

Joint Universities Accelerator School

JUAS 2014

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Normal-conducting accelerator magnets

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CERN



Lecture 4: Magnet production



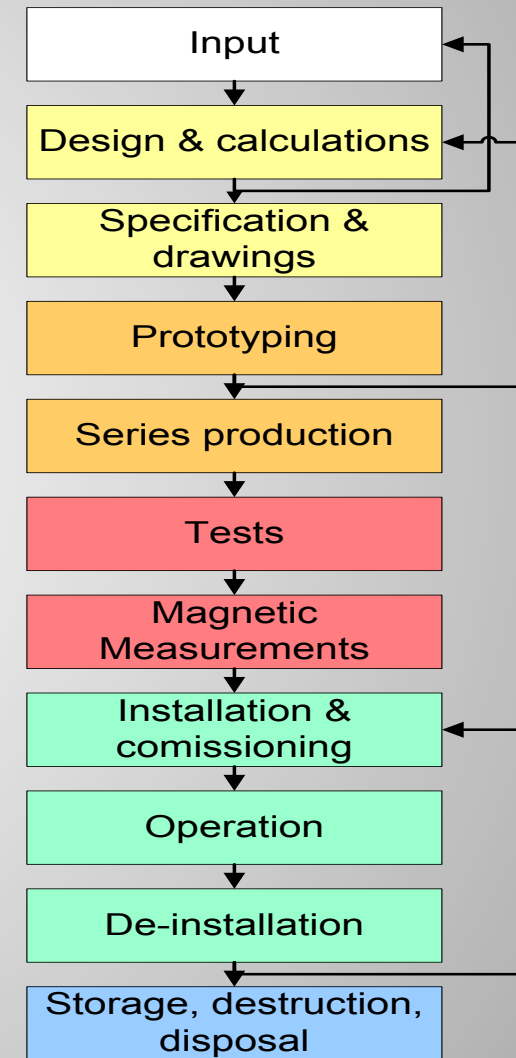
Cost estimates and optimization

Magnetic materials

Manufacturing techniques

- Yoke manufacturing
- Coil manufacturing

Assembly and auxiliary equipment





Cost estimate



Production specific tooling:

5 to 15 k€/tooling

Material:

Steel sheets: 1.0 - 1.5 € /kg

Copper conductor: 10 to 20 € /kg

Yoke manufacturing:

Dipoles: 6 to 10 € /kg (> 1000 kg)

Quads/Sextupoles: 50 to 80 € /kg (> 200 kg)

Small magnets: up to 300 € /kg

Coil manufacturing:

Dipoles: 30 to 50 € /kg (> 200 kg)

Quads/Sextupoles: 65 to 80 € /kg (> 30 kg)

Small magnets: up to 300 € /kg

Contingency:

10 to 20 %

Magnet	Magnet type	Dipole
	Number of magnets (incl. spares)	18
	Total mass/magnet	8330 kg
Fixed costs	Design	14 kEuros
	Punching die	12 kEuros
	Stacking tool	15 kEuros
	Winding/molding tool	30 kEuros
Yoke	Yoke mass/magnet	7600 kg
	Used steel (incl. blends)/magnet	10000 kg
	Yoke manufacturing costs	8 Euros/kg
	Steel costs	1.5 Euros/kg
Coil	Coil mass/magnet	730 kg
	Coil manufacturing costs	50 Euros/kg
	Cooper costs (incl. insulation)	12 Euros/kg
Total costs	Total order mass	150 Tonnes
	Total fixed costs	71 kEuros
	Total Material costs	428 kEuros
	Total manufacturing costs	1751 kEuros
	Total magnet costs	2250 kEuros
	Contingency	20 %
	Total overall costs	2700 kEuros

NOT included: magnetic design, supports, cables, water connections, alignment equipment, magnetic measurements, transport, installation

Prices for 2011



Cost estimate



Fixed costs		
Punching die [k€]	$\approx 25 \sqrt{\frac{Y_{cs}}{N_{ys}}}$	Ycs: yoke cross section SxH [m ²] Nys: number of yoke segments
Stacking tool [k€]	$\approx 8 \sqrt{\frac{Y_{mass}}{N_{ys}}} 10^{-3}$	Ymass: yoke mass [kg] Nys: number of yoke segments
Winding tool [k€]	$\approx 12 \text{ HTL}$	HTL – half turn length [m]
Impregnation mold [k€]	$\approx 400 \text{ CoilV}$	CoilV – volume of one coil [m ³]
Manufacturing costs		
Yoke manufacturing [k€] per magnet	$\approx 16 \cdot N_{ys} \sqrt{\frac{Y_{mass}}{N_{ys}}} 10^{-3}$	Ymass: yoke mass [kg] Nys: number of yoke segments
Coil manufacturing [k€] per magnet	if CoilMass ≥ 0.5 kg: $\approx 0.8 \cdot N_{coil} (\sqrt{2 \cdot \text{CoilMass}} - 0.945 \sqrt[3]{\text{CoilMass}})$ if CoilMass < 0.5 kg: $\approx 0.4 \cdot N_{coil} \cdot \text{CoilMass}$	CoilMass: mass of one coil [kg] Ncoil: number of coils/magnet
Magnet assembly [k€] per magnet	$\approx 0.25 \sqrt{\text{MagMass}}$	MagMass: magnet mass [kg]

Source: D. Tommsini, CERN (empiric formulas based on recently completed magnet projects at CERN)

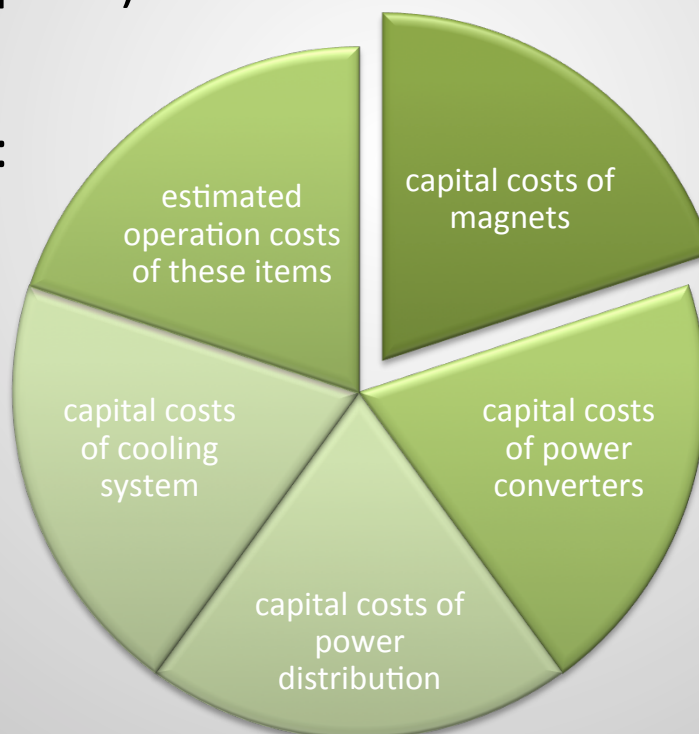


Cost optimization

Focus on economic design!

Design goal: Minimum total costs over projected magnet life time by optimization of capital (investment) costs against running costs (power consumption)

Total costs include:





Magnet procurement



Some questions to be answered:

