## Scaling Law of Coherent Synchrotron Radiation in a Rectangular Chamber

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### CSR Impedance of Parallel-Plates

An impedance with scaling property is given by

$$\left(\frac{\rho}{h}\right)\left(\frac{Z(n)}{n}\right)_{para} = (2\pi^2)\left(\frac{4\pi}{c}\right)\left[\frac{\hat{k}}{2}\right]^{-4/3} \sum_{p(odd) \ge 1}^{kh/\pi} [Ai'(u)(Ai'(u) - iBi'(u)) + uAi(u)(Ai(u) - iBi(u))]$$

where h is the distance between two plates,  $n=k\rho$ , Ai and Bi are Airy functions, and their argument u is defined as

$$u = \frac{\pi^2 p^2}{2^{2/3}} \hat{k}^{-4/3}$$

Dependence of n is all through

$$\hat{k} = n \frac{h^{3/2}}{\rho^{3/2}}$$

In fact, this scaling property holds for the CSR impedance in free space, formally

$$\left(\frac{\rho}{h}\right)\left(\frac{Z(n)}{n}\right)_{free} = \left(\frac{4\pi}{c}\right)\left(\frac{\Gamma(2/3)}{3^{1/3}}\left(\frac{\sqrt{3}}{2} + \frac{i}{2}\right)\left[n\left(\frac{h}{\rho}\right)^{3/2}\right]^{-2/3}$$

#### Scaling and Asymptotic Properties



The scale defines the strength of impedance and the location of the peak defines where the shielding effects start.

## Threshold of Instability

for CSR of Parallel Metal Plates



Threshold  $\xi^{\text{th}}$  becomes a function of the shielding parameter  $\chi = \sigma_z \rho^{1/2} / h^{3/2}$ . Simulation was carried out by Bane, Cai, and Stupakov, PRSTAB **13**, 104402 (2010). For a long bunch, the coasting beam theory agrees well with the VFP simulation.

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## Summary of the Comparisons

Machine	σ <sub>z</sub> [mm]	Radius ρ [m]	Height h [cm]	χ	<sup>ξth</sup> (theory)	ξ <sup>th</sup> (meas.)
BESSY II	2.6	4.23	5.0	0.48	0.67	0.89
MLS	2.6	1.53	5.0	0.29	0.60	0.39
ANKA	1.0	5.56	3.2	0.42	0.64	0.50
SSRL	1.0	8.14	3.4	0.46	0.66	?
Diamond	0.7	7.13	3.8	0.25	0.17 ?	0.33

We have used

 $\xi^{th}(\chi) = 0.5 + 0.34\chi$ 

where  $\chi = \sigma_z \rho^{1/2} / h^{3/2}$  is the shielding parameter. This simple relation was first obtained by fitting to the result of simulations (Bane, Cai, and Stupakov, PRSTAB **13**, 104402 (2010)).

Since the MLS's shielding parameter is very close to the dip. That may be a reason of its lower threshold.

### Statements of Problem and Solution

- Solve the Maxwell equation with a circulating charge inside a perfect conducting chamber
- Express the longitudinal impedance in terms of Bessel functions
- Approximate Bessel functions with Airy functions under the uniform asymptotic expansion

#### A section of vacuum chamber



For detail read: SLAC-PUB-15875, January 2014

#### CSR Impedance of Rectangular Chamber

An impedance with scaling property is given by

$$\left(\frac{\rho}{h}\right)\left(\frac{Z(n)}{n}\right)_{rect} = (-i2\pi^2)\left(\frac{4\pi}{c}\right)\left[\frac{\hat{k}}{2}\right]^{-4/3}\sum_{p(odd)\geq 1}^{k/\pi}\frac{\hat{s}(u,u^+)\hat{s}(u,u^-)}{\hat{s}(u^+,u^-)} + u\frac{\hat{p}(u,u^+)\hat{p}(u,u^-)}{\hat{p}(u^+,u^-)}\right]$$

where w is the width of chamber and h the height,  $n=k\rho$ , p and s hats are products of Airy functions and their derivatives. Similar to the parallel plates, one of arguments u is

$$u = \frac{\pi^2 p^2}{2^{2/3}} \hat{k}^{-4/3}$$

Dependence of n is all through

$$\hat{k} = n \frac{h^{3/2}}{\rho^{3/2}}$$

In addition, for aspect ratio of A = w/h, the other two arguments are

$$u^{\pm} = \frac{1}{2^{2/3}} (\pi^2 p^2 \hat{k}^{-4/3} \pm A \hat{k}^{2/3})$$

## The Cross Products

of the Bessel functions

of the Airy functions

 $p_{n}(x, y) = J_{n}(x)Y_{n}(y) - Y_{n}(x)J_{n}(y),$   $s_{n}(x, y) = J_{n}'(x)Y_{n}'(y) - Y_{n}'(x)J_{n}'(y)$   $\hat{p}(x, y) = Ai(x)Bi(y) - Bi(x)Ai(y),$  $\hat{s}(x, y) = Ai'(x)Bi'(y) - Bi'(x)Ai'(y)$ 

