

Joint Universities Accelerator School

JUAS 2014

Archamps, France, 17th – 21st February 2014

Normal-conducting accelerator magnets

Thomas Zickler,

CERN



Scope of the lectures



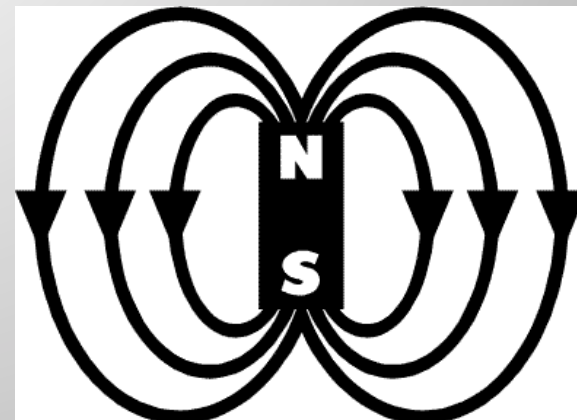
Overview of electro-magnetic technology as used in particle accelerators considering *normal-conducting, iron-dominated* electro-magnets (generally restricted to direct current situations)

Main goal is to:

- create a fundamental understanding in accelerator magnet technology
- provide a guide book with practical instructions how to start with the design of a standard accelerator magnet
- focus on applied and practical design aspects using 'real' examples
- introduce finite element codes for practical magnet design
- present an outlook into as aspects related to magnet production, testing and measurements

Not covered:

- permanent magnet technology
- super-conducting technology





Lecture 1: Basic principles

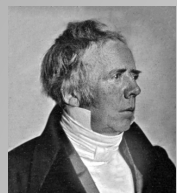


- A bit of history...
- Why do we need magnets?
- Magnet technologies
- Basic principles and concepts
- Magnet types and applications





A bit of history...



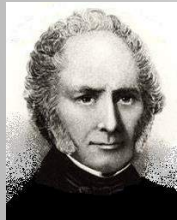
1820: **Hans Christian Oersted** (1777-1851)
finds that electric current affects a
compass needle



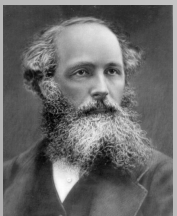
1820: **Andre Marie Ampere** (1775-1836) in
Paris finds that wires carrying current
produce forces on each other



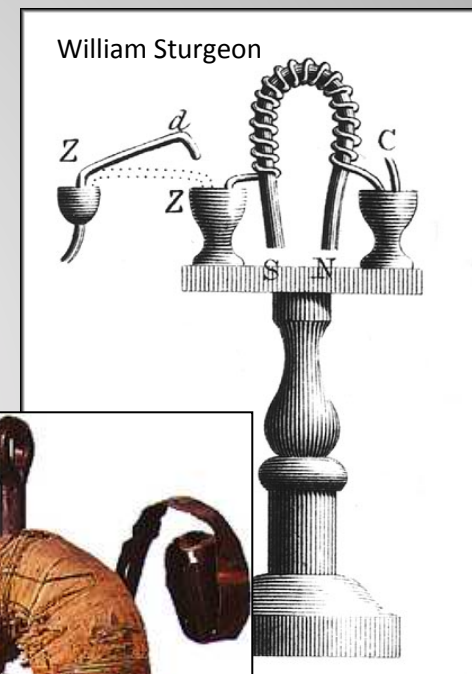
1820: **Michael Faraday** (1791-1867) at
Royal Society in London develops the
idea of electric fields and studies the
effect of currents on magnets and
magnets inducing electric currents



1825: British electrician, **William Sturgeon**
(1783-1850) invented the first
electromagnet



1860: **James Clerk Maxwell** (1831-1879), a
Scottish physicist and mathematician,
puts the theory of electromagnetism on
mathematical basis



Joseph Henry

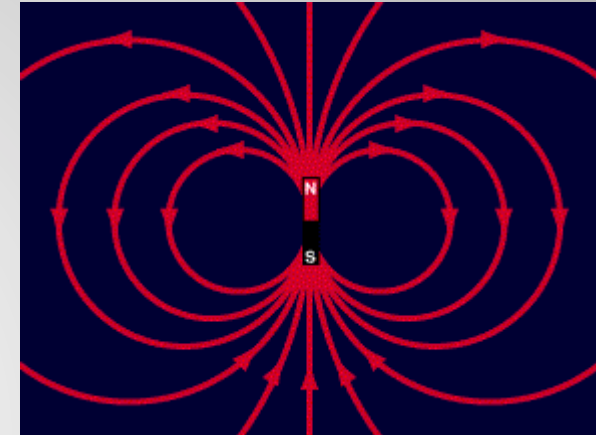


Magnetic units



IEEE defines the following units:

- **Magnetic field:**
 - H (vector) [A/m]
 - the magnetizing force produced by electric currents
- **Electromotive force:**
 - e.m.f. or U [V or $(\text{kg m}^2)/(\text{A s}^3)$]
 - here: voltage generated by a time varying magnetic field
- **Magnetic flux density or magnetic induction:**
 - B (vector) [T or $\text{kg}/(\text{A s}^2)$]
 - the density of magnetic flux driven through a medium by the magnetic field
 - Note: induction is frequently referred to as "Magnetic Field"
 - H , B and μ relates by: $B = \mu H$
- **Permeability:**
 - $\mu = \mu_0 \mu_r$
 - permeability of free space $\mu_0 = 4 \pi 10^{-7}$ [V s/A m]
 - relative permeability μ_r (dimensionless): $\mu_{\text{air}} = 1$; $\mu_{\text{iron}} > 1000$ (not saturated)
- **Magnetic flux:**
 - Φ [Wb or $(\text{kg m}^2)/(\text{A s}^2)$]
 - surface integral of the flux density component perpendicular through a surface





Maxwell's equations

In 1873, [Maxwell](#) published "Treatise on Electricity and Magnetism" in which he summarized the discoveries of Coulomb, Oersted, Ampere, Faraday, et. al. in four mathematical equations:

Gauss' law for electricity:

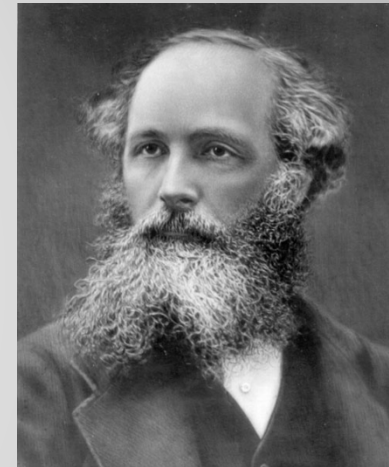
$$\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$$

$$\oint_{\partial V} \vec{E} \cdot d\vec{A} = \frac{q}{\epsilon_0}$$

Gauss' law of flux conservation:

$$\nabla \cdot \vec{B} = 0$$

$$\oint_{\partial V} \vec{B} \cdot d\vec{A} = 0$$



Faraday's law of induction:

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\oint_{\partial A} \vec{E} \cdot d\vec{s} = -\frac{d\Phi}{dt} = -\frac{d}{dt} \int_A \vec{B} \cdot d\vec{A}$$

Ampere's circuital law:

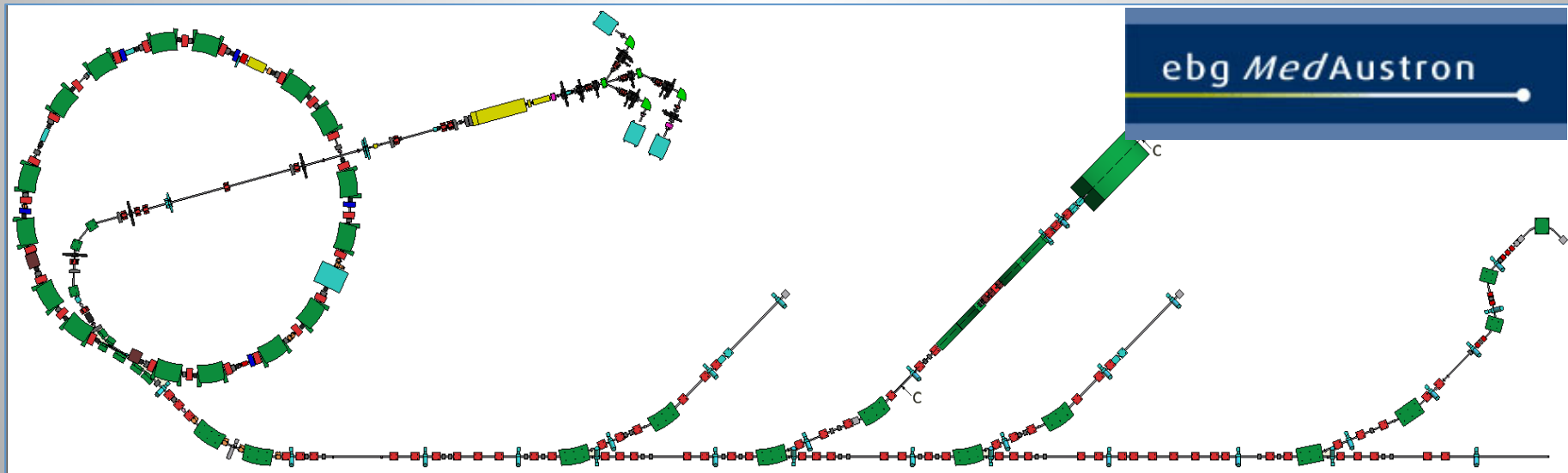
$$\nabla \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

$$\oint_{\partial A} \vec{B} \cdot d\vec{s} = \int_A \mu_0 \vec{J} \cdot d\vec{A} + \frac{d}{dt} \int_A \mu_0 \epsilon_0 \vec{E} \cdot d\vec{A}$$



