Superconductivity for accelerators - why bother?

Abolish Ohm's Law

- no power consumption
    (although do need refrigeration power)

- high current density ⇒ compact windings, high gradients

- ampere turns are cheap, so don't need iron
    (although often use it for shielding)

Consequences

- lower power bills

- higher magnetic fields mean reduced bend radius
    ⇒ smaller rings
    ⇒ reduced capital cost
    ⇒ new technical possibilities
        (eg muon collider)

- higher quadrupole gradients
    ⇒ higher luminosity

Plan of the Lectures

1 Introduction to Superconductors
- critical field, temperature & current
- superconductors for magnets
- manufacture of superconducting wires
- high temperature superconductors HTS

2 Magnetization, Cables & AC losses
- superconductors in changing fields
- filamentary superconductors and magnetization
- coupling between filaments $\Rightarrow$ magnetization
- why cables, coupling in cables
- AC losses in changing fields

3 Magnets, 'Training' & Fine Filaments
- coil shapes for solenoids, dipoles & quadrupoles
- engineering current density & load lines
- degradation & training minimum quench energy
- critical state model & fine filaments

4 Quenching and Cryogenics
- the quench process
- resistance growth, current decay, temperature rise
- quench protection schemes
- cryogenic fluids, refrigeration, cryostat design

5 Practical Matters
- LHC quench protection
- current leads
- accelerator magnet manufacture
- some superconducting accelerators

Tutorial 1: Fine Filaments
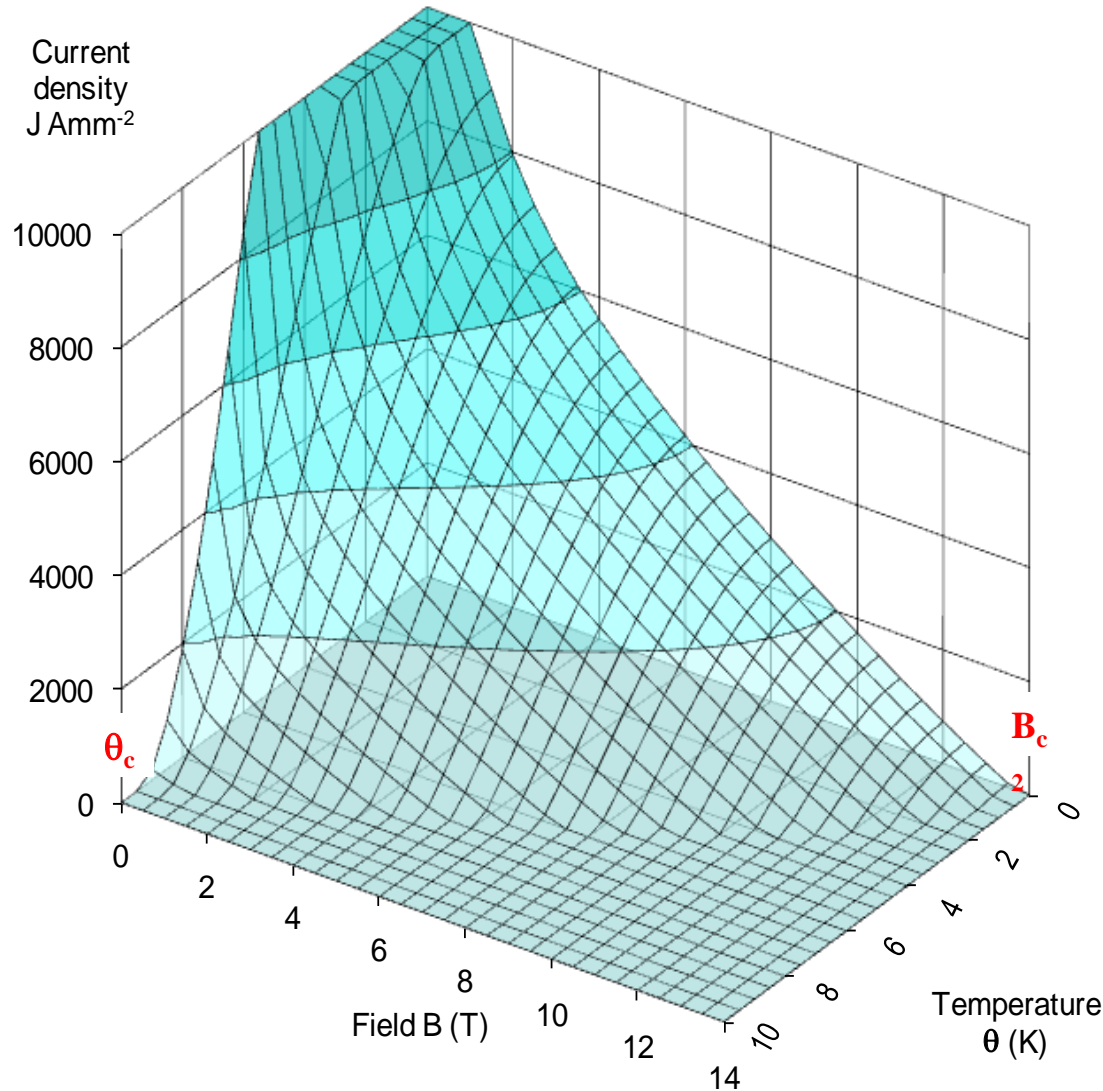- how filament size affects magnetization

Tutorial 2: Quenching
- current decay and temperature rise

*get a feel for the numbers,
bring a calculator*

The critical surface of niobium titanium

- **NbTi** is the standard commercial 'work horse' of the superconducting magnet business

Current density J Amm^{-2}

10000

8000

6000

4000

2000

0

θ_c

B_c

2

0

Field B (T)

0　2　4　6　8　10　12　14

Temperature θ (K)

10　8　6　4　2　0

- *critical surface* is the boundary between superconductivity and normal resistivity in *J, B, θ* space

- superconductivity prevails everywhere below the surface, resistance everywhere above it

- upper critical field B_{c2} (at zero temperature and current)

- critical temperature θ_c (at zero field and current)

- B_{c2} and θ_c are characteristic of the alloy composition

- critical current density J_c depends on processing

- keep it cold!

The critical line at 4.2K
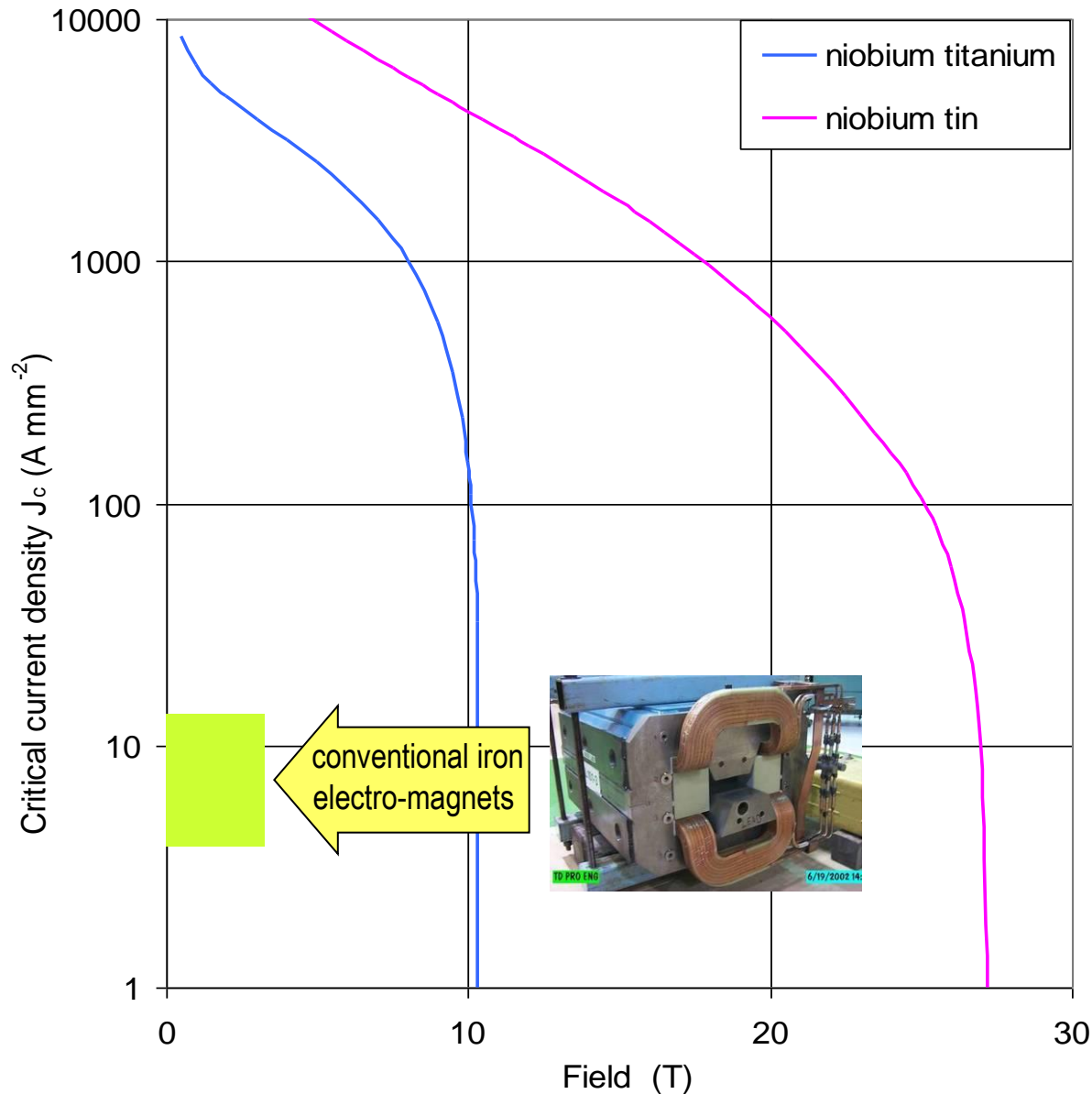
- magnets usually work in boiling liquid helium, so the critical surface is often represented by a curve of current versus field at 4.2K

- niobium tin Nb_3Sn has a much higher performance than NbTi

- **but** Nb_3Sn is a brittle intermetallic compound with poor mechanical properties

- both the field and current density of both superconductors are way above the capability of conventional electromagnets

Two kinds of superconductor: type 1

- the materials first discovered by Kammerlingh Onnes in 1911 - soft metals like lead, tin mercury

- sphere of metal at room temperature

- apply magnetic field

- reduce the temperature - resistance decreases

- reduce the temperature some more - resistance decreases some more

- at the critical temperature θ_c the field is pushed out - the **Meissner effect** - superconductivity!

- increase the field - field is kept out

- increase the field some more - superconductivity is extinguished and the field jumps in

- thermodynamic critical field B_c is trade off between **reducing** energy via condensation to superconductivity and **increasing** energy by pushing out field ~ 0.1T
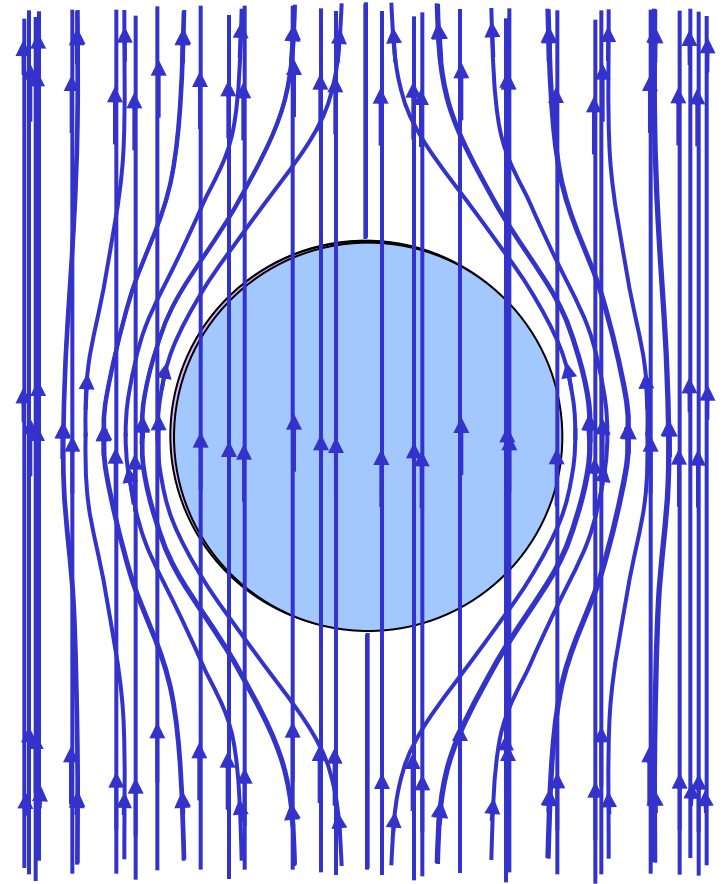

*useless for magnets!*

Two kinds of superconductor: type 2

- apply magnetic field

- reduce the temperature - resistance decreases

- at the critical temperature θ_c the field is pushed out

- increase the field - field jumps back in without quenching superconductivity

- it does so in the form of quantized fluxoids

- lower critical field B_{c1}

- supercurrents encircle the resistive core of the fluxoid thereby screening field from the bulk material