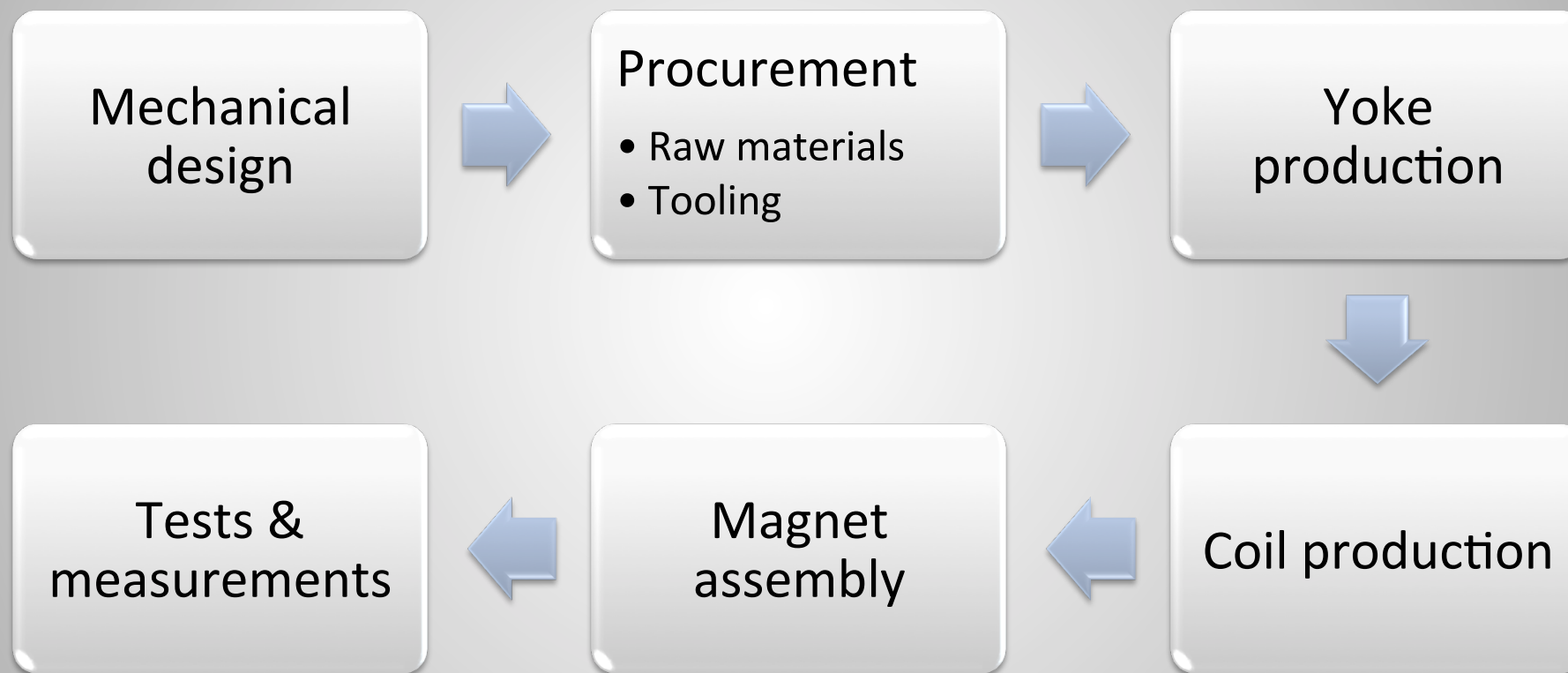
- to which detail shall the magnet be defined and specified?
- who will be responsible for the final magnetic performance: the client or the magnet manufacturer?
- who will do the detailed magnetic, electrical, and mechanical design?
- who will perform the acceptance tests?
- who will perform the magnetic measurements and which measurement technology is suitable?
- where does the responsibility of the magnet manufacturer start, where does it end?

Depending on the above choices, the scope of the supply needs to be sufficiently defined in a Specification

Low level of specified details	High level of specified details
Functional/performance specification	Technical specification with manufacturing drawings
Main responsibility with magnet manufacturer	Main responsibility with client



Magnet manufacturing

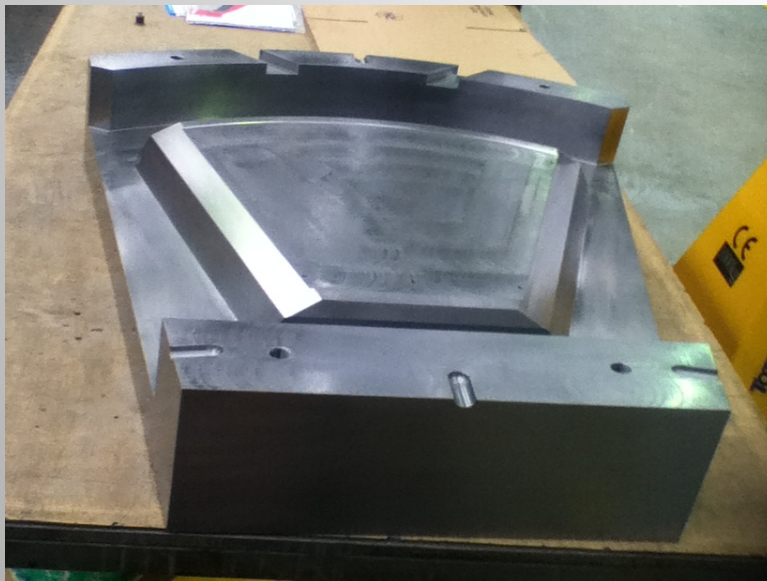




Massive or laminated yokes

Historically, the primary choice was whether the magnet is operated in persistent mode or cycled (**eddy currents**)

- + no stamping, no stacking
- + less expensive for prototypes and small series
- time consuming machining, in particular for complicated pole shapes
- difficult to reach similar magnetic performance between magnets
- + steel sheets less expensive than massive blocks (cast ingot)
- + less expensive for larger series
- + steel properties can be easily tailored
- + uniform magnetic properties over large series
- expensive tooling





Magnetic steel



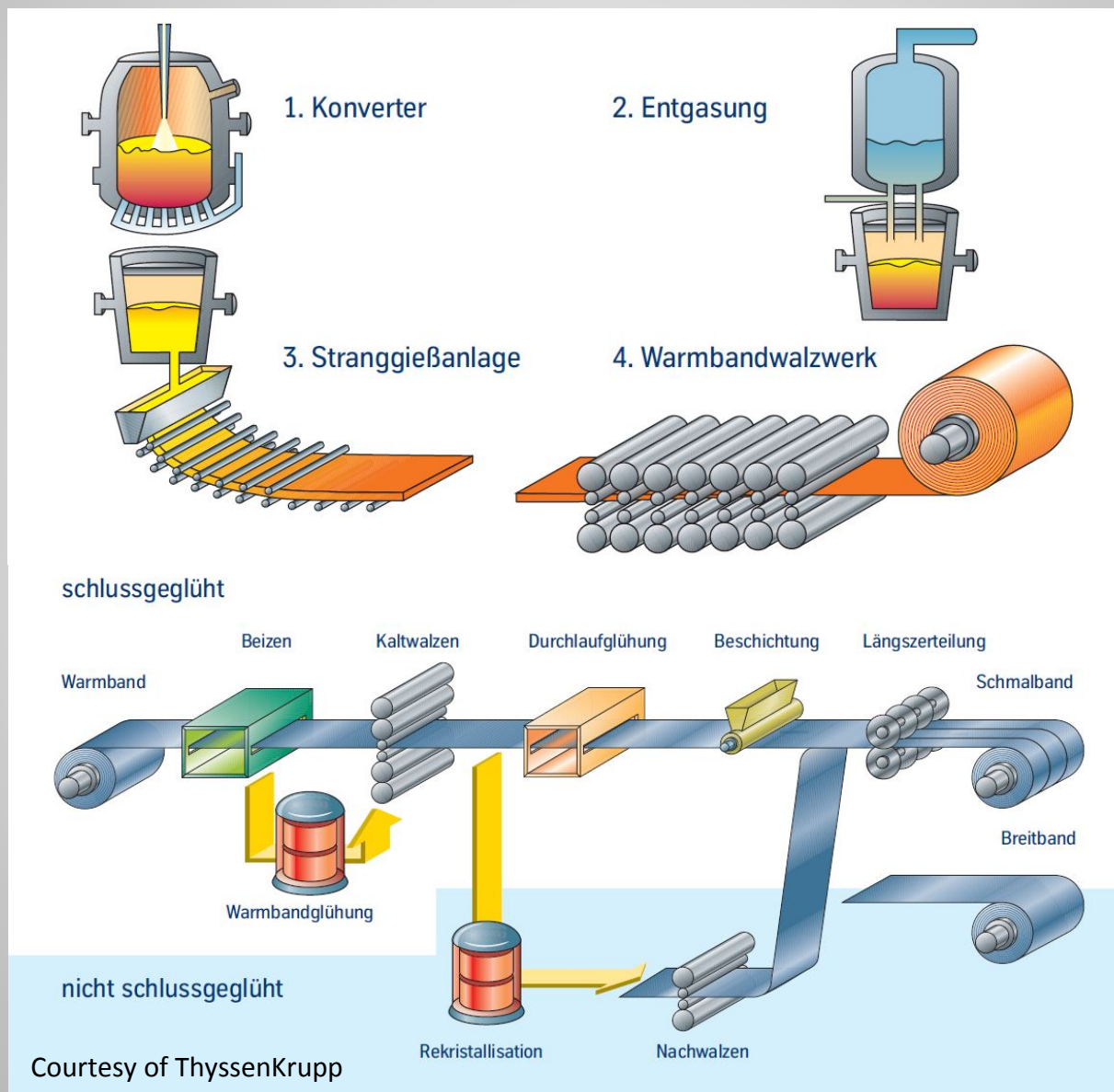
Today's standard: cold rolled, non-oriented electro-steel sheets (EN 10106)

- Magnetic and mechanical properties can be adjusted by final annealing
- Reproducible steel quality even over large productions
- Magnetic properties (permeability, coercivity) within small tolerances
- Homogeneity and reproducibility among the magnets of a series can be enhanced by selection, sorting or shuffling
- Organic or inorganic coating for insulation and bonding
- Material is usually cheaper, but laminated yokes are labour intensive and require more expensive tooling (fine blanking, stacking)





