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## Experiment Hall High Load Target Refrigeration Recovery at the ESR

P. Knudsen, V. Ganni, E. Yuksek, J. Creel  
*Thomas Jefferson National Accelerator Facility  
Newport News, Virginia*

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# Introduction

- **JLab has three experiment halls to which beam is delivered**
  - » Halls A, B, C
- **Cryogenic loads for these halls are supported by the End Station Refrigerator (ESR)**
- **Loads are:**
  - » 4.5-K magnet refrigeration
  - » Magnet lead cooling (4.5-K liquefaction)
  - » Cryogenic target; typically 13.5 K 12 atm supply and 20-22 K 2.5 atm return (for a hydrogen target)
- **ESR comprised of:**
  - » 1500 W cold box – built by CTI/Helix in mid-1970's – has LN pre-cooling & two Sultzter turbines (20-13 K, and JT expander)
  - » 250 Hp 1<sup>st</sup> stage & 1000 Hp 2<sup>nd</sup> stage Sullair compressors
  - » 10,000 liter liquid helium (LHe) dewar
  - » Associated distribution system (valve box, hall distribution cans)





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# Introduction

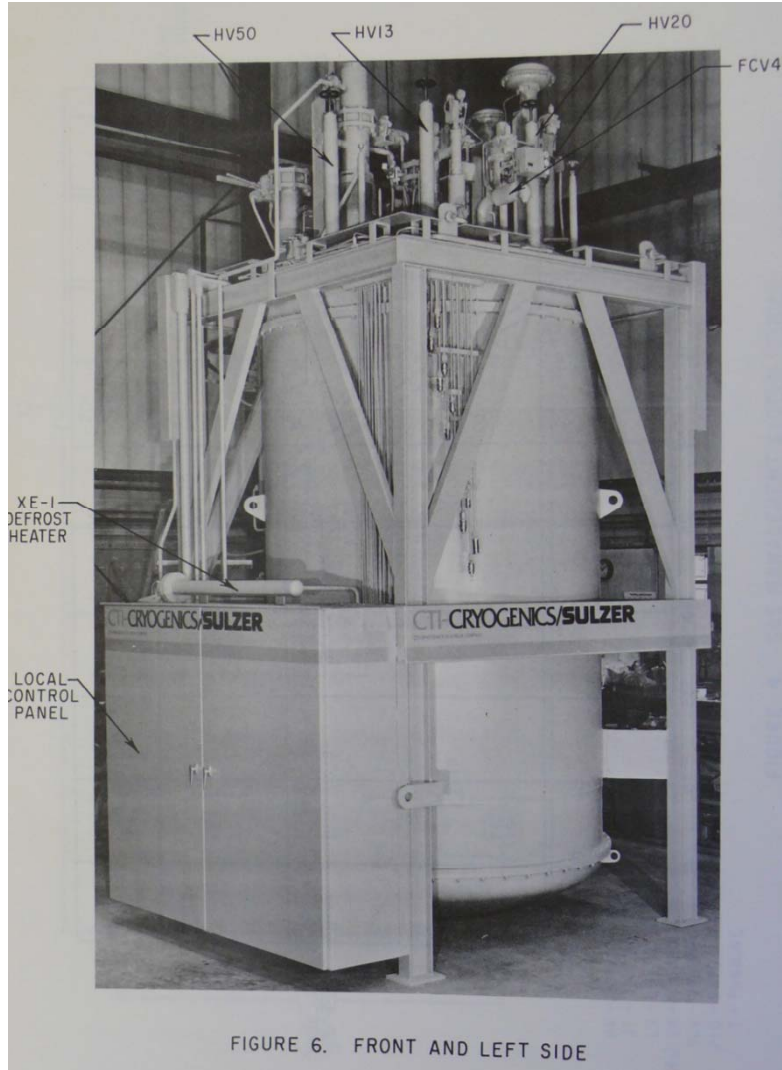
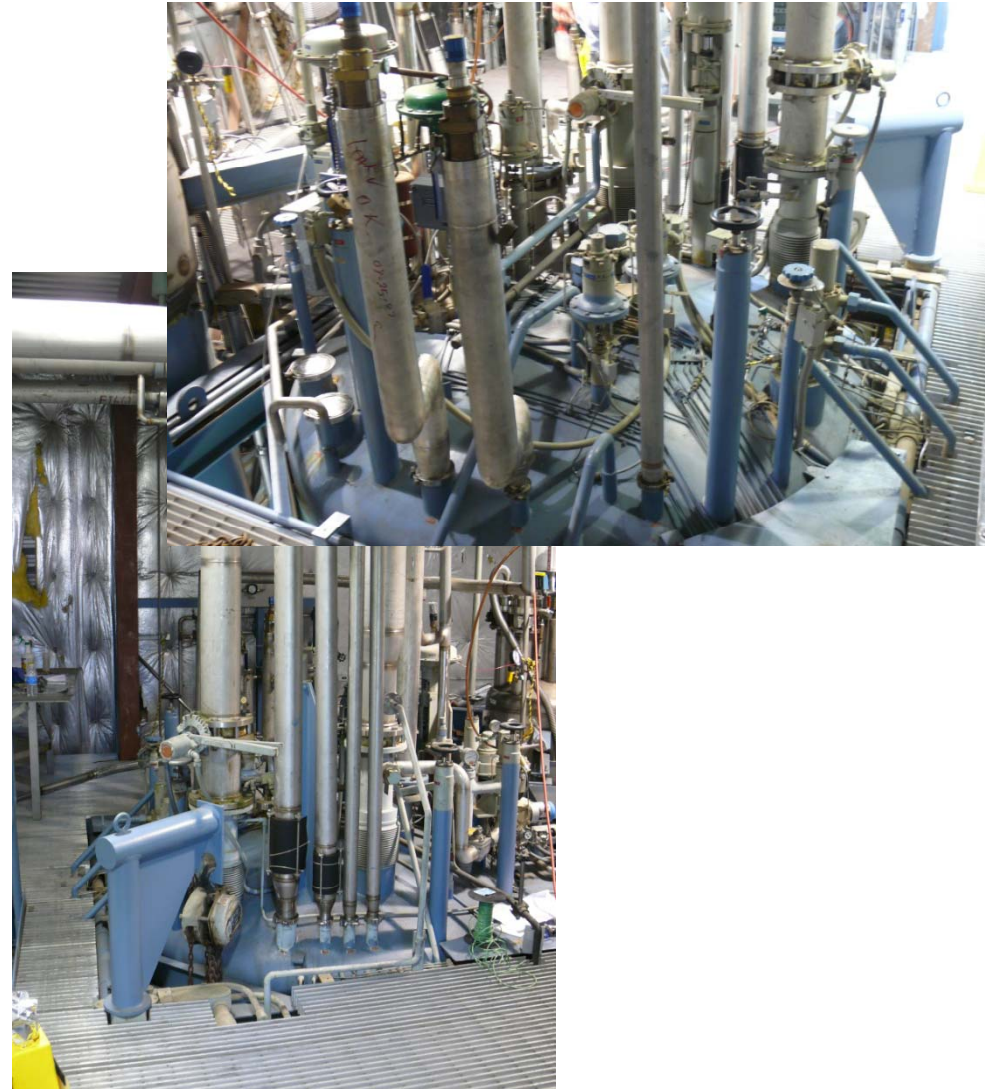