- higher field $\Rightarrow$ closer vortex spacing

- superconductivity is extinguished at the (much higher) upper critical field B_{c2}
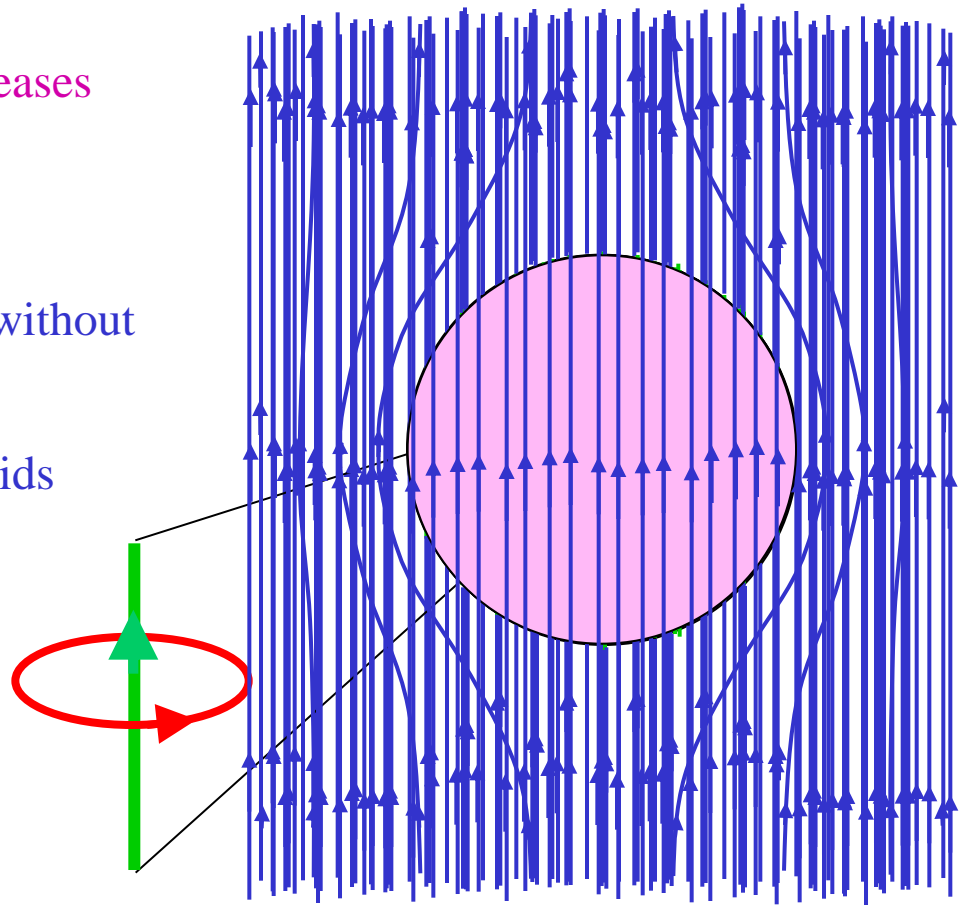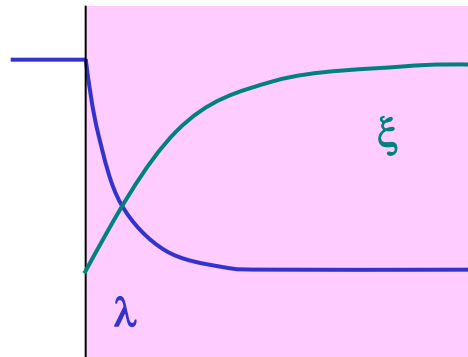
Type 1 and type 2 superconductors
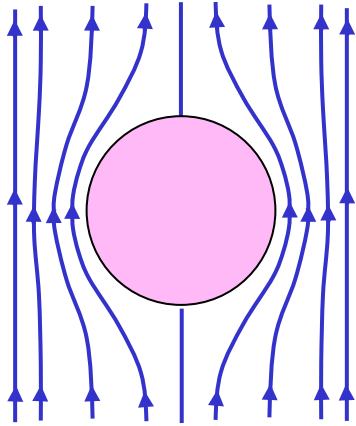
- Meissner effect is not total

- magnetic field penetrates a small distance λ
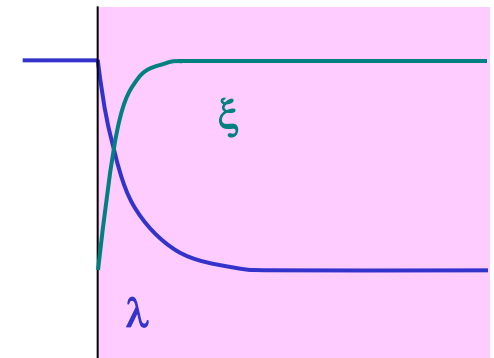
- the **London Penetration Depth.**
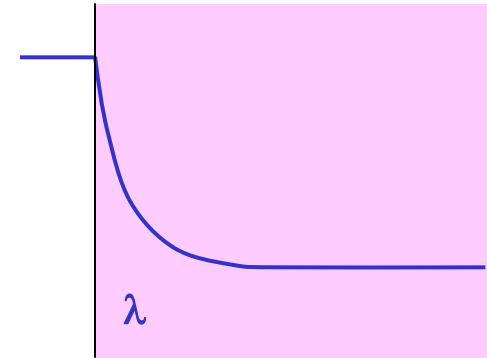
- another characteristic distance is the **coherence length** ζ - the minimum distance over which the electronic state can change from superconducting to normal

- theory of Ginsburg, Landau, Abrikosov and Gorkov **GLAG** defines the ratio $\kappa = \lambda / \xi$

if $\kappa < 1/\sqrt{2}$ material is **Type 1**
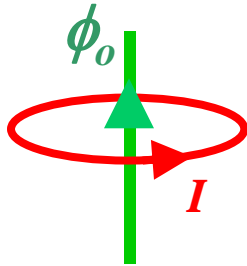

if $k > 1/\sqrt{2}$ material is **Type 2**

Critical fields of type 2 superconductors

- recap thermodynamic critical field B_c

- lower critical field $B_{c1} = B_c / \kappa$

- above B_{c1} magnetic field penetrates as discrete quantized *fluxoids*

a fluxoid encloses flux

ϕ_o

I

$$\phi_o = \frac{h}{2e} = 2 \times 10^{-15} Wb$$

h = Planck's constant
e = electronic charge

human hair in earth's magnetic field ~ 50ϕ_o

upper critical field $B_{c2} = \sqrt{2} \kappa B_c$ in the 'dirty limit' $\kappa \approx 2.4 \times 10^6 \gamma^{\frac{1}{2}} \rho_n$ where ρ_n is the normal state resistivity
- best superconductors are best resistors!

thus the upper critical field $B_{c2} = 3.1 \times 10^3 \gamma \rho_n \theta_c$

for NbTi: $\gamma \sim 900$ J m^{-3} K^{-2} $\rho_n \sim 65 \times 10^{-8}$ W m $\theta_c = 9.3$ K   hence   **B_{c2} ~ 18.5 T**

*Sommerfeld coefficient of electronic specific heat $C_e = \gamma \theta$*

Critical current density: type 2 superconductors

- fluxoids consist of resistive cores with supercurrents circulating round them.

  spacing between the fluxoids is:-

  $$d = \left\{ \frac{2}{\sqrt{3}} \frac{\phi_o}{B} \right\}^{\frac{1}{2}} = 22nm \quad at \ 5T$$

- each fluxoid carries one unit of flux,
  so density of fluxoids = average field
  uniform density $\Rightarrow$ uniform field
  $\Rightarrow$ zero J (because $Curl \ B = \mu_o J$)

- to get a current density we must produce a gradient in the density of fluxoids
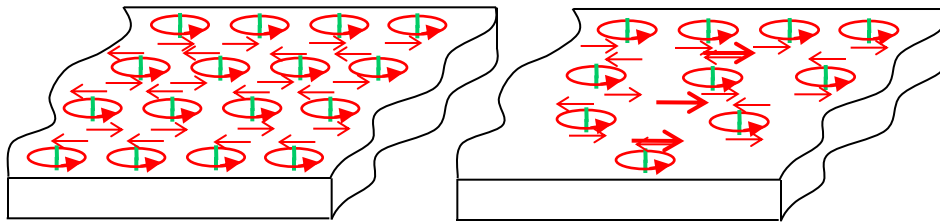
- fluxoids like to distribute uniformly

- so we must impose a gradient by inhomogeneities in the material, eg dislocations or precipitates

precipitates of α Ti in Nb Ti


200nm
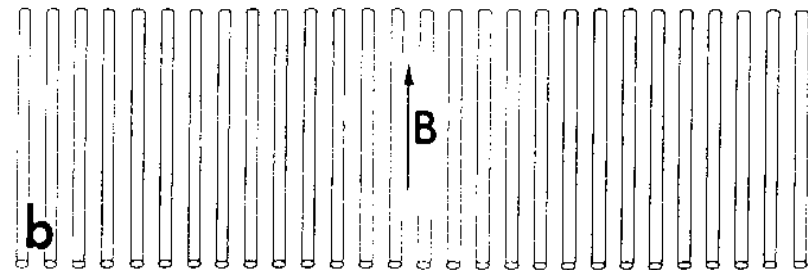
fluxoid lattice at 5T on the same scale

Critical properties

- **Critical temperature** θ_c: choose the right material to have a large energy gap or 'depairing energy'
  property of the material

- **Upper Critical field B_{c2}:** choose a Type 2 superconductor with a high critical temperature and a high normal state resistivity
  property of the material

