

Detection of ionizing radiation by intrinsic optical fiber sensors: preliminary results

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Purpose

- To develop a totally passive miniature radiation sensor based on optical fiber resonant cavity
- Basic idea: radiation-induced effect on fiber material (SiO_2) \rightarrow refractive index variations \rightarrow prospectively absorbed dose measurements

Background

“Radiation domain”

- Recent technological advances in RT have increased the use of small fields (<4 cm x 4 cm) reinforcing the demand for novel dosimeter technology
 - ✓ R. Alfonso et al , Med. Phys. 2008
- Among the available dosimetry systems none of them have the characteristics of an ideal dosimeter
 - ✓ J. Andersson et al, Med. Phys. 2012

“Optical fiber domain”

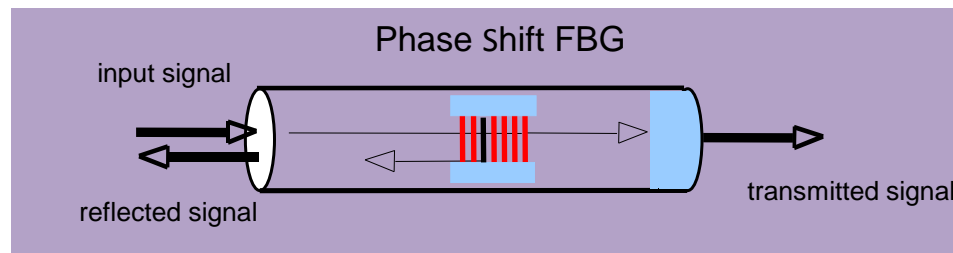
- Optical fiber detectors as extrinsic sensors (transmission of light)
 - ✓ S. O’Keeffe et al Sens. Rev. 2008, A. L. Huston et al Nucl. Instrum. Methods Phys. Res. 2001
- Radioluminescent dosimeters based on doped SiO₂ optical fiber as active sensors (light-emitting fibers) but some limitations are present (i.e. “stem effect” for MV photons)
 - ✓ E. Mones et al Radiat. Meas. 2008, M. Aznar et al Phys. Med. Biol. 2004, I. Veronese et al Rad. Meas. 2010

Theories

- Different theories on Ge-doped silica refractive index variations after exposure to IRs:
 - “**color center model**” → creation of defect centers by interaction of high-energy photons with OH radicals and Ge, naturally present in silica fibers, or with added dopants
 - » Skuja L. et al, J. Non-Cryst. Solids 1998
 - “**compaction effect**” → a radiation induced densification process
 - » Buscarino G. et al, J. Phys. Condens. Matter 2010
 - A combination of the above theories
 - » Takshashi M. et al J. App. Phys. 2002

Materials and methods

- We employed totally passive Ge_{6%mol}-doped optical fiber sensors based on special Bragg-grating (FBG) cavity reflectors.