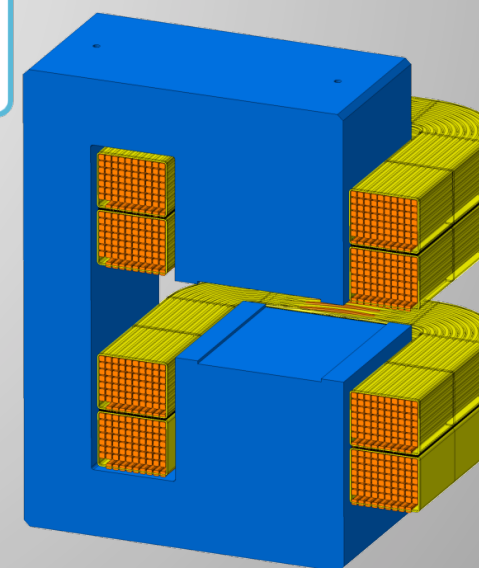
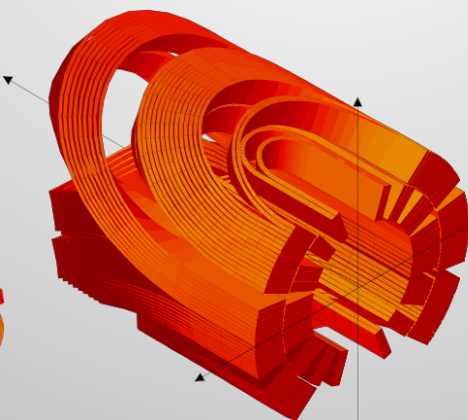
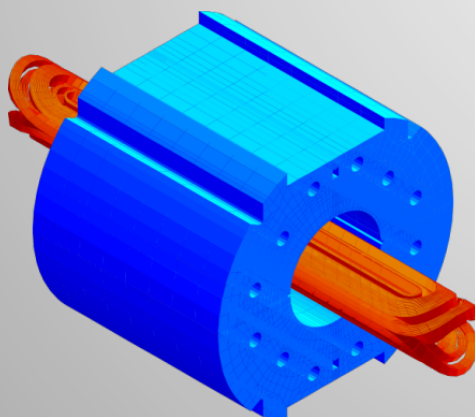
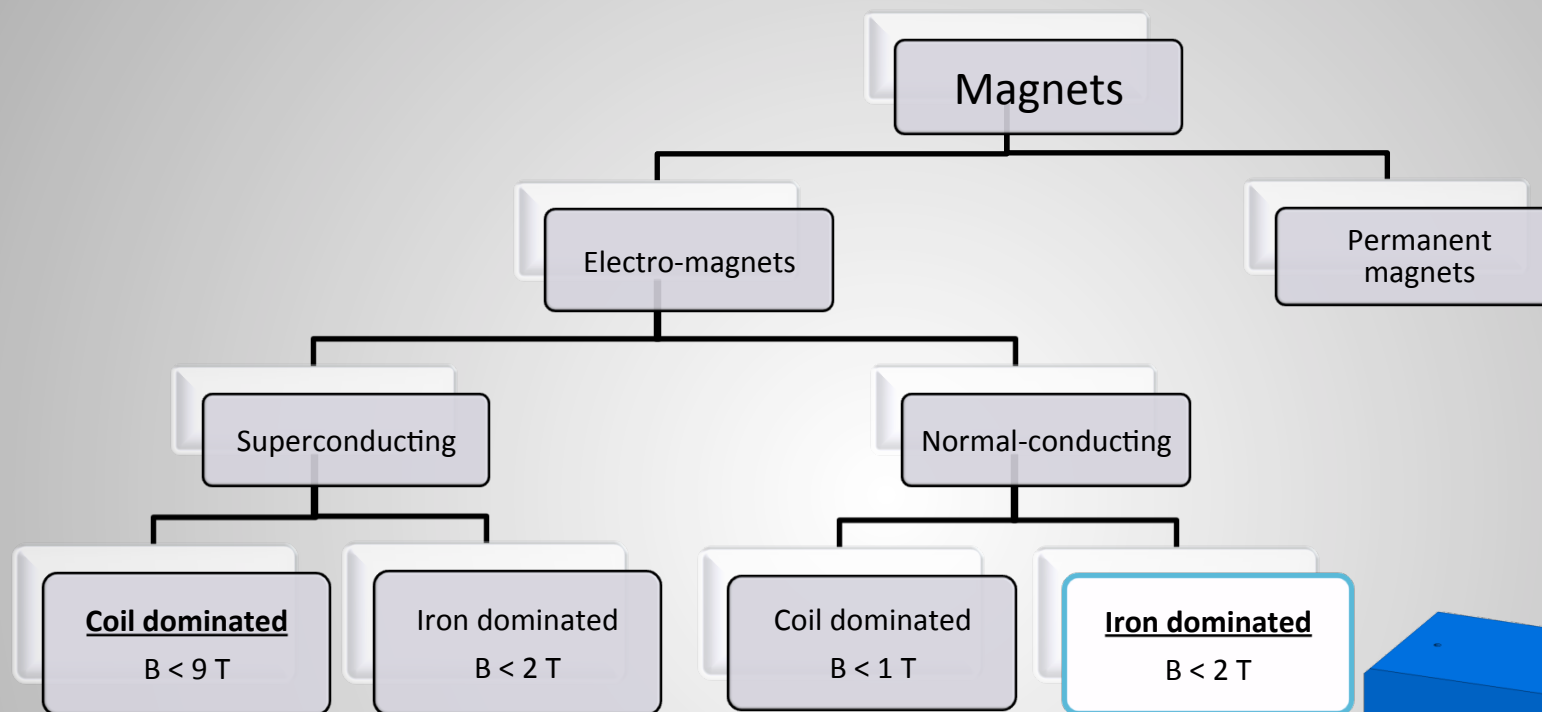
Why do we need magnets?

- Interaction with the beam
 - guide the beam to keep it on the orbit
 - focus and shape the beam
- Lorentz's force: $\vec{F} = q(\vec{E} + \vec{v} \times \vec{B})$
 - for relativistic particles this effect is equivalent if $\vec{E} = c\vec{B}$
 - if $B = 1 \text{ T}$ then $E = 3 \cdot 10^8 \text{ V/m}$





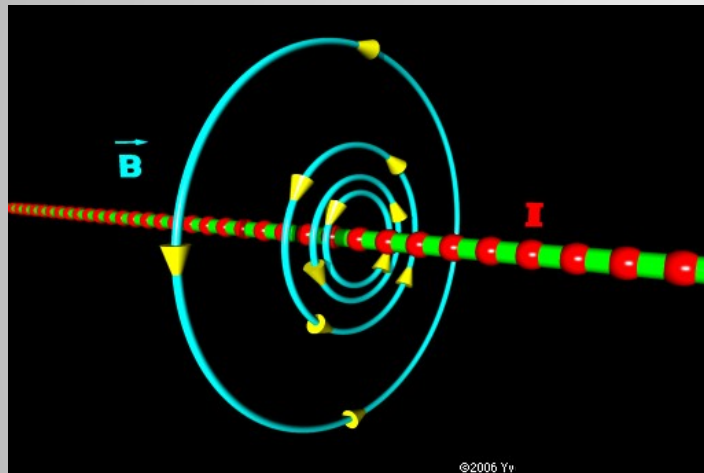
Magnet technologies





How does a magnet work?

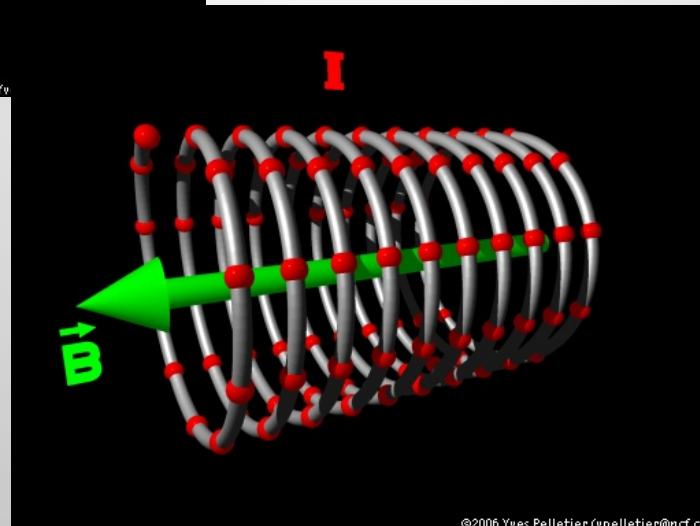
- Permanent magnets provide only constant magnetic fields
- Electro-magnets can provide adjustable magnetic fields



Maxwell & Ampere:

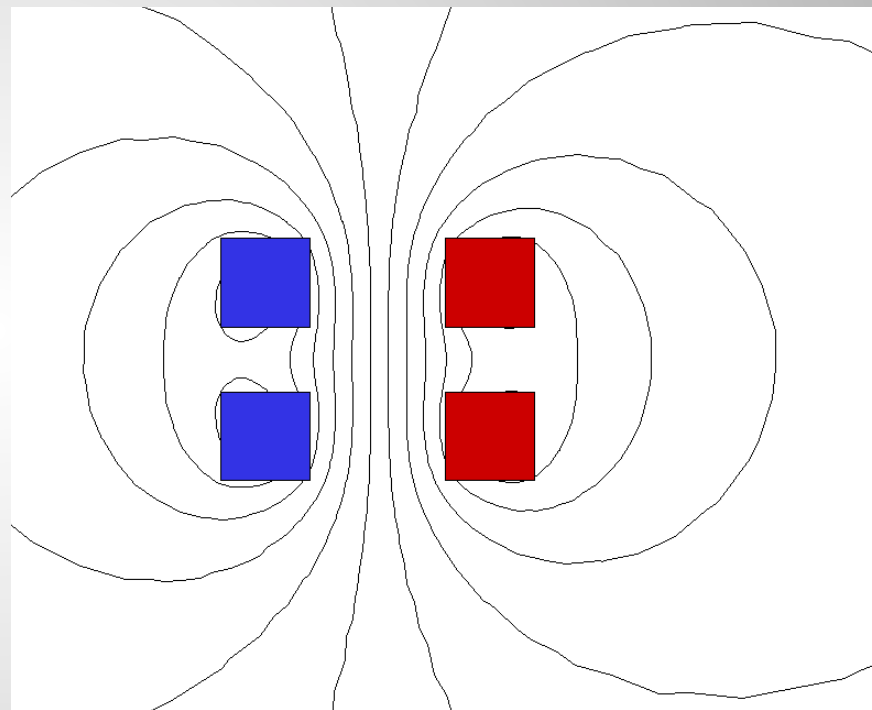
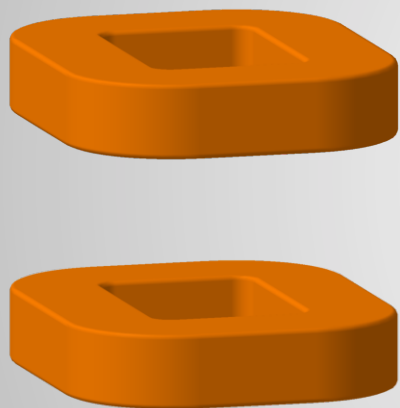
$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

„An electrical current is surrounded by a magnetic field“





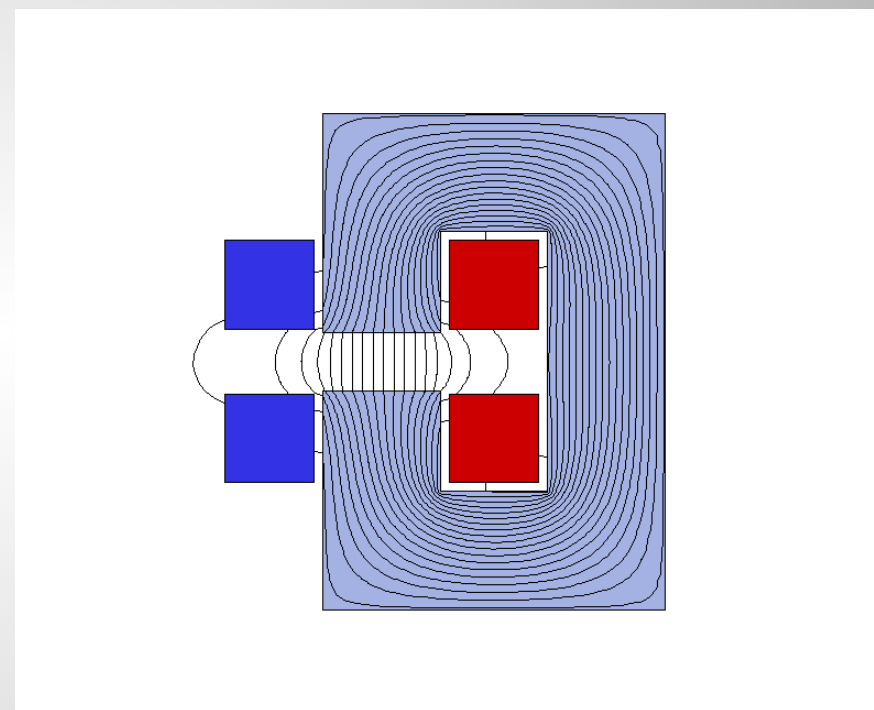
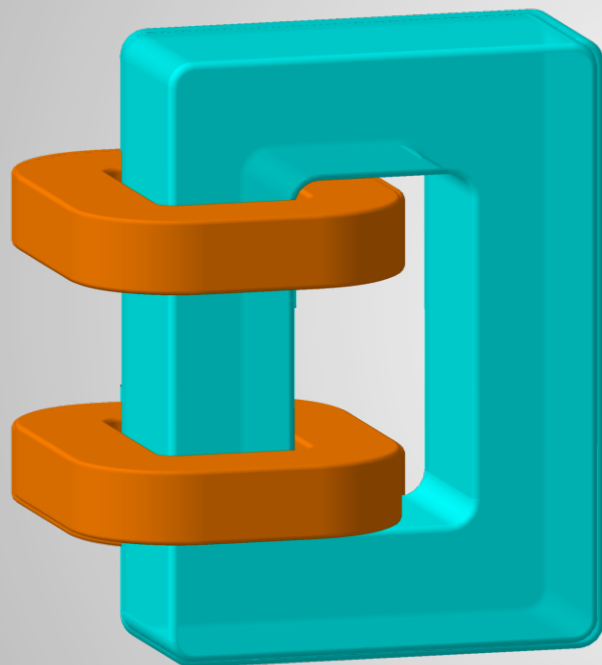
Magnetic circuit



Flux lines represent the magnetic field
Coil colors indicate the current direction