- **Critical current density J_c**: mess up the microstructure by cold working and precipitation heat treatments
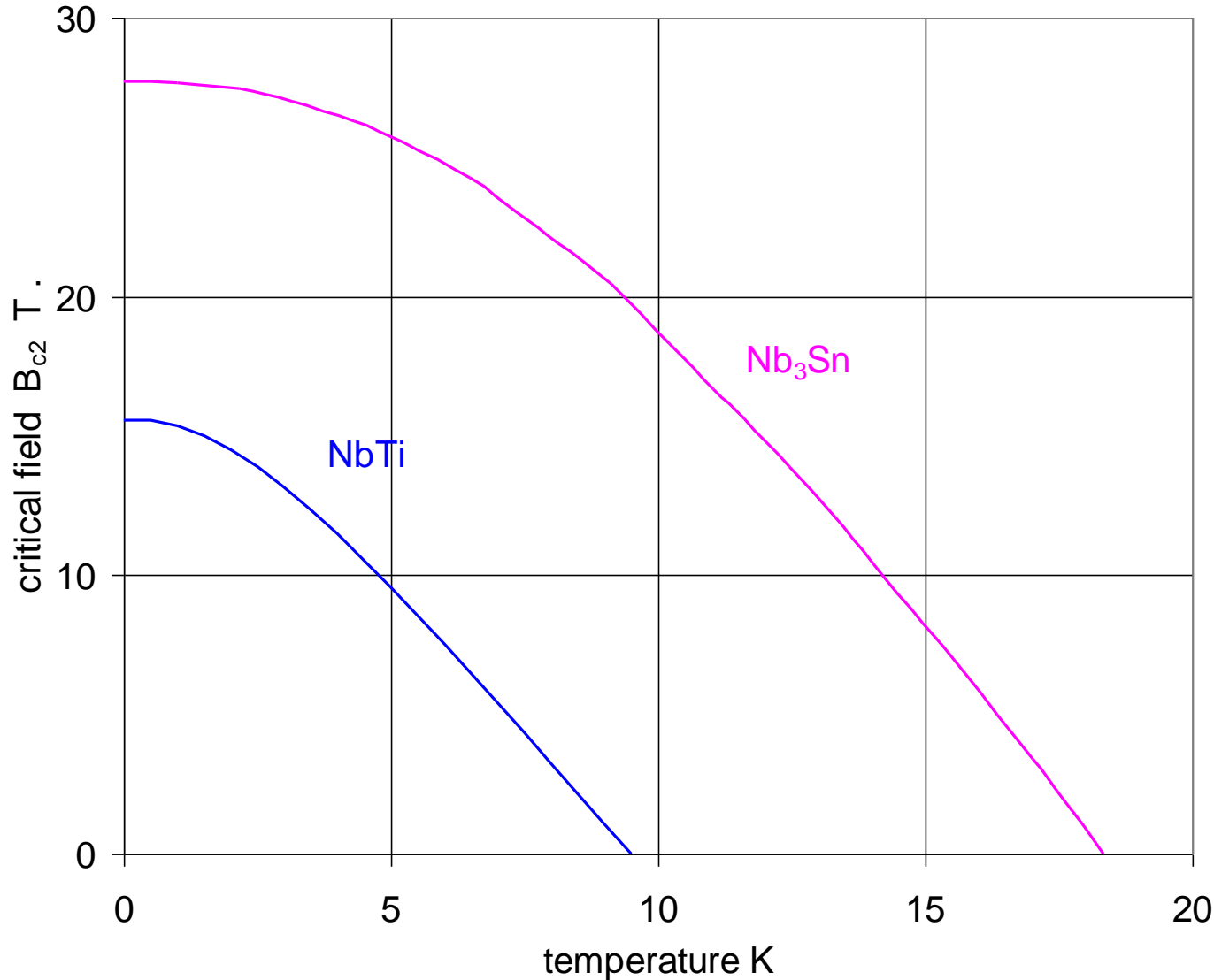 *hard work by the producer*
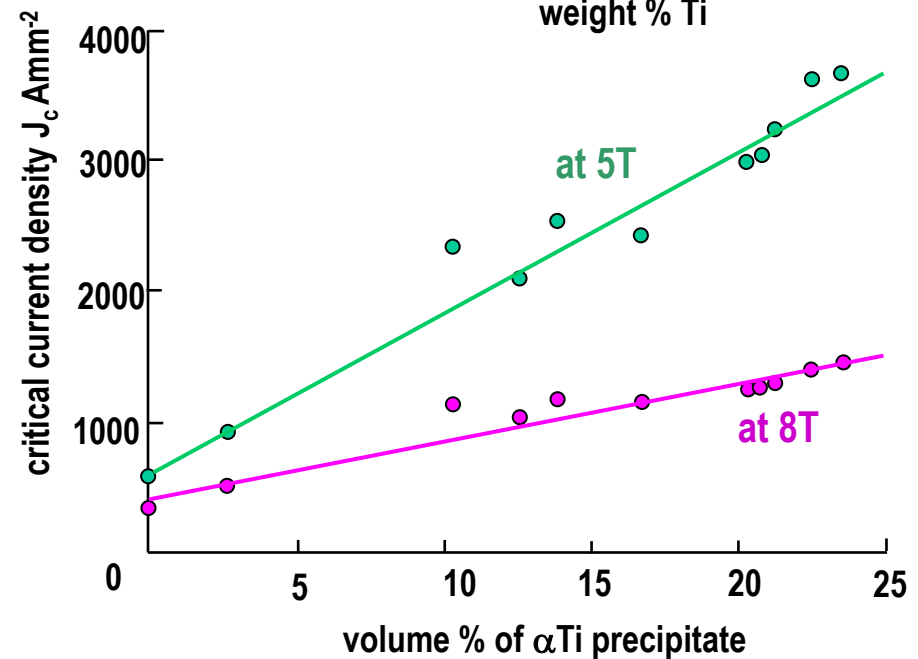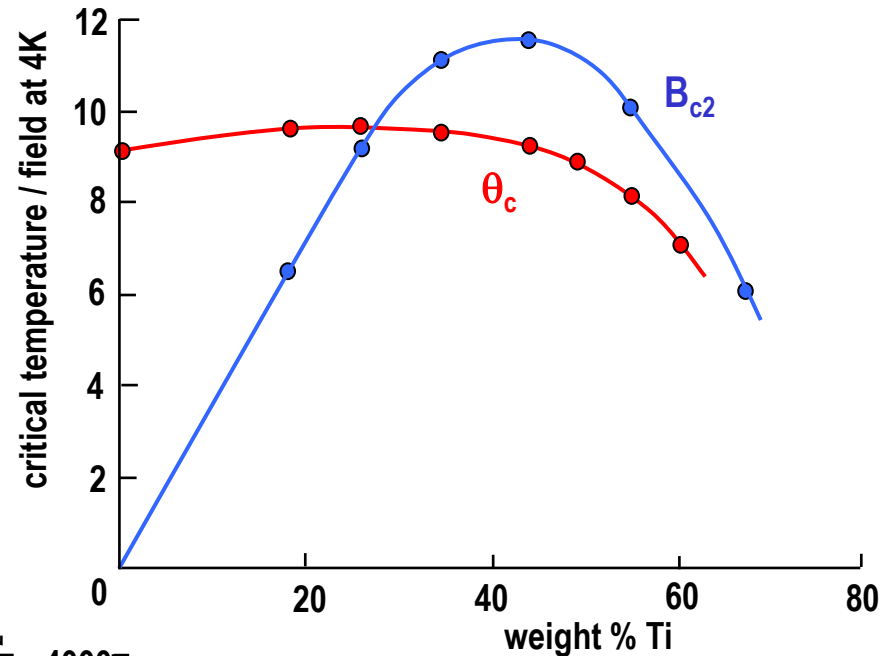
Critical field & temperature of metallic superconductors
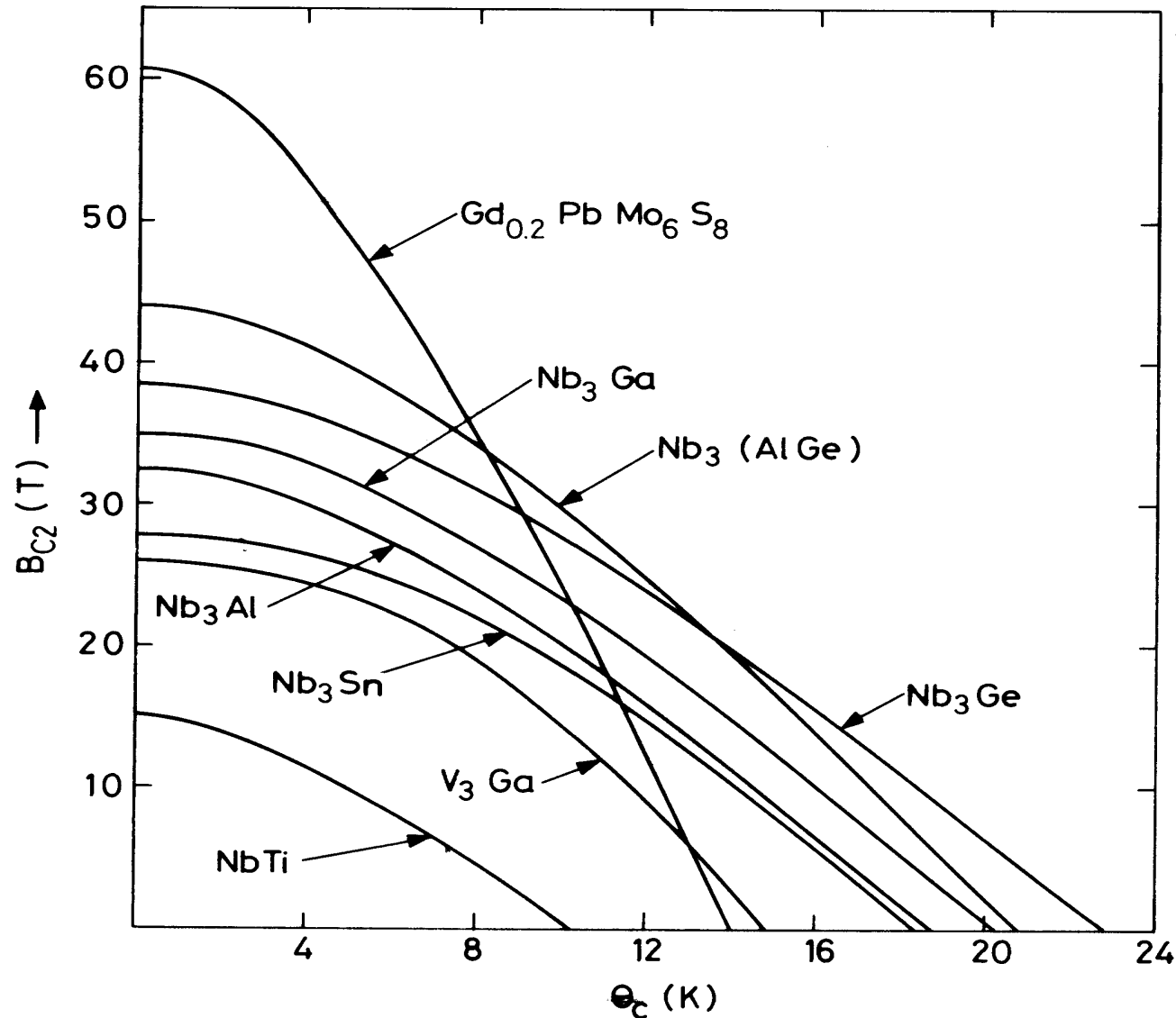
Note: of all the metallic superconductors, only NbTi is ductile.

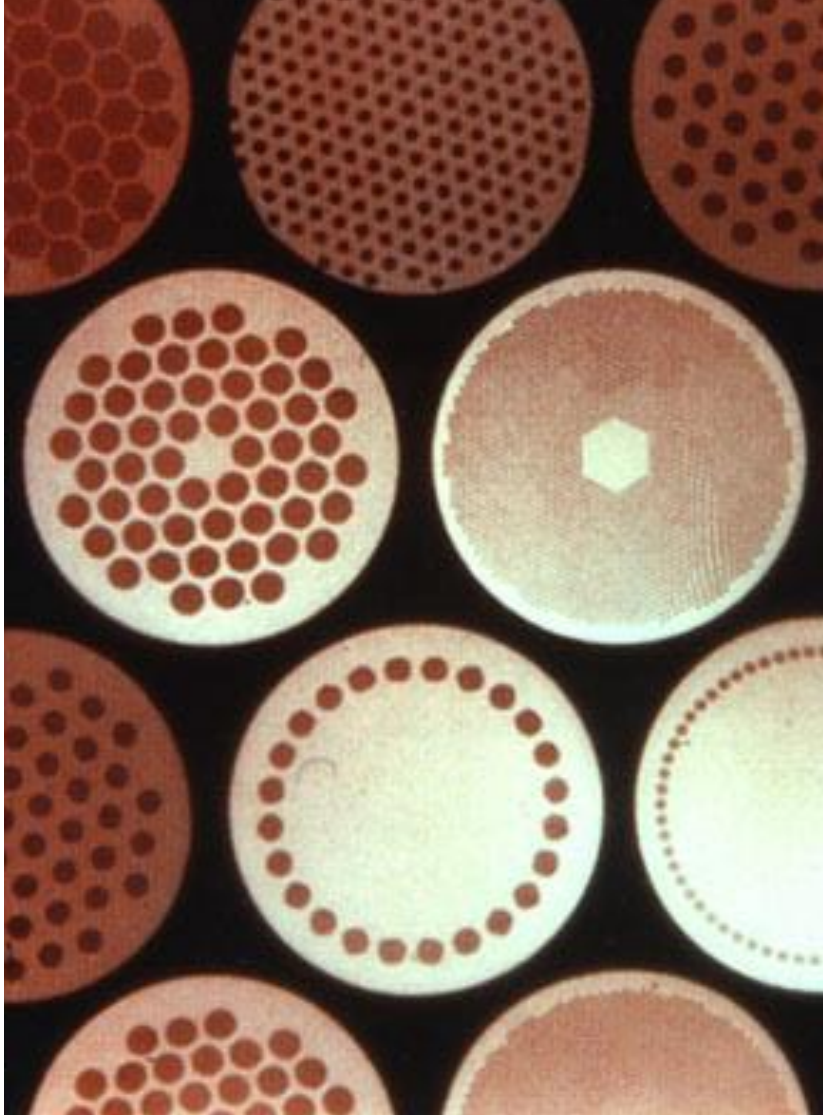All the rest are brittle intermetallic compounds

Critical field & temperature of metallic superconductors

To date, all superconducting accelerators have used NbTi.

Of the intermetallics, only Nb_3Sn has found significant use in magnets

Practical wires for magnets

- some 40 years after its development, NbTi is still the most popular magnet conductor, with Nb_3Sn being used for special high field magnets and HTS for some developmental prototypes.

- for reasons that will be described later, superconducting materials are always used in combination with a good normal conductor such as copper

- to ensure intimate mixing between the two, the superconductor is made in the form of fine filaments embedded in a matrix of copper

- typical dimensions are:
  - wire diameter = 0.3 - 1.0mm
  - filament diameter = 5 - 50µm

- for electromagnetic reasons, the composite wires are twisted so that the filaments look like a rope (see Lecture 3)

NbTi manufacture
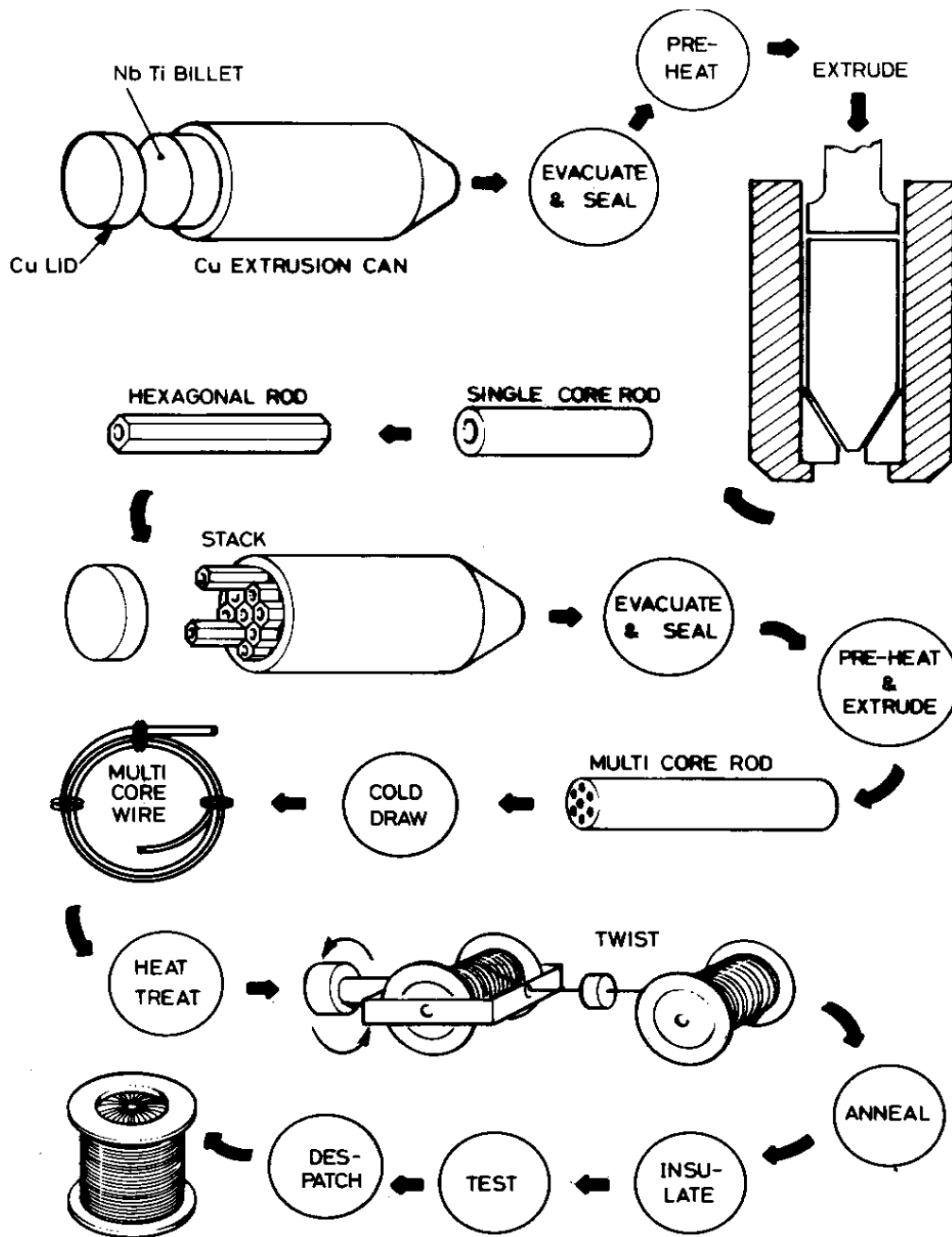
- vacuum melting of NbTi billets