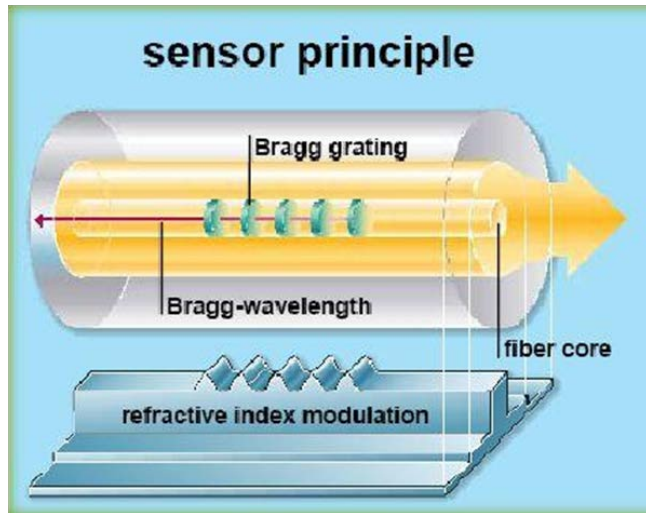
*Bragg
Peak reflectivity*

$$\lambda_B = 2n_{eff} \Lambda$$

Λ = Grating pitch

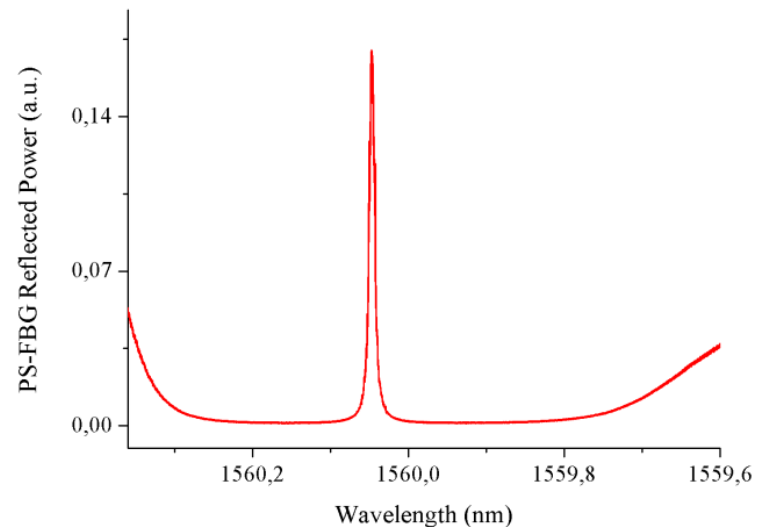
**Any change in the grating
pitch and/or refractive index
results in a shift of λ_B**

Sensors characteristics (1)



- The effective interaction volume of the sensor
 $= 6 \times 10^{-4} \text{ mm}^3$

- Transmission and reflection spectrum with only one narrow mode at the center of Bragg curve



Experimental apparatus: FBG irradiation

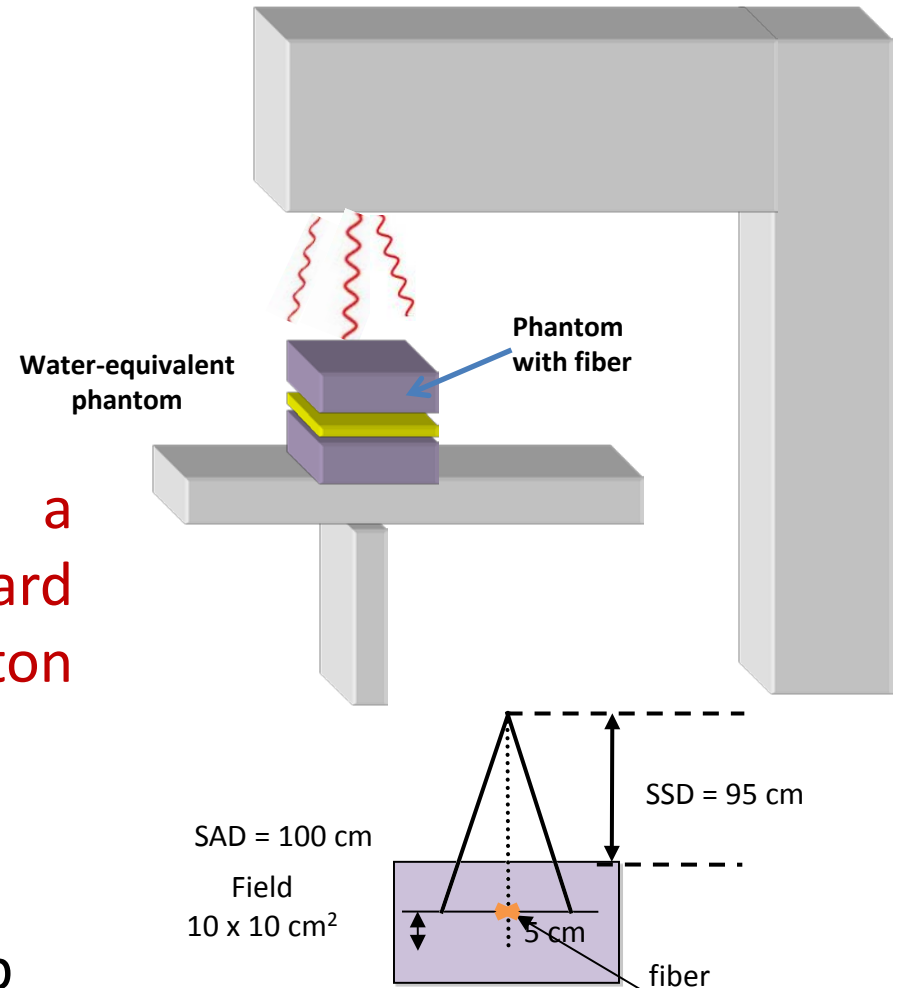
2 sensors with different spectral features:

- ✓ FBG1
- ✓ FBG2 (higher reflectivity)

The FBGs were inserted into a phantom irradiated in standard conditions by a 6MV linac photon beam

2 dose steps:

- ✓ FBG1 with 10 Gy increments up to 30 Gy
- ✓ FBG2 with 1 Gy and 2 Gy



Sensors characteristics (2)