The uniform asymptotic expansion:

$$J_{n}(n\sqrt{1-x^{2}}) \approx (\frac{2}{n})^{1/3} Ai((\frac{2}{n})^{2/3}x^{2}),$$
  

$$Y_{n}(n\sqrt{1-x^{2}}) \approx -(\frac{2}{n})^{1/3} Bi((\frac{2}{n})^{2/3}x^{2}),$$
  

$$J_{n}'(n\sqrt{1-x^{2}}) \approx -(\frac{2}{n})^{2/3} Ai'((\frac{2}{n})^{2/3}x^{2}),$$
  

$$Y_{n}'(n\sqrt{1-x^{2}}) \approx (\frac{2}{n})^{2/3} Bi'((\frac{2}{n})^{2/3}x^{2}),$$

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#### Scaling Property of Point-Charge Wakefield

The integrated wake can be written as

$$W[\hat{z}] = \frac{\rho}{h^2} \sum_{j} \hat{k}_j \frac{R_s}{Q} (\hat{k}_j) [\theta(-\hat{z}) \cos(\hat{k}_j \hat{z}) - \frac{\operatorname{sgn}(\hat{z})}{2} \exp(-\hat{k}_j |\hat{z}|)]$$

where  $\rho$  is bending radius and h height of chamber. We have defined a dimensionless longitudinal position:

$$\hat{z} = z \rho^{1/2} / h^{3/2}$$

which naturally leads to the shielding parameter

$$\chi = \sigma_z \rho^{1/2} / h^{3/2}$$

if we introduce the normalized coordinate  $q=z/\sigma_z$ .

- An LRC resonance with infinite quality factor
- Decay term is due to the curvature

# Dimensionless $R_s/Q$ (A=1)



Point-Charge Wakefield (A=1)



## Comparisons of Bunch Wake

Agoh, PRSTAB, 12, 094402 (2009)

Stupakov & Kotelnikov, PRSTAB, 12 104401 (2009)



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## Longitudinal Beam Dynamics

Hamiltonian is given as

$$H = \frac{1}{2}(q^2 + p^2) - I_n \int_{-\infty}^{q} dq'' \int_{-\infty}^{\infty} dq' \lambda(q') W(q'' - q')$$

where  $I_n$  is the normalized current introduced by Oide and Yokoya (1990)

$$I_n = \frac{r_e N_b}{2\pi v_s \gamma \sigma_\delta}$$

 $q=z/\sigma_z$ ,  $p=-\delta/\sigma_\delta$  and W(q) is the integrated wake per turn (convention used in Alex Chao's book). The independent variable is  $\theta=\omega_s t$ .

Vlasov-Fokker-Planck equation is written as

$$\frac{\partial \Psi}{\partial \theta} - \{H, \Psi\} = 2\beta \frac{\partial}{\partial p} (p\Psi + \frac{\partial \Psi}{\partial p})$$

where  $\Psi(q,p;\theta)$  is the beam density in the phase space and  $\beta = 1/\omega_s \tau_d$ . A robust numerical solver was developed by Warnock and Ellison (2000).

# Scaling Law of the Threshold

In the normalized coordinate, it can be shown easily

$$I_n W[q] = \xi \chi^{4/3} \sum_j \hat{k}_j \frac{R_s}{Q} (\hat{k}_j) [\theta(-q) \cos(\hat{k}_j \chi q) - \frac{\operatorname{sgn}(q)}{2} \exp(-\hat{k}_j \chi |q|)]$$

where  $\xi = I_n \rho^{1/3} / \sigma_z^{4/3}$  is the dimensionless current and  $\chi = \sigma_z \rho^{1/2} / h^{3/2}$ the shielding parameter. We redefine a dimensionless wake as

$$W_{\xi}[q] = \chi^{4/3} \sum_{j} \hat{k}_{j} \frac{R_{s}}{Q} (\hat{k}_{j}) [\theta(-q) \cos(\hat{k}_{j} \chi q) - \frac{\operatorname{sgn}(q)}{2} \exp(-\hat{k}_{j} \chi |q|)]$$

Clearly, this wake depends on  $\chi$  and aspect ratio A through the values of  $k_j$ Based on the VFP equation. we conclude that the dimensionless current

$$\xi = \xi^{th}(\chi, A, \beta)$$

is a function of other three dimensionless parameters.

# $R_s/Q$ for Rectangular Chamber



Envelopes are very similar, also similar to the real part of Z(n)/n of the parallel model shown previously.

## **VFP** Simulation



A square chamber has a much lower threshold:  $\xi^{th}=1/4$ .