- hot extrusion of the copper NbTi composite

- sequence of cold drawing and intermediate heat treatments to precipitate αTi phases as flux pinning centres

- for very fine filaments, must avoid the formation of brittle CuTi intermetallic compounds during heat treatment
  - usually done by enclosing the NbTi in a thin Nb shell

- twisting to avoid coupling - see lecture 2

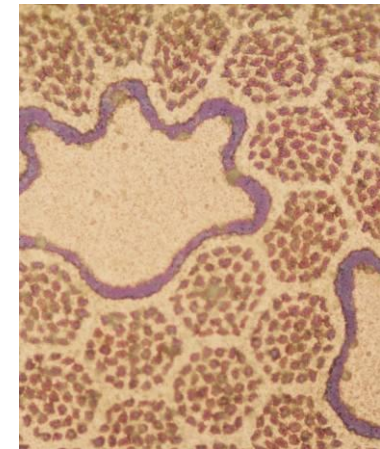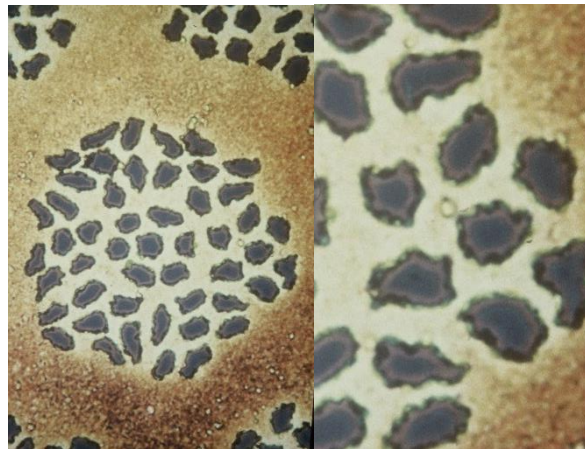# *Filamentary Nb_3Sn wire via the bronze route*

Nb_3Sn is a brittle material and cannot be drawn down.

Instead must draw down pure niobium in a matrix of bronze (copper tin)

At final size the wire is heated (~700C for some days) tin diffuses through the Cu and reacts with the Nb to form Nb_3Sn

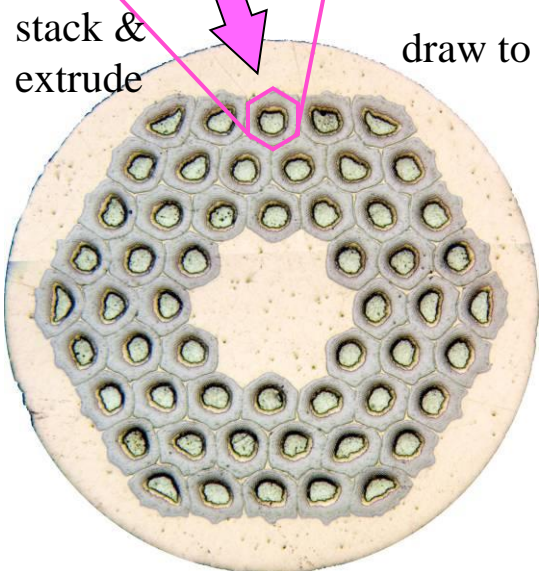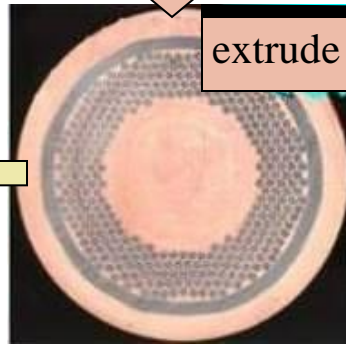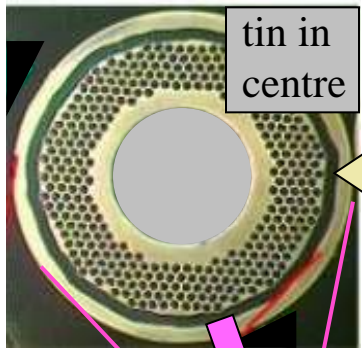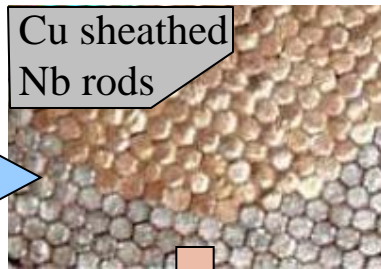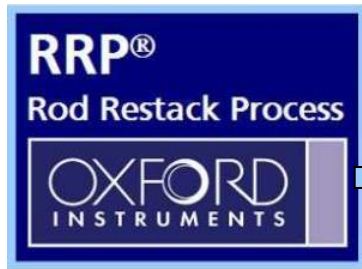The remaining copper still contains ~ 3wt% tin and has a high resistivity ~ $6\times10^{-8}\Omega$m.
So include 'islands' of pure copper surrounded by a diffusion barrier
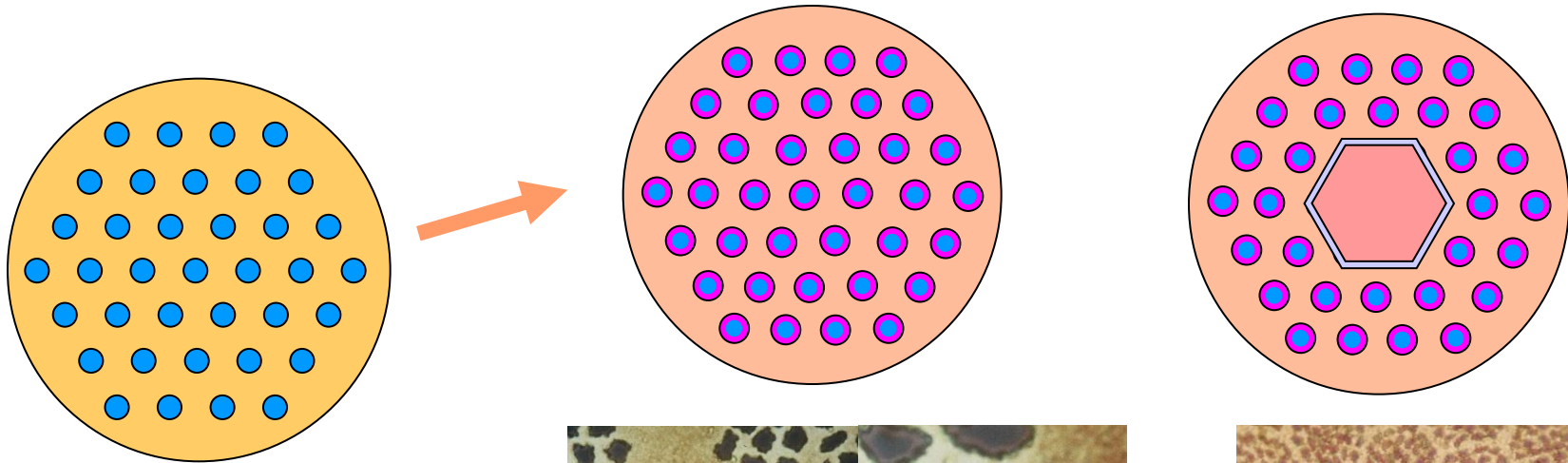
- *BUT maximum ductile bronze is ~13wt% tin,*
- *reaction slows at ~ 3wt%*
- *so low engineering J_c*

Nb_3Sn with higher engineering J_c

RRP®
Rod Restack Process
OXFORD INSTRUMENTS

Cu sheathed Nb rods

extrude

tin in centre

stack & extrude

draw to wire

heat treat to form 'macro filaments' of Nb_3Sn

SMI SHAPEMETAL INNOVATION B.V.

Powder in tube PIT

$NbSn_2$ powder
Cu jacket
Nb tube

stack & extrude
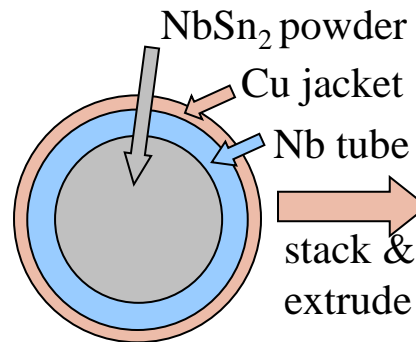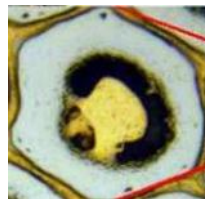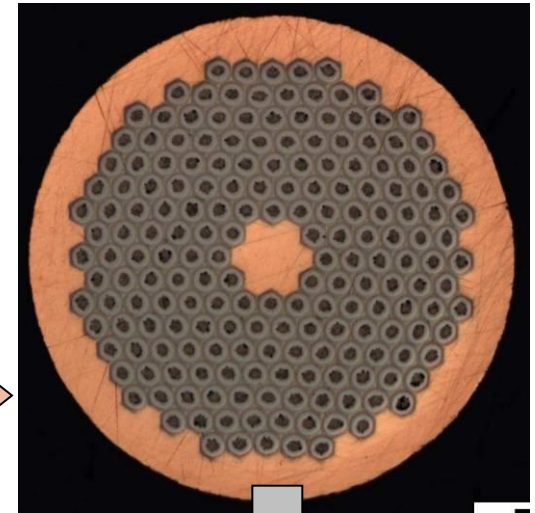
draw to wire

heat treat
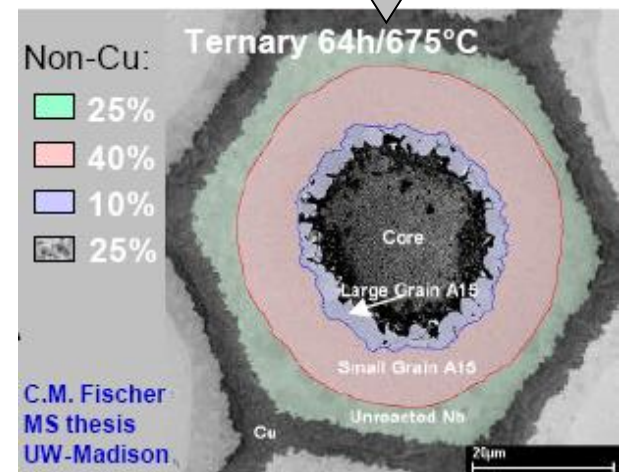
both make high J_{eng} (RRP is the highest)