$d_{core} = 8 \mu\text{m}$ Ge-doped (6% mol) SiO_2

$d_{cladding} = 125 \mu\text{m}$ SiO_2

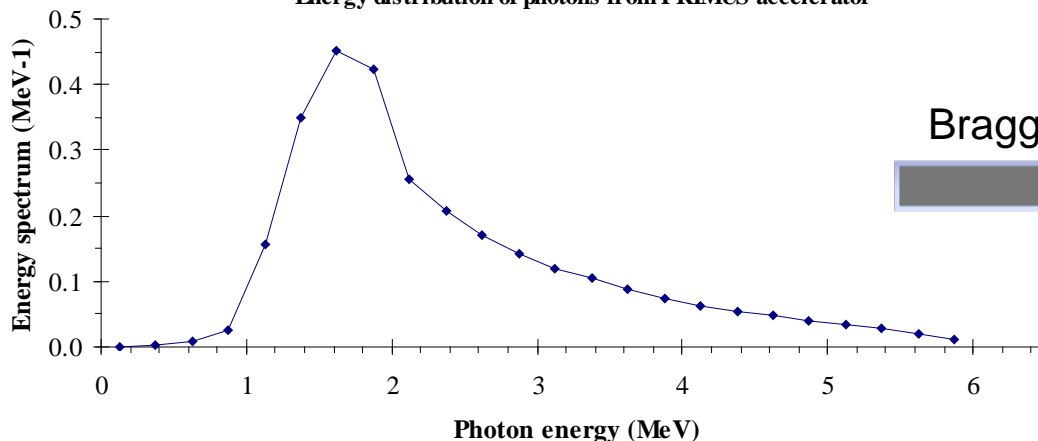
core

cladding

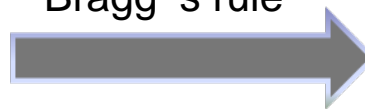
$w_{\text{Si}} = 43.4\%$	$w_{\text{Si}} = 46.7\%$
$w_{\text{Ge}} = 7.2\%$	$w_{\text{O}} = 53.3\%$
$w_{\text{O}} = 49.4\%$	

	Z	Z/A	I (eV)	ρ (g/cm ³)	M (molar mass) (g/mol)
Si	14	0.49848	173.0	2.330	28.086
Ge	32	0.44071	350.0	5.323	72.63
O	16	0.50002	95.0	1.332×10^{-3}	15.999
SiO₂				2.63	60.08

Energy distribution of photons from PRIMUS accelerator



Bragg's rule

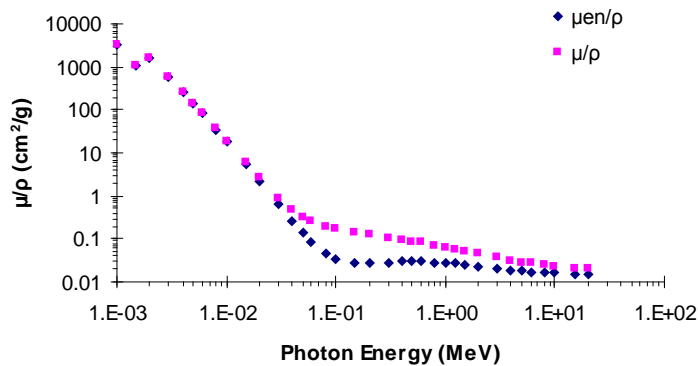


$$\left(\frac{\mu_e n}{\rho} \right)_m \text{ mixture} = \sum_i w_i \left(\frac{\mu_e n}{\rho} \right)_i$$

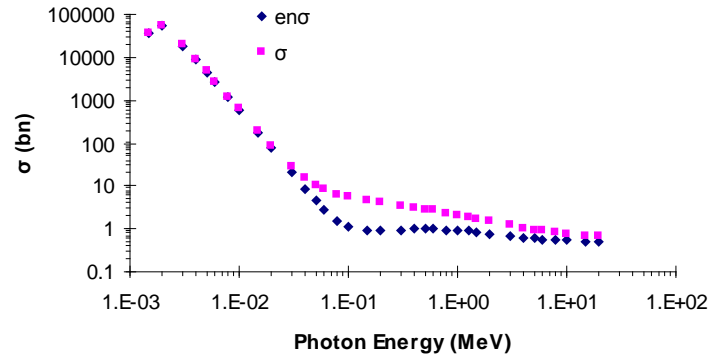
The mass attenuation coefficients (μ_m) and the effective atomic number (Z_{eff}) of the sensors were calculated as function of the photon energy in the range 1-6 MeV