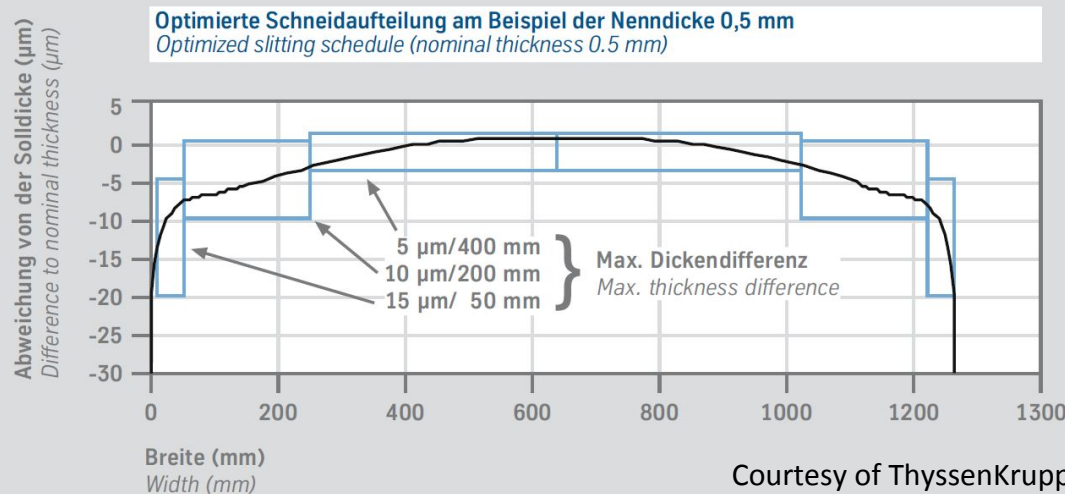
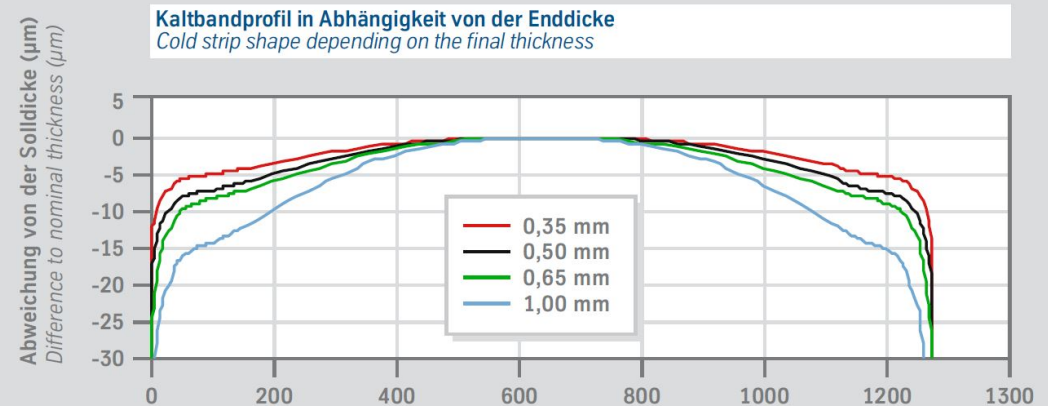
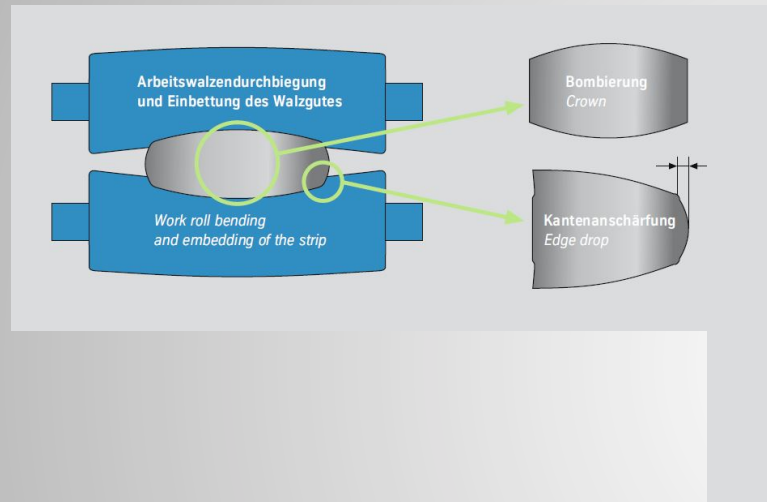
NGO Steel manufacturing



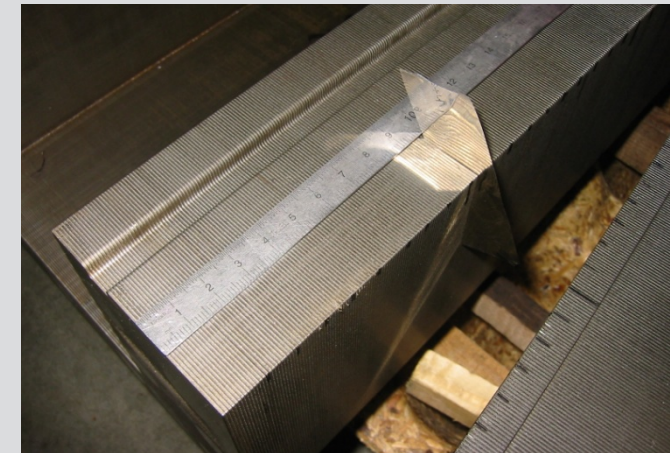


Profile of steel strips

The rolling process produces a thickness variation perpendicular to the rolling direction:



Courtesy of ThyssenKrupp



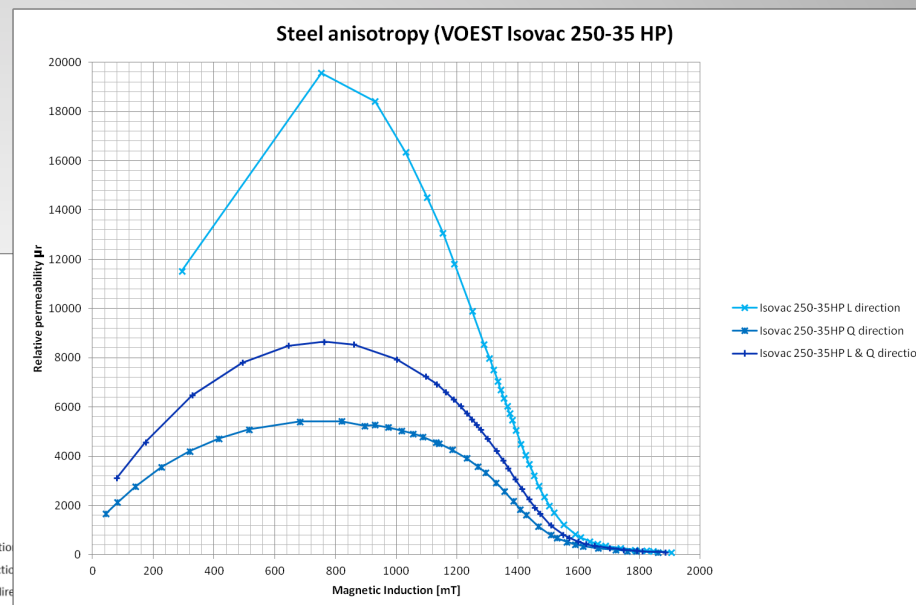
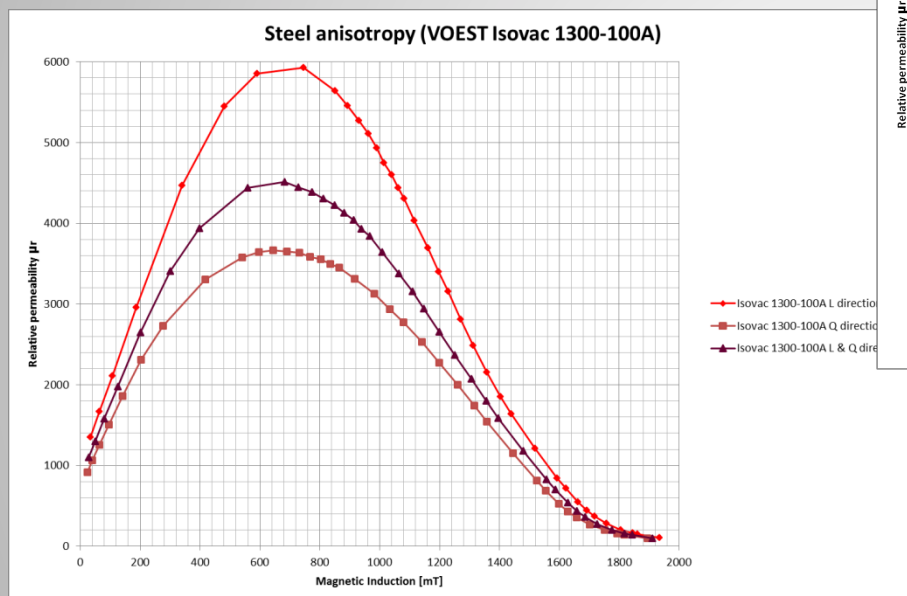
Courtesy of ThyssenKrupp



NGO steel properties



ISOVAC 1300-100A: $H_c = 65 \text{ A/m}$



ISOVAC 250-35HP: $H_c = 30 \text{ A/m}$

Sheet thickness:
 $0.3 \leq t \leq 1.5 \text{ mm}$

Specific weight:
 $7.60 \leq \delta \leq 7.85 \text{ g/cm}^3$

Electr. resistivity @20°C:
 $0.16 \text{ (low Si)} \leq \rho$
 $\leq 0.61 \text{ } \mu\Omega\text{m (high Si)}$