but large filaments

Non-Cu:
- 25%
- 40%
- 10%
- 25%

Ternary 64h/675°C

Core
Large Grain A15
Small Grain A15
Unreacted Nb
Cu
20μm

C.M. Fischer
MS thesis
UW-Madison

Measurement of critical current

- spiral sample with current leads and voltage taps

- place in the bore of a superconducting solenoid

- put in cryostat

- immerse in liquid helium

- at each field level slowly increase the current is and measure the voltage across the test section
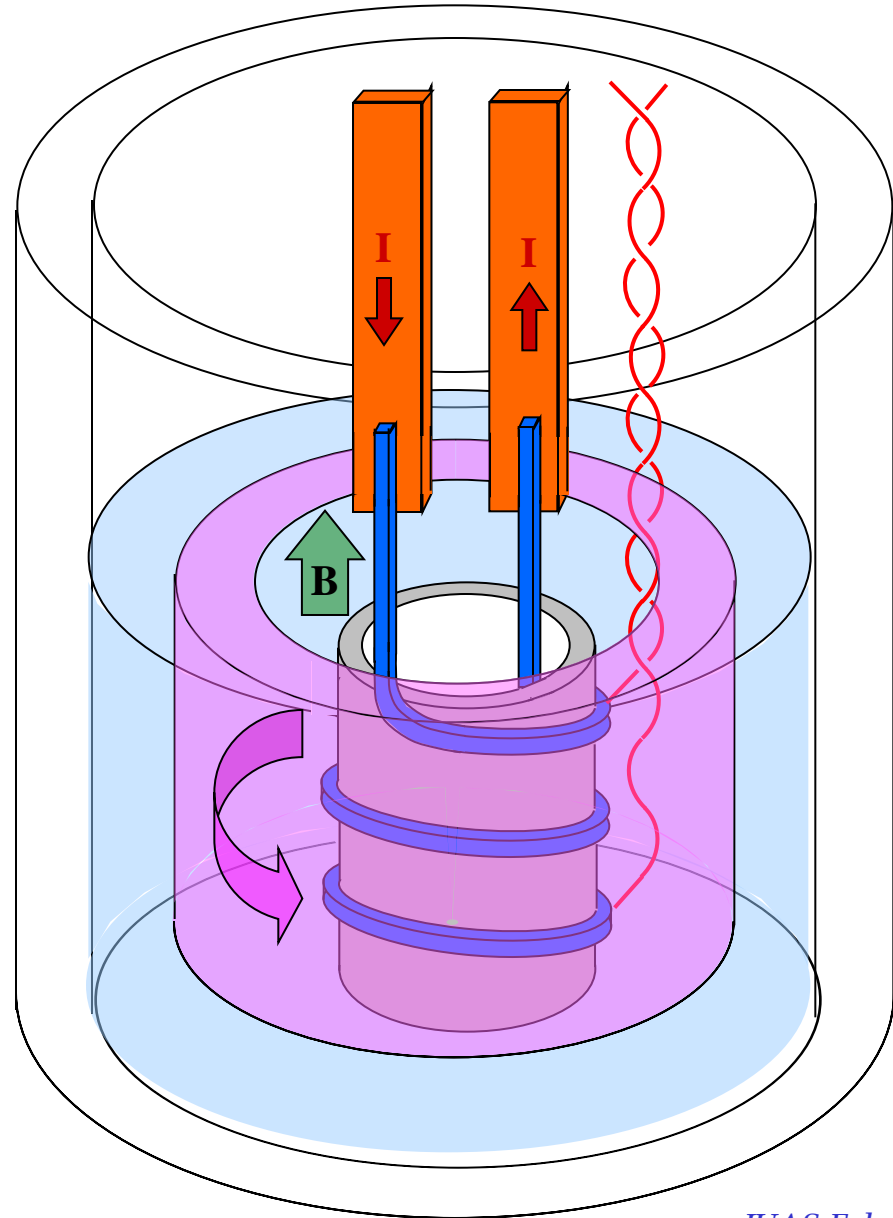
Resistive transition 1

When measured sensitively, the boundary between superconducting and resistive states is not sharp, but slightly blurred.

If we measure J_c with voltage taps across the sample, we see that the voltage rises gradually.

To define Jc, we must therefore define a measurement sensitivity in terms of electric field or effective resistivity.

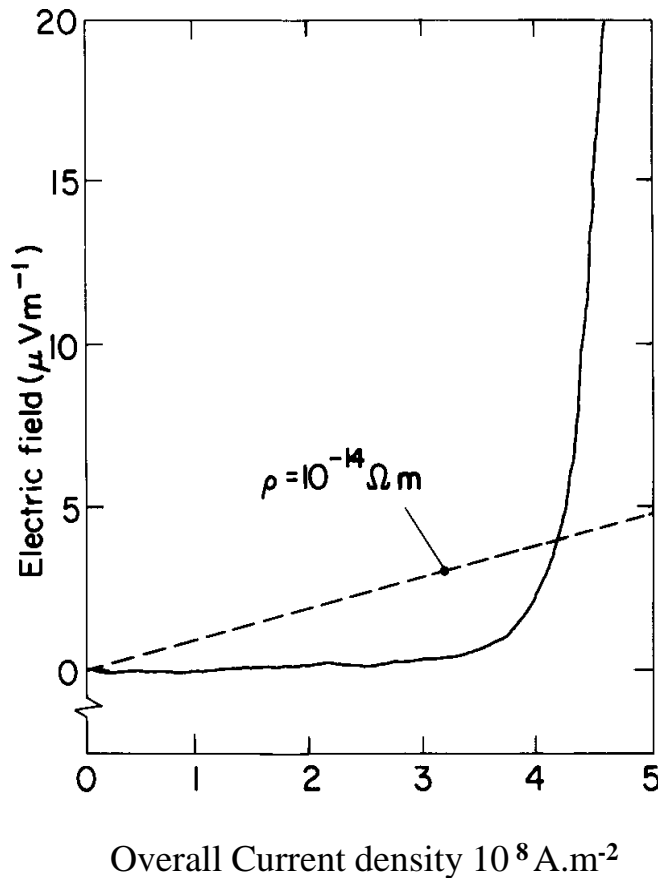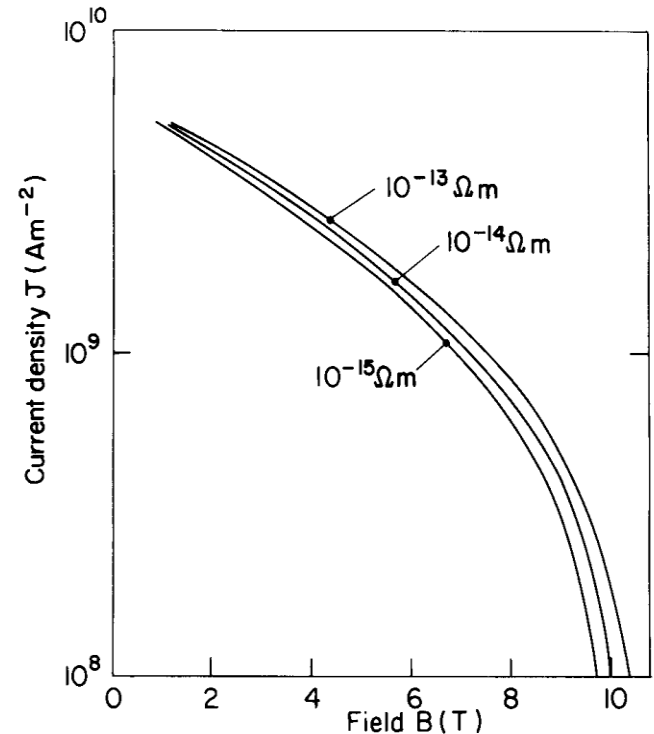Commonly used definitions are $\rho = \mathbf{10^{-14}\ \Omega m}$ or $\mathbf{E = 1\ \mu V.m^{-1}}$

Critical current defined at this level is about what you would expect the conductor in a resin impregnated solenoid to achieve. At higher resistivity, self heating would start to raise the internal temperature and reduce the critical current

Overall Current density 10^{8} A.m^{-2}

Resistive transition 2

It has been found empirically that the resistive transition may be represented by a power law

$$\rho(J) = \rho_o \left\{ \frac{J}{J_o} \right\}^n$$

where n is called the resistive transition index.

- the effect is partly within the filaments (flux flow) and partly between the filaments

- 'sausaging of the filaments, forces current to cross the copper matrix as critical current is approached.
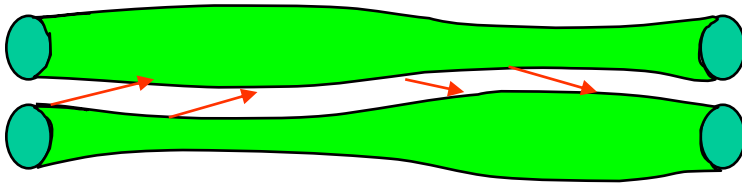
- resistive transition can be the main source of decay in persistent magnets

- 'n' is often taken as a measure of quality - look for n > 50

- HTS conductors so far have low n ~ 5 - 10

a) perfect filament
b) mid sausaging
c) bad sausaging
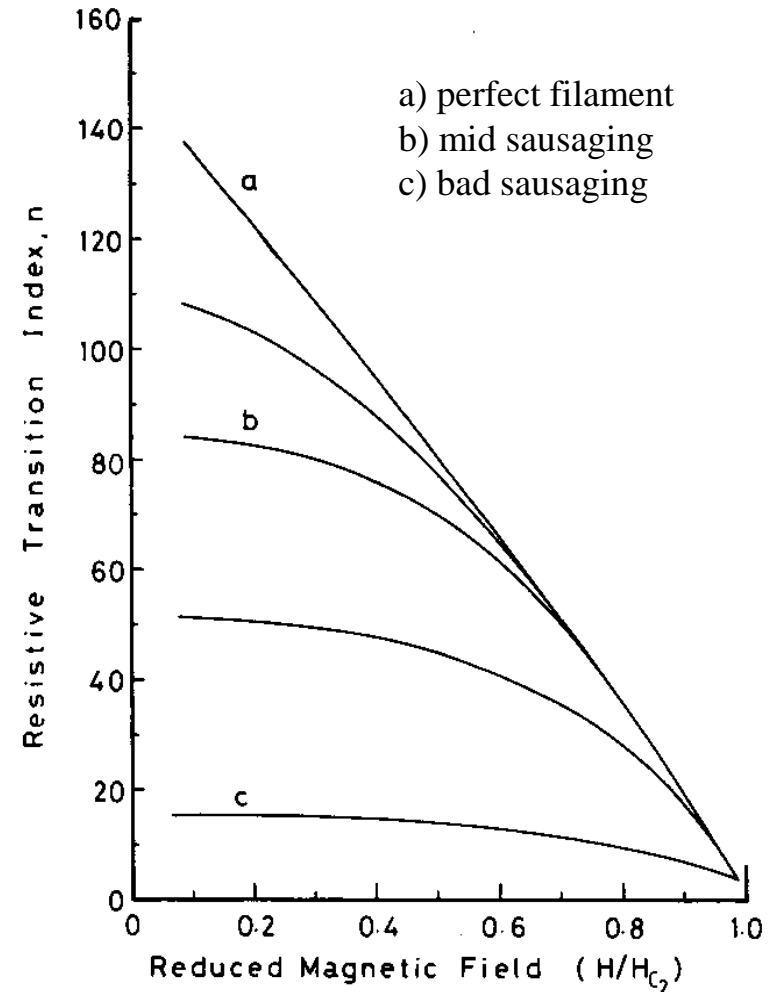
Conductors for accelerator magnets

single stack
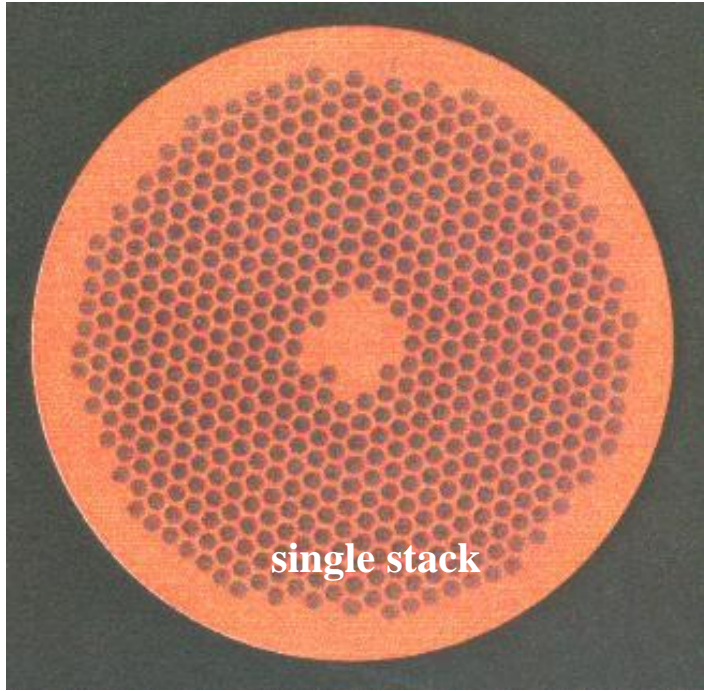
- to date, all superconducting accelerators have used NbTi superconductor.

- to control field errors and ac losses, the filaments must be < 10μm diameter (lectures 2 & 3)

double stack
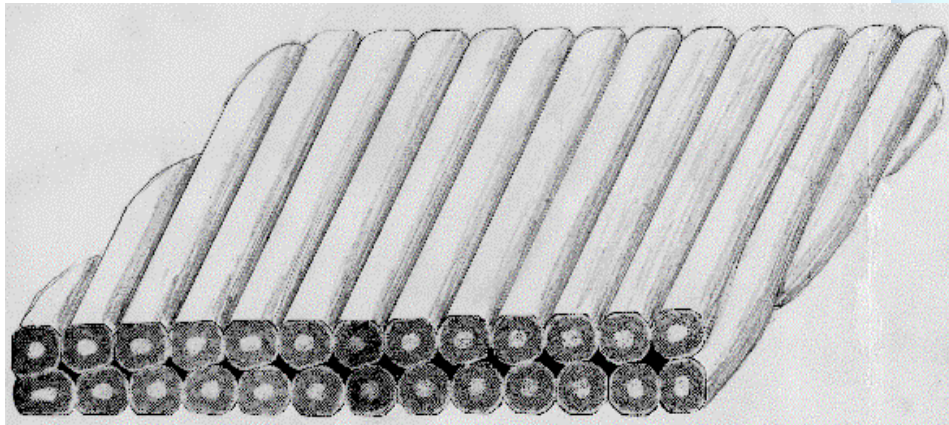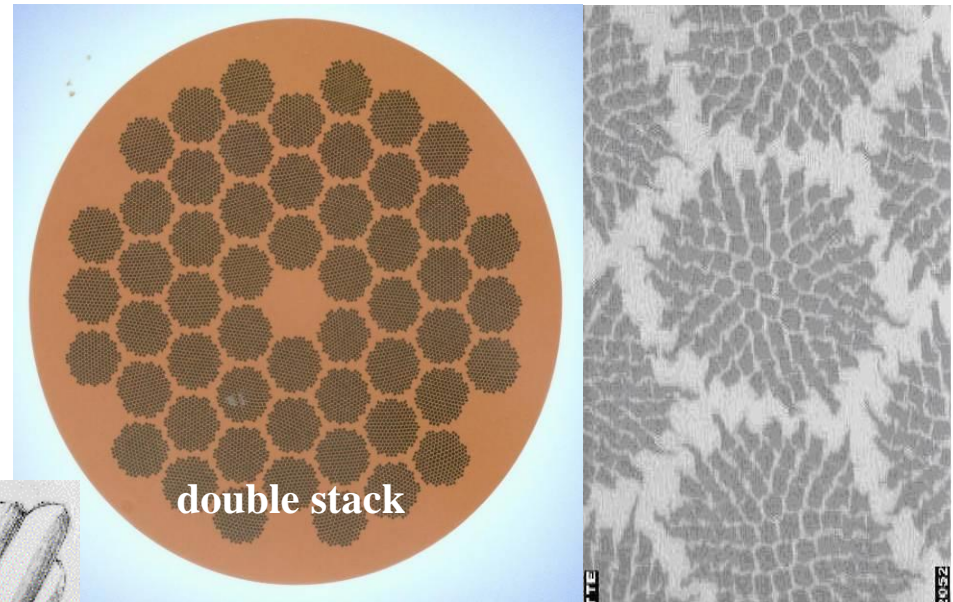
- to get the necessary high operating currents, many wires must be cabled together.