FIGURE 6. FRONT AND LEFT SIDE



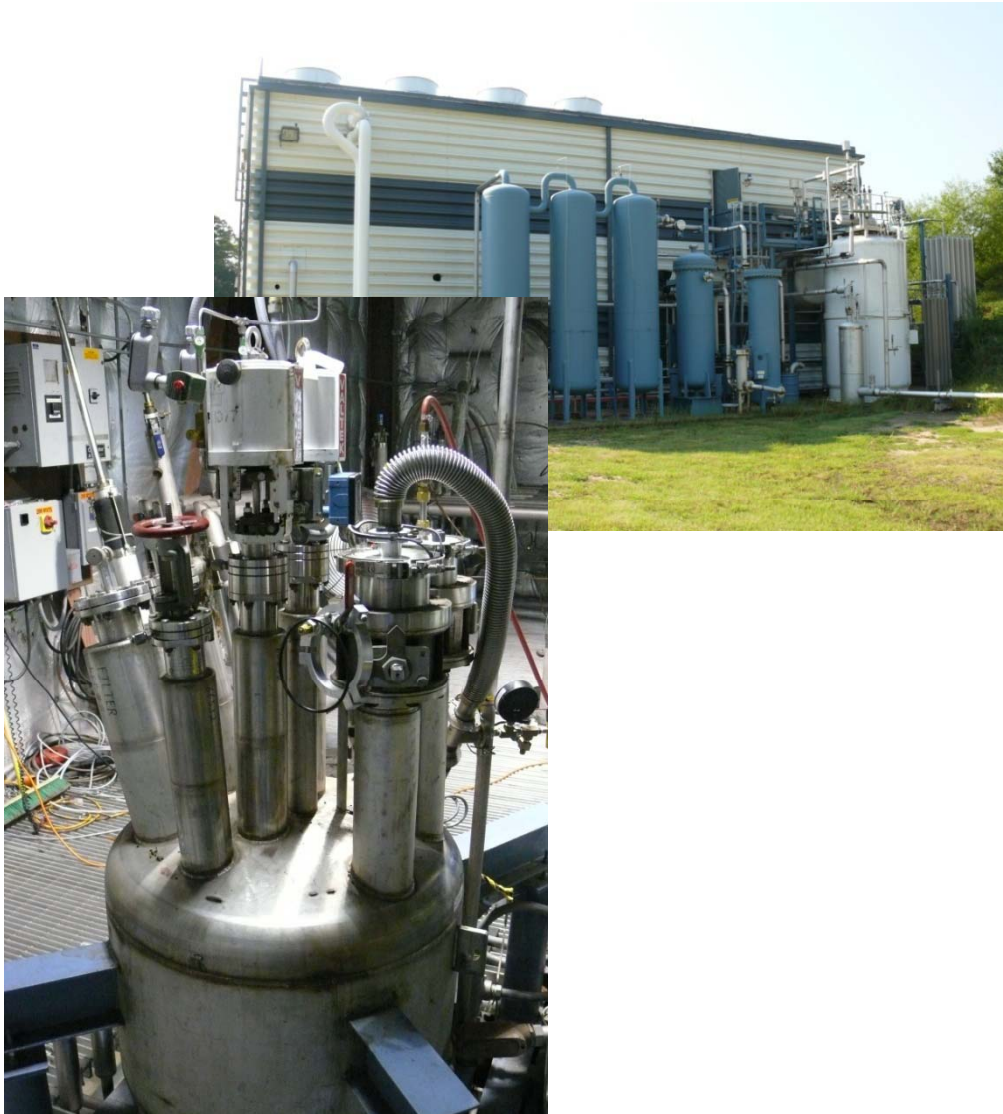
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# Introduction

- **ESR does not have the following systems; i.e., it depends on the Central Helium Liquefier (CHL) system for:**
  - » Warm gas purification system
  - » Gas storage system
  - » LN storage
- **CHL – ESR interconnections**
  - » 1100 ft. cryogenic transfer-line supplying LN and 4.5-K (nominal) LHe
  - » High pressure (HP) clean gas supply
  - » Low pressure (LP) clean and 'dirty' gas return
- **ESR capacity:**
  - » 1100 W 4.5-K refrigeration + 1250 W 15-K (non-isothermal) target load
  - » Present hall loads typically require an additional  $\sim 5$  g/s of 4.5-K (3 atm) LHe from CHL





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# Introduction

- **During summer 2004 – single use, 1.5 week duration, high load target required some low cost modifications to ESR.**
  - » Mods included a large ambient air vaporizer
  - » Load is supported via. CHL transfer-line using 4.5-K 3 atm LHe, and returned at LP to CHL
  - » Since the initial 2 week run, there has been considerable usage of this capability totaling ~58 weeks
- **In fall of 2004,**
  - » Was apparent that usage of high power target capability would not only continue, but increase, and
  - » Need for further modifications to support Qweak experiment in mid-2009 – requiring an even higher target load (for two year run)
  - » Proposed concept and rough cost estimate for modifications to more efficiently support high load targets and provide for Qweak requirements

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# Concept

- **Proposed concept**
  - » Recover 7-20 K LP target return to cool slip stream from HP ESR compressor discharge, which is then injected at the first turbine temperature level in the cold box
- **For large 20-K targets ( $\sim 2.5$  kW or  $\sim 25$  g/s from CHL) and Qweak experiment using two target HX's (4.5-K He, 15-K He)**
  - » Reduce 4.5-K 3 atm CHL supply by  $\sim 50\%$ , allowing either
    - CHL to support loads at other locations (i.e., increased flexibility) or,
    - A reduction in CHL input electrical power of  $\sim 100$  kW ( $\sim \$4.2\text{K/month}$ ) w/ corresponding increase in reliability
  - » Reduce LN usage
    - $\sim 3.3$  gph of LN per 1 g/s of 4.5-K He from CHL
    - $\sim 20$  gph at ESR (i.e., a reduction of  $\sim 50\%$ )
    - Total of  $\sim 60$  gph (at 12 g/s reduction from CHL) is  $\sim \$10\text{K/month}$

