



3MOrC1-04



# Essential Design, Construction and Test Elements of ITER Axial Insulation Breaks

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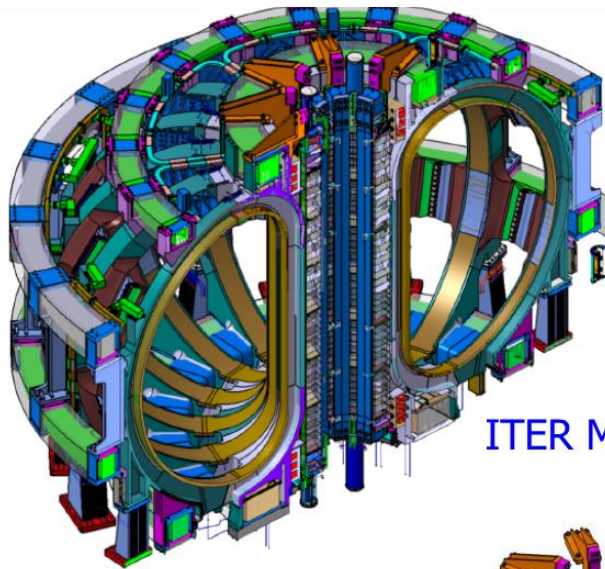
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# Outline

- ❖ Purpose and Need in ITER Magnets
- ❖ Conceptual design
- ❖ Specification Outline
  - Mechanical, Electrical, Leak and Pressure aspects
- ❖ Critical Design Areas and Influence of Composite Properties
  - Bonded Joints and Joint Integrity
- ❖ Realisation of concept and results
  - (with IPR limitations)
- ❖ Summary and conclusions

# ITER Magnets

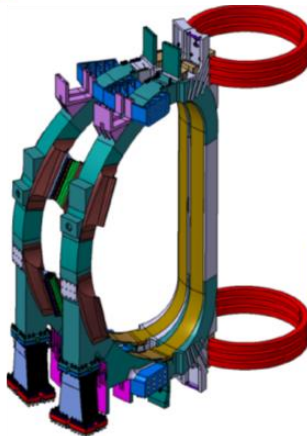
- The ITER magnet system is made up of
  - 18 Toroidal Field (TF) Coils,
  - a 6-module Central Solenoid (CS),
  - 6 Poloidal Field (PF) Coils,
  - 9 pairs of Correction Coils (CC's).