Engineering current density and filling factors

In magnet design, what really matters is the overall 'engineering' current density **J_{eng}**

Cu   NbTi   insulation

unit cell

J_{eng} = *current / unit cell area* = $J_{sup} \times \lambda$

where λ = filling factor of superconductor in winding

filling factor within the wire $\lambda_{wire} = 1 / (1+mat)$

where *mat* = matrix : superconductor ratio

typically:

for NbTi   *mat* = 1.2 to 3.0 ie λ_{sup} = 0.45 to 0.25

for Nb_3Sn *mat* = 2.0 to 4.0   ie λ_{sup} = 0.33 to 0.2

for B2212 *mat* = 3.0 to 4.0 ie λ_{sup} = 0.25 to 0.2

For Nb_3Sn and B2212 the area of superconductor is not well defined, so often define J_{sup} over 'non matrix' or 'non Cu' area, which is greater than superconductor area.

$\lambda_{winding}$ takes account of space occupied by insulation, cooling channels, reinforcement etc: typically ~ 0.7 to 0.8

over the winding $\lambda = \lambda_{sup} \times \lambda_{winding}$

So typically J_{eng} is only 15% to 30% of $J_{supercon}$
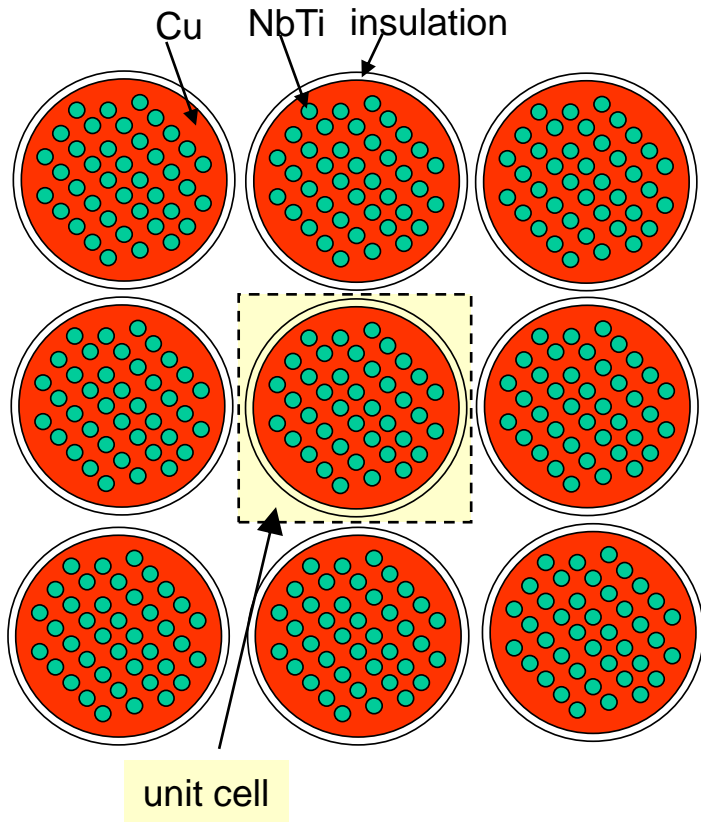
A century of critical temperatures

Woodstock of Physics 1987

Alex Mueller

Georg Bednortz

Paul Chu

B2223

YBCO

B2212

BaLaCuO

MgB_2

Nb_3Sn

Nb_3Ge

Nb

NbZr
NbTi

$PbMo_6S_8$

Pb

Hg

Sn

- critical temperature K (y-axis: 0, 20, 40, 60, 80, 100, 120, 140, 160)
- year (x-axis: 1910, 1930, 1950, 1970, 1990, 2010)
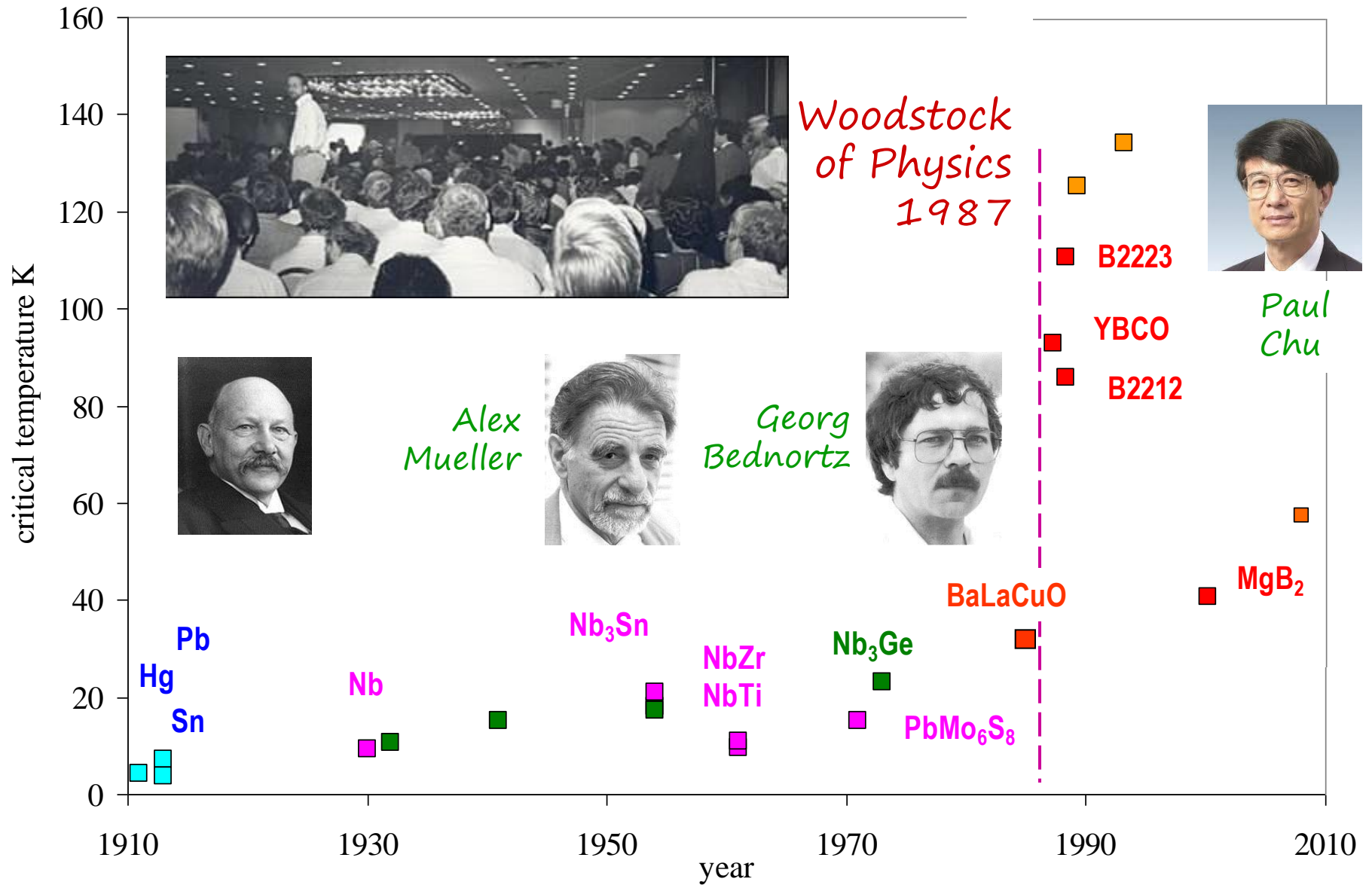
Wonderful materials for magnets

but for two problems

- **flux flow resistance**
- **grain boundary mismatch**

YBCO
B2223
B2212
PbMo$_6$S$_8$
Nb$_3$Sn
MgB$_2$
NbTi
NbZr
PbBi
MoRe
Nb

upper critical field (T)

year

1) Flux flow resistance

critical field B_{c2} T .