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# Concept

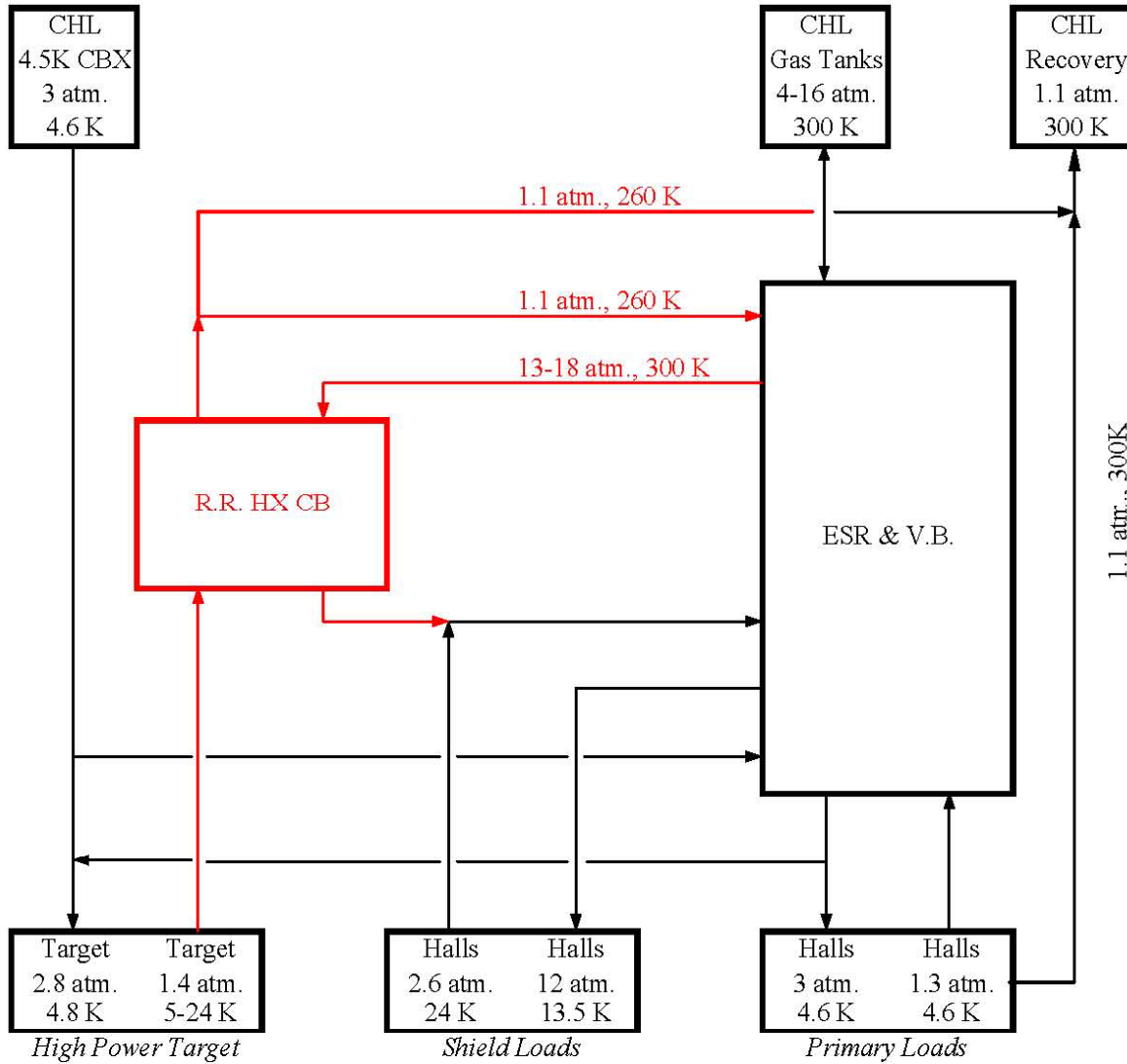
- **For large 4.5-K targets (~500 W)**
  - » Reduce CHL 4.5-K supply LHe by ~20% (i.e., ~5 g/s of LHe)
  - » Reduce LN usage – same as for large 20-K targets
  - » Total of ~35 gph (at 5 g/s reduction from CHL) is ~\$6K/month
- **Rough cost estimate for new hardware (in 2005)**
  - » \$75K
  - » ~6 months of large 20-K target ops for pay-back
  - » One year from funding to initial operation if HX purchased in advance
  - » Long lead – brazed-Aluminum plate-fin HX
    - ~9-12 months
    - \$30K





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# Concept



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# Concept

- Turbine T1 provides cooling required for HX  $\Delta T$  losses, liquefaction load and target load between 13.5 and 80 K
- Enthalpy between 20 K (for a hydrogen target) and 80 K (since the CBX has LN pre-cooling) otherwise lost in the ambient vaporizer is recovered, freeing T1 refrigeration capacity for the target load
- Target load return at  $\sim 1.2$  atm, but CBX T1 outlet pressure (i.e., MP stream) is at  $\sim 2.7$  atm
- So, use portion of HP compressor discharge (13 to 18 atm) flow to recover refrigeration from target load, then drop to MP stream pressure
- Primary equipment limitations
  - » 2<sup>nd</sup> stage compressor displacement (2905 m<sup>3</sup>/hr,  $\sim 80\%$  volumetric efficiency), and
  - » T1 flow coefficient  $\{w^*T_i^{0.5} / p_i \approx 33.2 \text{ (g/s)-K}^{0.5}/\text{atm}\}$





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# Concept

- **Basis for hydrogen target concept**

- »  $W_{TG}$  - 4.5-K flow req'd from CHL without recovering refrigeration
- »  $W_{TG}^{\circ}$  - 4.5-K flow req'd from CHL, recovering the refrigeration
- » Let,  $\omega = W_{TG}^{\circ} / W_{TG}$
- » Exergy recovered from refrigeration (from 20 to 80 K, that would otherwise be wasted in the ambient vaporizer) = Exergy of additional 20 K target flow from ESR;  $\omega_{\epsilon} \approx 0.66$
- » Enthalpy of refrigeration recovered (from 20 to 80 K) = 20 K target enthalpy from ESR;  $\omega_j \approx 0.33$
- » Actual  $\omega$  will be somewhere in between these two values; so, use average,  $\omega \approx 0.50$





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# Concept

- Qweak target load estimate

## CHL T.L.:

|          |        |
|----------|--------|
| $q_{LK}$ | 75 [W] |
|----------|--------|

*CHL to ESR heat leak*

## ESR 15-K:

|          |        |
|----------|--------|
| $q_{LK}$ | 50 [W] |
|----------|--------|

*15-K supply heat leak*

## Target:

|           |                              |
|-----------|------------------------------|
| $(de/dx)$ | 4.8 [MeV-cm <sup>2</sup> /g] |
| $\rho$    | 72.49 [g/l]                  |
| $\ell$    | 35 [cm]                      |
| $I$       | 180 [ $\mu$ A]               |
| $q_B$     | 2192 [W]                     |

*Beam energy dissipation*

*Target density*

*Target length*

*Beam current*

*Beam power on target*

|            |             |
|------------|-------------|
| $w$        | 1087 [g/s]  |
| $Q$        | 15 [l/s]    |
| $\rho$     | 72.49 [g/l] |
| $\Delta p$ | 0.136 [atm] |
| $\eta_i$   | 40% [-]     |
| $P_p$      | 517 [W]     |

*Target loop (LH<sub>2</sub>) mass flow*

*Target loop (LH<sub>2</sub>) volume flow*

*Fluid (LH<sub>2</sub>) density*

*Pump pressure rise*

*Isentropic pump efficiency*

*Pump (shaft) input power*

## Total Required:

|           |          |
|-----------|----------|
| $q_{tot}$ | 2834 [W] |
|-----------|----------|