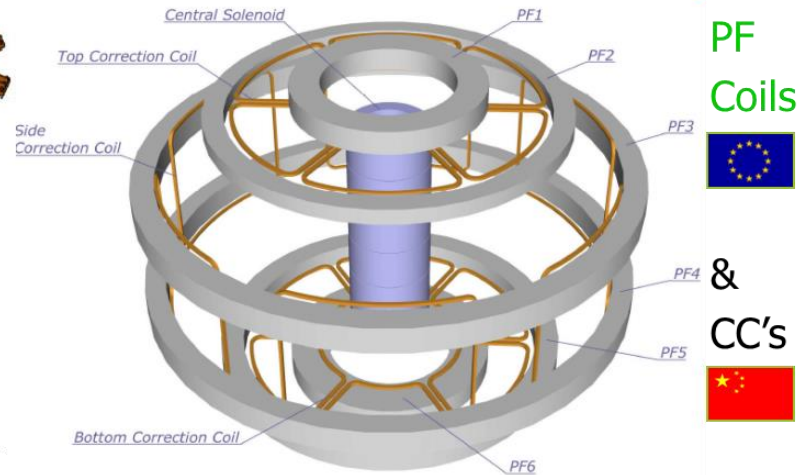
ITER Magnet System



Pair of TF Coils



CS Coil



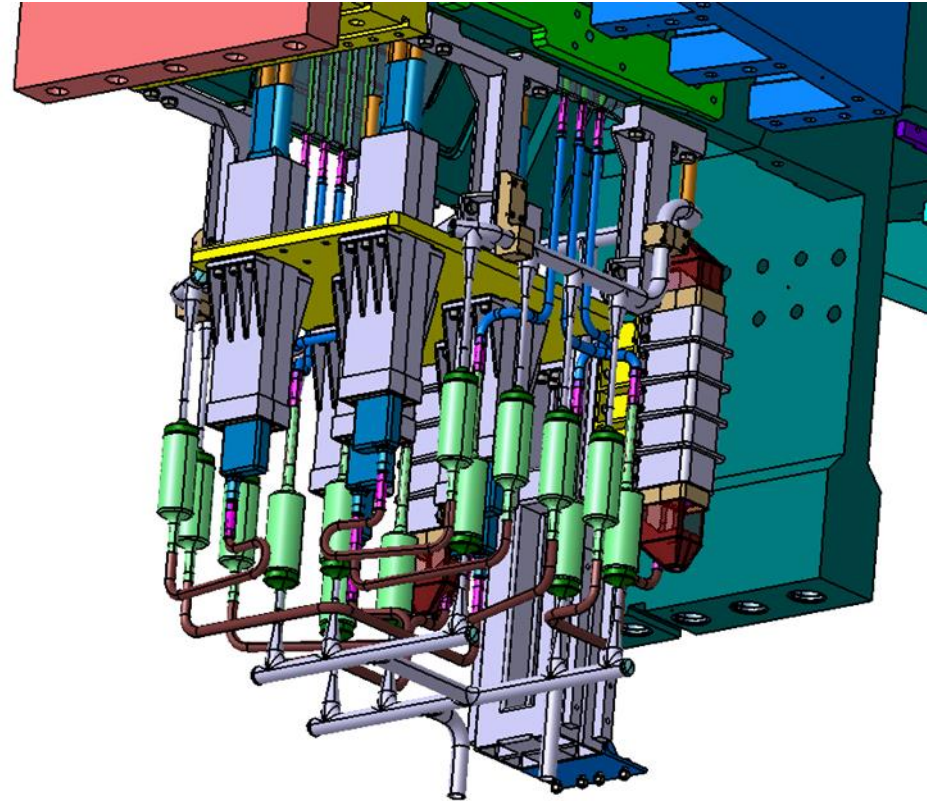
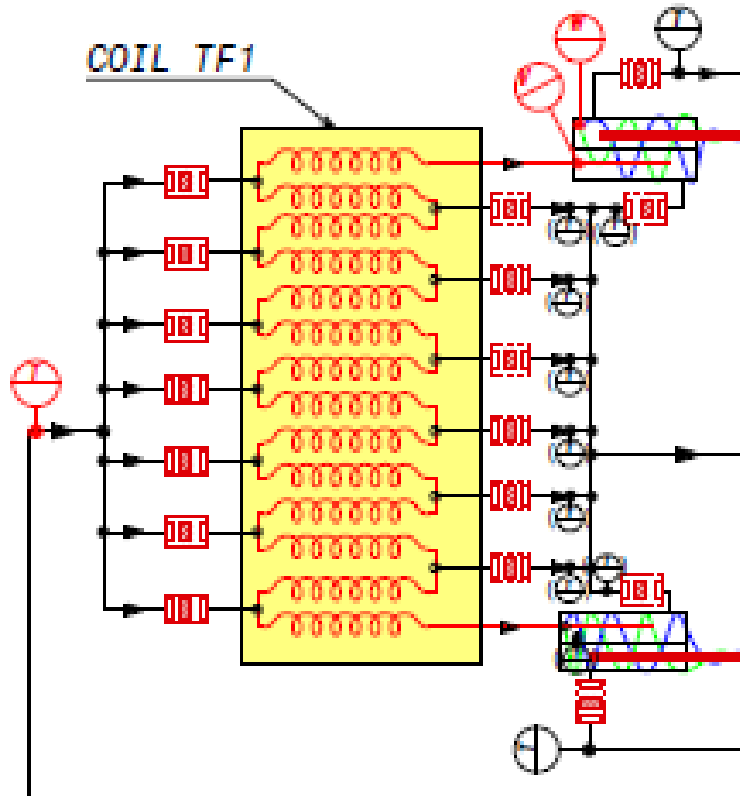
PF Coils

& CC's

# Purpose and Need

- ❖ Axial insulation breaks must electrically isolate the cryogenic distribution system from the high voltage of the ITER magnets and bus bars.
- ❖ Cable-in-conduit conductors and the supercritical helium distribution system are **electrically connected**
- ❖ The pulsed magnets of ITER experience a rapid rise in voltage
- ❖ Under some conditions electric potentials may rise to **28kV** in some of the magnets
- ❖ Possible high internal pressures
  - ❖ Quench pressure : 30 b