Interaction mechanisms of radiation within the sensor material

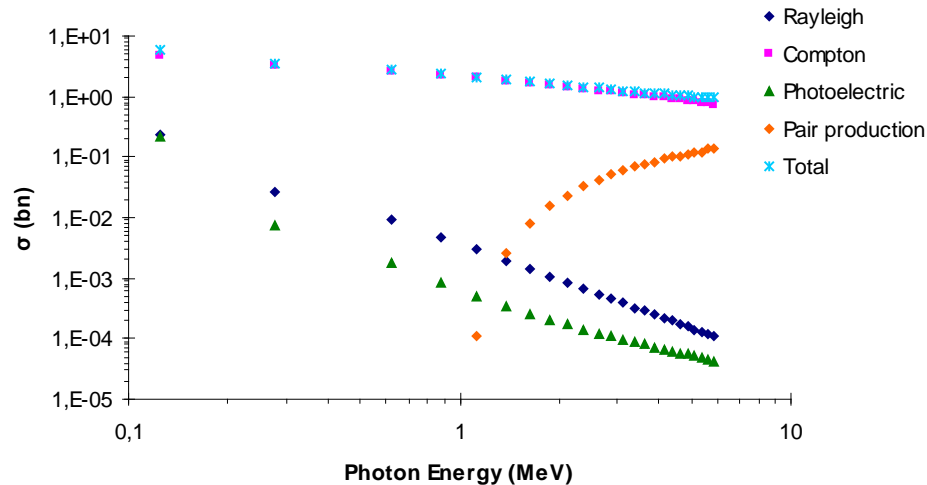
Mass attenuation and the mass energy absorption coefficients vs photon energy