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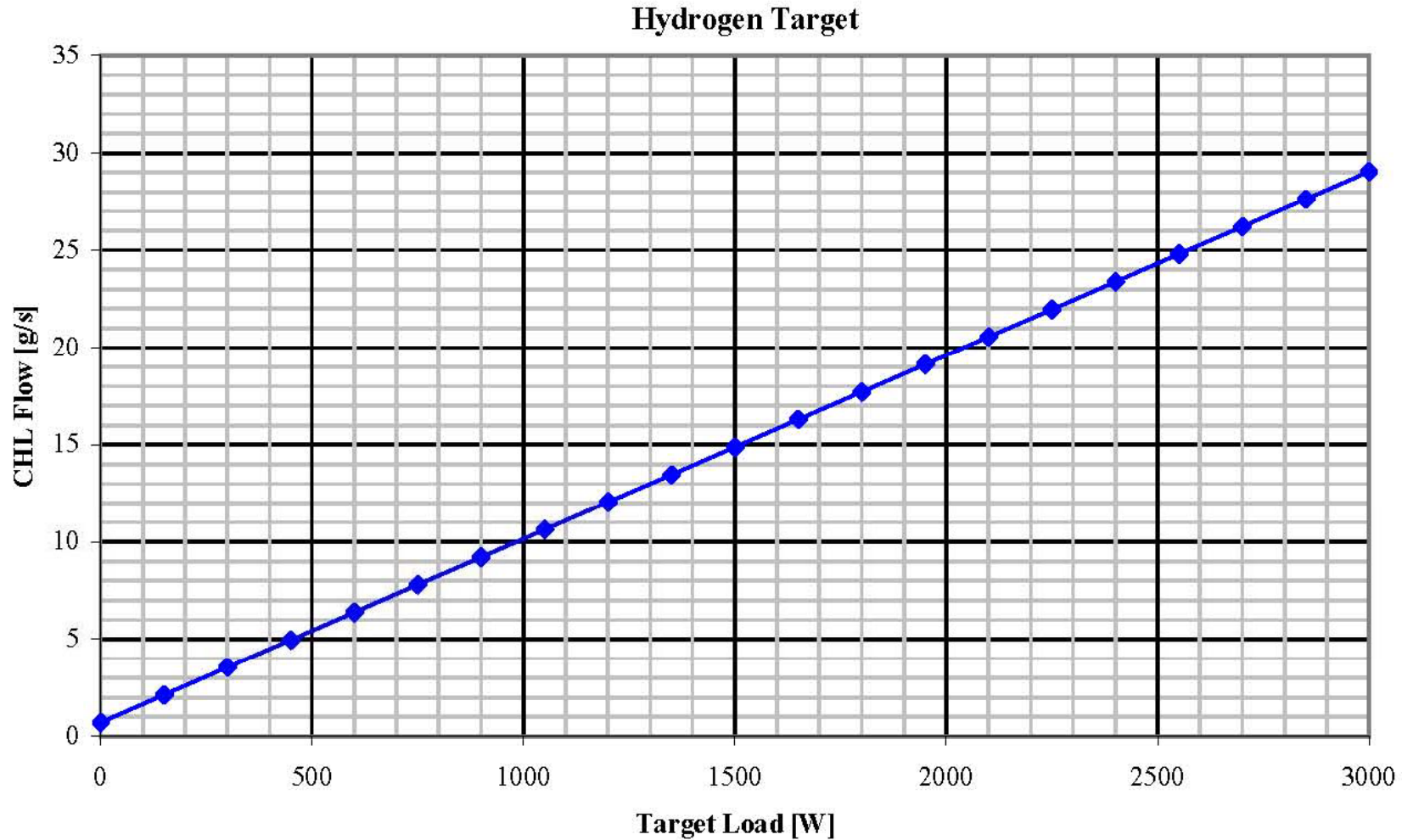




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# Concept

## (General) Hydrogen target load



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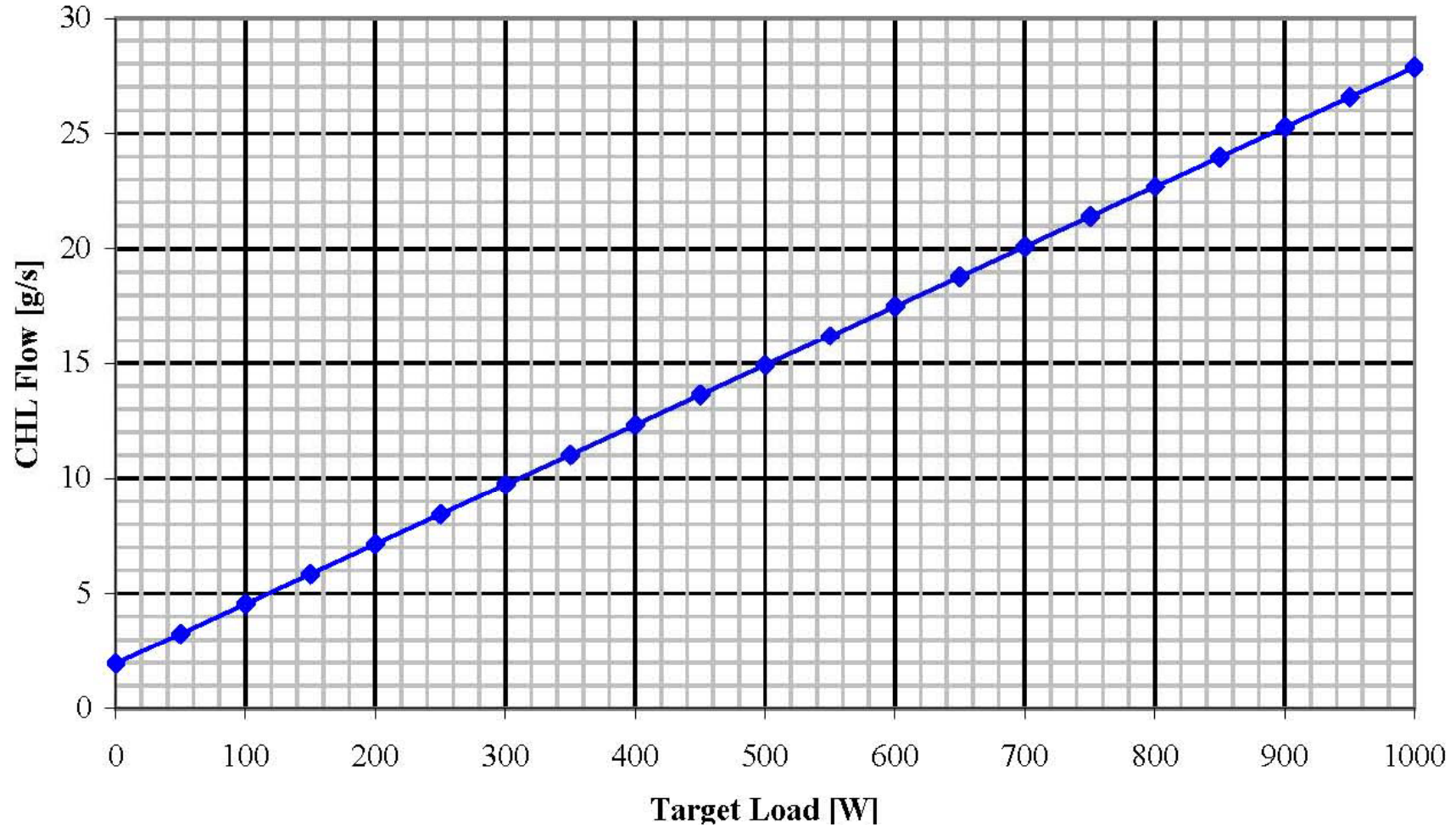