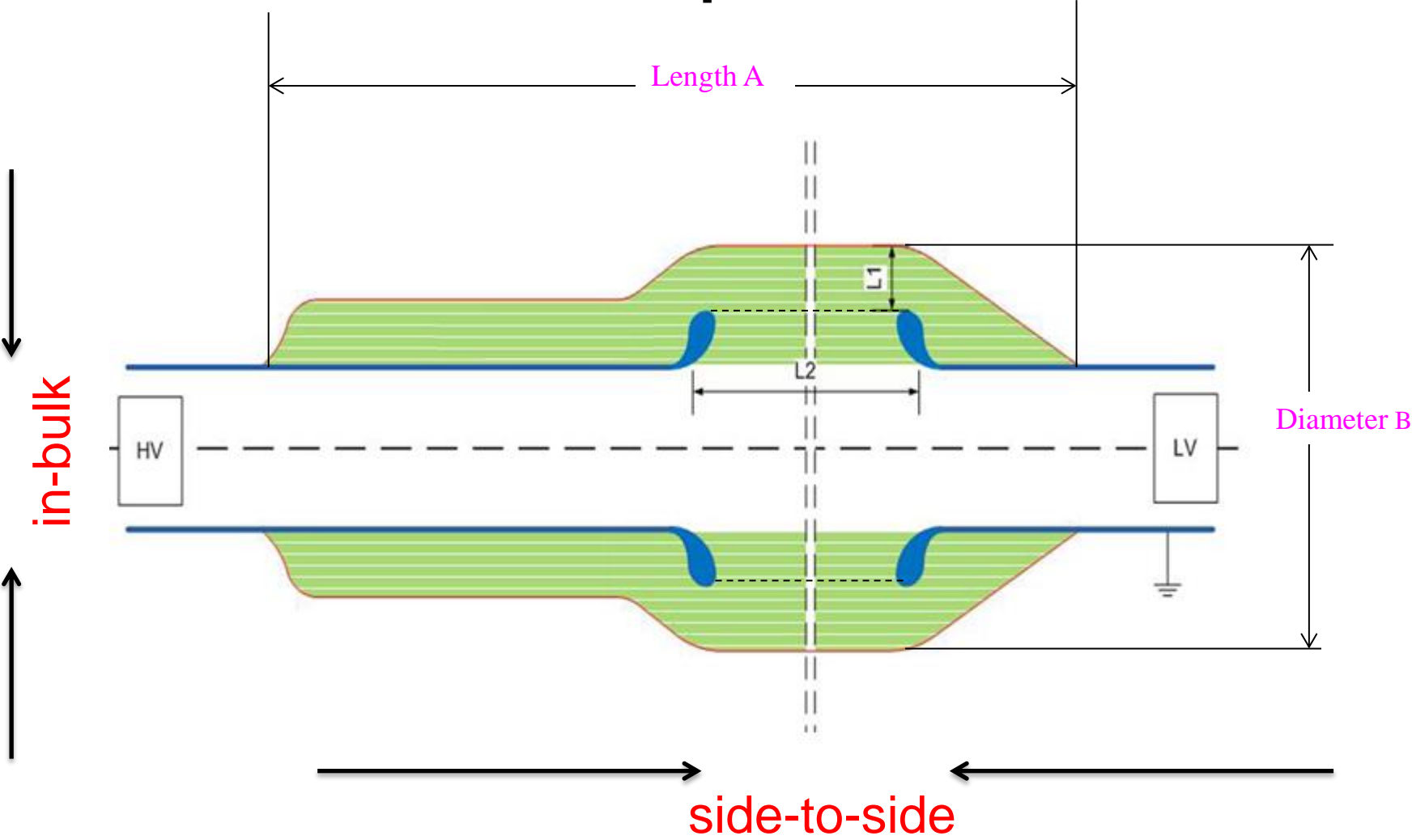
# ITER Magnets and Insulation Breaks



 Insulation Break (IB)

About 1400 units required

# A Conceptual View



# Salient aspects from the specification

	Units	Value/Range	Note
Temperature of the inner fluid	[K]	4.2 - 6	Super-critical helium ( <sup>4</sup> He)
Pressure	[bar]	4 - 6	Absolute
Maximum pressure at <u>quench</u>	[bar]	30	Absolute
Maximum inner flow rate	[g/s]	20	Super-critical helium ( <sup>4</sup> He)
Maximum operating voltage level	[kV] DC	15	PF Coils
Worst case <u>failure</u> voltage	[kV] impulse	28 / 4	PF Coils/CC Coils
Outside pressure	[Pa]	1x10 <sup>-4</sup>	Presence of gaseous He in Paschen conditions