Attenuation and energy-absorption cross sections vs photon energy

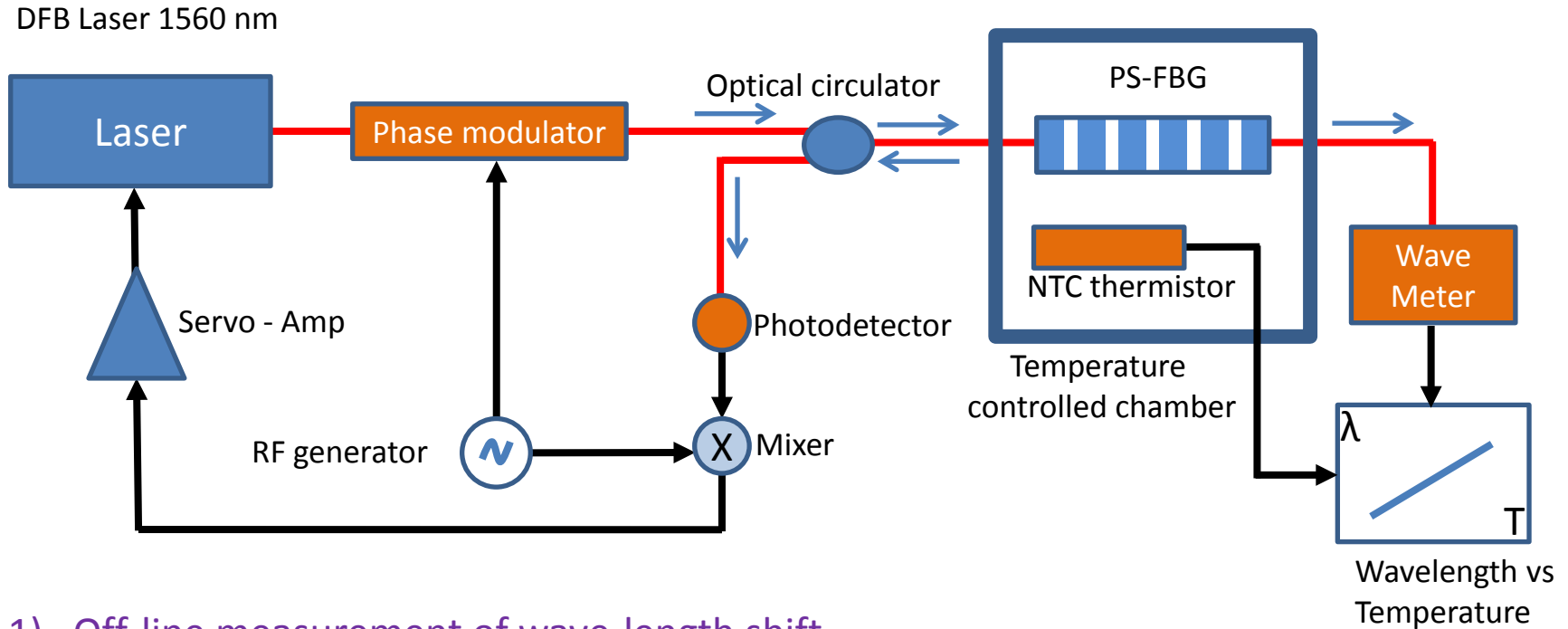


Attenuation cross sections vs photon energy for each interaction process

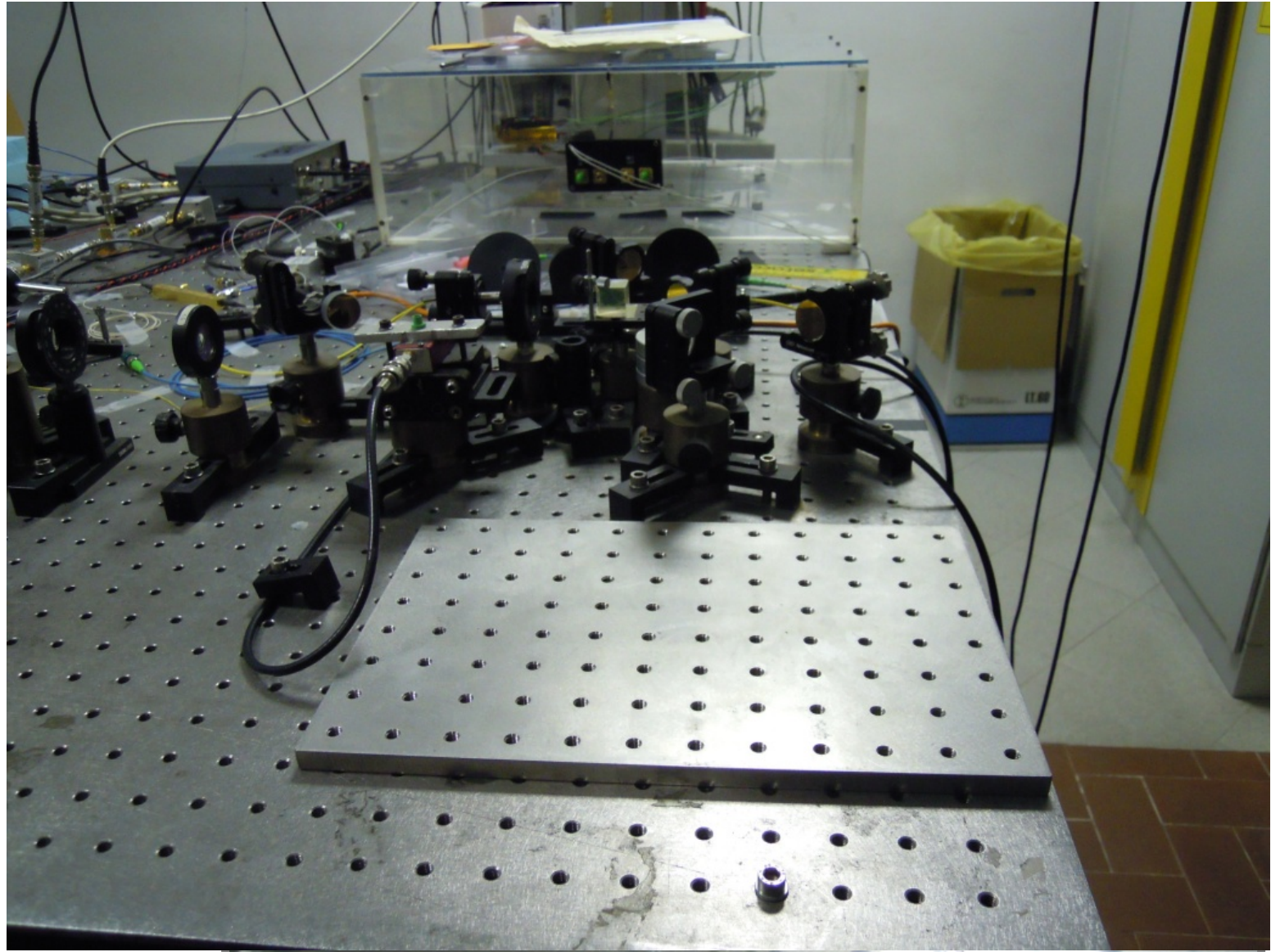


- The weighted average $\mu_m = 0.044 \text{ cm}^2/\text{g}$ (1-6 Mev)
- The weighted average $Z_{\text{eff}} = 10.04$ (1-6 Mev),
“nearly water equivalent” ($Z_{\text{eff}} = 7,42$)