## Mitigation of CSR Effects

Rewrite the threshold in terms of some practical parameters. The beam becomes unstable if

$$I_{b} > \frac{8\pi^{2}\xi^{th}\sigma_{z}^{7/3}(V_{rf}f_{rf})f_{rev}\cos\varphi_{s}}{c^{2}Z_{0}\rho^{1/3}}$$

- Extremely unfavorable scaling in terms of shortening bunch
- Stronger longitudinal focusing is very helpful
- Superconducting RF at higher frequency

#### Shorten the bunch to 1 ps in PEP-X



## Conclusion

- The scaling law found in the parallel-plate mode is extended to the rectangular chamber by adding another parameter: A (aspect ratio of the chamber)
- The threshold of a square chamber is lower by a factor than the one of a rectangular chamber with A > 2
- More effective mean to shorten a bunch to a ps scale is to use superconducting RF at higher frequency

#### Important and Relevant References

- R. Warnock and P. Morton, "Fields Excited by a Beam in a Smooth Toroidal Chamber," SLAC-PUB-5462 March (1988); Also Pat. Accel.
- J. Murphy, S. Krinsky, and R. Gluckstern, "Longitudinal Wakefield for an Electron Moving on a Circular Orbit," Pat. Accel. 57, pp. 9-64 (1997)
- T. Agoh and K. Yokoya, "Calculation of coherent synchrotron radiation using mesh," Phys. Rev. ST Accel. Beams 7, 0544032 (2004)
- T. Agoh, "Steady fields of coherent synchrotron radiation in a rectangular pipe," Phys. Rev. ST Accel. Beams **12**, 094402 (2009)
- G. Stupakov and I. Kotelnikov, "Calculation of coherent synchrotron radiation impedance using mode expansion method," Phys. Rev. ST Accel. Beams **12**, 104401 (2009)
- K. Bane, Y. Cai, and G. Stupakov, "Threshold studies of microwave instability in electron storage rings," Phys. Rev. ST Accel. Beams 13, 104402 (2010)

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### Transverse Impedance

An impedance with scaling property is given by

$$Z^{\perp}(k) = \left(\frac{-i8\pi^2}{h}\right)\left(\frac{4\pi}{c}\right) \sum_{p(even)\geq 2}^{kh/\pi} u\left[\frac{\hat{s}(u,u^+)\hat{s}(u,u^-)}{\hat{s}(u^+,u^-)} + u\frac{\hat{p}(u,u^+)\hat{p}(u,u^-)}{\hat{p}(u^+,u^-)}\right]$$

where w is the width of chamber and h the height,  $n=k\rho$ , p and s hats are products of Airy functions and their derivatives. Similar to the parallel plates, one of arguments u is

$$u = \frac{\pi^2 p^2}{2^{2/3}} \hat{k}^{-4/3}$$

Dependence of n is all through

$$\hat{k} = n \frac{h^{3/2}}{\rho^{3/2}}$$

In addition, for aspect ratio of A = w/h, the other two arguments are

$$u^{\pm} = \frac{1}{2^{2/3}} (\pi^2 p^2 \hat{k}^{-4/3} \pm A \hat{k}^{2/3})$$

#### Transverse Wakefield

The integrated wake can be written as

$$W_{1}[\hat{z}] = \frac{\rho^{1/2}}{h^{5/2}} \sum_{j} \frac{cR_{s}}{Q} (\hat{k}_{j}) [\theta(-\hat{z})\sin(\hat{k}_{j}\hat{z}) + \frac{1}{2}\exp(-\hat{k}_{j}|\hat{z}|)]$$

where  $\rho$  is bending radius and h height of chamber. We have defined a dimensionless longitudinal position:

$$\hat{z} = z \rho^{1/2} / h^{3/2}$$

which naturally leads to the shielding parameter

$$\chi = \sigma_z \rho^{1/2} / h^{3/2}$$

if we introduce the normalized coordinate  $q=z/\sigma_z$ .

- An LRC resonance with infinite quality factor
- Decay term is due to the curvature

# Dimensionless $cR_s/Q$ (A=1)



## Transverse Instability

In the normalized coordinates, Hamiltonian is given by

$$H = \frac{1}{2} \left(\frac{k_{\beta}}{k_{s}}\right) \left(\hat{y}^{2} + \hat{p}_{y}^{2}\right) + \frac{1}{2} \left(q^{2} + p^{2}\right) - \frac{\hat{y}\hat{F}_{y}(q,\theta)}{E_{0}k_{\beta}k_{s}},$$

where the force is written as

$$\frac{\hat{F}_{y}}{E_{0}} = -\frac{r_{e}N}{\gamma} \int_{-\infty}^{\infty} dq' \lambda(q') \hat{D}(q') (\frac{W_{1}(q-q')}{2\pi\rho})$$

If we define a dimensionless current

$$I = (\frac{r_e N}{\gamma})(\frac{1}{h^{5/2}\rho^{1/2}})(\frac{1}{k_{\beta}k_s})$$

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we derive a scaling law

$$I = I^{th}(\chi, A, \frac{k_{\beta}}{k_s})$$