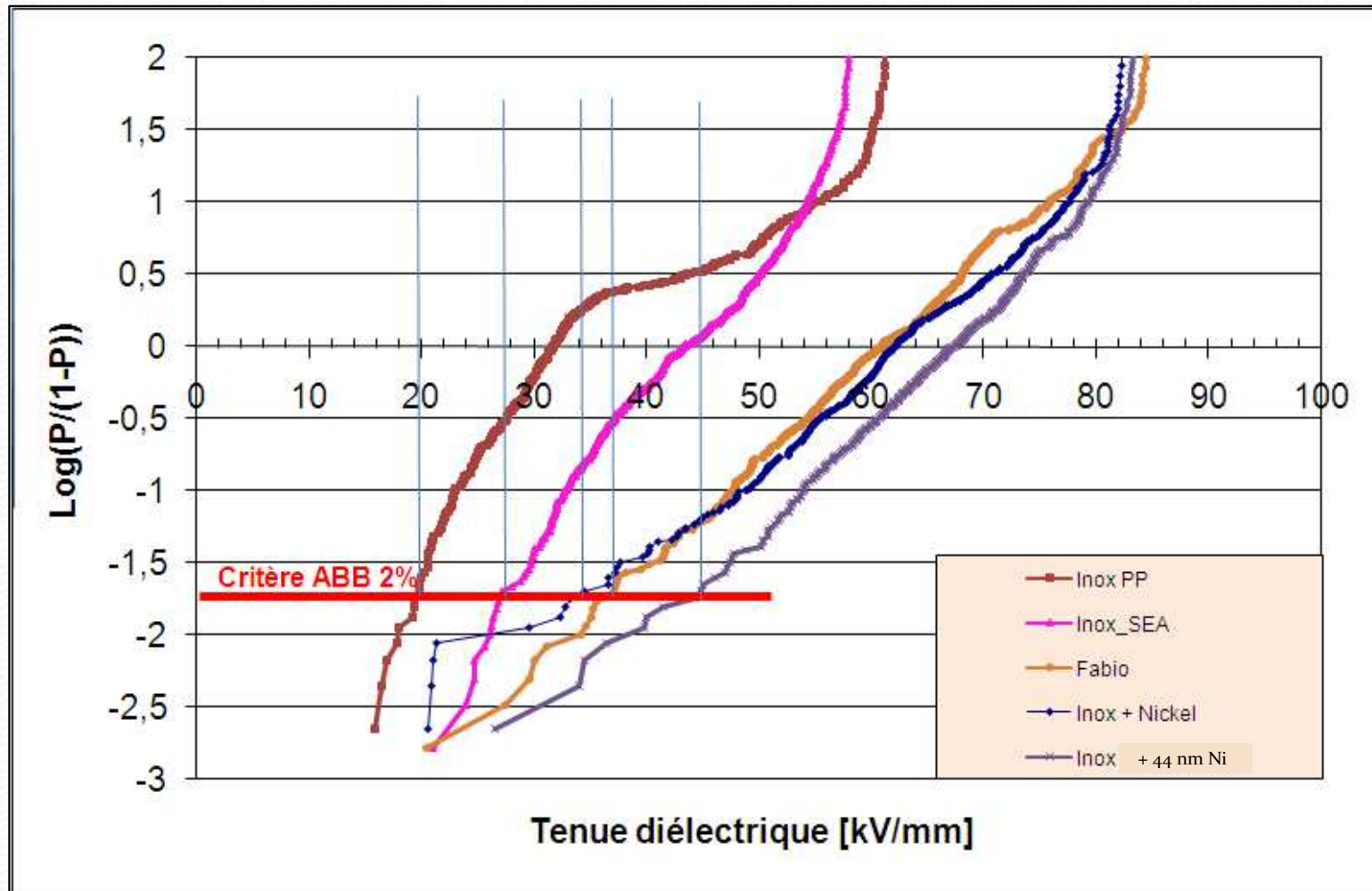


## Conclusion inox

Deux solutions sur trois validées:

- Electrolyse sélective → 50% d'amélioration
- Dépôt Ni de 44 nm → 57% d'amélioration
- Résultats avec le maraging steel : marginal