Magnetic circuit



Coils hold the electrical current
Iron holds the magnetic flux



Excitation current in a dipole

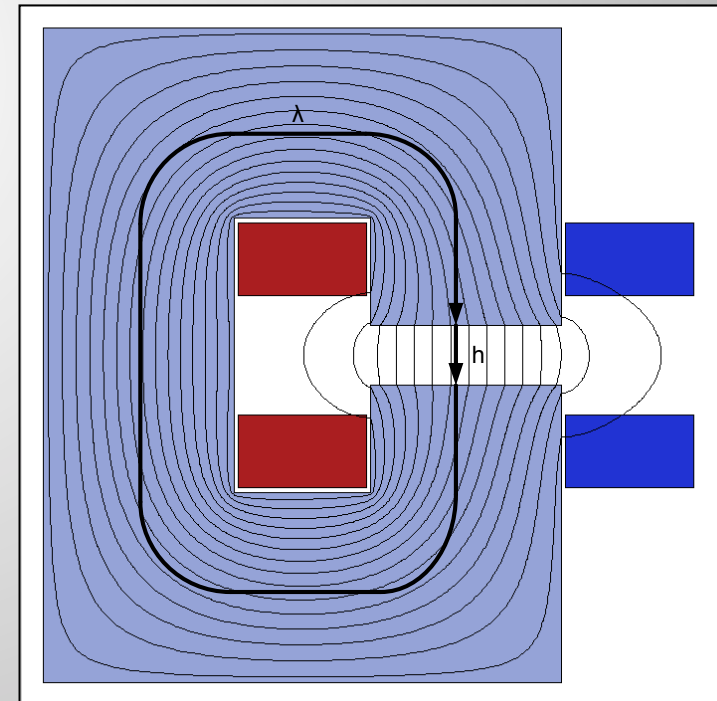
Ampere's law $\oint \vec{H} \cdot d\vec{l} = NI$ and $\vec{B} = \mu \vec{H}$ with $\mu = \mu_0 \mu_r$

leads to
$$NI = \oint \frac{\vec{B}}{\mu} \cdot d\vec{l} = \int_{\text{gap}} \frac{\vec{B}}{\mu_{\text{air}}} \cdot d\vec{l} + \int_{\text{yoke}} \frac{\vec{B}}{\mu_{\text{iron}}} \cdot d\vec{l} = \frac{Bh}{\mu_{\text{air}}} + \frac{B\lambda}{\mu_{\text{iron}}}$$

assuming, that B is constant along the path

If the iron is not saturated:
$$\frac{h}{\mu_{\text{air}}} \gg \frac{\lambda}{\mu_{\text{iron}}}$$

then:
$$NI_{(\text{per pole})} \approx \frac{Bh}{2\mu_0}$$





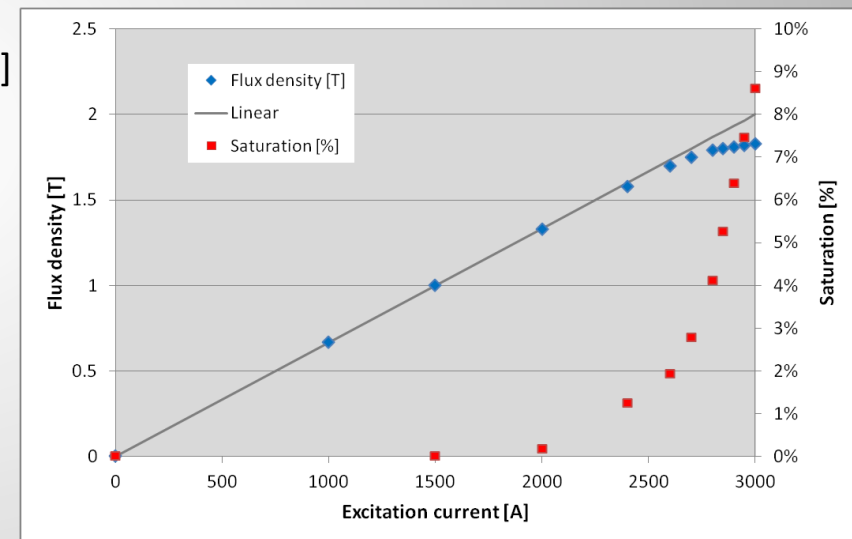
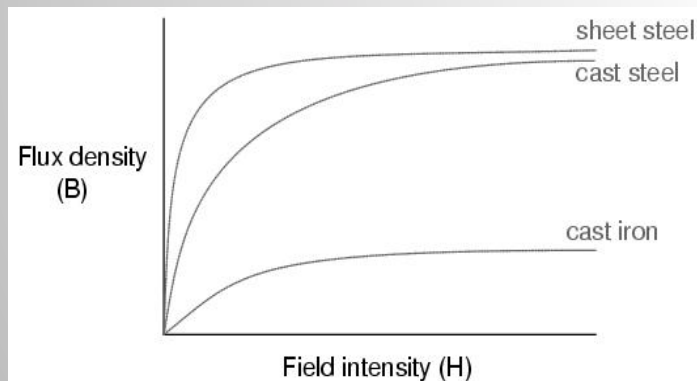
Reluctance and efficiency



Similar to Ohm's law, one can define the 'resistance' of a magnetic circuit, called 'reluctance', as:

- σ : conductivity [S/m]
- NI : magneto-motive force [A]
- Φ : magnetic flux [Wb]
- l_M : flux path length in iron [m]
- A_M : iron cross section perpendicular to flux [m²]

$$R_E = \frac{U}{I} = \frac{l_E}{A_E \sigma} \quad \longrightarrow \quad R_M = \frac{NI}{\Phi} = \frac{l_M}{A_M \mu_r \mu_0}$$

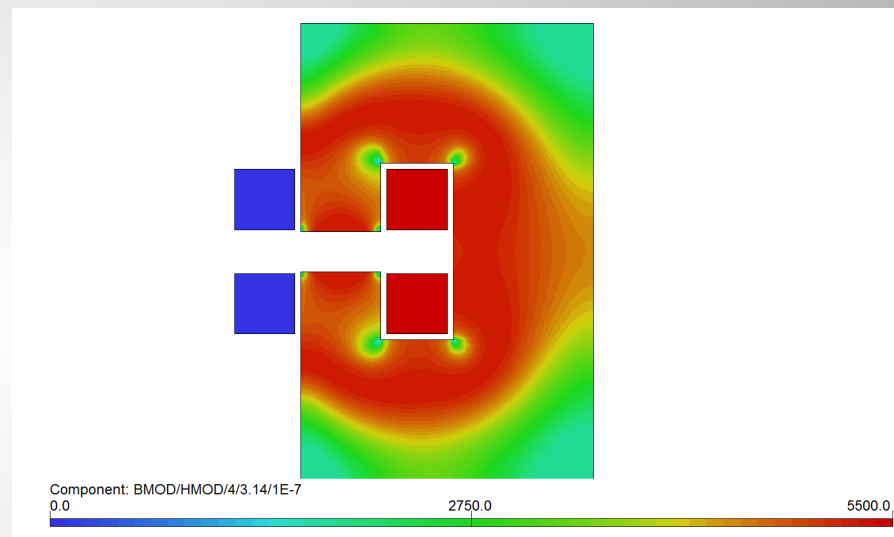
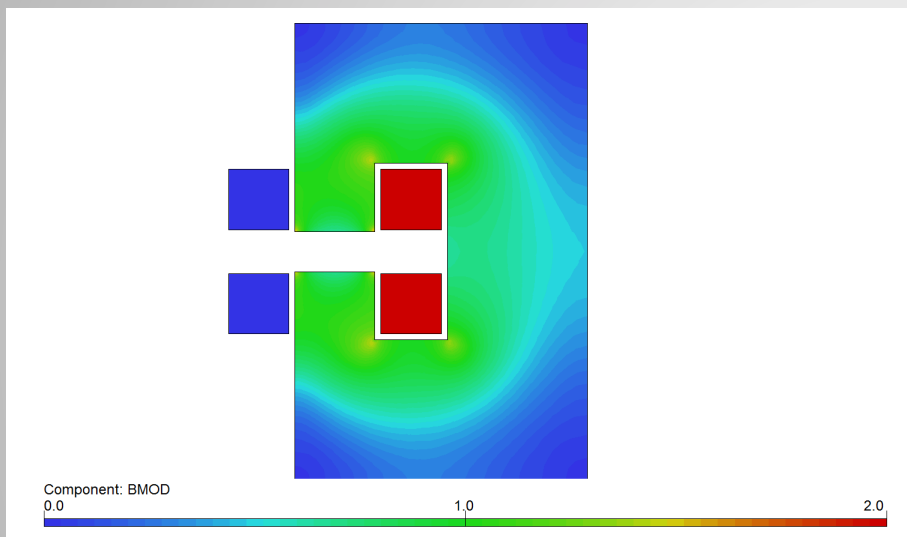


- Increase of B above 1.5 T in iron requires non-proportional increase of H
- Iron saturation (small μ_{iron}) leads to inefficiencies





Iron saturation



Keep yoke reluctance small by providing sufficient iron cross-section!



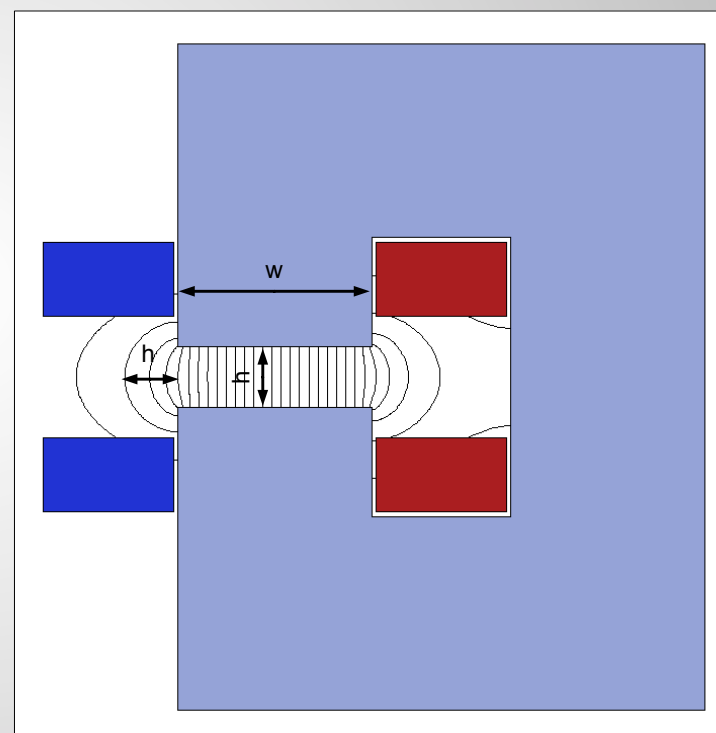
Magnetic flux



Flux in the yoke includes the gap flux and stray flux

Total flux in the return yoke:

$$\Phi = \int_A B \cdot dA \approx B_{gap} (w + 2h) l_{mag}$$

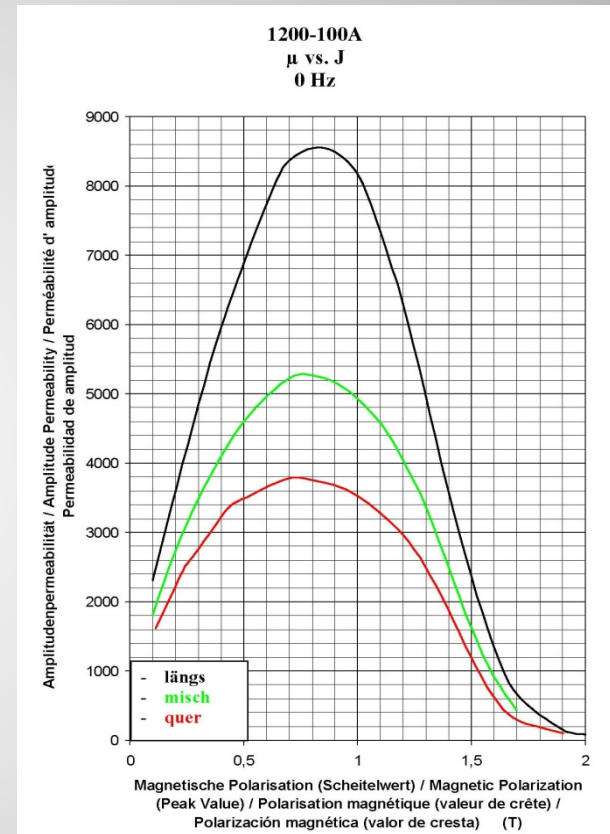
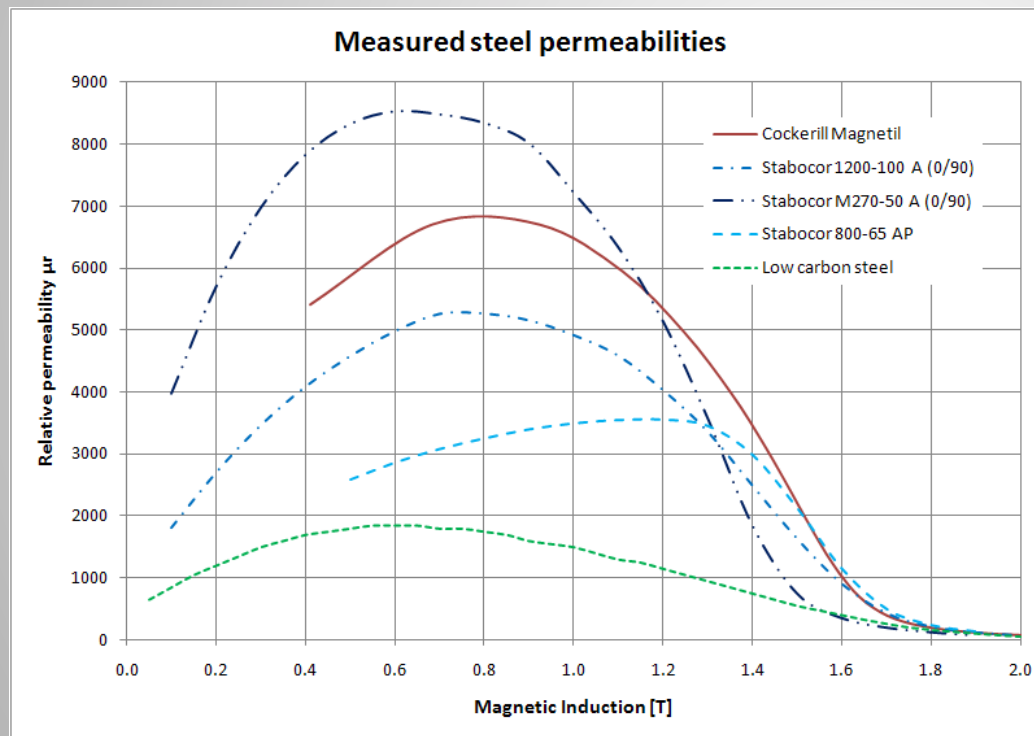




Permeability



Ferro-magnetic materials: high permeability ($\mu_r \gg 1$), but not constant



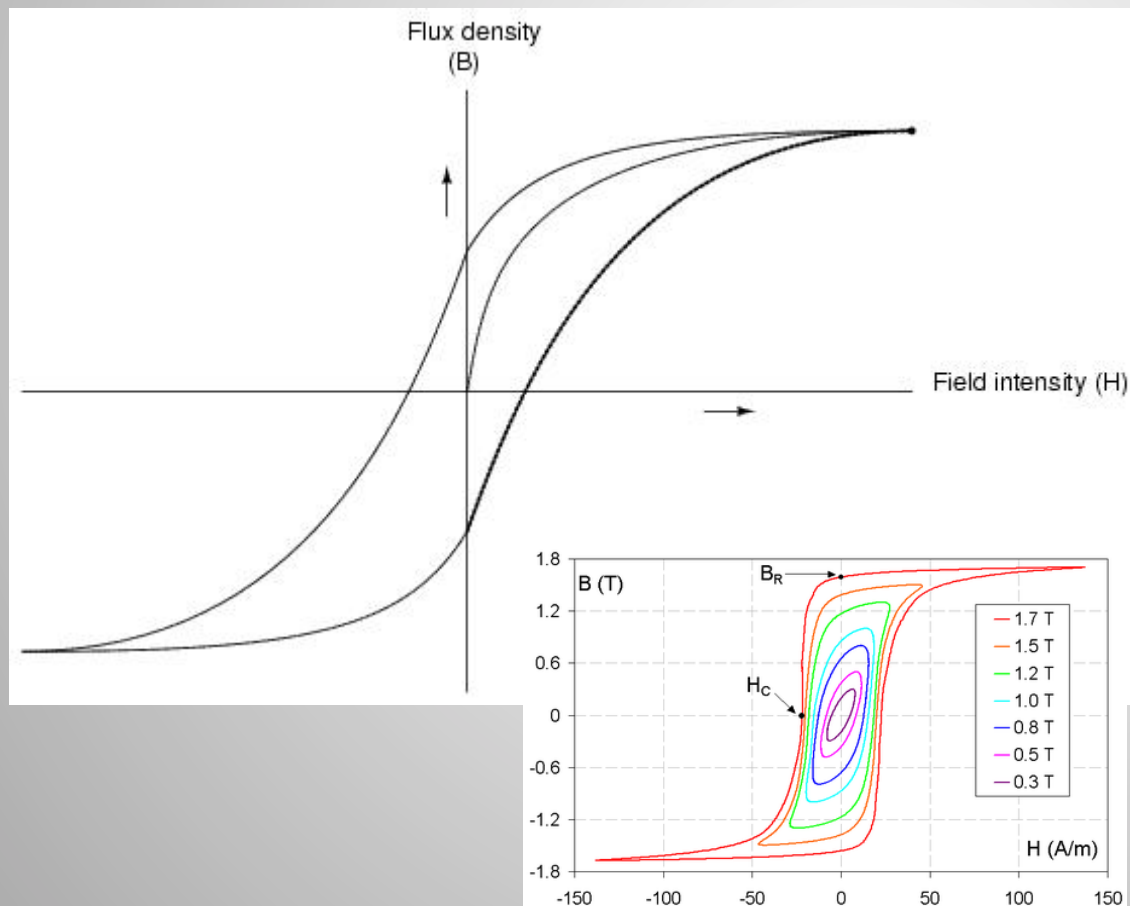
Data source: Thyssen/Germany

Anisotropy in sheet material can be partly cured by final annealing



Steel hysteresis

Flux density $B(H)$ as a function of the field strength is different, when increasing and decreasing excitation

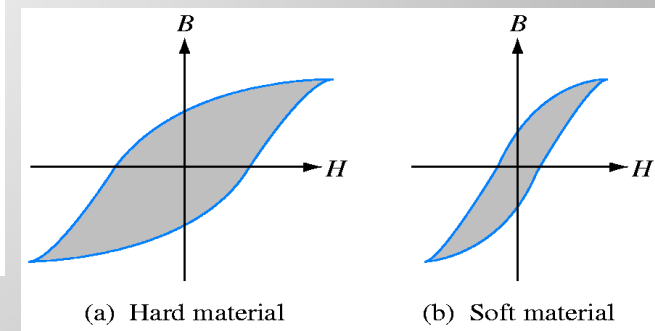


Remanent field (Retentivity):

$$H = 0 \rightarrow B = B_r > 0$$

Coercivity or coercive force:

$$B = 0 \rightarrow H = H_c < 0$$





Residual field in a magnet

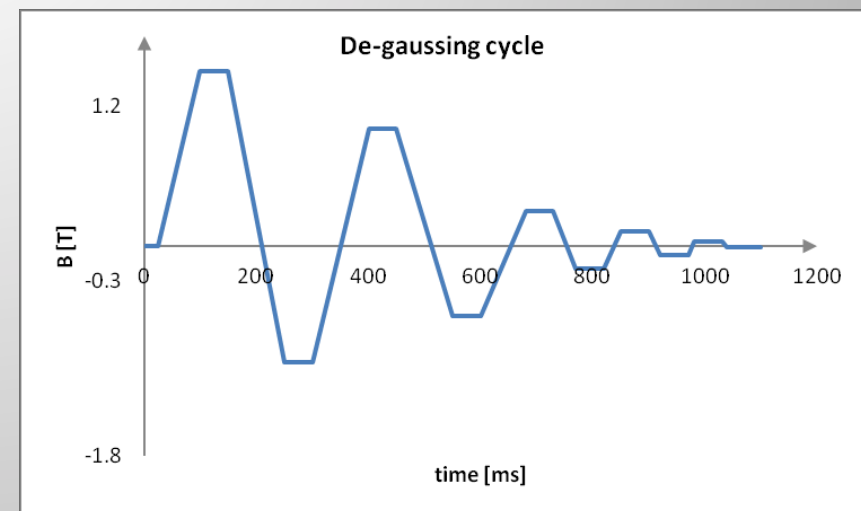
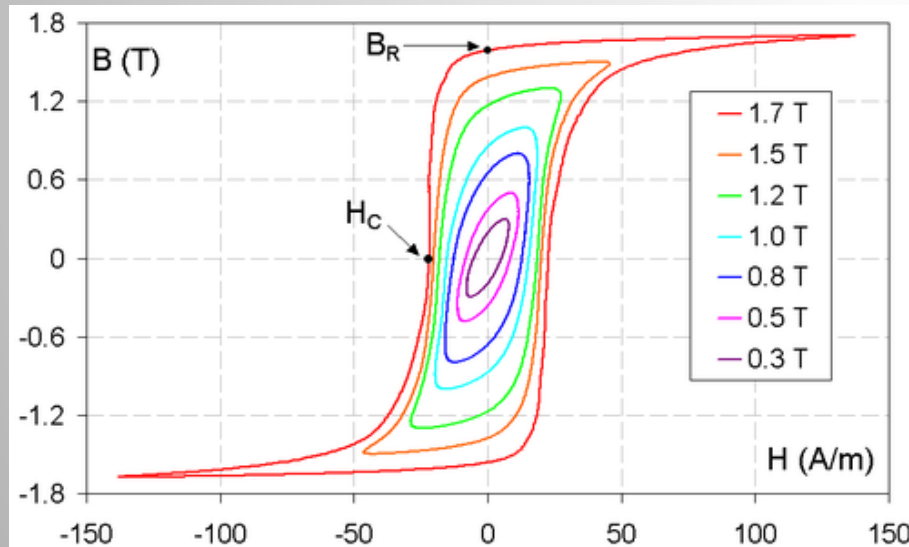
In a continuous ferro-magnetic core (transformer) the residual field is determined by the remanent field B_r

In a magnet core (gap), the residual field is determined by the coercivity H_c

Assuming the coil current $I=0$:

$$\oint \vec{H} \cdot d\vec{l} = \int_{gap} \vec{H}_{gap} \cdot d\vec{l} + \int_{yoke} \vec{H}_c \cdot d\vec{l} = 0$$

$$B_{residual} = -\mu_0 H_c \frac{l}{g}$$



Demagnetization cycle!