temperature K

YBCO

B2212

Nb₃Al

MgB₂

Nb₃Sn

NbTi

B2223

critical line

resistive

flux flow

irreversibility line

superconducting

flux pinning

Field

Temperature

V
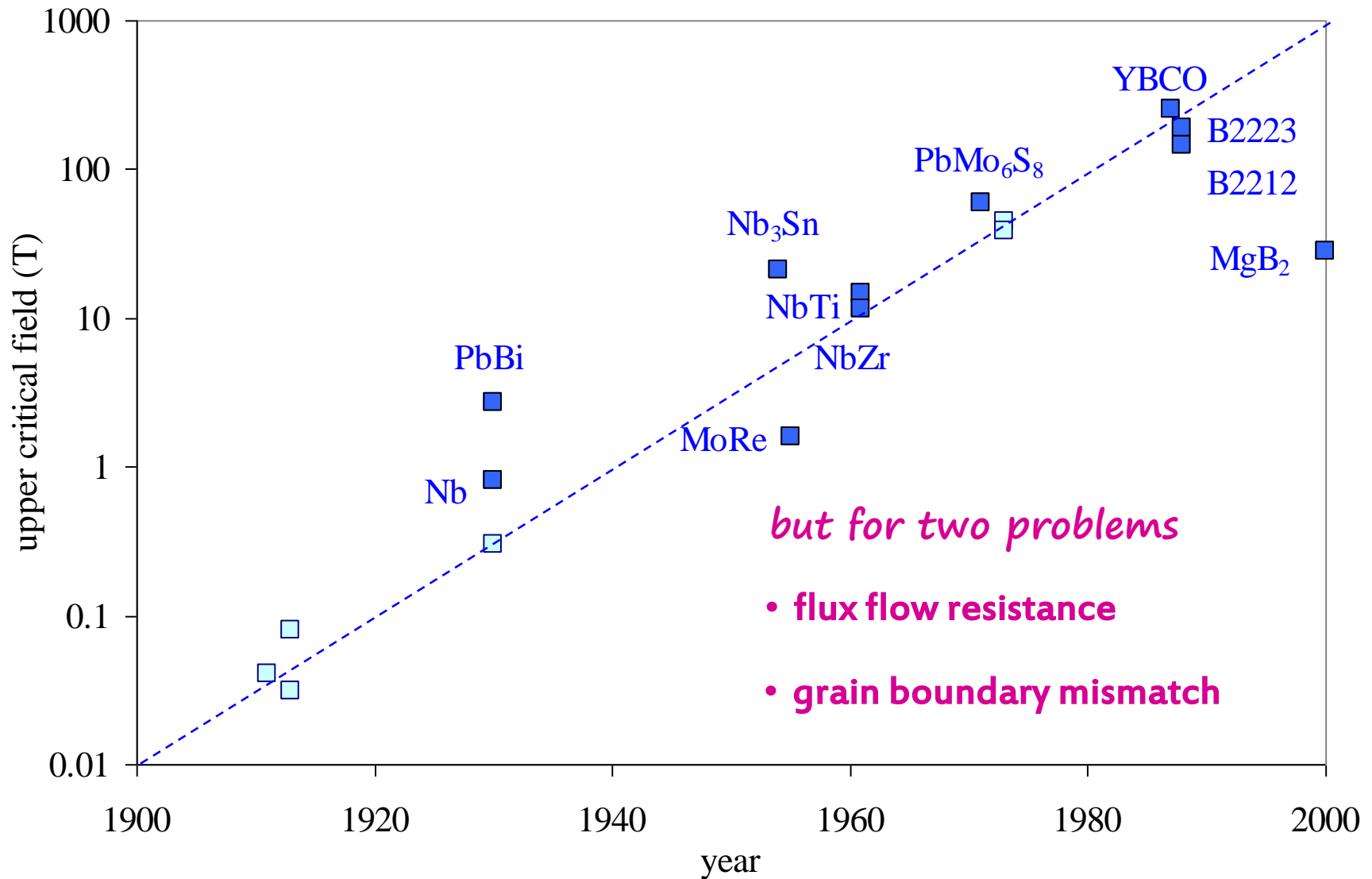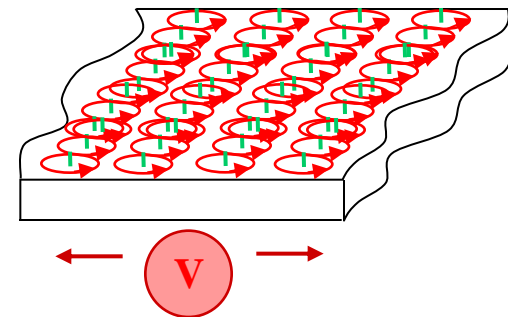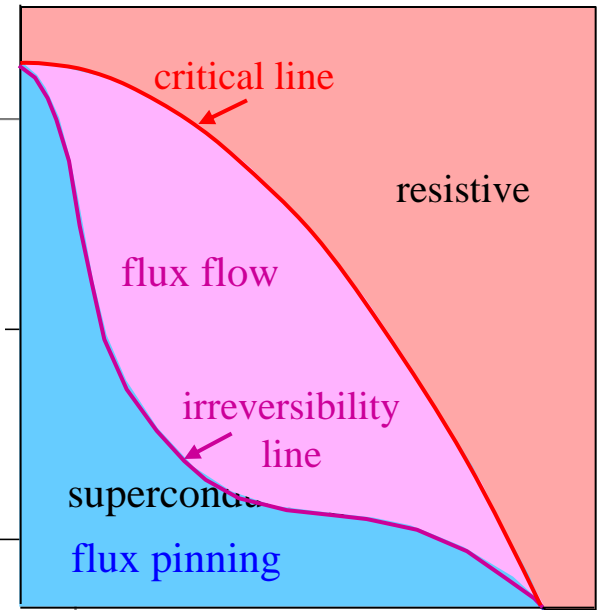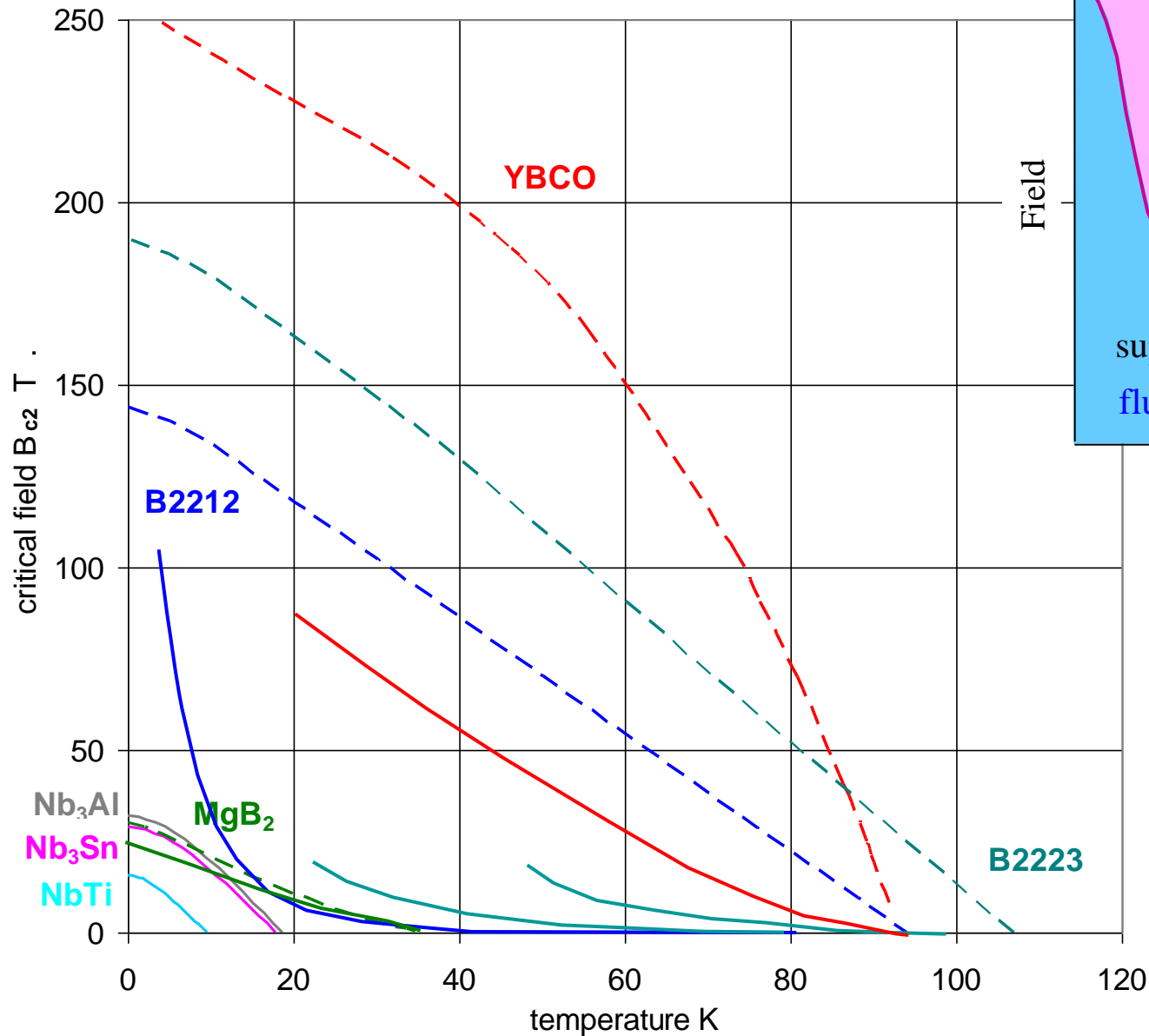
Accessible fields for magnets
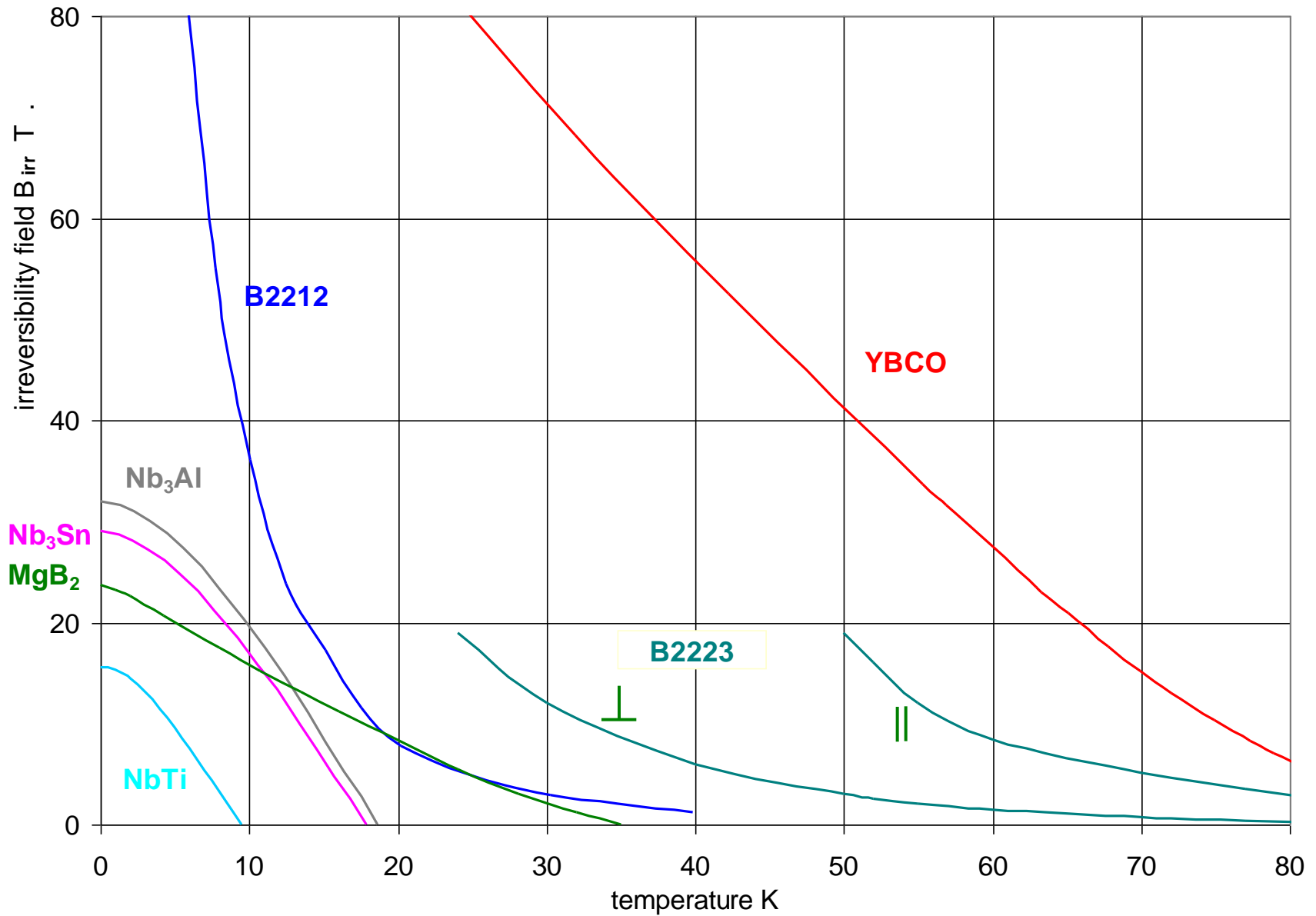
2) Grain boundary mismatch

- crystal planes in grains point in different directions

- critical currents are high within the grains

- J_c across the grain boundary depends on the misorientation angle

- For good J_c must align the grains to within a few degrees

*data on YBCO from Dimos et al Phys Rev Let **61** 219 (1988)*

bridge on grain A

bridge on grain boundary

bridge on grain B
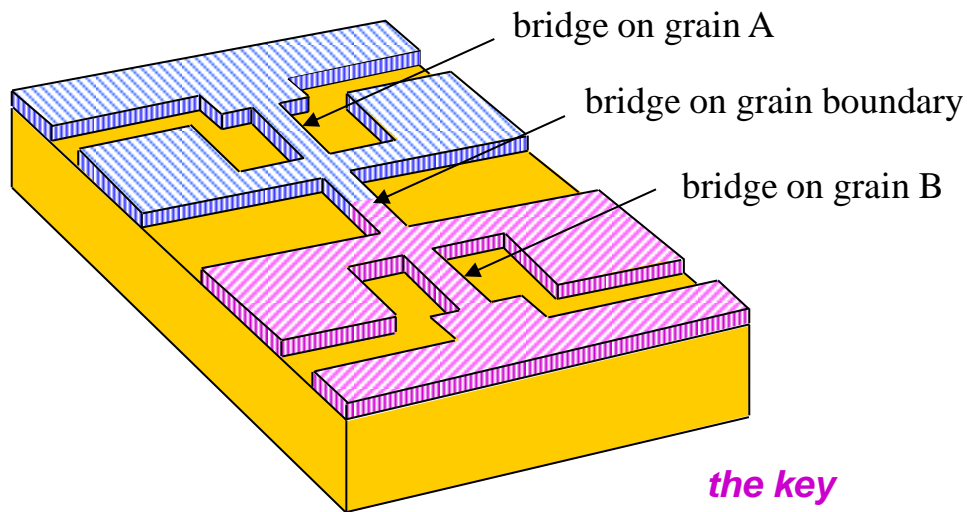
the key measurement of Dimos et al
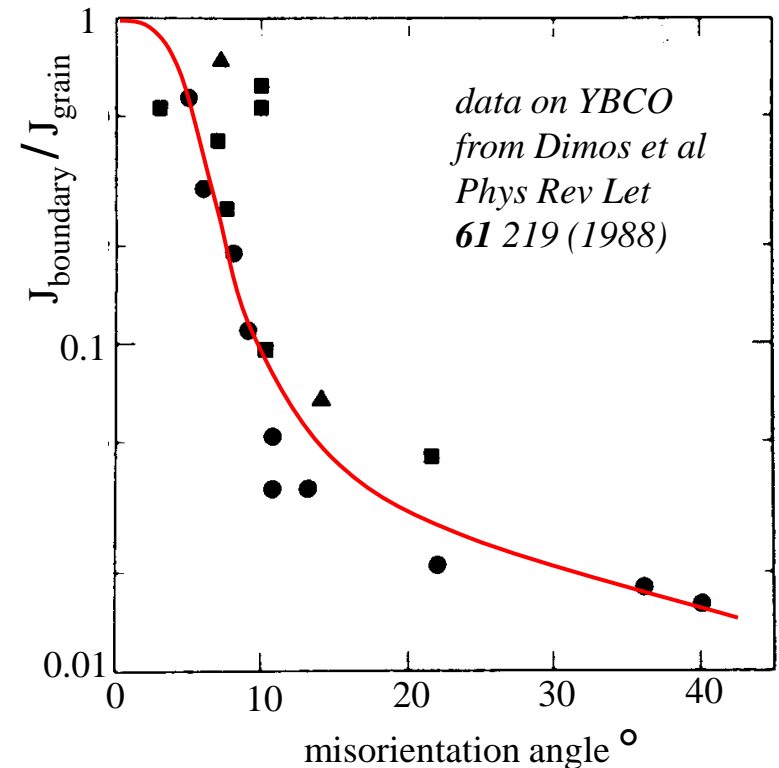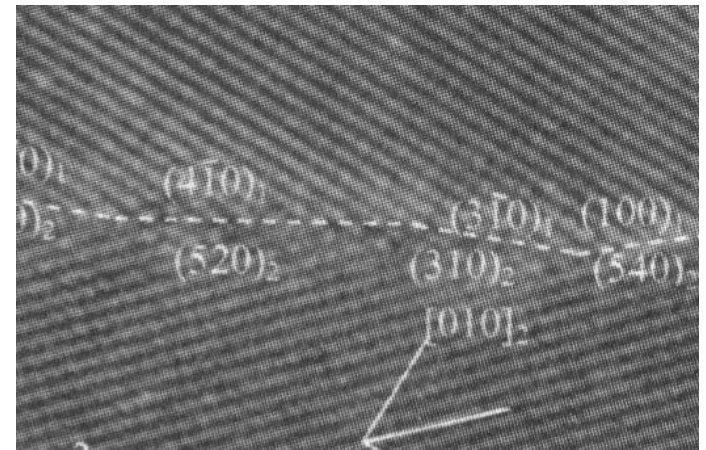
Production of BSCCo wires & tapes