Experimental apparatus: high sensitivity interrogation scheme



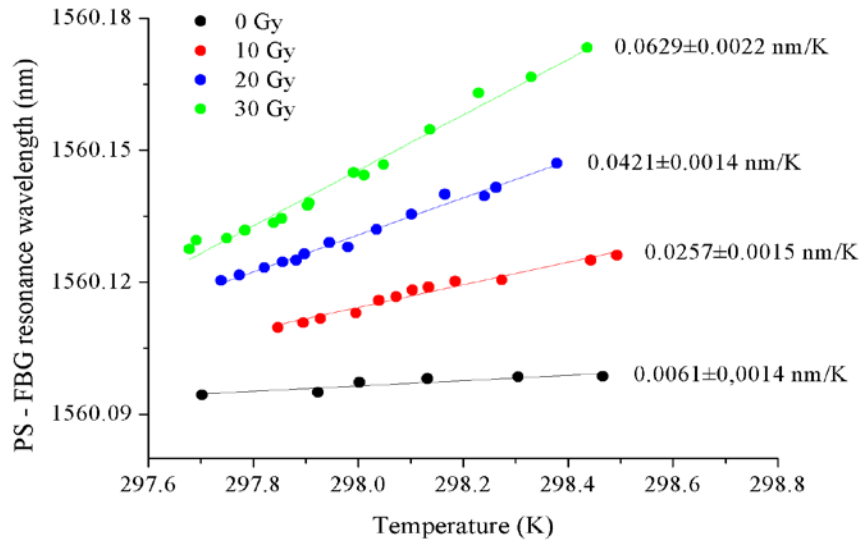
- 1) Off-line measurement of wave-length shift
- 2) The FBG is placed in a temperature controlled chamber (negative temperature coeff thermistor, 1 mK)
- 3) To check if λ -shift were due to thermal shift, the temperature is scanned and the thermo-optic response (λ_B vs T) measured (uncertainty on thermoptic response $\approx 1\text{pm/k}$)