Sheet insulation



Surface coating:

- electrical insulation of several μm thickness
- one or both sides
- oxid layer, phosphate layer, organic or inorganic coating

Insulation designation IEC 60404-1-1	Insulation type	Color ¹⁾	Coating	Coating thickness each side in μm	Insulation resistance at room temperature to ASTM A717/A717M-95 $\Omega\text{m}^2/\text{Lamelle}$
STABOLIT 10 EC-3 by prior arrangement only	organic	yellow-green	both sides	max. 1.5	> 15
STABOLIT 20 EC-5-P	inorganic with organic components	grey-green	both sides	0.5 – 1.5	> 5
STABOLIT 30 EC-5-P	inorganic with organic components	light grey	both sides	0.5 - 1.5	> 5
STABOLIT 40 EC-6	organic pigmented	grey	one or both sides	3.0 - 5.0 4.0 - 7.0 6.0 - 9.0	> 90
STABOLIT 60 EC-5	inorganic with organic components pigmented	grey	both sides	0.3 - 1.0 1.0 - 2.0 2.0 - 3.5	> 5 > 15 > 50
STABOLIT 70	organic bonding lacquer (active)	colorless	one or both sides	5.0 - 8.0	-
Combined insulation	organic bonding lacquer with one side heat treatment (passive)	colorless	both sides	active 5.0 - 8.0 passive max. 1.5	-

Source: ThyssenKrupp



Steel specification



For MedAustron, the following steel parameters have been specified (and achieved)

Material thickness:

<i>Parameter</i>	<i>Value</i>	<i>Unit</i>
Nominal thickness of steel strips	1.00	mm
Max. deviation from nominal thickness	± 0.03	mm
Max. thickness variation in rolling direction	0.004	mm/2 m
Max. thickness variation perpendicular to rolling direction*)	0.007	mm

*) over a width of 1100 mm

Mechanical/electrical properties:

<i>Parameter</i>	<i>Value</i>	<i>Unit</i>
Electrical resistivity	0.13	μΩm
Density	7.800	g/cm ³
Tensile strength R _m	380 ± 10	MPa
Yield strength Re _h	270 ± 20	MPa
Hardness HV5	138 ± 5	
Surface roughness R _a	0.4 – 0.9	μm

Magnetic properties:

<i>Parameter</i>	<i>Value</i>	<i>Unit</i>
Average coercivity	70 ± 2	A/m
Permeability spread at 500 A/m (~1.45 T)	± 1	%

Surface coating:

<i>Parameter</i>	<i>Value</i>	<i>Unit</i>
Coating thickness	4 - 6	μm
Bonding strength of coating (DIN 53262)	> 6	N/mm ²
Surface resistance of coating in B-stage	> 1000	Ω cm



Other magnetic materials

1. High purity irons

- Iron referred to as "high purity" when total concentration of impurities (mainly C, N, O, P, S, Si and Al) does not exceed a few hundred ppm
- Otherwise Low Carbon Steel or Non-alloyed Steel
- Very pure Fe: high electrical conductivity → not suitable for AC applications
- For high permeability at $B > 1.2$ T it is advisable to anneal at max. 800 °C and cool slowly

2. Low-Carbon Steels

- e.g. type 1010
- Disadvantage: Magnetic ageing (increase of coercivity with time)

3. Non-grain oriented Silicon Steels (NGO)

Advantages:

- Increase in permeability
- Decrease in hysteresis loss
- Eddy current loss decrease due to higher resistivity (Al and Mn added as well)
- No ageing

4. Grain-oriented Silicon Steels

5. Iron alloys

- a. Iron-Nickel
- b. Iron-Cobalt alloys with high magnetic saturation

6. Compressed powdered Iron and Iron alloys

7. Ferrites

8. Innovative materials and rare earths

Reference: S. Sgobba: Physics & Measurements of Magnetic Materials, CAS 2009, Brugges



Yoke manufacturing

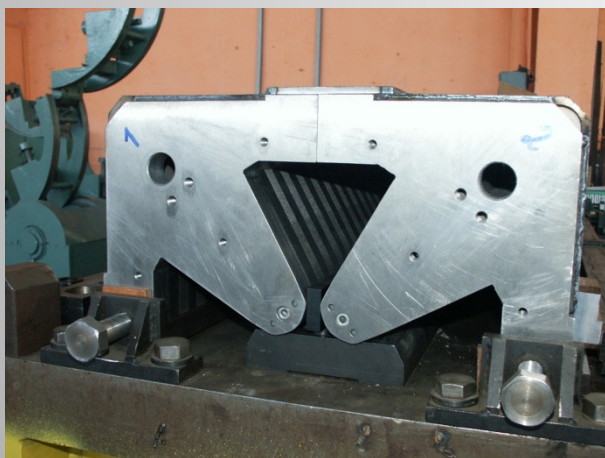
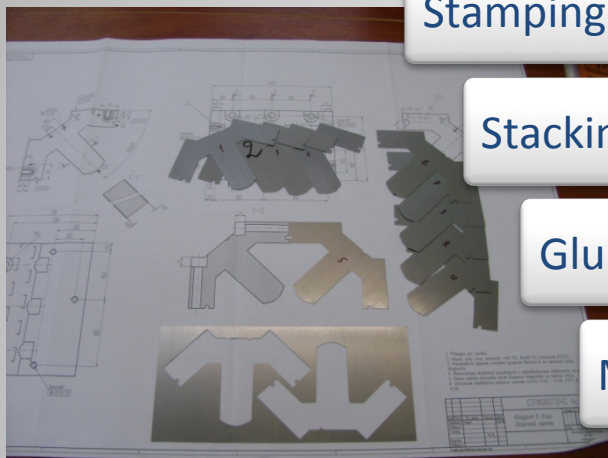
Stamping laminations

Stacking laminations into yokes

Gluings and/or welding

Machining

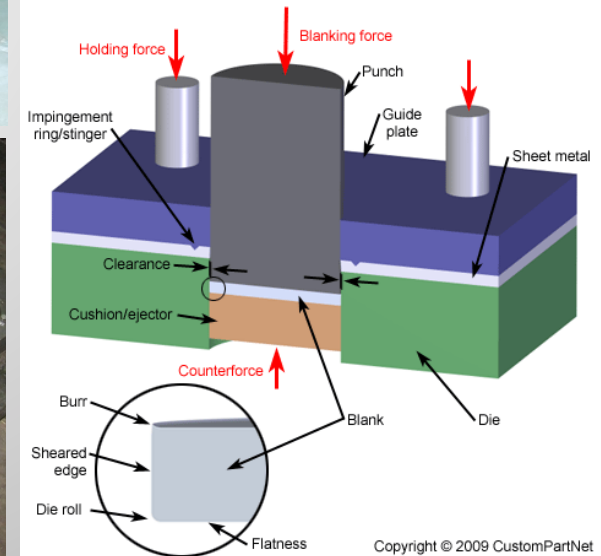
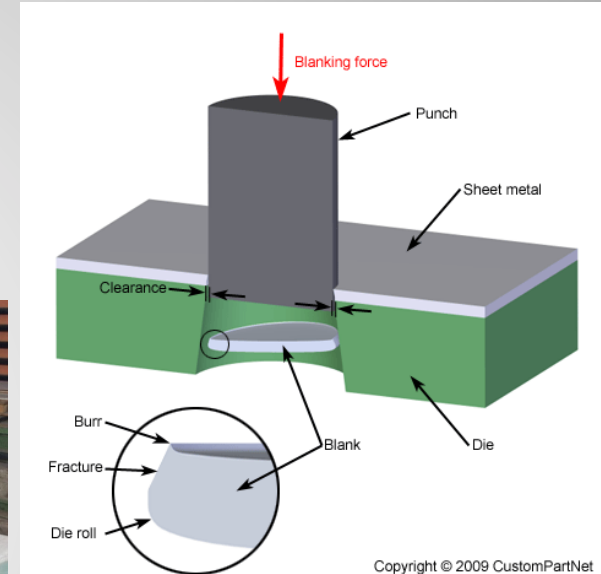
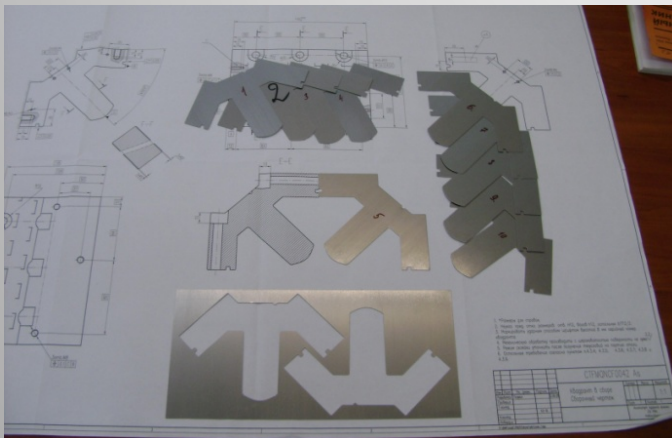
Assembly (preliminary)