B2212 wire

- draw down B2212 powder in silver tube

- restack, draw down round and heat treat

- grains align when processed with silver
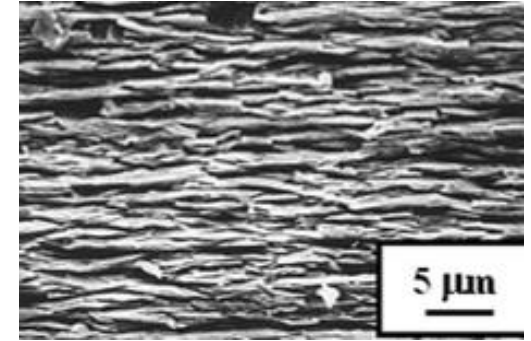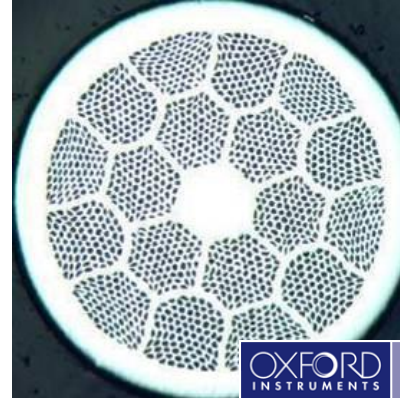
B2223 tape

- roll flat $\Rightarrow$ heat treat.....produces B2223 $\Rightarrow$ press flat $\Rightarrow$ heat treat …, fills voids, heals cracks, helps alignment
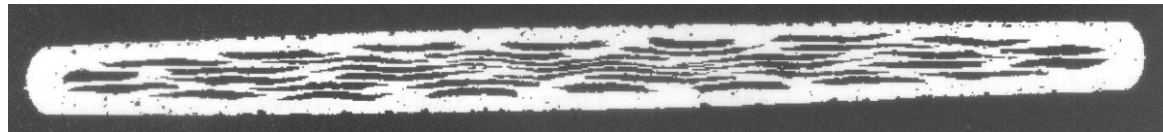
NST

- size ~ 4mm × 0.2mm, piece length ~ 1 - 2km, filling factor 25% - 40%

- can be made with gold alloy (low conductivity) matrix for current leads

- can be laminated with stainless steel foil to improve mechanical properties

but low irreversibility field/temperature

Coated YBCO tape

- YBCO has the best irreversibility field, but it is very sensitive to grain boundary misalignment

- the grains do not line up naturally - they must be persuaded

- deposit YBCO on a substrate where the grains are aligned and the lattice roughly matches YBCO
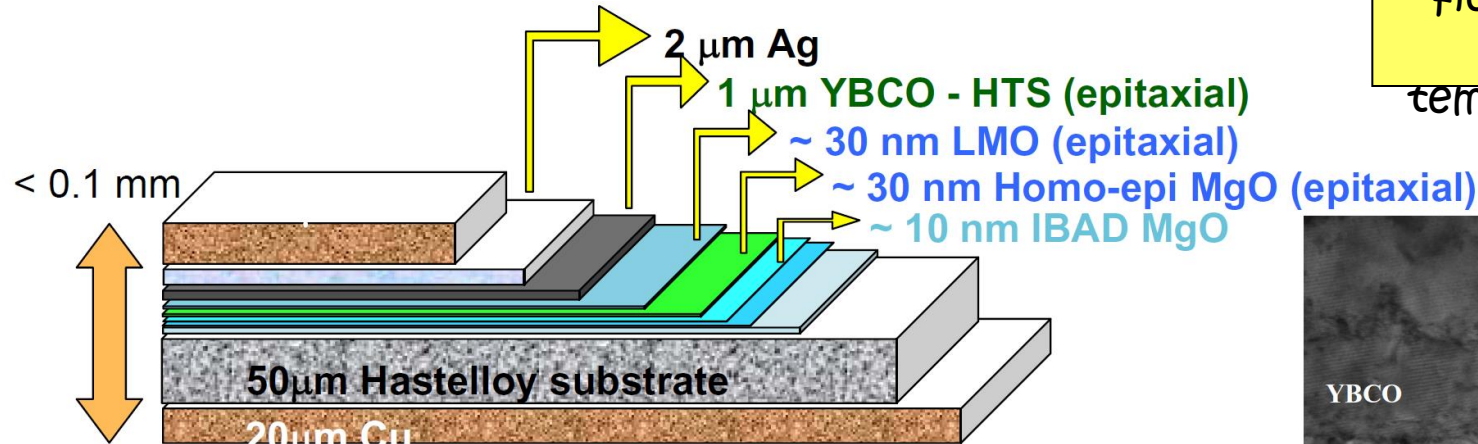
OK high field **and** high temperature

2 μm Ag
1 μm YBCO - HTS (epitaxial)
~ 30 nm LMO (epitaxial)
~ 30 nm Homo-epi MgO (epitaxial)
~ 10 nm IBAD MgO

< 0.1 mm

50μm Hastelloy substrate

20μm Cu

100 nm

YBCO

LaMnO₃

MgO (IBAD + Epi layer)

Y₂O₃

Al₂O₃

Hastelloy C-276

100 μm
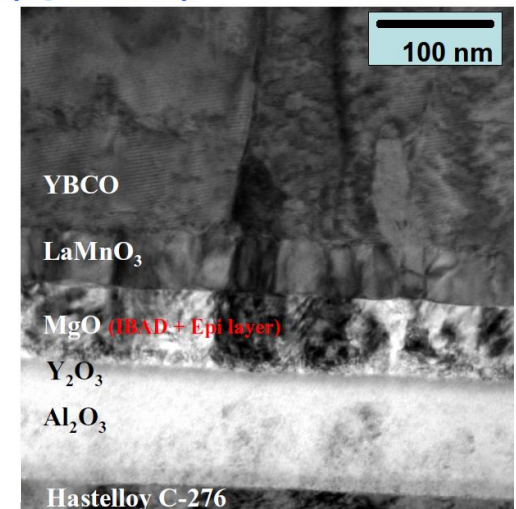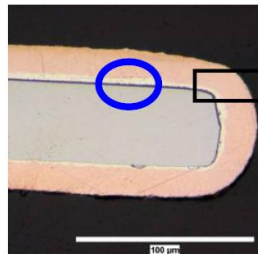
SuperPower Inc.

SuperPower Inc.

YBCO coated tape at **SuperPower** Inc.

IBAD

MOCVD

IBAD

Ag sputtering

Buffer

Buffer

2 μm Ag
1 μm YBCO - HTS (epitaxial)
~ 30 nm LMO (epitaxial)
~ 30 nm Homo-epi MgO
~ 10 nm IBAD MgO

50 μm Hastelloy substrate

20 μm Cu
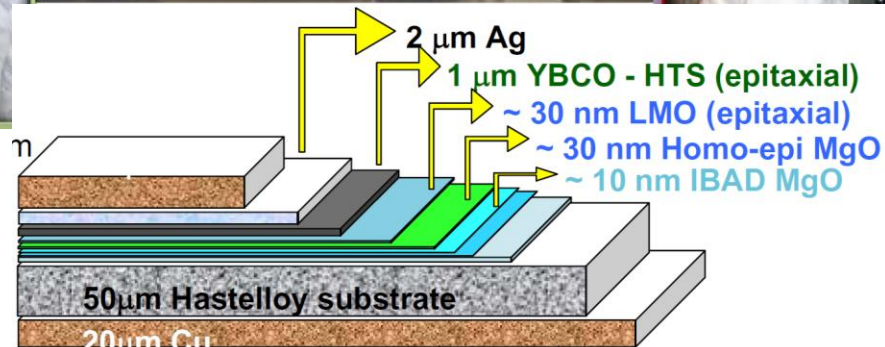
Lecture 1: concluding remarks

- superconductors allow us to build magnets which burn no power (except refrigeration)

- ampere turns are cheap, so don't need iron
  $\Rightarrow$ fields higher than iron saturation (but still use iron for shielding)

- performance of all superconductors described by the critical surface in **$B \ J \ \theta$** space,

- three kinds of superconductor
  - **type 1**: low temperature, unsuitable for high field
  - **type 2**: low temperature, good for high field - but must create flux pinning to get current density
  - **HTS**: high temperature, high field - but current density is still a problem

- NbTi is the most common commercial superconductor - standard production process

- Nb_3Sn has higher critical field & temperature - specialized commercial production

- BSCO high temperature **or** high field, but not both - prototype commercial production

- YBCO high temperature **and** high field, but must align the grains - prototype commercial production

- measure I_c to check specification, the index n indicates quality

- for accelerators, so far it's only been NbTi, usually in Rutherford cables

Some useful references

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- High Field Superconducting Magnets: FM Asner, pub Oxford University Press (1999) ISBN 0 19 851764 5
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- Proc Applied Superconductivity Conference: pub as IEEE Trans Applied Superconductivity, Mar 93 to 99, and as IEEE Trans Magnetics Mar 75 to 91
- Handbook of Applied Superconductivity ed B Seeber, pub UK Institute Physics 1998

Cryogenics

- Experimental Techniques for Low-temperature Measurements: J. W. Ekin Pub. Oxford University Press, ISBN 978-0-19-857054-7
- Helium Cryogenics Van Sciver SW, pub Plenum 86 ISBN 0-0306-42335-9
- Cryogenic Engineering, Hands BA, pub Academic Press 86 ISBN 0-012-322991-X
- Cryogenics: published monthly by Butterworths
- Cryogenie: Ses Applications en Supraconductivite, pub IIR 177 Boulevard Malesherbes F5017 Paris France

Materials Mechanical

- Materials at Low Temperature: Ed RP Reed & AF Clark, pub Am. Soc. Metals 1983. ISBN 0-87170-146-4
- Handbook on Materials for Superconducting Machinery pub Batelle Columbus Laboratories 1977.
- Nonmetallic materials and composites at low temperatures: Ed AF Clark, RP Reed, G Hartwig pub Plenum
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- Superconductivity of metals and Cuprates, JR Waldram, Institute of Physics Publishing (1996) ISBN 0 85274 337 8
- High Temperature Superconductors: Processing and Science, A Bourdillon and NX Tan Bourdillon, Academic Press, ISBN 0 12 117680 0
- Superconductivity: A Very Short Introduction by Stephen J. Blundell: Oxford University Press (2009) ISBN978-0-19-954090-7

on the Web

- **Lectures on Superconductivity** http://www.msm.cam.ac.uk/ascg/lectures.
  A series of lectures produced for SCENET by Cambridge University: fundamentals, materials, electronics, applications. Also available as a DVD

- **Superconducting Accelerator Magnets** http://www.mjb-plus.com.
  A course developed from SSC experience, available from website for $20

- www.superconductors.org website run by an enthusiast; gives some basic info and links

- **Superconductivity Course** at the (UK) Open University.
  http://openlearn.open.ac.uk/course/view.php?id=2397 Good coverage of basics.

- **Wikipedia** on Superconductivity http://en.wikipedia.org/wiki/Superconductivity
  Good on basics with lots of references and links.

- **European Society for Applied Superconductivity** http://www.esas.org/
  News, events and people in the area of applied superconductivity

- **CONECTUS** Consortium of European Companies determined to use Superconductivity
  http://www.conectus.org/

- **IEEE Council on Superconductivity** http://www.ewh.ieee.org/tc/csc/
  News, events and people in the area of applied superconductivity (US based)

Materials data on the Web

- Cryogenic properties (1-300 K) of many solids, including thermal conductivity, specific heat, and thermal expansion, have been empirically fitted and the equation parameters are available free on the web at **www.cryogenics.nist.gov**

- Thermodynamic properties of gases (and liquids) available free as a programme which you can interrogate for your own temperature interval etc.
  http://webbook.nist.gov/chemistry/fluid/

- Plots and automated data-look-up using the NIST equations are available on the web for a fee from **www.cpia.jhu.edu**

- Other fee web sites that use their own fitting equations for a number of cryogenic material properties include: **www.cryodata.com** (cryogenic properties of about 100 materials), and **www.jahm.com** (temperature dependent properties of about 1000 materials, many at cryogenic temperatures).

- Commercially supplied room-temperature data are available free online for about 10 to 20 properties of about 24,000 materials at **www.matweb.com**

thanks to Jack Ekin of NIST and Charles Monroe for this information

Cryodata Software Products

GASPAK
properties of pure fluids from the triple point to high temperatures.

HEPAK
properties of helium including superfluid above 0.8 K, up to 1500 K.

STEAMPAK
properties of water from the triple point to 2000 K and 200 MPa.

METALPAK, CPPACK, EXPAK
reference properties of metals and other solids, 1 - 300 K.

CRYOCOMP
properties and thermal design calculations for solid materials, 1 - 300 K.

SUPERMAGNET
four unique engineering design codes for superconducting magnet systems.

KRYOM
numerical modelling calculations on radiation-shielded cryogenic enclosures.