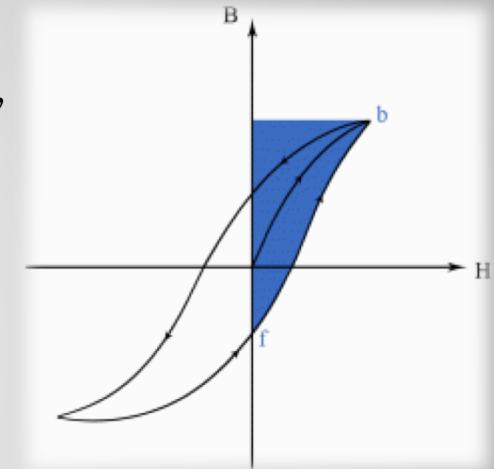
Stored energy & Inductance



Stored energy E_s [J, joules] in a magnet depends on (non-uniform) field distribution in the gap, coils, and iron yoke:

$$E_s = \int_V \int_f^b H \cdot dB \cdot dv \quad \text{and in case } \mu_r \text{ is linear:} \quad E_s = \frac{1}{2} \int_V H \cdot B \cdot dv$$

- difficult to calculate analytically
- usually done by numerical computations
- most of the energy is stored in the air gap



Inductance L [H] of a magnet is given by: $L = \frac{2E_s}{I^2}$

- total voltage on a pulsed magnet: $V_{tot} = RI + L \frac{dI}{dt} = RI + \frac{2E_s}{I^2} \frac{dI}{dt}$
- low inductance allows fast changes of magnetic field
- inductance depends on the magnetization in the iron



Eddy currents

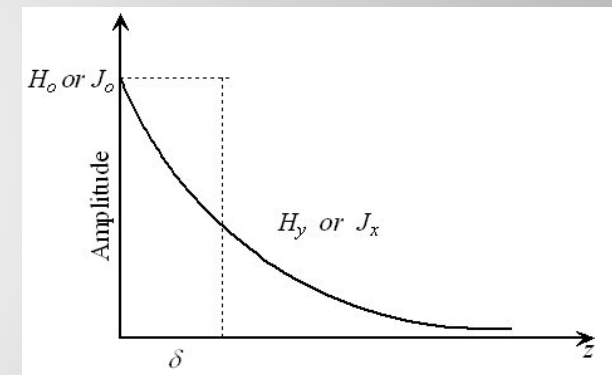


Faraday's law: varying magnetic field induces an e.m.f. (voltage) $U = -\frac{\partial \Phi}{\partial t}$

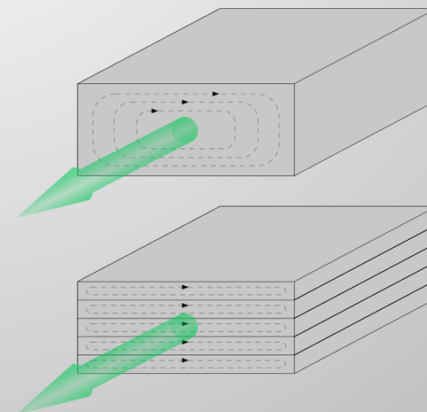
- Circulating (eddy) currents are generated in electrical conducting materials
 - creating a magnetic field opposing the original change in magnetic flux (Lenz's law)
 - opposing to the penetration of the magnetic field (skin effect)
 - producing losses (Joule heating)
 - causing delays to reach stable field value
 - damping high order modes (ripples)

$$H_y(z) = H_0 \cdot e^{-z/\delta} \quad \delta = \frac{1}{\sqrt{\pi \cdot \mu_0 \cdot \mu_r \cdot f \cdot \sigma}}$$

- δ : skin depth [m]



- Magnetic circuits are made of insulated laminations to reduce eddy currents,
 - decrease lamination thickness ($d < \delta/2$)
 - increase resistivity
 - decrease permeability
 - decrease frequency ($\partial \Phi / \partial t$)





Losses

Losses in the coils:

Ohmic power loss P_{Ω} per length unit [W/m] in a coil conductor

$$\frac{P_{\Omega}}{l} = \frac{\rho}{a_{cond}} I^2$$

- ρ : resistivity [Ωm] (for copper: $1.86 \cdot 10^{-8} \Omega\text{m}$ @ 40°C)
- a_{cond} : conductor cross-section [m^2]

Losses in the iron yoke:

Hysteresis losses: Power loss P_H per mass unit [W/kg] up to 1.5 T using Steinmetz's law

$$\frac{P_H}{m} = \eta \cdot f \cdot B^x$$

- η : material depending coefficient: $0.01 < \eta < 0.1$; $\eta \approx 0.02$ for silicon steel
- x : Steinmetz exponent: for iron $x = 1.6$
- f : operation frequency [Hz]

Eddy current losses: Power loss P_E per volume unit [W/m³] if $d_{lam} \ll \delta$

$$\frac{P_E}{V} = \frac{\pi^2 d_{lam}^2 f^2 B^2}{6\rho}$$

- d_{lam} : lamination thickness [m]

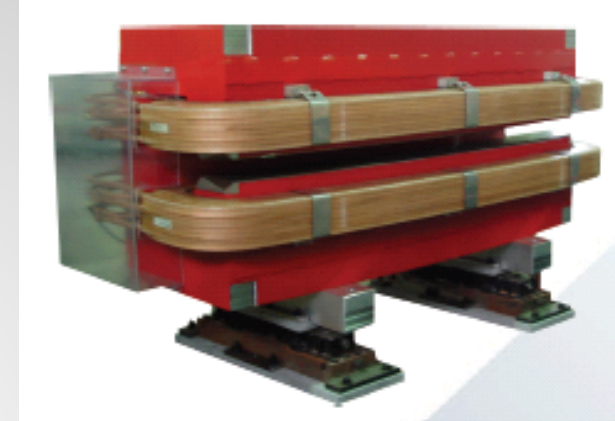


Magnetic length



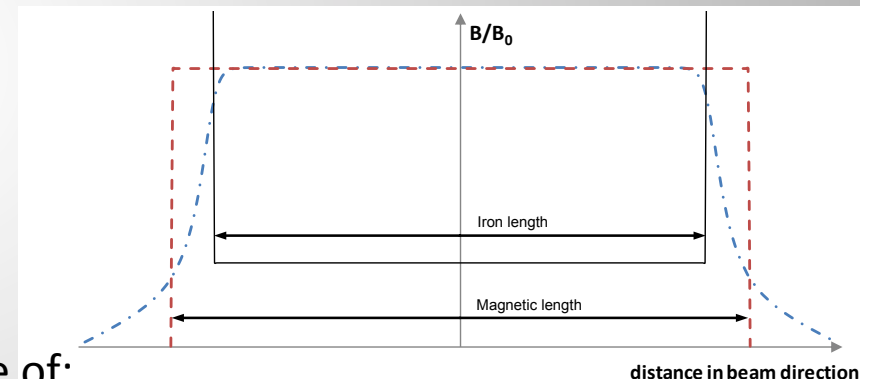
Coming from ∞ , B increases towards the magnet center (stray flux)

Magnetic length:
$$l_{mag} = \frac{\int_{-\infty}^{\infty} B(z) \cdot dz}{B_0}$$



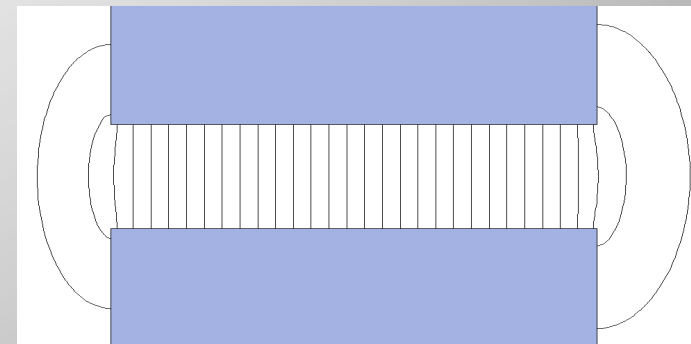
‘Magnetic’ length > iron length

Approximation for a dipole:
$$l_{mag} = l_{iron} + 2hk$$



Geometry specific constant k gets smaller in case of:

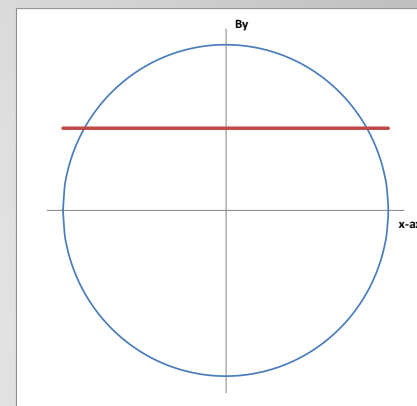
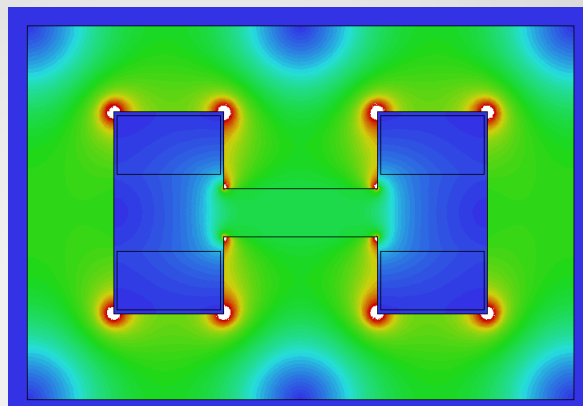
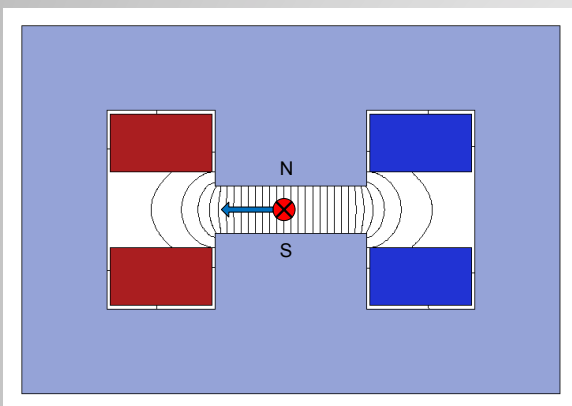
- pole length < gap height
- saturation
- precise determination only by measurements or numerical calculations





Dipoles

- Purpose: bend or steer the particle beam

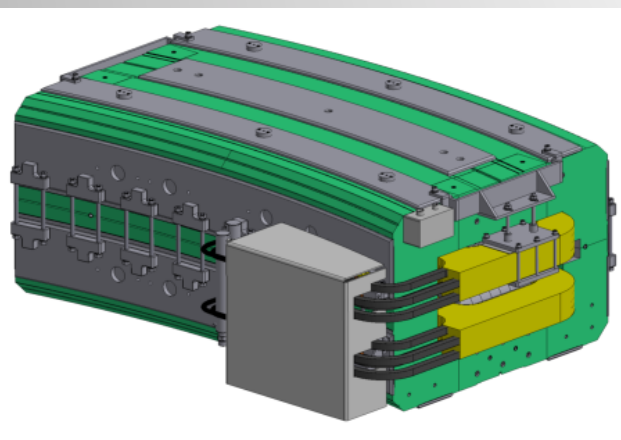
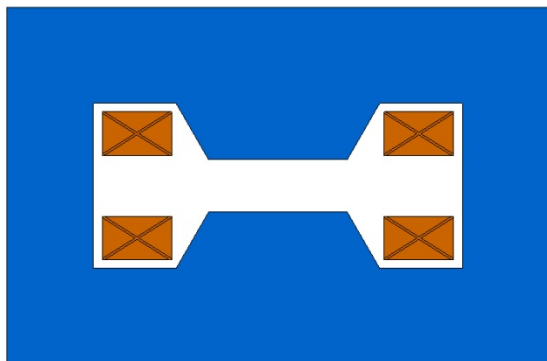


- Equation for normal (non-skew) ideal (infinite) poles: $y = \pm r$
(r = half gap height)
- Magnetic flux density: $B_x = 0$; $B_y = b_1 = \text{const.}$
- Applications: synchrotrons, transfer lines, spectrometry, beam scanning

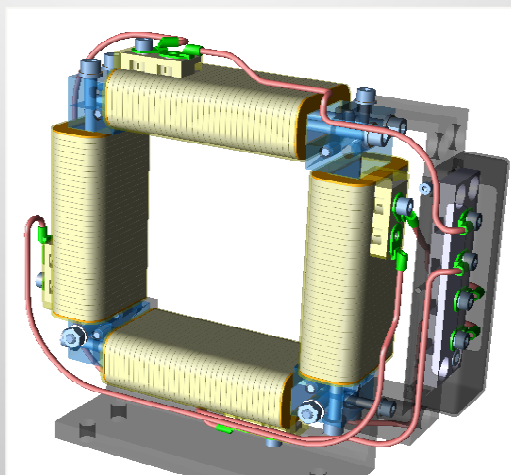
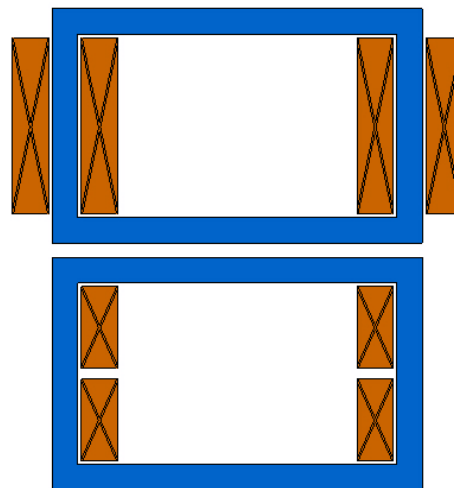