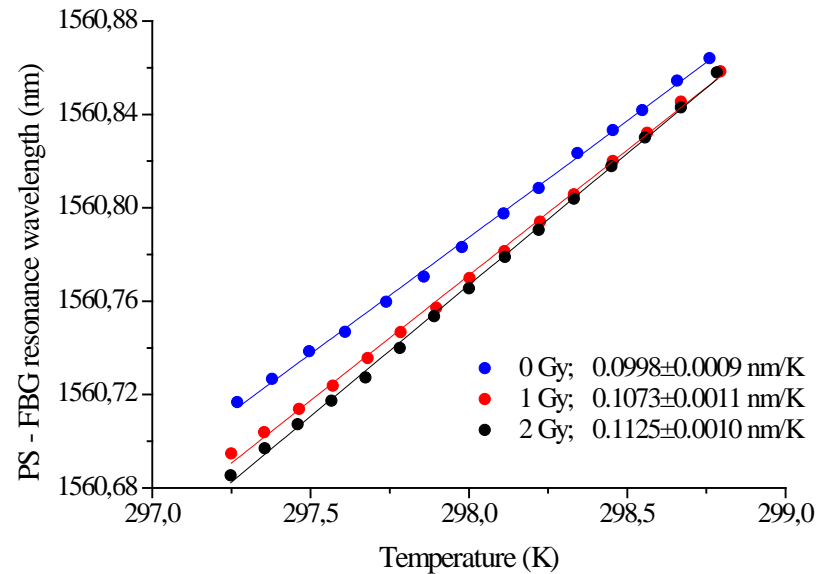
RESULTS

A net **wavelength shift** was measured after each irradiation

FBG-1

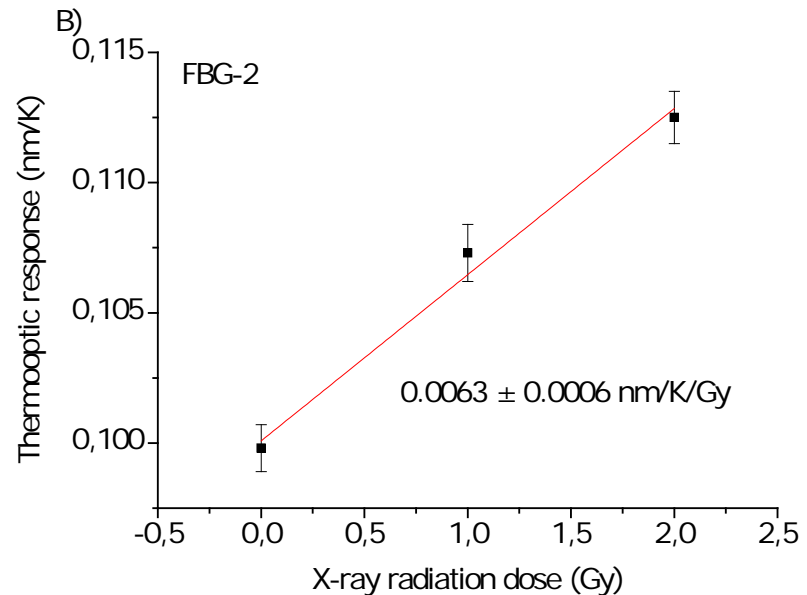
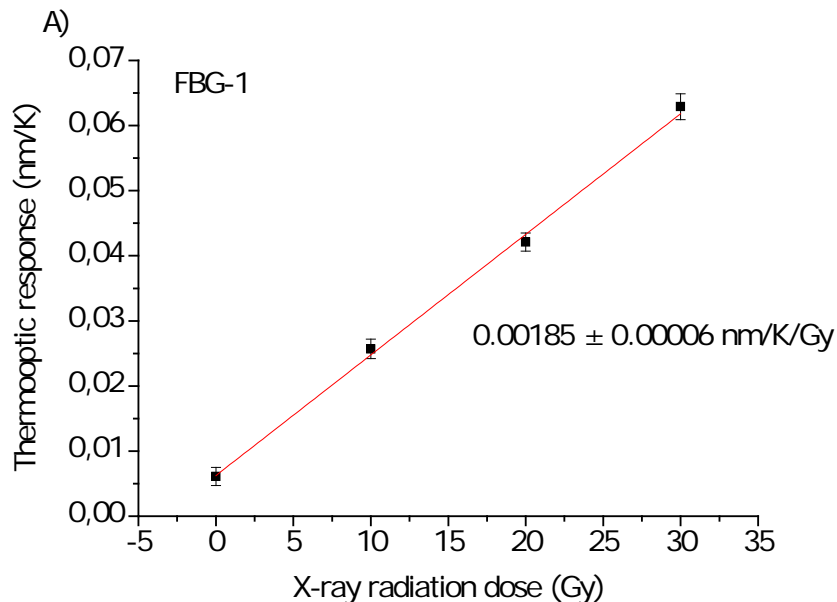


FBG-2



RESULTS

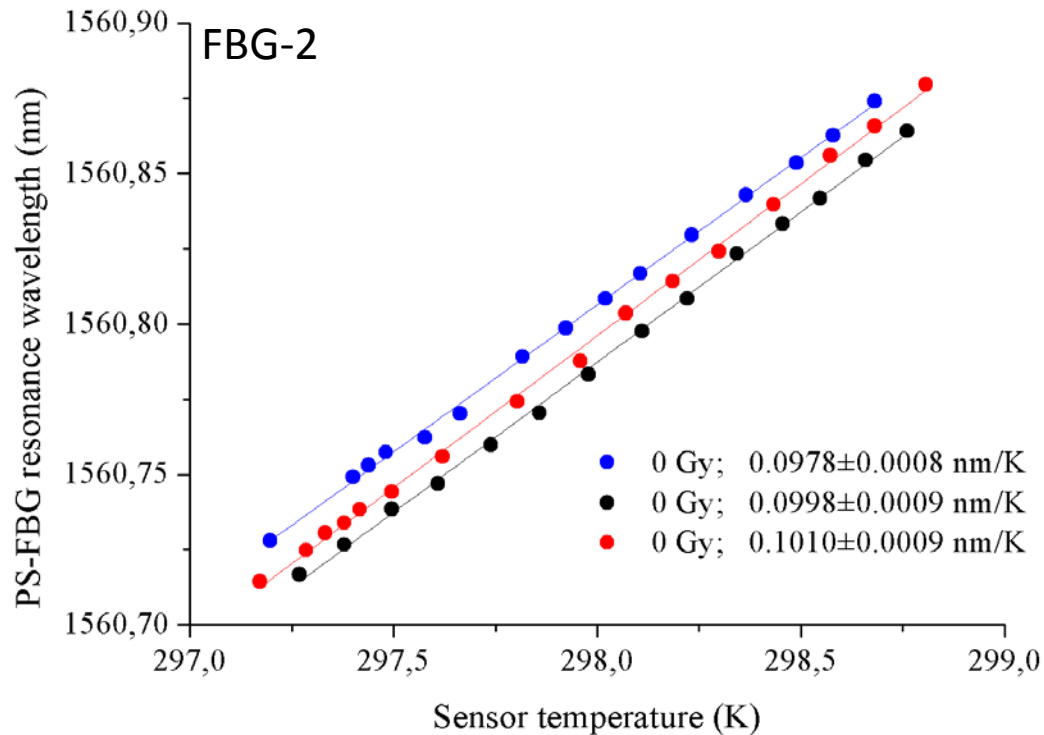
Additional phenomenon: a radio-induced change of the fiber **thermo-optic response** measured by tuning the resonant mode wavelengths with temperature



Dividing the dose response coefficient (FBG-2) by the average value of the uncertainty on the single measurement of the thermo-optic response (1 pm/K) we obtain a final resolution of 0.16 Gy.