Lamination punching

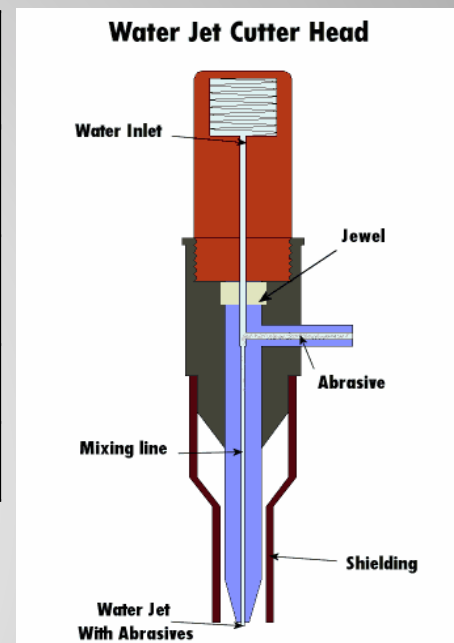
- Punching or fine blanking
- Fine blanking requires more expensive tooling
- Tolerances less than $\pm 8 \mu\text{m}$ achievable (depending on thickness, material and layout)
- Material can be delivered in sheets or strips (coils)



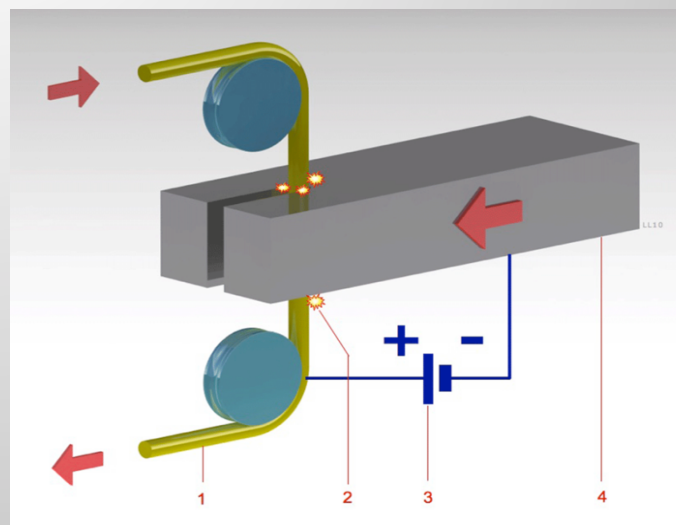
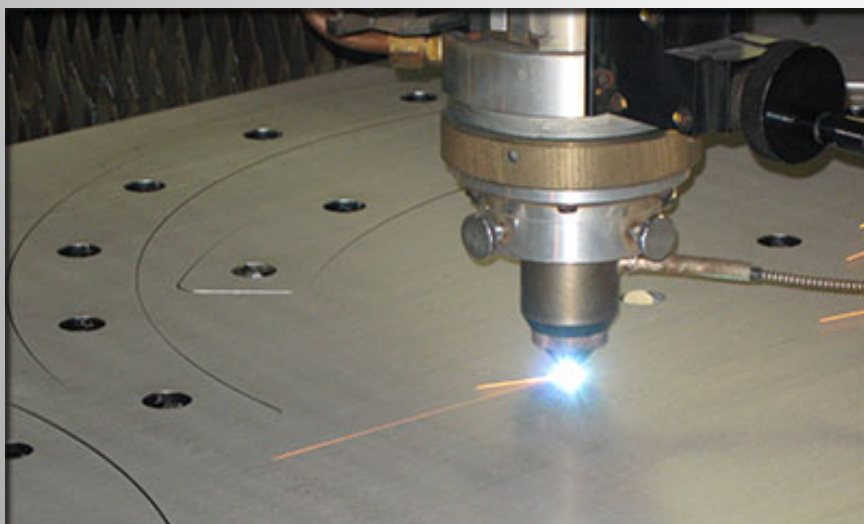


Alternatives to punching

Technique	Accuracy [mm]	Repeatability [mm]	Drawbacks
Water jet cutting	> 0.13	>0.025	rough cutting edge, relatively slow
Laser cutting	>0.01	>0.005	cutting edge ,burnt', relatively slow
CNC machining	0.01-0.001	0.01-0.001	stacks only
Wire-cut EDM	> 0.002	>0.001	very slow, limited size



...or a combination of different techniques





Lamination sorting

Smallest homogenous entity: Melt of several 100 tonnes
(same chemical composition → similar magnetic properties)

- Mother coils of ~20 tonnes (width ~ 1200 mm)
- Split coils of several tonnes → lamination stamping
- Single sheets → lamination stamping

Shuffling/mixing/sorting of laminations might be necessary to obtain
max. homogeneity of material properties in a series of magnets

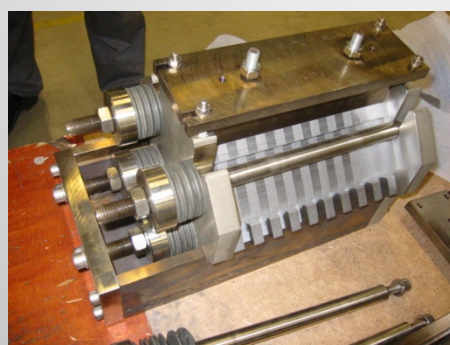
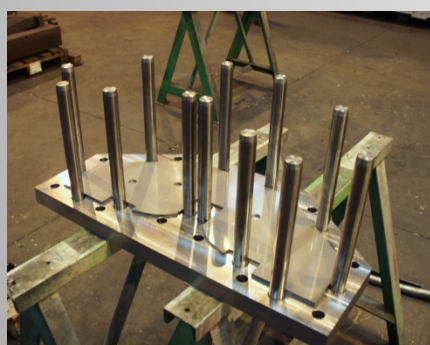
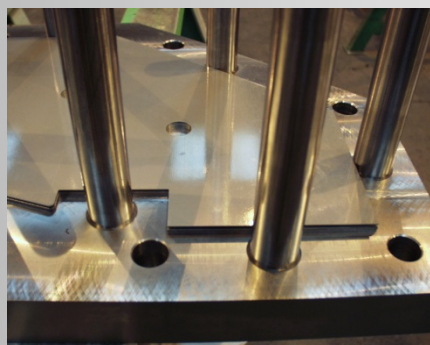
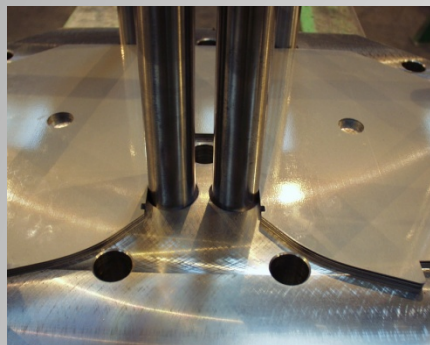




Yoke stacking

Tooling for:

- stacking
- baking
- welding





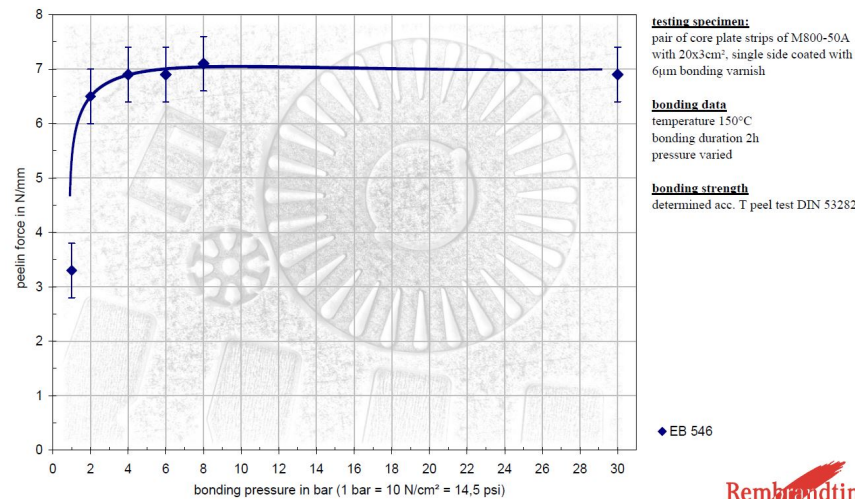
Bonding & insulation



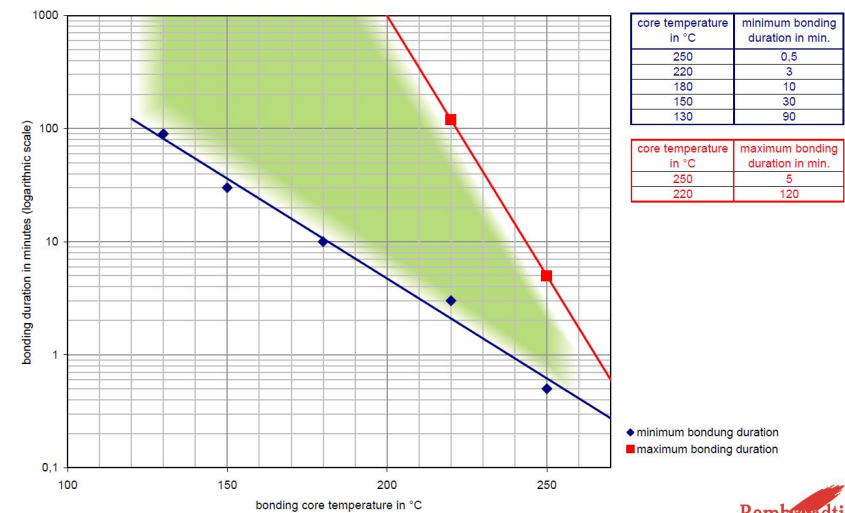
Special coatings have been developed for the adhesive bonding of laminations:

- provide electrical insulation and mechanical bonding
- based on epoxy resins
- available in B-stage (partly cured) and C-stage (fully cured)
- Referred to as **STABOLIT 70** by ThyssenKrupp

influence of bonding pressure to bonding strength of Remisol EB 546



bonding duration plot for Remisol EB 546/548 at 8 bar



Courtesy of Rembrandtin



Gluing vs. Welding

Welding

- + mechanically more rigid
- + no aging
- massive end plates/tension straps needed
- continuous welding introduces stress and deformation
- sophisticated welding procedure
- / requires stacking fixture

Glueing

- + no stress, no distortions
- + no tension straps, no end plates
(→ no eddy currents)
- glue sensitive to radiation and aging
- requires clean laminations and conditions
- requires baking oven
- / requires stacking fixture

Recommendation: combine gluing, welding & bolting





Coil manufacturing

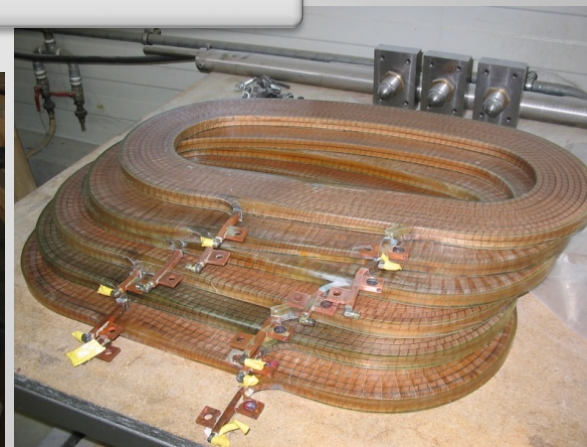
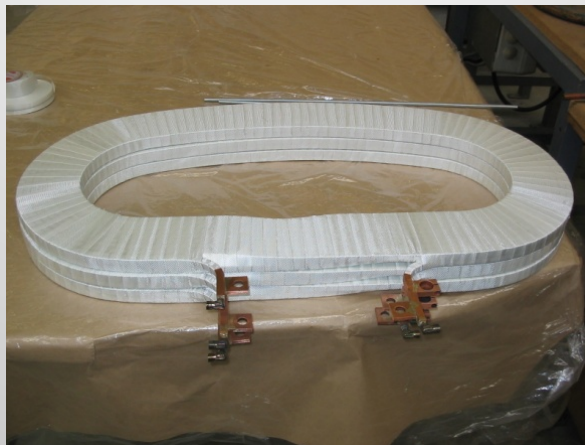
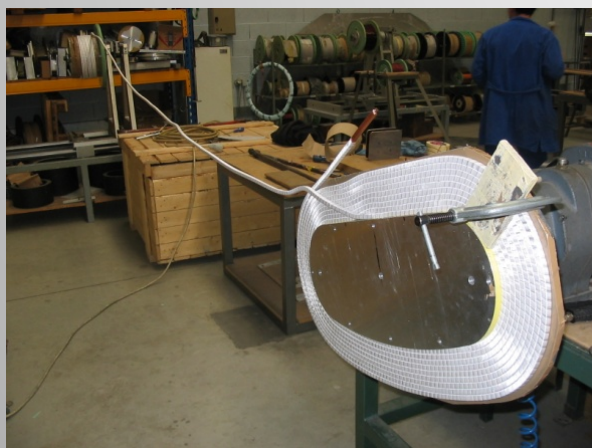
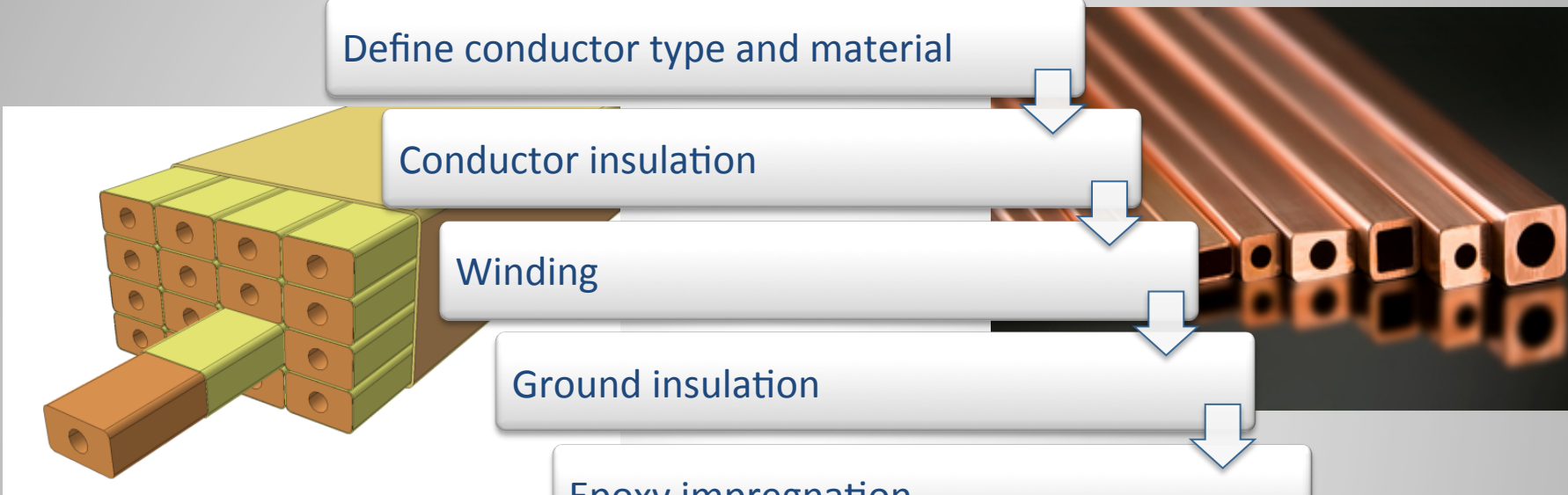
Define conductor type and material

Conductor insulation

Winding

Ground insulation

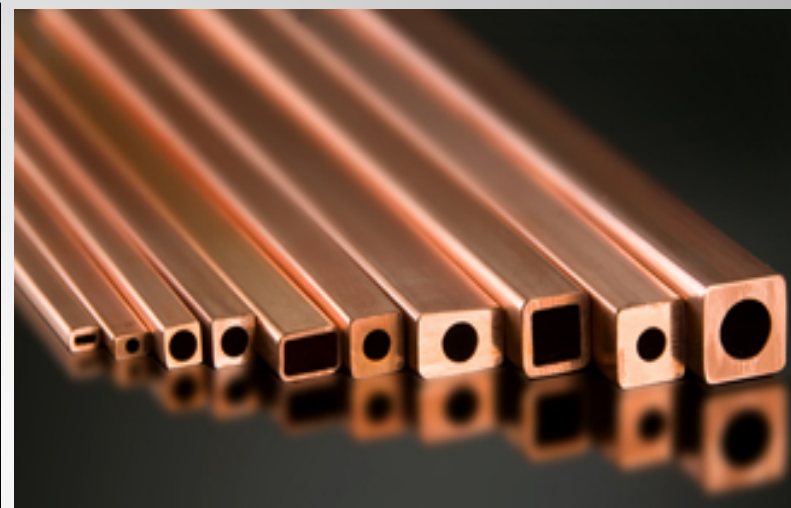
Epoxy impregnation



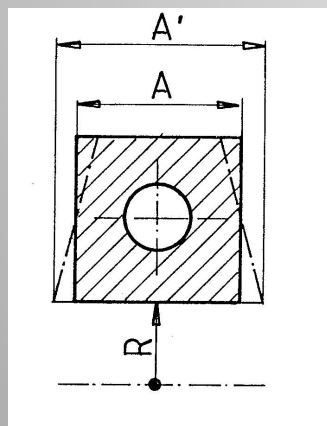


Conductor materials

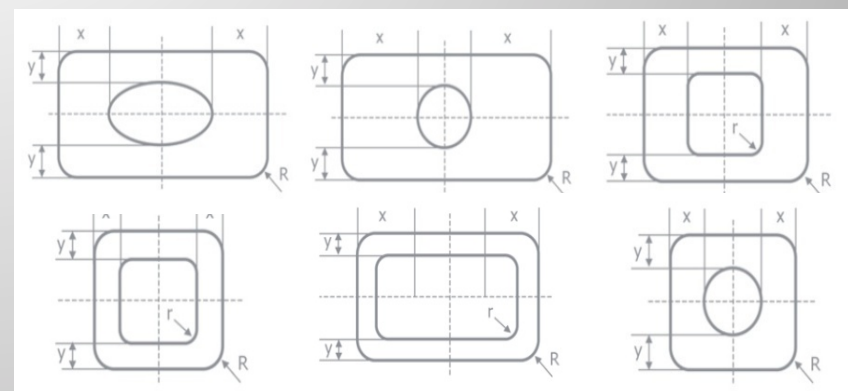
	Al	Cu (OF)
Purity	99.7 %	99.95 %
Resistivity @ 20°C	2.83 $\mu\Omega$ cm	1.72 $\mu\Omega$ cm
Thermal resistivity coeff.	0.004 K ⁻¹	0.004 K ⁻¹
Specific weight	2.70 g/cm ³	8.94 g/cm ³
Thermal conductivity	2.37 W/cm K	3.91 W/cm K