Dipole types

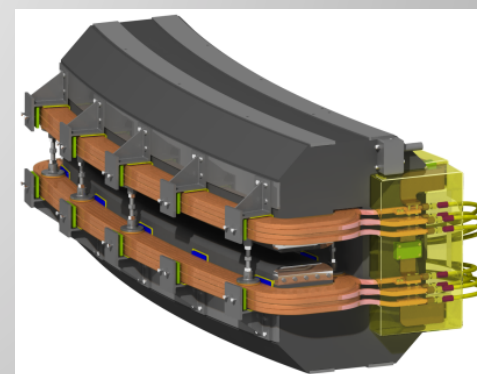
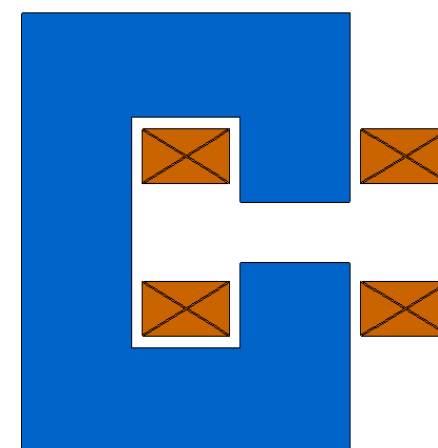
H-Shape



O-Shape



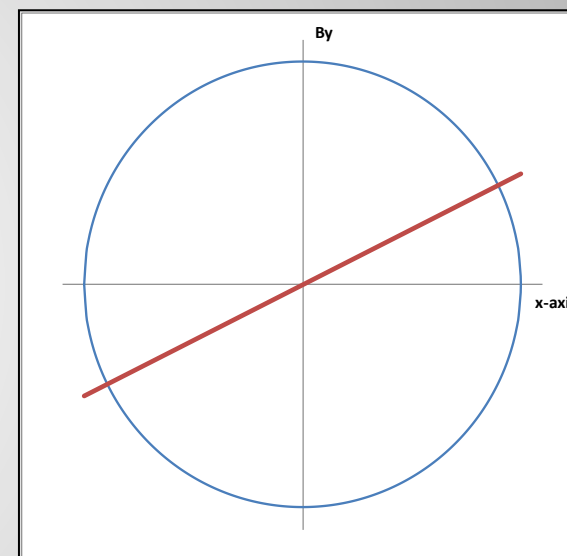
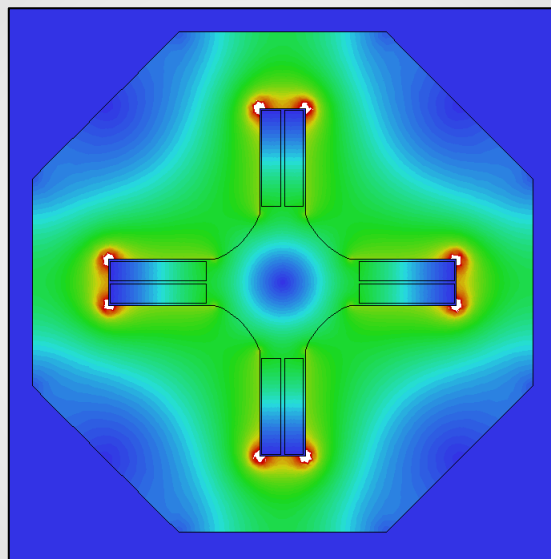
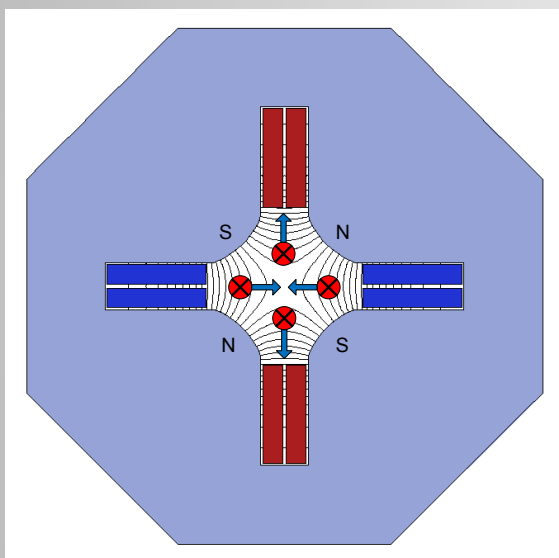
C-Shape





Quadrupoles

- Purpose: focusing the beam (horizontally focused beam is vertically defocused)

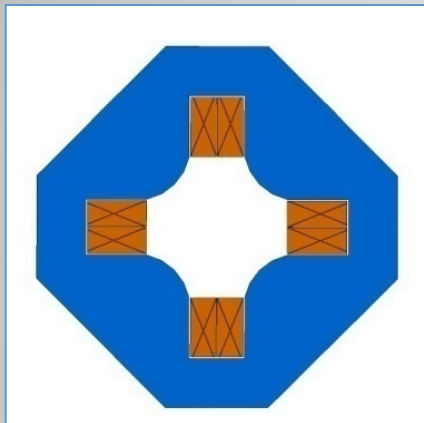


- Equation for normal (non-skew) ideal (infinite) poles: $2xy = \pm r^2$
(r = aperture radius)
- Magnetic flux density: $B_x = b_2 y$; $B_y = b_2 x$

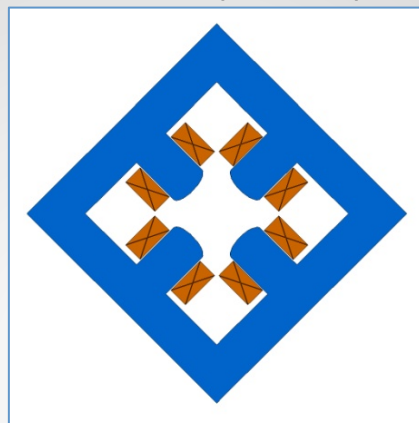


Quadrupole types

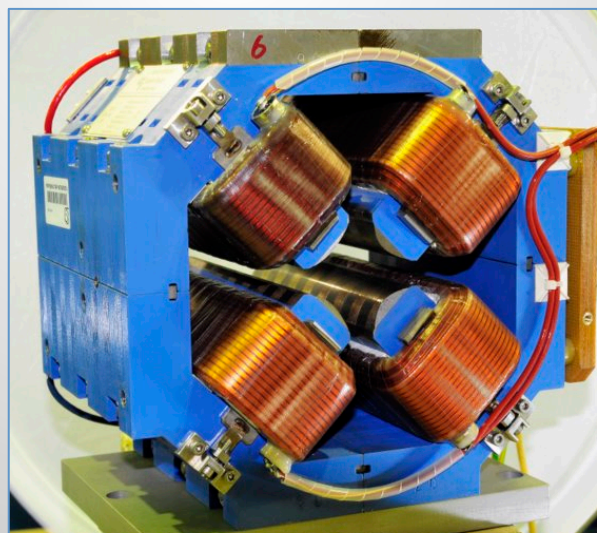
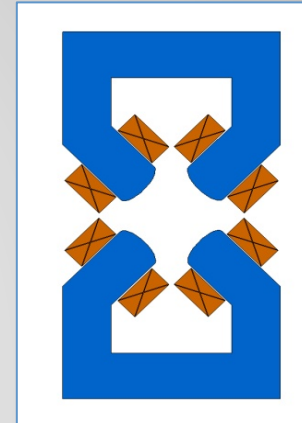
Standard quadrupole



Standard quadrupole



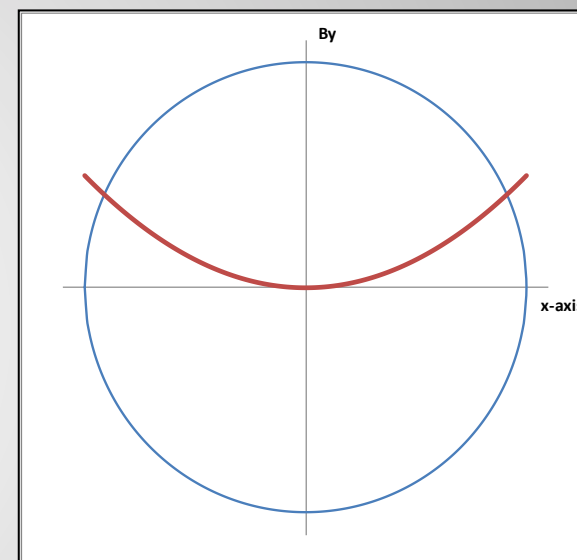
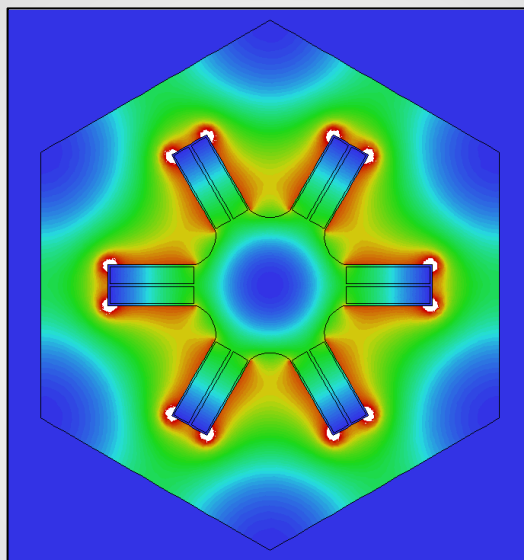
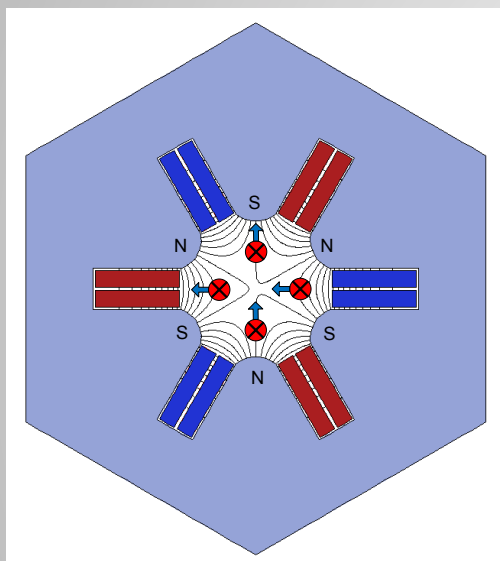
Collins or Figure-of-Eight





Sextupoles

- Purpose: correct chromatic aberrations of 'off-momentum' particles

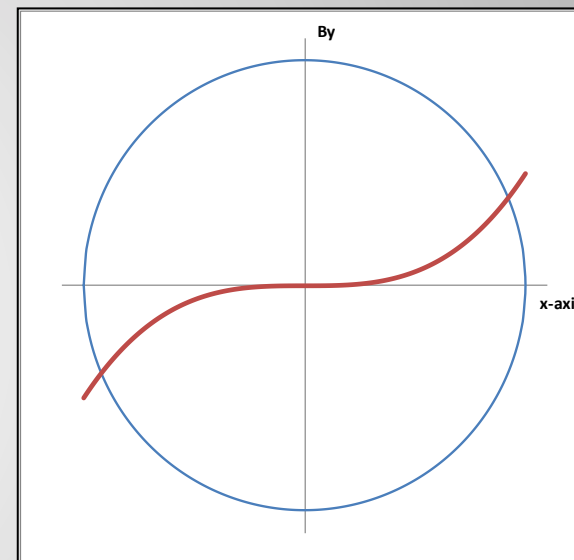
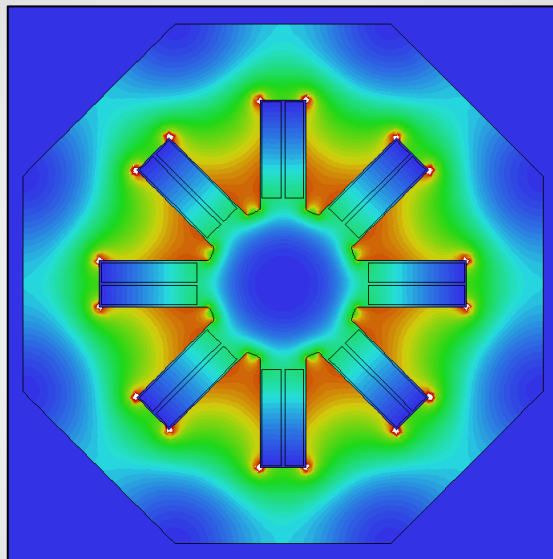
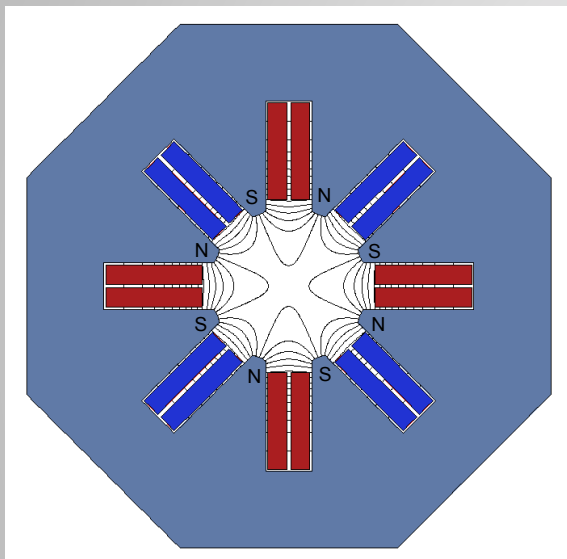