Reproducibility

Reproducibility test: repeated measurement of the thermo-optic response before irradiation



Reproducibility $\sim 2\%$

Conclusion

“To function as a radiation dosimeter, a sensor must possess at least one **physical property that is a function of the measured dosimetric quantity** and that can be used for radiation dosimetry with proper calibration”

The observed effect of IRs delivered to the FBG sensor is two-fold :

1) A wavelength shift

2) A change of the fiber thermo-optic response





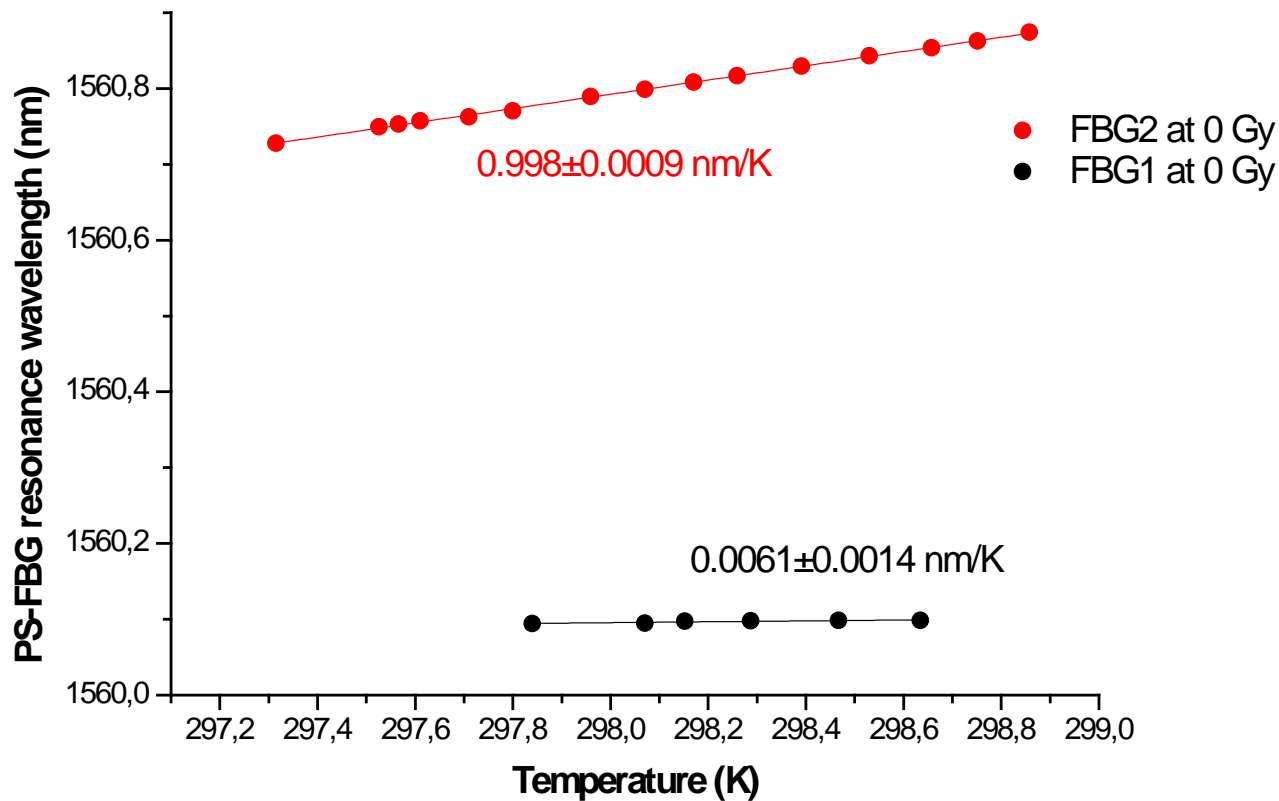
It could work!!!!!!!!!!!!!!

Thank you for your attention

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- 1) **wavelength shift** : undesired effects of mechanical strains and temperature fluctuations on the fiber that may reduce the accuracy and even mask the desired information at small doses
- 2) **thermo-optic response** : substantially immune to environmental conditions.

FBG1 vs FBG2: higher reflectivity of FBG-2



higher resolution of FBG-2