## Resumé : Inox



# Discussion of results & Summary

- Introduction
- contexte de stage
- premier partie

## Significant improvement

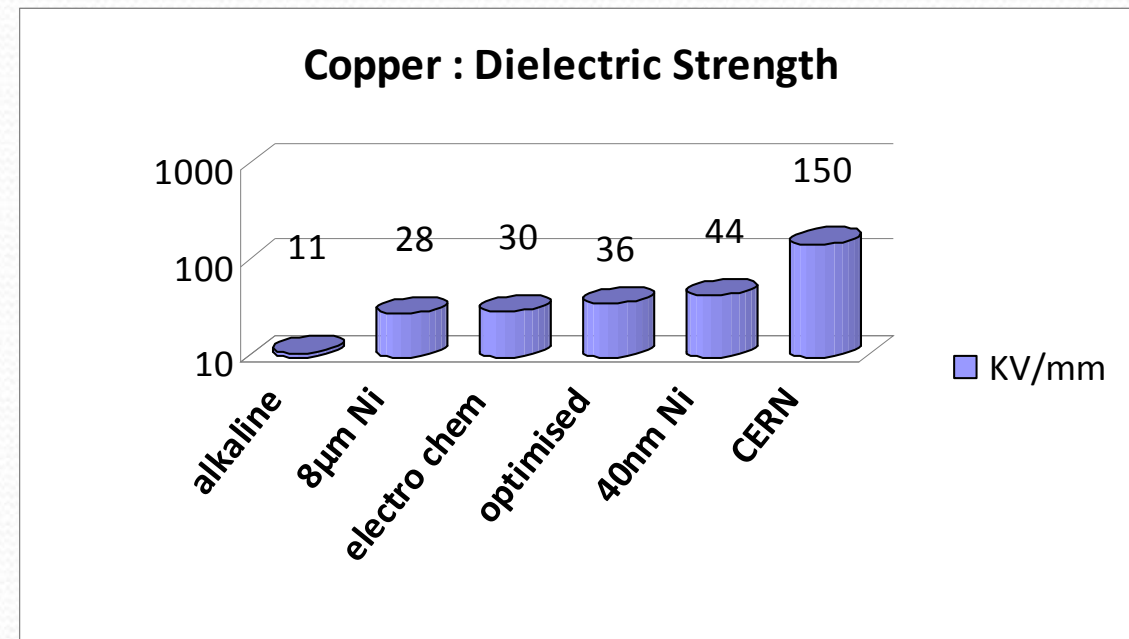
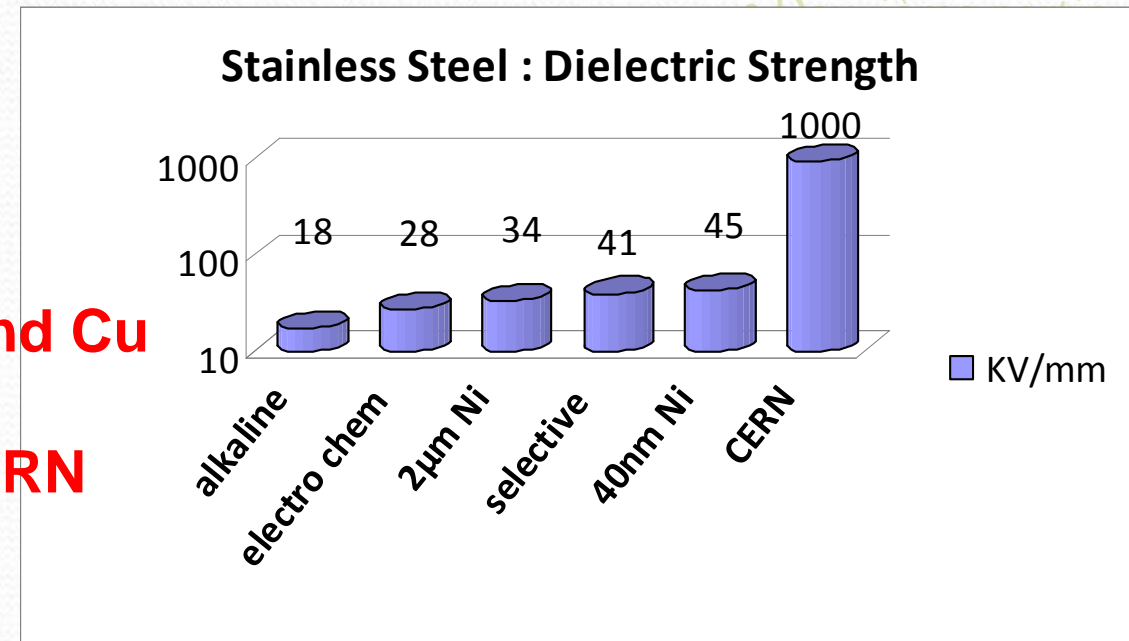
- 250% \* StSt
- 400% \* Cu

No difference between StSt and Cu

Significant difference with CERN

## Possible causes

- Pollution after cleaning due to handling ?
- Cleaning still inefficient due to oxydes or alike ?





**Thank you for your attention**