- Equation for normal (non-skew) ideal (infinite) poles: $3x^2y - y^3 = \pm r^3$
(r = aperture radius)
- Magnetic flux density: $B_x = b_3xy$; $B_y = b_3(x^2 - y^2)/3$



Octupoles

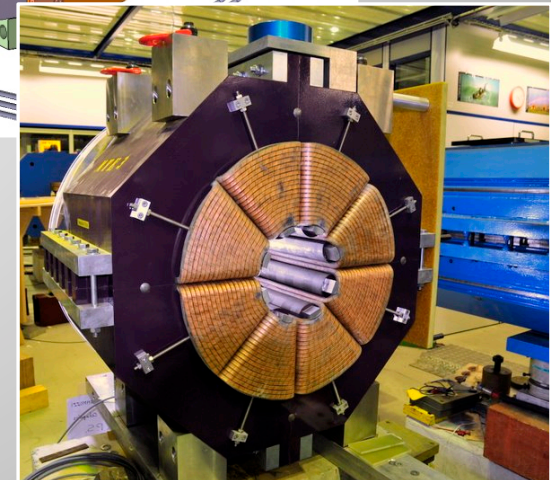
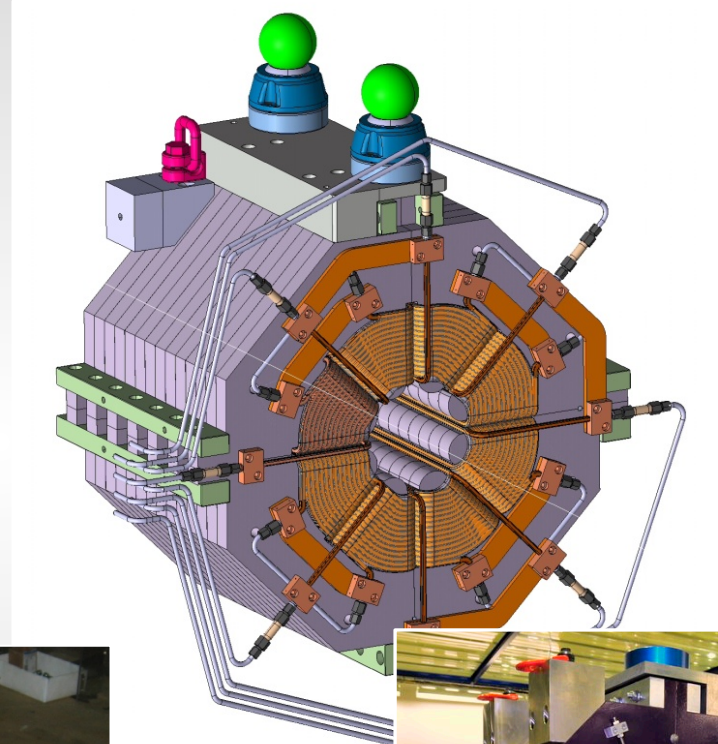
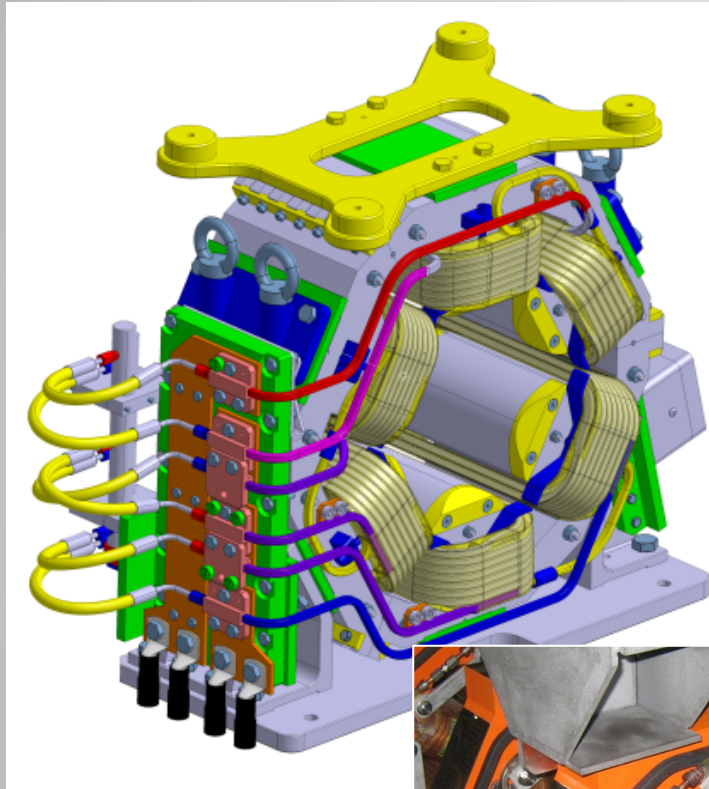
- Purpose: 'Landau' damping



- Equation for normal (non-skew) ideal poles: $4(x^3y - xy^3) = \pm r^4$
(r = aperture radius)
- Magnetic flux density: $B_x = b_4(3x^2y - y^3)/6$; $B_y = b_4(x^3 - 3xy^2)/6$



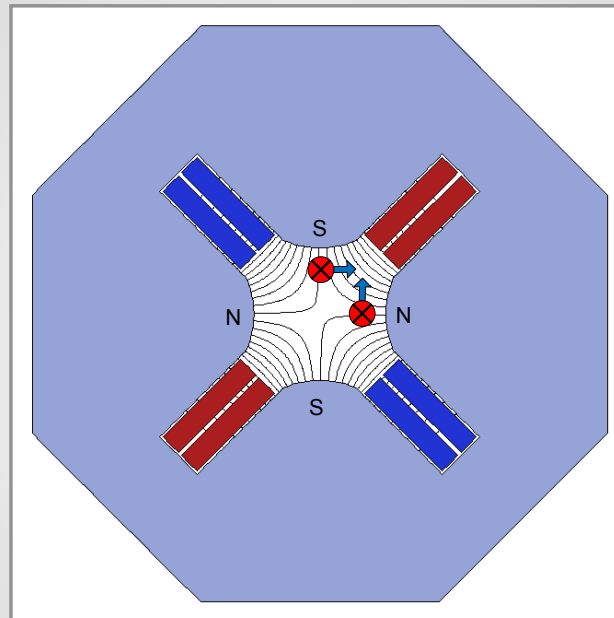
Sextupoles & Octupoles





Skew quadrupole

- Purpose: coupling horizontal and vertical betatron oscillations



Rotation by $\pi/2n$

- Beam that has horizontal displacement (but no vertical) is deflected vertically
- Beam that has vertical displacement (but no horizontal) is deflected horizontally



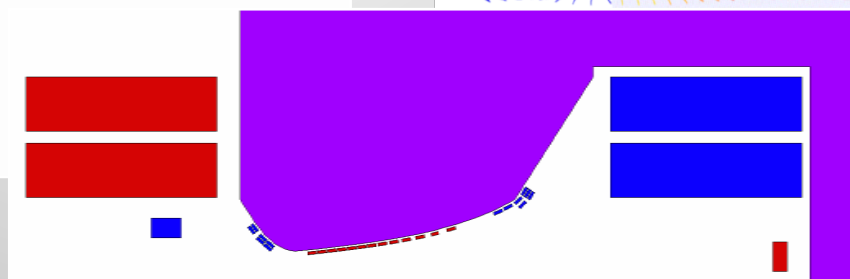
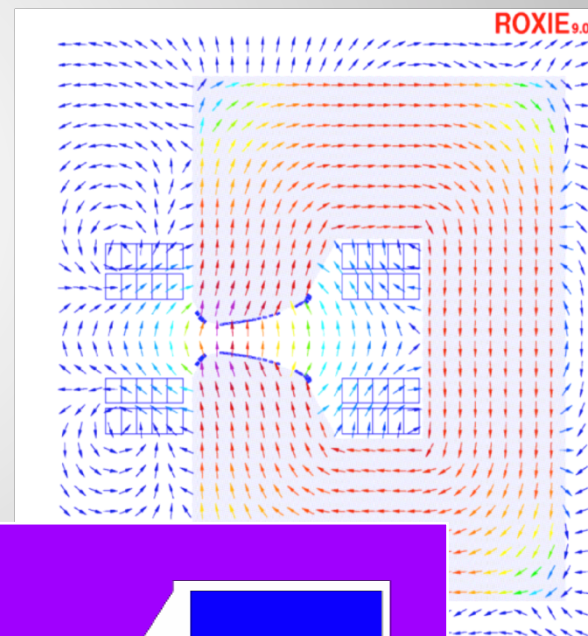
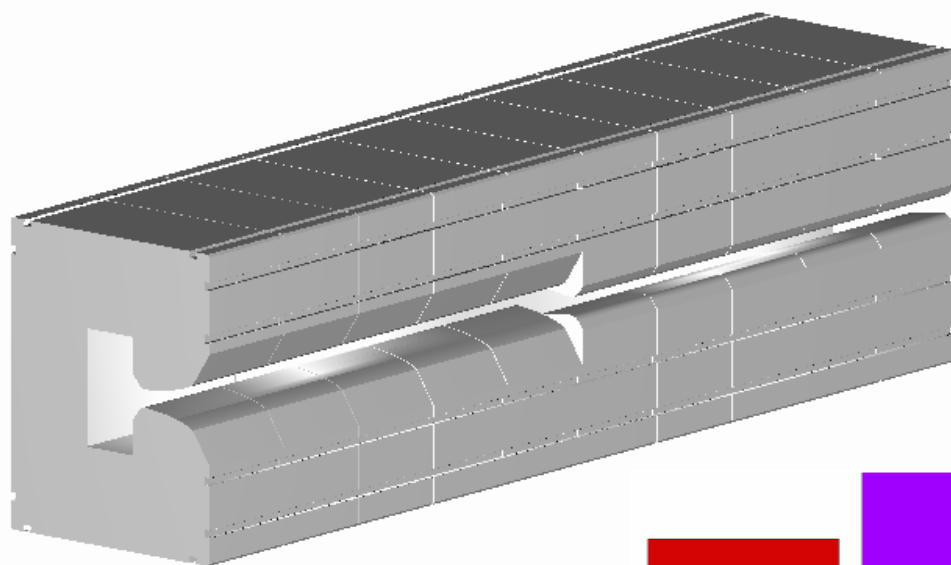
Combined function magnets



Functions generated by pole shape (sum a scalar potentials):

Amplitudes cannot be varied independently

Dipole and quadrupole: PS main magnet (PFW, Fo8...)