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# Concept

## (General) Helium target load

Helium Target



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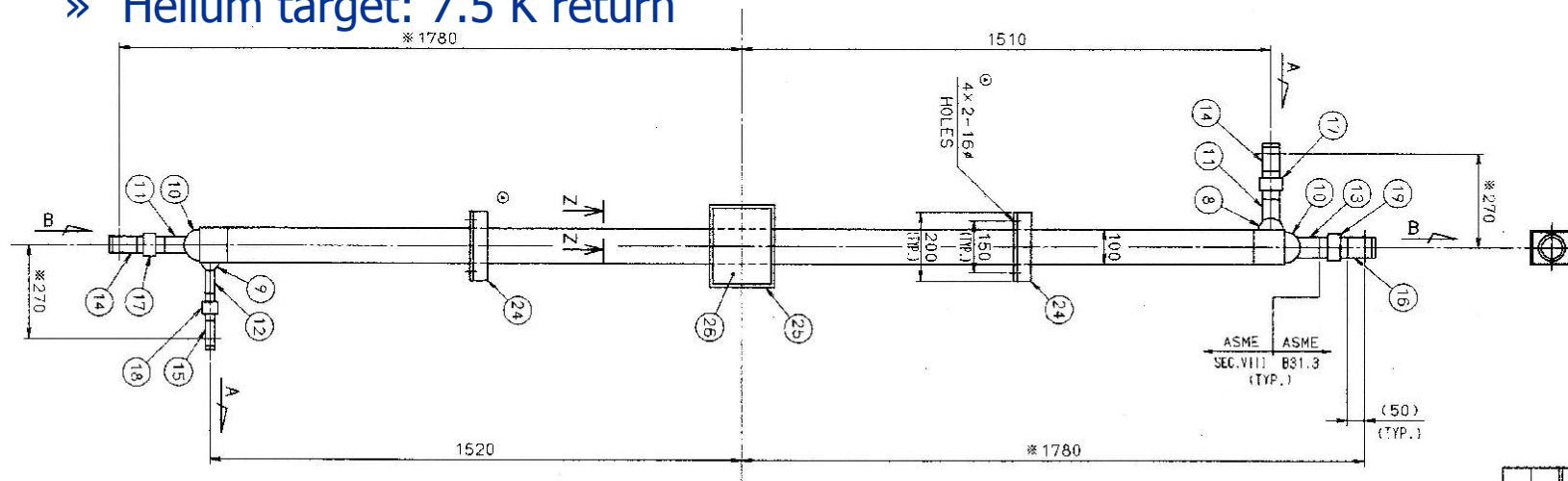




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# Process Study

- HX design
  - » 30 g/s of target return flow (max.)
  - » Approx. 90% flow ratio
  - » 98.5% effectiveness
  - » Approx. 25 Ntu's (3 m long)
  - » HP stream: 14 atm, .02 atm  $\Delta p$
  - » LP stream: 1.2 atm, .04 atm  $\Delta p$
  - » Hydrogen target: 20 K return
  - » Helium target: 7.5 K return



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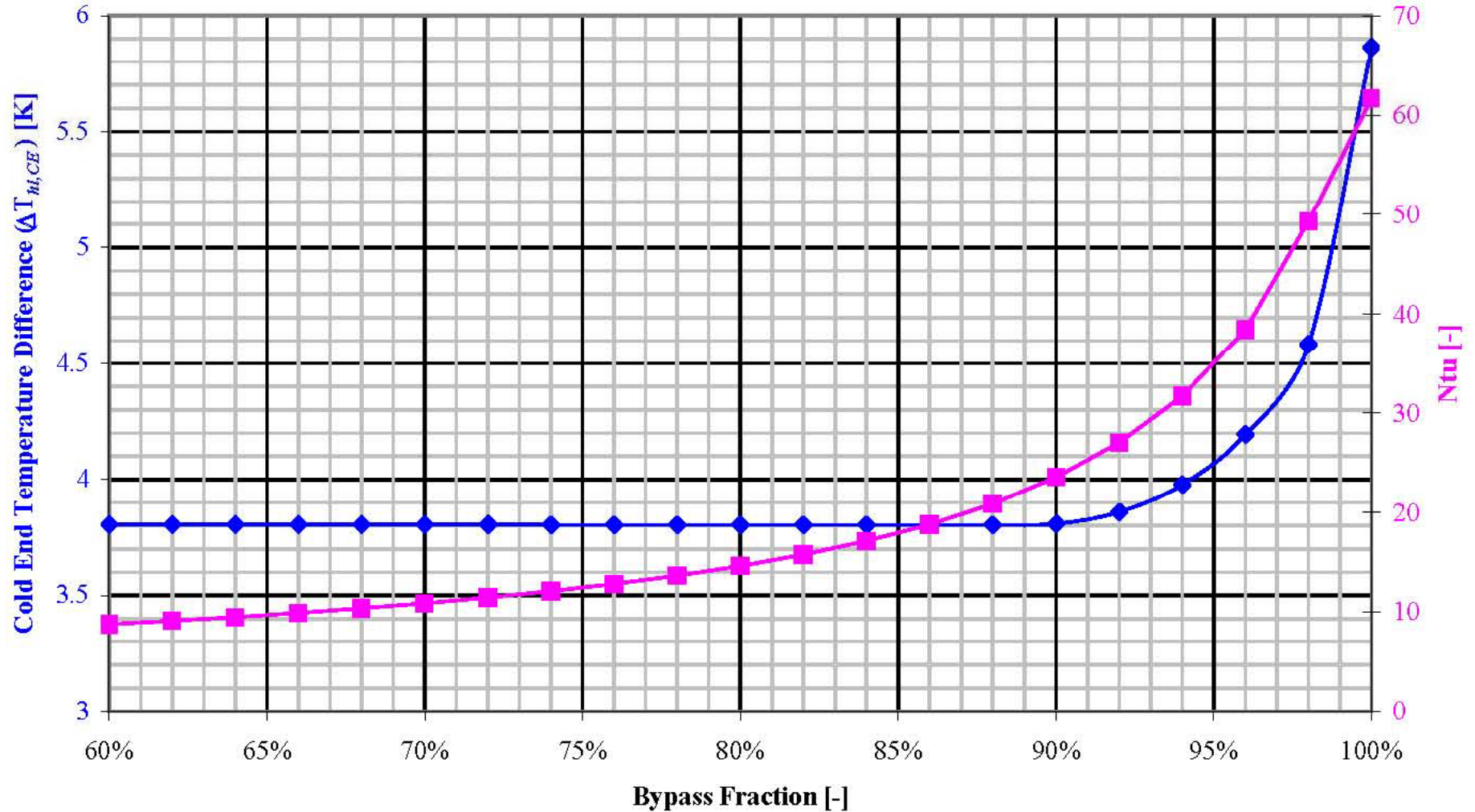




