

Enhancement of critical currents in wires of MgB₂ using different sheath materials

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Outline

- PIT method: some previous results
- Wires with different sheath materials:
 - Structural characterization
 - Superconducting characterization
- Conclusions

OBJECTIVES

✤ Optimization of thermal heat treatments for mono and multifilamentary wires prepared with different sheath materials (Cu, Ti, SS 316L).

To analyze the correlation between actual defects and improving J_c

Process for PIT MgB2 wires - tapes

Ex-situ process:

- Stainless steel as sheath material
- MgB2 (Alfa Aesar) + 5 % at Mg excess
- MgB2 (Alfa Aesar) + 5 % at SiC
- MgB2 + ??

Annealings:

- Intermediate annealings at 500-900°C
- Final annealing: needed for removal o microcracks formed in the cold working



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Carbon nanotubes effects on the relaxation properties and critical current densities of MgB_2 superconductor

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Journal of Applied Physiscs (2013) in press.

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Sheath

• SS.

• Ti.

• Ag

• Cu

- Powder in Tube (PIT) method: desired performance (J_c) already achieved in a small scale by
 - Optimization of post-annealings (R. Flukiger et al. [review: Physica C 385 (2002) 286]; G. Grasso et al. [Supercond. Sci. Technol. 16 (2003) 271; A. Serquis et al [APL 82 (2003) 1754]; A. Serquis et al [JAP 94 (2003) 4024]
 - ✓ HIPing (Serquis *et al.* APL 82 (2003) 2847)
 - Intermediate annealings Serano et al IEEE 15 (2005) 318
 - doping with SiC (Dou *et al.* APL 81 (2002) 3419); Serquis et al IEEE 15 (2005) 3188; Serrano et al. JAP 103 (2008) 023907, Da Silva et I. IEEE Transactions on Applied Superconductivity 19 (2009) 2730-2734.
 - Several intermediate heat treatments at high temperatures degrade the inter-grain critical current more than the increase in intra-grain $J_{\rm c}$ due to SiC addition
 - Connectivity of MgB₂ core is a first order key parameter for obtaining good superconducting properties.

Effect of heat treatments for different sheaths

Optimiza • heat trea suitable material

	Sample	Sheath	sample	Size (mm)	(N) and temperature (T)
otimization of eat treatments itable for each aterial	SS1	stainless steel	tape	0.42 x 2.58	N = 4+2, T = 900°C
	SS2	stainless steel	tape	0.35 x 2.85	N = 4+2, T = 600° C
	Ti1	titanium	tape	0.35 x 2.5	$N = 4, T = 600^{\circ}C$
	Ti2	titanium/copper	tape	0.62 x 3.1	$N = 1$, $T = 600^{\circ}C$
	Ti3	titanium (wire) titanium/copper	multifilament tape	0.75 x 1.86	N = $4+3$, T = 600° C
	Ag1	silver	tape	0.45 x 3.7	$N = 8, T = 250 \ ^{\circ}C$
	Ag2	silver	tape	0.75 x 2.7	N = 8, T = 250 °C
Diffusion? EDS analysis	(a) 10 8 6 6 8 2 2 2	$SS MgB_2$ $= SS MgB_2$ $= SS MgB_2$ $= SS1$ $= SS1$ $= SS1$ $= SS1$ $= SS2$ $= Mg$ $= Fe$	(b) 100 + ** 500 + ** 100 + **	i MgB_2 (• • • • • • • • • • • • • • • • • • •	Ag MgB_2 Ag AgB_2 Ag AgB_2 Ag AgB_2 Ag $Ag2$ Ag $Ag2$ Ag $Ag2$ Ag $Ag2$ Ag Ag Ag $Ag2$ Ag Ag Ag
M.T. Malac	hevsky	et al IEEE Tra	ins. on Appl.	Superc.19	9 (2009) 2730-2734.

Composite sheaths microstructure



Effects of SiC doping



Intragranular critical currents in **bulk** samples

- Presence of Mg(B,O)₂ precipitates: X.Z. Liao et al APL 92, 351(2002)
- Samples sintered with different parameters



Atrition milling: reducing initial particle and crystallite size





Molido con circonia

Molido con acero inoxidable

Molido con carburo de tungsteno

Powder	D [nm]	ε _g x 10 ⁻³	T _c [K]
Ζ	27	0.6	38.4
SS	27	1.10	38.3
WC	17	4.25	38.2

D = tamaño de grano $\varepsilon_g = microdeformación (dislocaciones)$ Tc = temperatura crítica

Results

Wires preparation:

✓ MgB2 milled with WC balls
✓ Sheath materials
✓ Intermediate treatments
✓ Final annealing

XRD Characterization:

 ✓ Rietveld analysis
 ✓ Presence of MgO: crystal size ~7-8 nm



Sample	a (Å)	c (Å)	Strain XRD	Cristal Size XRD (nm)	R-Bragg
Powder	3.087	3.524	62	115	3.36
SS	3.086	3.523	70	91	2.38
SST1	3.083	3.526	45	58	3.4
CuT1	3.085	3.526	44	76	2.95



SEM of wires cross sections

a) Cooper
b) Titanium
c) Stainless Steel 316L
d) Stainless Steel 316L (MgB2 + SiC)



Superconducting properties: T_c

- Slightly below 38 suggests strain [A. Serquis et al Appl. Phys. Lett. 79, 4399 (2001)]



Superconducting properties: J_c

As-made wires

Intermediate treatments: 500°C
for Cu and Ti and 550°C for SS
Slightly difference for samples
before final heat treatment (even for Cu)





Wires after the final annealing

Final annealing at 800°C during one hour under Ar atmosphere
Particular improvement for SS: Matching field for defects?

Superconducting properties: J_c

Matching field

♦ Vortex distance = 1,075 (ϕ_0 /B)^1/2

a (2T) ~ 35 nm, a (3T) ~ 29 nm,

Sample	Tc [K]	Jc (5K, 3T) [A/cm ²]	J₀ (20K, 3T) [A/cm ²]
Cu	37.8	0.49	0.054
Ti	37.8	0.38	0.044
SS	37.8	0.51	0.074
SSSiC	37.3	0.58	0.081
CuT1	37.9	0.31	
TiT1	37.9	0.38	0.047
SST1	37.5	1.15 x 10^4	0.151



Wires after the final annealing

Final annealing at 800°C during one hour under Ar atmosphere
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TEM : before final TT





Initial MgB2 after milling

MgB2 + SiC / SS



TEM: after final TT



TEM: after final TT

MgB2 / SS + TT



Vortex distance = 1,075 (φ₀/B)^1/2
a (2T) ~ 35 nm, a (3T) ~ 29 nm,

Mg(B, O)2 ?



Conclusions

PIT with different sheath materials and appropriated intermediate thermal treatment (SS, Cu, Ti)

 ✓ Final treatment at 800 C is detrimental for Cu but beneficial for SS

Possible presence of Mg(B,O)₂ precipitates with a density that corresponds to a matching field between 2 and 3 T

Work in progress

11th European Conference on Applied Superconductivity

September 15-19 2013 - Genova, Italy

 \checkmark



- ✓ Transport measurements
- ✓ Current transfer length
 - New MgB₂ powder preparation method from boron mineral



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QUESTIONS?

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