## Summary of HV Levels for tests

Description	Voltage Level	
	HV	LV
Type Test across L2 (‘side-to-side’, dry air)	56kV	8kV
Type Test across L1 (‘in-bulk’, dry air)	56kV	8kV
Routine Test L2 (acceptance test voltage + 20%)	35kV	6kV
Routine Test L1 (acceptance test voltage + 20%)	35kV	6kV
Acceptance Test L2 (‘side-to-side’, dry air)	29kV	5kV
Acceptance Test L1 (‘in-bulk’, dry air)	29kV	5kV



# Mechanical requirements (design values)

- ❖ 2kN in tension and compression at 300K and 77K
- ❖ Bending moments of 100N.m at 300K and 77K
- ❖ Torsion 100N.m at 300K and 77K
- ❖ Fatigue resistance over 60000 cycles for +/-50% of above loads at 300K and 77K
  - The number of fatigue cycles represents a safety factor of 2
- ❖ Radiation withstand 100 kGy ( $10^{19}$  fast neutrons/m<sup>2</sup> and gamma)

# Requirements for Thermal Cycles, Leak and Pressure (design values)

- ❖ Total of 50 thermal cycles from 300K to 77K with a predefined cooling rate
- ❖ 50 pressure cycles at 77K and at 300K, up to 39 bar
- ❖ Measurement of the leak rate at 300K and 77K after every 5 pressure cycles ( $<10^{-9}$  Pa m<sup>3</sup>/s)
- ❖ Thermal cycles, pressure cycles and leak rate measurements alternated with mechanical tests

# From Concept to Reality (and Results)

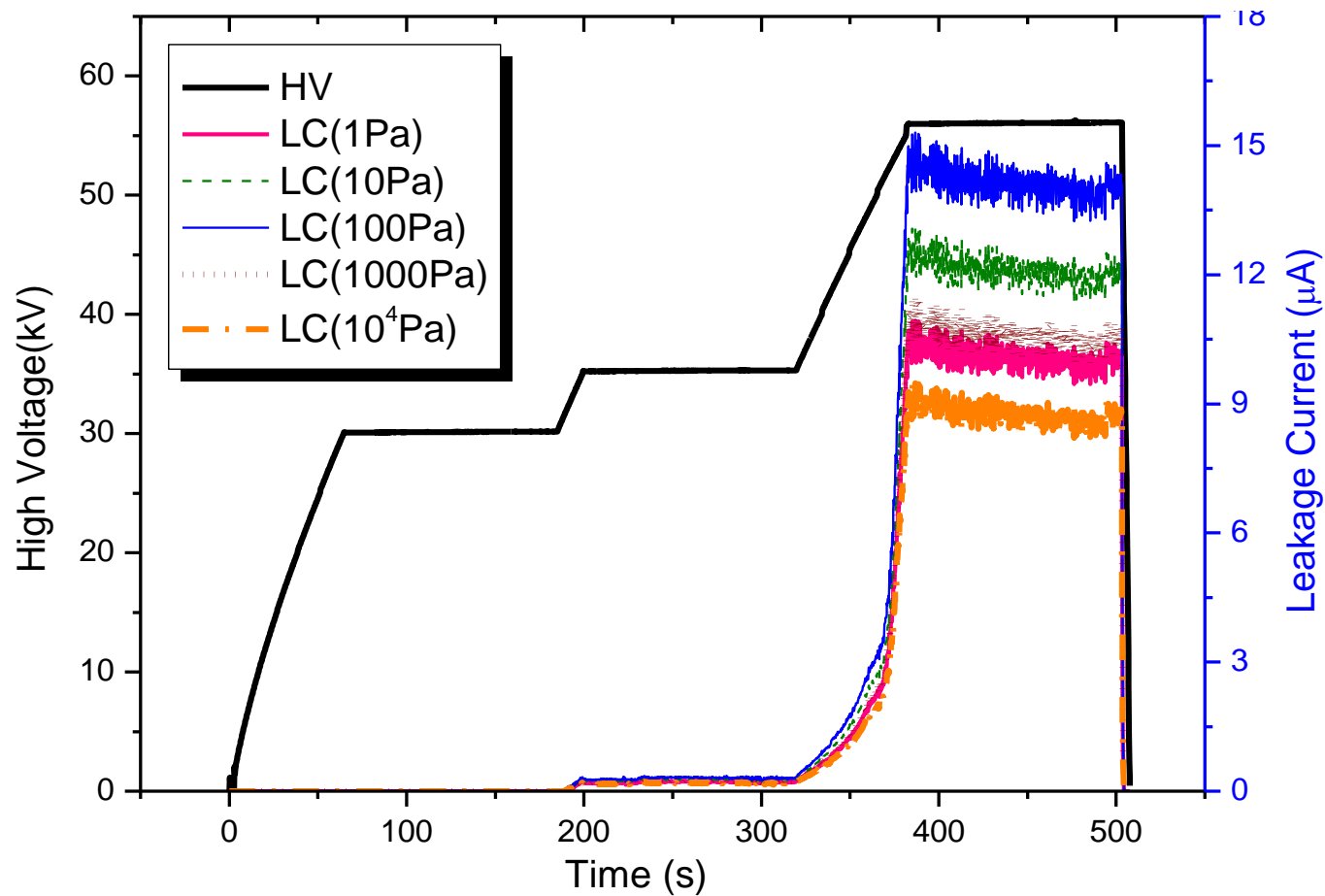
- ❖ Three contracts completed – each supplier submitted eight prototypes
- ❖ All submitted insulating breaks fully tested by supplier
- ❖ Independently tested afterwards for IO (CERN\* & HVPD)
- ❖ Destructive Analysis to confirm (or other wise) compliance with design plan
- ❖ Determine from destructive analysis freedom from internal cracking (or other wise)
- ❖ Units from supplier Z showed presence of cracking in bulk