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# Process Study

## HX Design: Hydrogen Target



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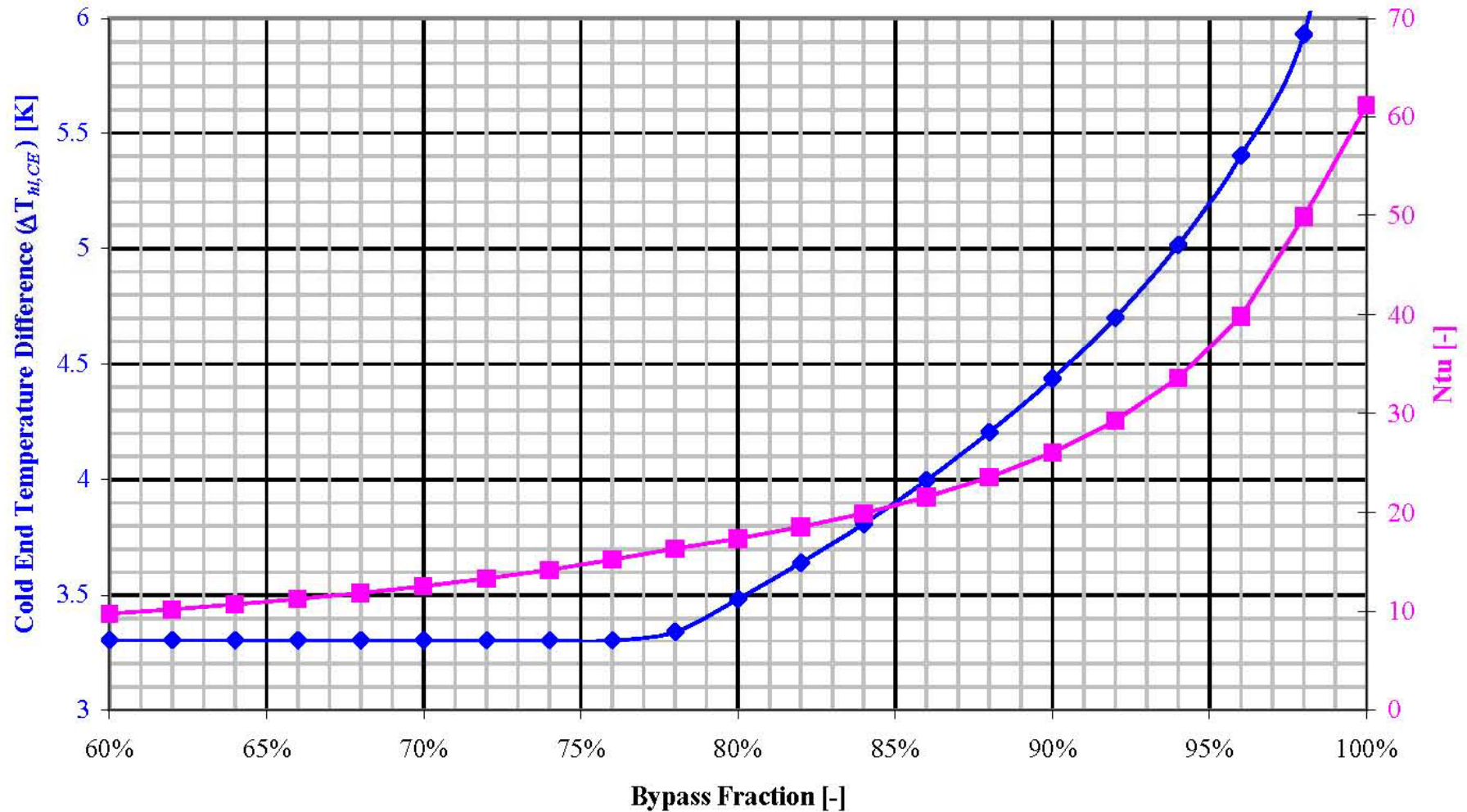




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# Process Study

## HX Design: Helium Target



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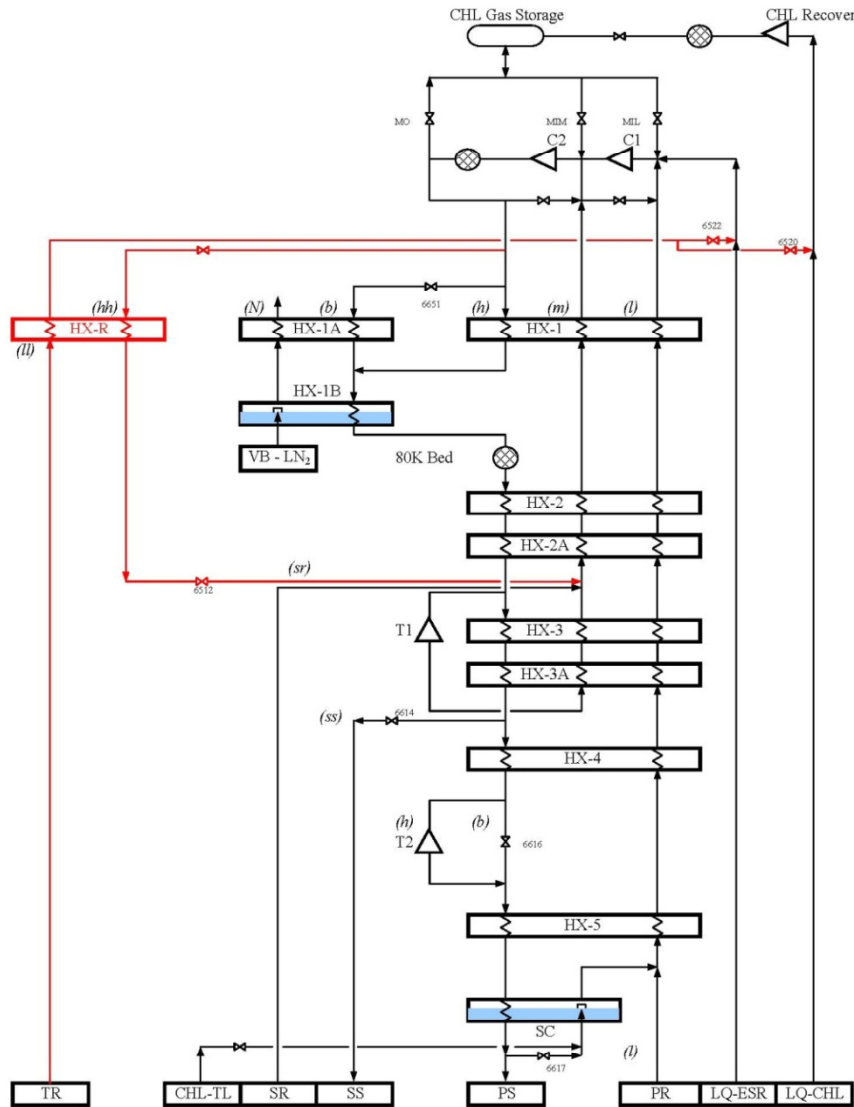