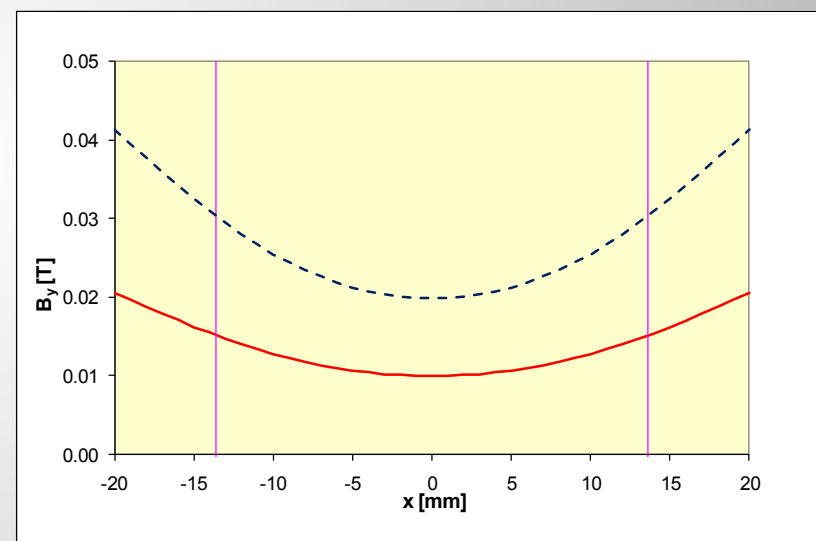
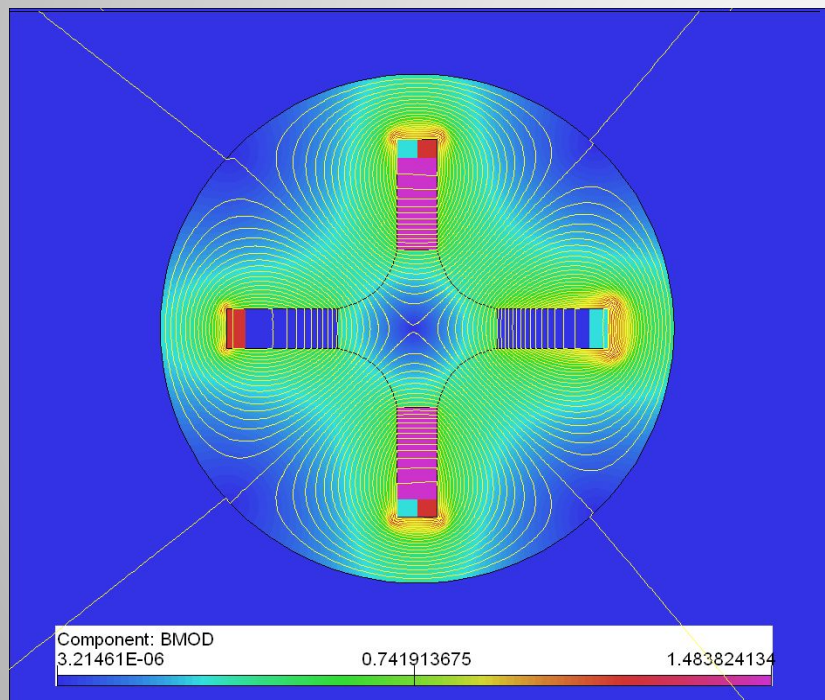


Combined function magnets



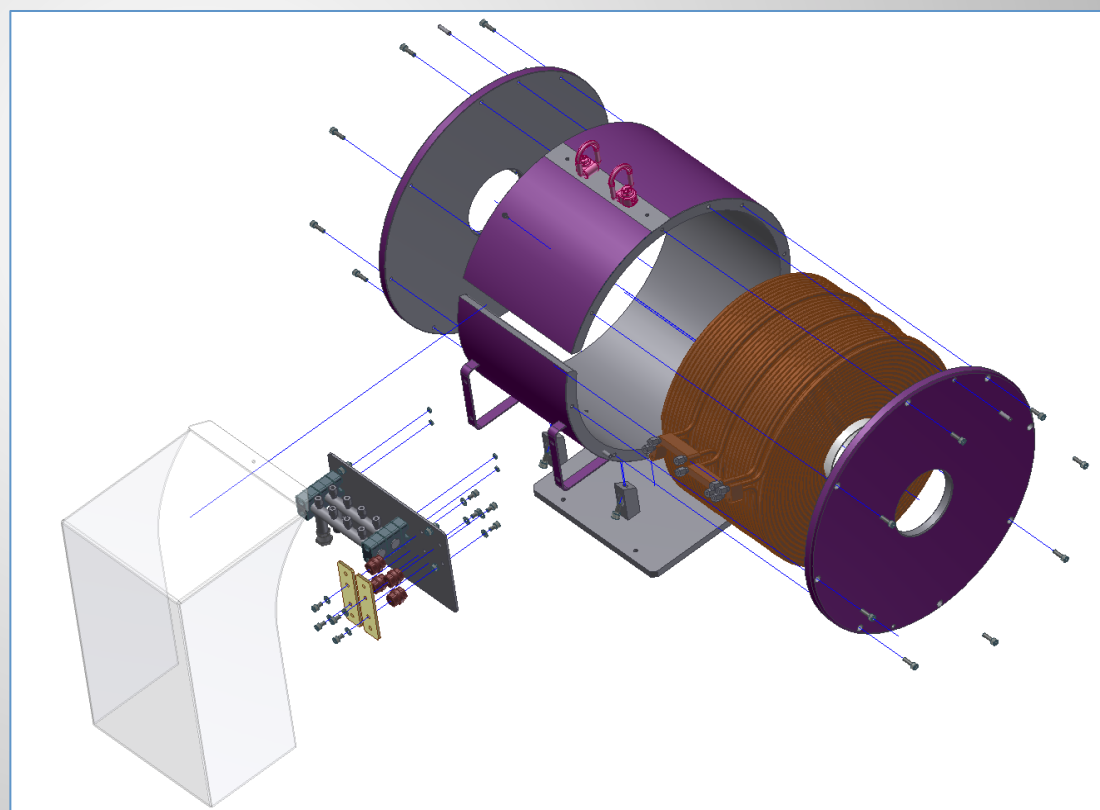
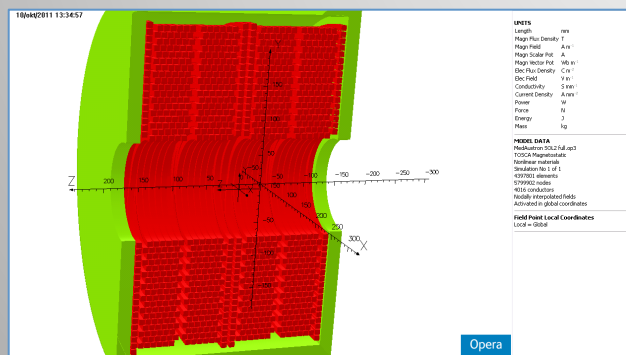
Functions generated by individual coils:

Amplitudes can be varied independently



Quadrupole and corrector dipole
(strong sextupole component in dipole field)

- Weak focusing, non-linear elements
- Main field component in z-direction, focusing by end fields
- Usually only used in experiments or low-energy beam lines

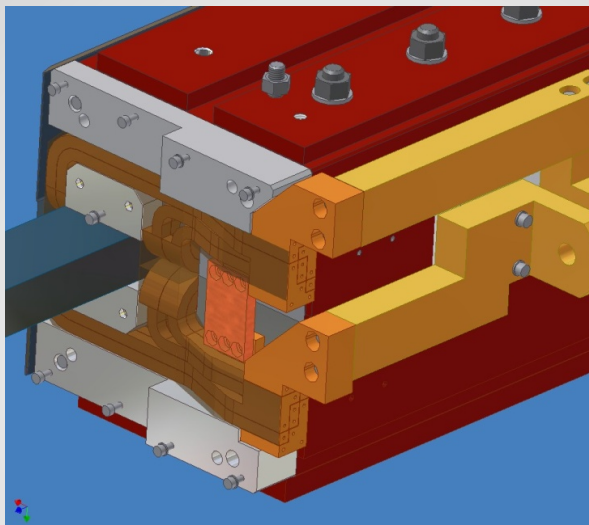




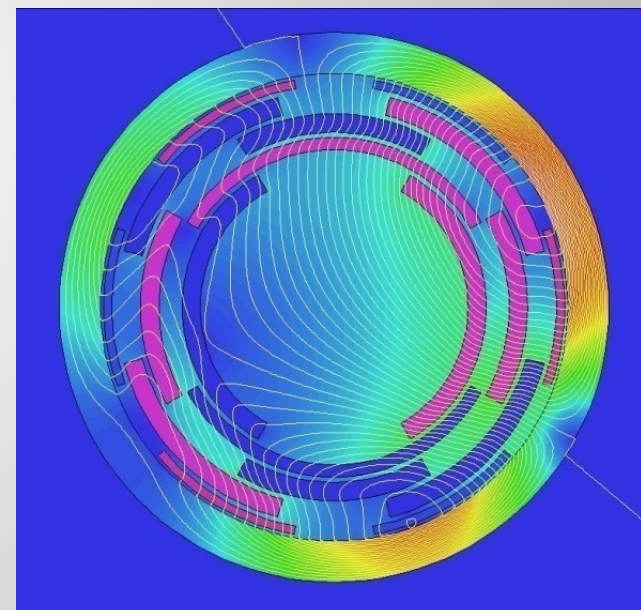
Special magnets

For beam injection and extraction

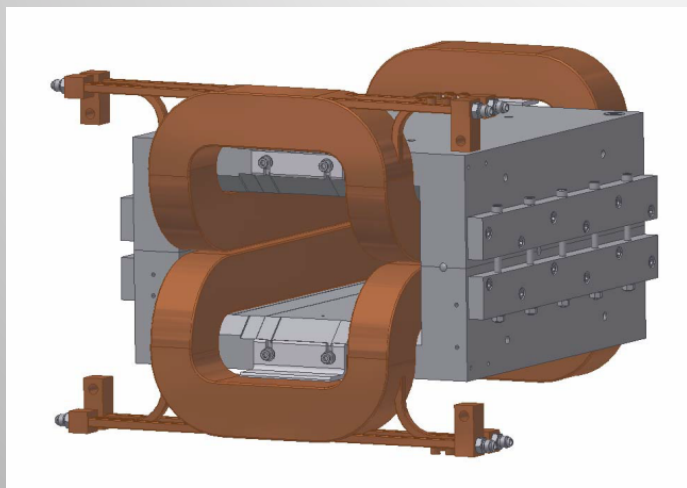
- Septa
- Kicker magnets
- Bumper magnets



Coil-dominated magnets



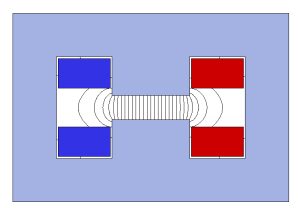
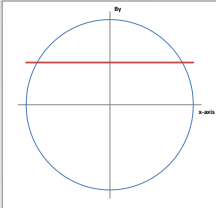
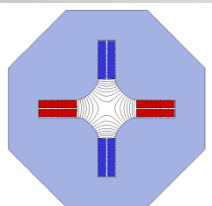
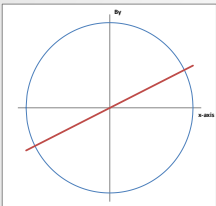
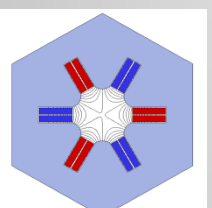
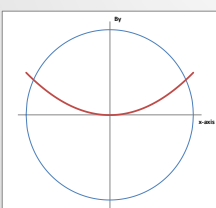
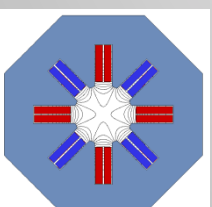
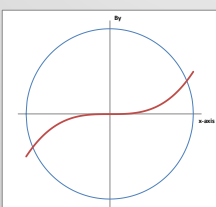
Scanning magnets





Overview



Pole shape	Field distribution	Pole equation	B_x, B_y
		$y = \pm r$	$B_x = 0$ $B_y = b_1 = B_0 = \text{const.}$
		$2xy = \pm r^2$	$B_x = b_2 y$ $B_y = b_2 x$
		$3x^2y - y^3 = \pm r^3$	$B_x = b_3 xy$ $B_y = b_3(x^2 - y^2)/2$
		$4(x^3y - xy^3) = \pm r^4$	$B_x = b_4(3x^2y - y^3)/6$ $B_y = b_4(x^3 - 3xy^2)/6$



Summary



- Magnets are needed to guide and shape particle beams
- Coils carry the electrical current, the iron yoke carries the magnets flux
- Steel properties have a significant influence on the magnet performance
- In case of time-varying fields, eddy currents can appear
- Different magnet types providing different functions