*\*See 1EOrF3-02 by J. Kosek et al.*

# Typical Results – HV Testing

<b>Test Condition / t=2 min</b>	<b>Leakage Current</b>
<b>29kV in bulk</b>	<b>0.1<math>\mu</math>A</b>
<b>29kV side to side in dry air</b>	<b>0.1<math>\mu</math>A</b>
<b>35kV in bulk</b>	<b>0.2<math>\mu</math>A</b>
<b>35kV side to side in dry air</b>	<b>0.5<math>\mu</math>A</b>
<b>56kV in bulk</b>	<b>9.2<math>\mu</math>A</b>
<b>56kV side to side in dry air</b>	<b>3.1<math>\mu</math>A</b>

# Typical Results from Paschen Test



# Partial Discharge

Supplier	Length (mm)		PDIV (kV)	
	A	B	Internal *	Surface**
X	160	55	--	14
Y	405	65	--	16
Z	270	95	--	14

\* No internal PD observed up to 56 kV

\*\* Surface PD measured side-to-side

# He Leak Test after 50 Thermal Cycles (Typical Results)

Test Condition / t= 10 min	Result
Vacuum leak at 300K, 1MPa	3.2 E-10 Pa·m <sup>3</sup> /s
25 cycles at 1MPa, 300K	3.3 E-10 Pa·m <sup>3</sup> /s
25 cycles at 4MPa, 77K	3.4 E-10 Pa·m <sup>3</sup> /s
Vacuum leak at 300K and 77K (*)	3.3 E-10 Pa·m <sup>3</sup> /s

Results after 25 mechanical cycles (tension/compression, bending and torsion) at each 300K and 77K

(\*) Final verification after 60kcycles fatigue test without any measurable change in leak rate

# Summary and Conclusions

- ❖ Prototypes manufactured by three potential suppliers – all prototypes delivered to IO meet specification
- ❖ Primary ‘seal’ in compression in all designs, no visible dis-bond in this joint
- ❖ Possibility that other bonds to stainless steel may be in tension – no visible dis-bonds
- ❖ Possibility of axial shear stress – no visible dis-bonds
- ❖ ‘Predictable’ failure observed in thick composite tube – longer term consequences under consideration
- ❖ Destructive analysis indicated deviations from manufacturers design plan
- ❖ Longer term ‘quality is king’ – strict adherence to QAP and Manufacturing and Inspection Plan to ensure that composite design & performance along with adhesive bond strengths are maintained
- ❖ Contract for 80% of total quantity has been already placed



# ITER today ...



# Thanks for your attention