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# Process Study

- Detailed process study was performed to verify the performance suggested by the concept and ascertain the behavior at less than full load conditions



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# Process Study

| Case # | 4.5-K Target Flow [g/s] | CHL Supplied Target Load [kW] | ESR Supplied Target Load [kW] | Total Target Load [kW] | ESR LN Req'd Flow [g/s] | R.R. HX Flow Ratio [-] | Limiting Component |
|--------|-------------------------|-------------------------------|-------------------------------|------------------------|-------------------------|------------------------|--------------------|
| 1      | 0                       | 0.00                          | 0.41                          | 0.41                   | 26.8                    | N/A                    | T1                 |
| 2      | 2                       | 0.20                          | 0.84                          | 1.04                   | 24.7                    | 89.3%                  | T1                 |
| 3      | 5                       | 0.50                          | 1.30                          | 1.81                   | 20.7                    | 87.9%                  | T1                 |
| 4      | 7.5                     | 0.76                          | 1.64                          | 2.40                   | 17.5                    | 86.6%                  | T1                 |
| 5      | 10                      | 1.01                          | 1.89                          | 2.90                   | 14.0                    | 85.6%                  | C2                 |
| 6      | 12.5                    | 1.26                          | 1.97                          | 3.23                   | 9.8                     | 84.6%                  | C2                 |
| 7      | 15                      | 1.51                          | 2.00                          | 3.51                   | 5.8                     | 83.6%                  | C2                 |
| 8      | 17                      | 1.71                          | 2.02                          | 3.73                   | 2.6                     | 83.2%                  | C2                 |
| 9      | 18                      | 1.81                          | 2.03                          | 3.84                   | 1.1                     | 82.9%                  | C2                 |
| 10     | 19                      | 1.91                          | 2.04                          | 3.95                   | 0.0                     | 82.6%                  | C2                 |
| 11     | 20                      | 2.01                          | 2.05                          | 4.06                   | 0.0                     | 82.3%                  | C2                 |

- Notes:
1. Nominal ESR load of 1 kW 4.5-K refrigeration + 4 g/s 4.5-K liquefaction.
  2. Assumed 20 K target return temperature

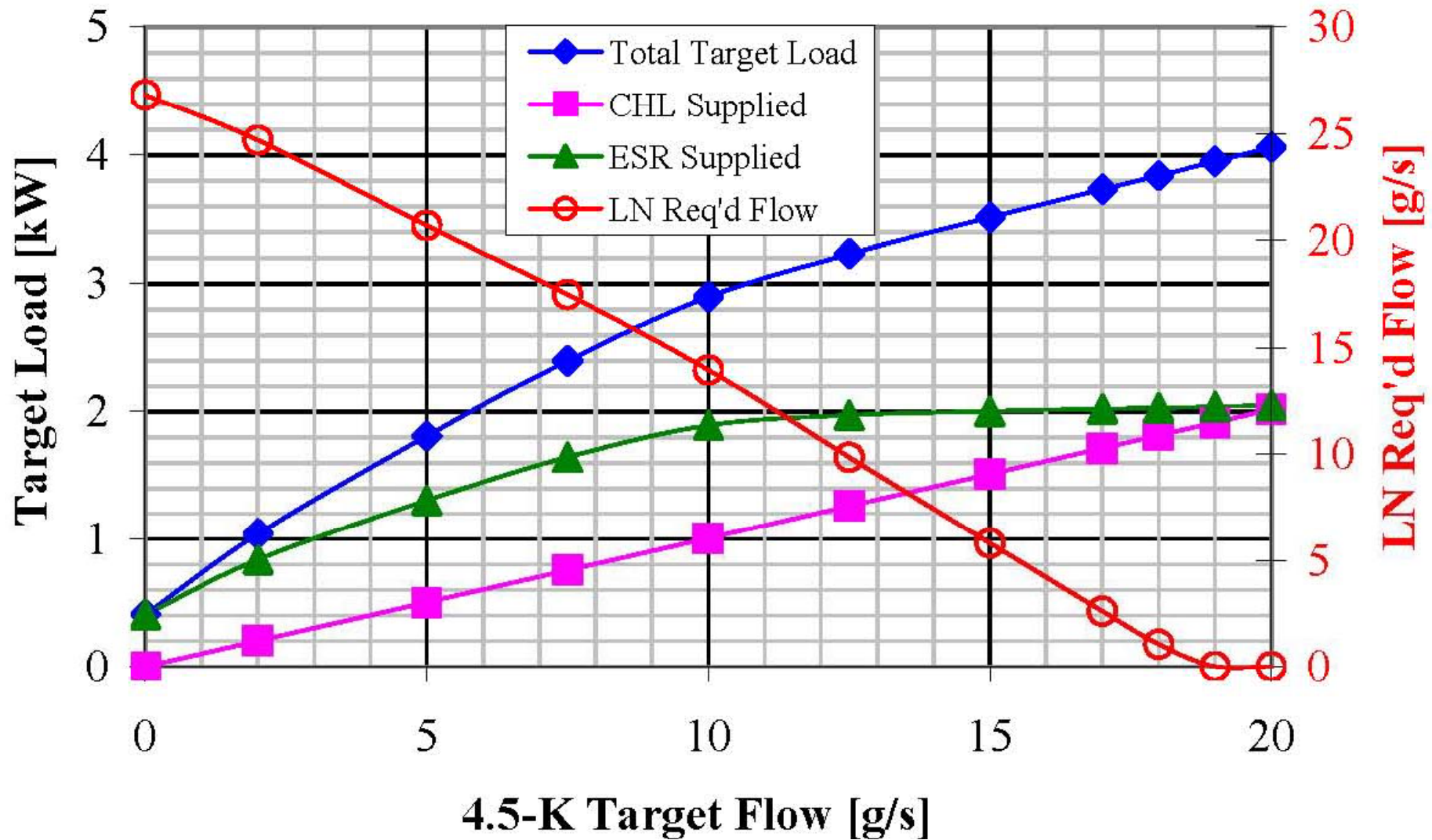
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# Process Study



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# Process Study

- **Results indicate that to support a 3 kW target load (i.e.,  $Q_{weak}$ ):**
  - » CHL supplied flow = 10.5 g/s (64% reduction from 29 g/s)
  - » LN req'd flow = 13.2 g/s (61% total reduction)
  - » HX flow ratio (HP to LP) = 85.4%
- **For a 2 kW target load (of the kind typical since 2004):**
  - » CHL supplied flow = 5.8 g/s (70% reduction from 19.6 g/s)
  - » LN req'd flow = 19.7 g/s (68% total reduction)
  - » HX flow ratio (HP to LP) = 87.5%