Key-stoning: risk of insulation damage & decrease of cooling duct cross-section

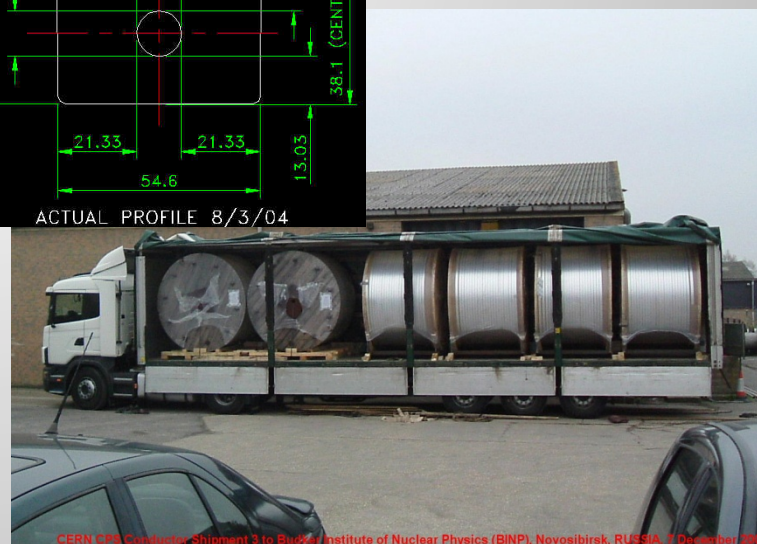
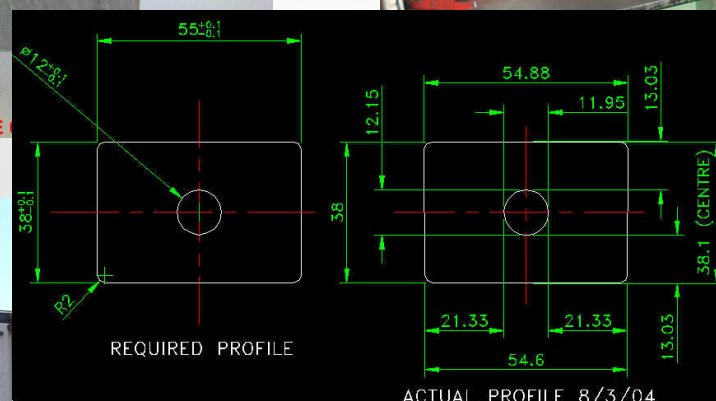
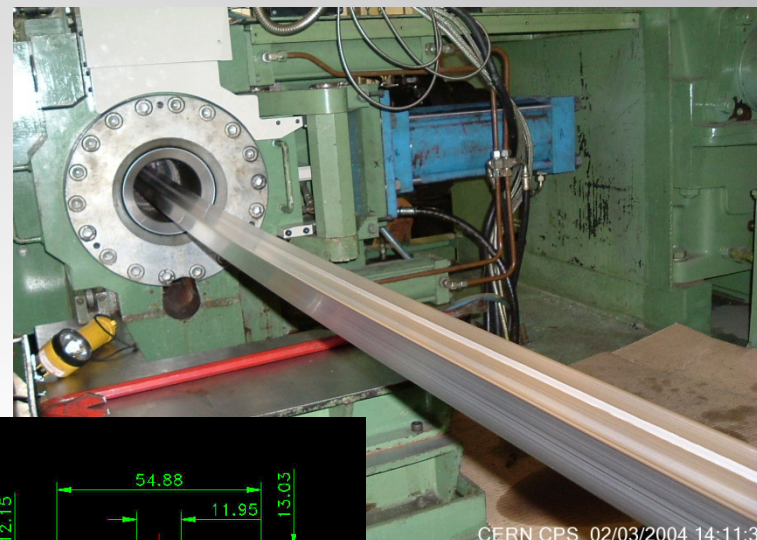


$$R = 3 \cdot A \Rightarrow \frac{\Delta A}{A} = 3.6\%$$





Hollow Aluminium Conductor





Coil insulation



In a magnet coil, the electrical insulation ensures that current flows only along the conductors and not between individual conductors or between the conductors and other parts of the magnet. We distinguish electrical insulation between:

- the individual turns in a coil
- different active parts
- active parts and ground

The electrical insulation is stressed by several factors:

- electric
- thermal
- mechanical
- chemical (including oxidation),
- radiation
- contamination

→ These factors can produce short and/or long term degradation



A weak electrical insulation may produce:

- current leaks with local heating up to melting and possible fire
- progressive damage of the leakage path up to a short circuit
- unbalanced circulating currents (→ magnetic field distortion)
- incorrect functioning of protections

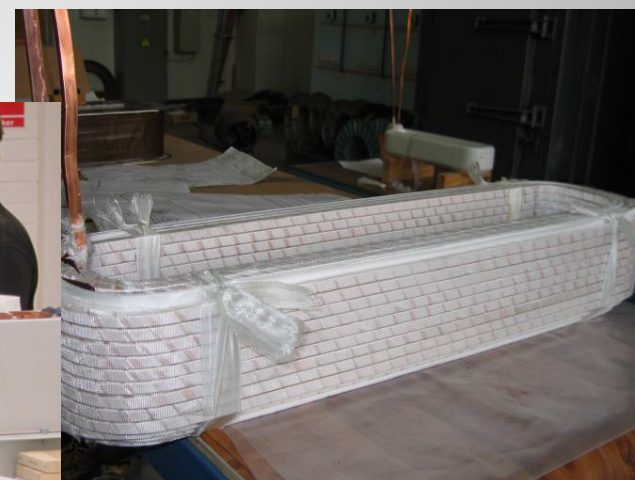
Reference: D. Tommasini: Dielectric insulation and high-voltage issues, CAS 2009, Brugges



Coil insulation

Conductors with small cross-section:

straightening → cleaning → conductor insulation → winding → ground insulation





Coil insulation



Conductors with large cross-section:

straigthening → winding → sand blasting → cleaning → conductor insulation → ground insulation





Insulation materials



Dielectric materials can be gaseous, liquid, or solid

For coil insulation, mainly solid dielectric materials are relevant

Solid dielectric materials can be distinguished in three main classes:

- inorganic materials:
 - Ceramics: porcelain, alumina
 - Glass, quartz
 - Cements and minerals (e.g. mica)
- organic materials:
 - thermoplastic: Rubber (natural, butyl, silicone), Polyamide (Nylon), Polyester (Mylar), Polypropylene (PP), Polystyrene (PS), Polyvinyl chloride (PVC), Polymethylmetachrylate (PMMA), Polycarbonate (PC), Polytetrafluoroethylene (PTFE)
 - thermosetting: Polyethylene (PE, LDPE, MDPE, HDPE, XLPE), Ethylene-Propylene (EPR), Polyimide (PI), Polyetheretherketone (PEEK), Epoxy, phenolic, silicon, polyester resins
- composites:
 - fully organic (aramidic fibres-epoxy tapes) or mixed (epoxy-mica tapes)