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# Mechanical Design

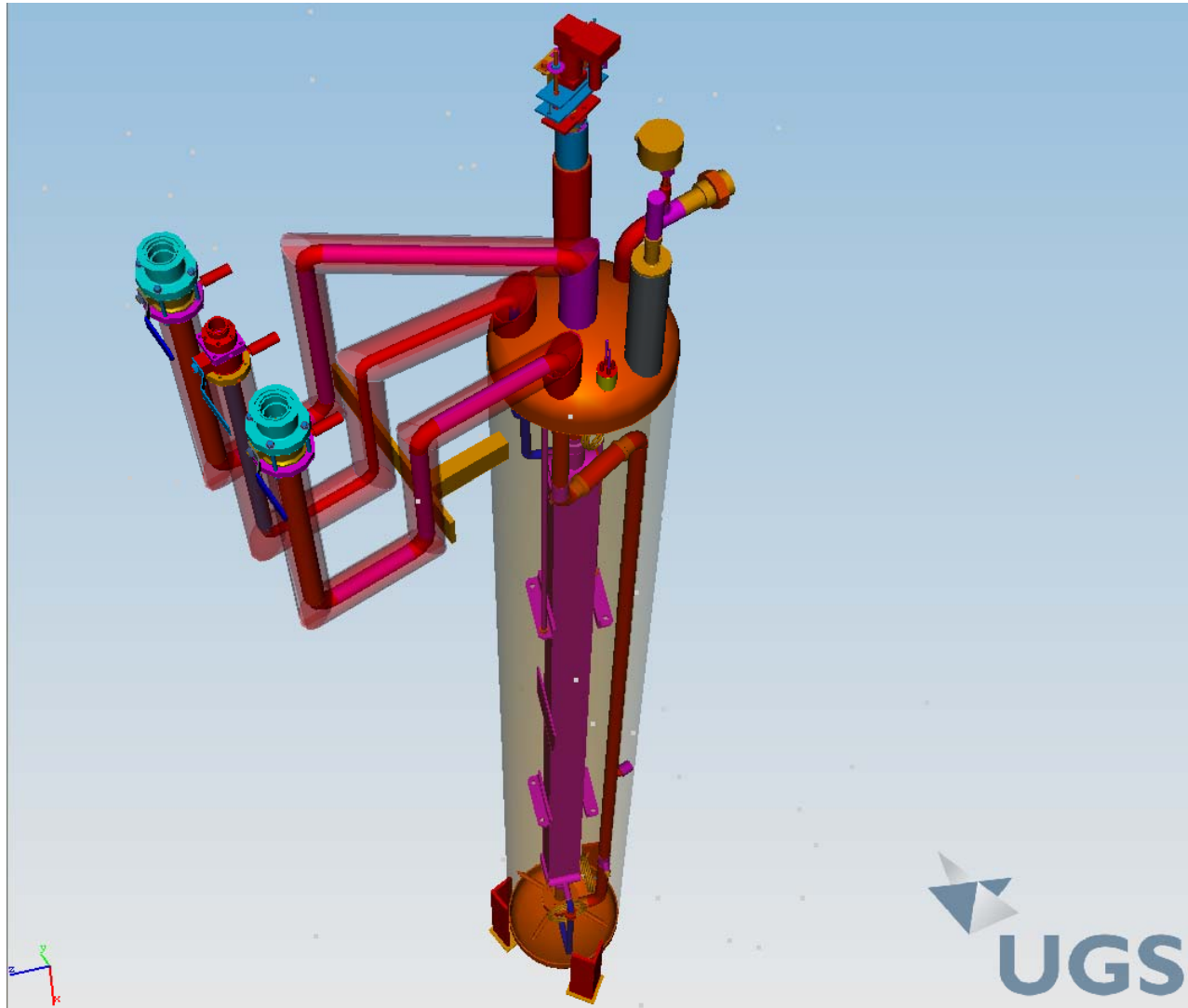
- **Major component – HX 'can'**
  - » Located on west side of ESR building; next to Hall A
  - » (4) process connections
- **Req'd existing system interfaces (5)**
  - » HP warm gas supply
  - » 15-K injection to ESR cold box
  - » LP cold target return from hall
  - » LP warm target return out of HX 'can' to CHL and/or ESR compressor suction





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# Mechanical Design



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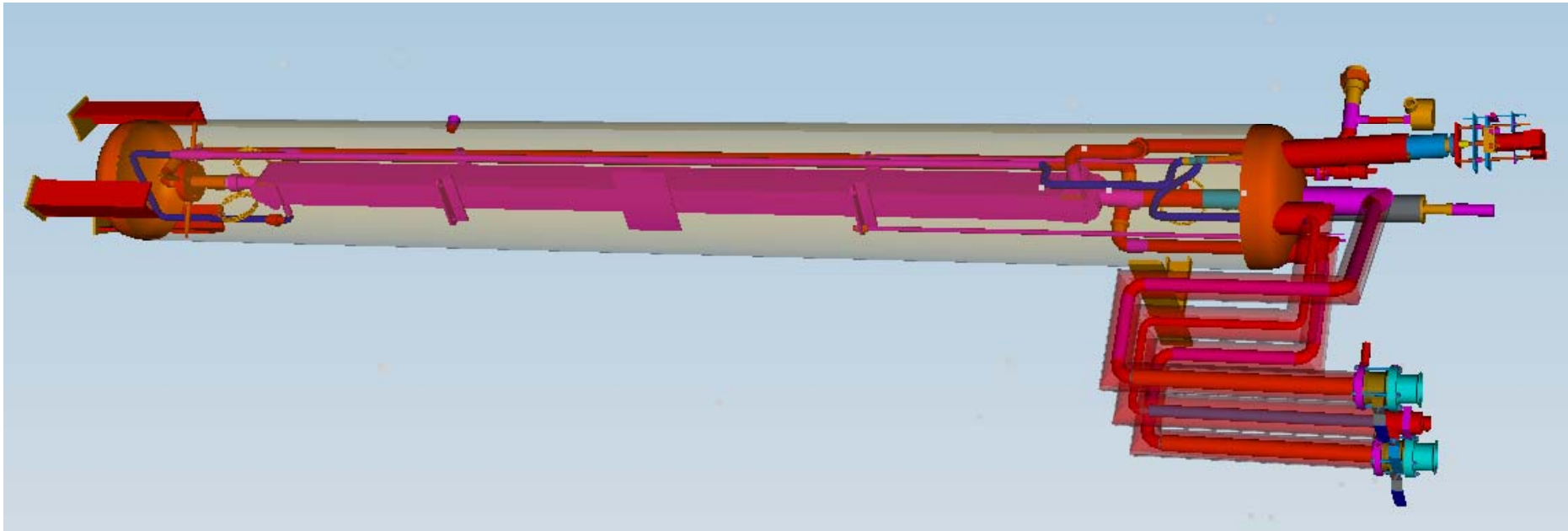






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# Mechanical Design





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# Mechanical Design



New Refrigeration  
Recovery HX 'Can'

*Note: other  
equipment shown  
is existing*

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# Status

- **Major component (\$30 K)**
  - » HX purchased and on-site
- **Mechanical components (\$22 K); i.e., shell/heads, valves, machined parts**
  - » All items either on-order or on-site
- **Piping fittings (\$8 K)**
- **Instrumentation (\$15 K)**
  - » All items either on-order or on-site
- **Design at 90%**
- **Fabrication: 4 months (Oct 2008 – Jan 2009)**
- **Installation: Jan – Feb 2009**
- **Commissioning (for Qweak): March 2009**