Montsinger's rule / Arrhenius equation: $L(T + 10K) \approx 0.5L(T)$

A temperature rise of 10 K halves the expected live time of an insulation system

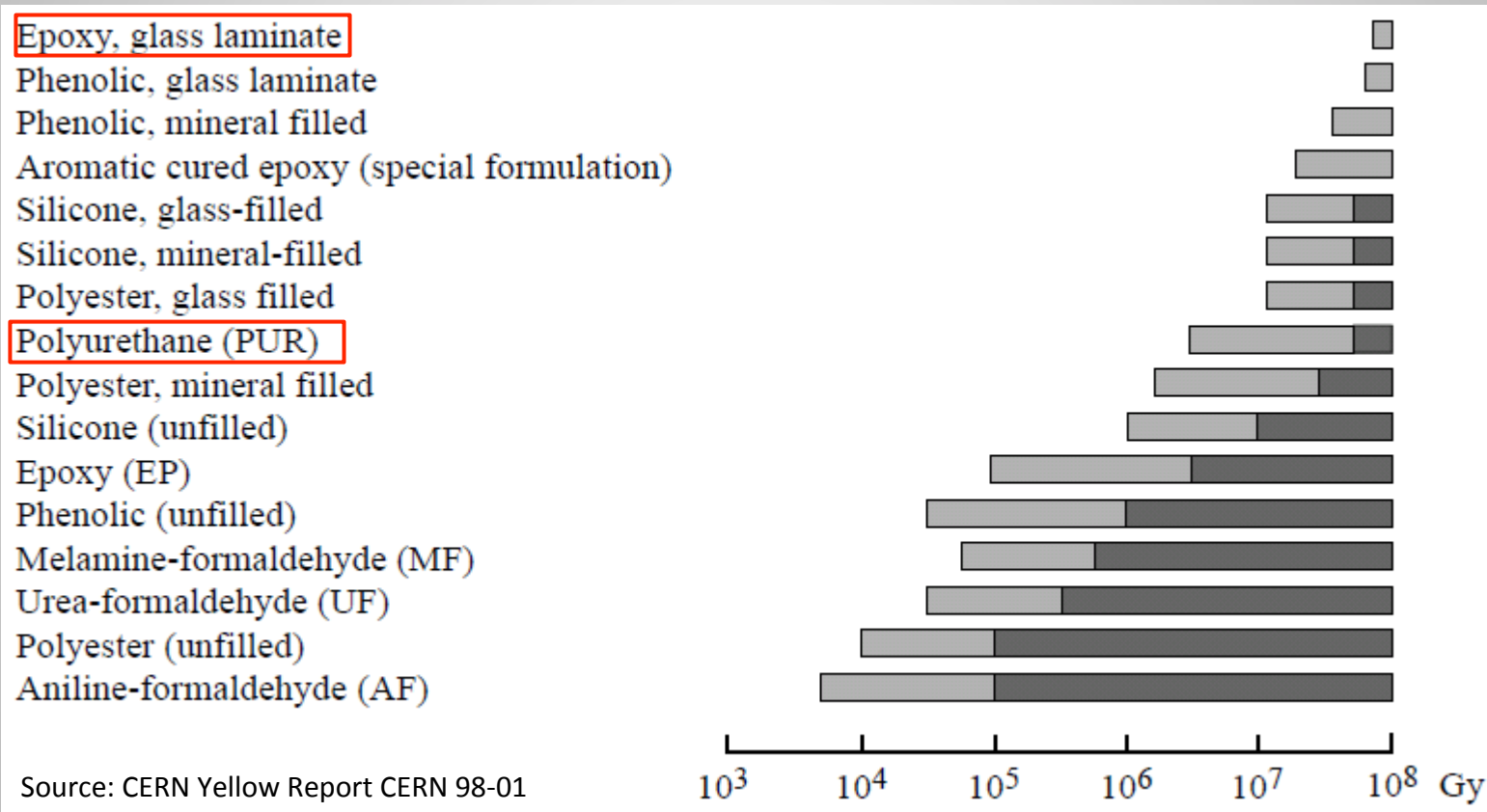




Radiation hardness



Radiation hardness is an important criterion for insulation materials used for accelerator applications

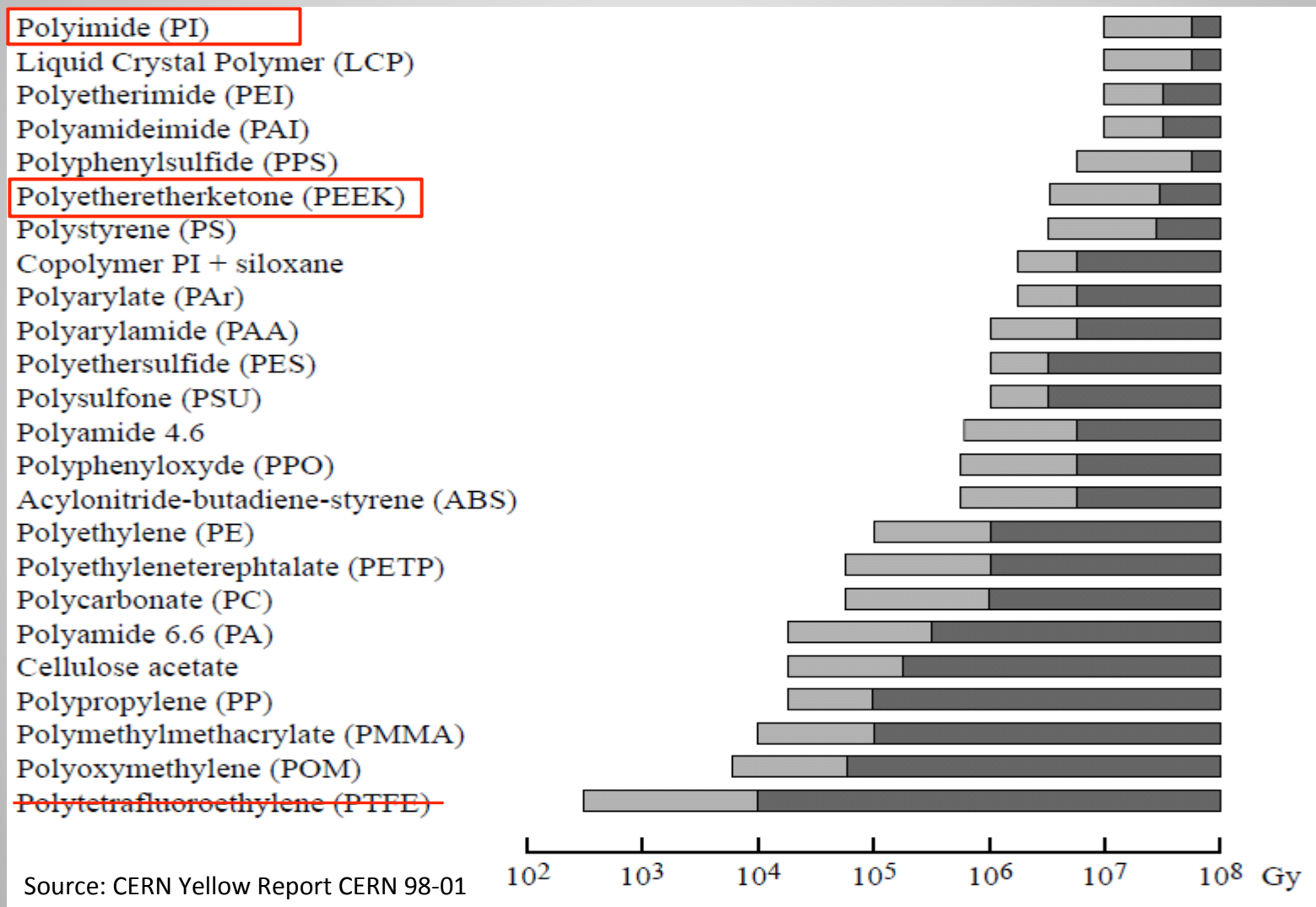


Above 10⁸ Gy special insulation techniques are required!





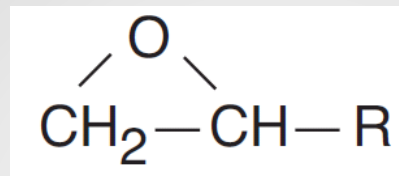
Radiation hardness





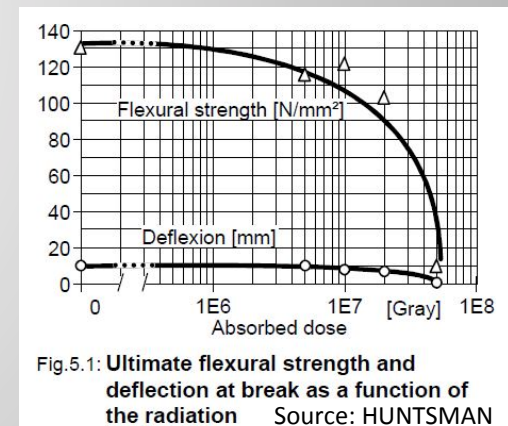
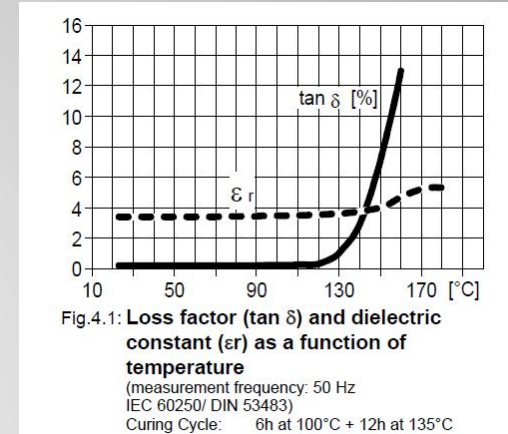
Epoxy resins

- Invented in 1938 (patent by P. Castan)
- They contain the epoxyde group:



- Composed by:
 - base resin (aromatic, cycloaliphatic, or phenolic)
 - hardener (amine, anhydride)
 - accelerator
 - flexibilizer
 - fillers (Al_2O_3 , MgO , quartz, Dolomite...)
 - other additives (to modify the viscosity for example)

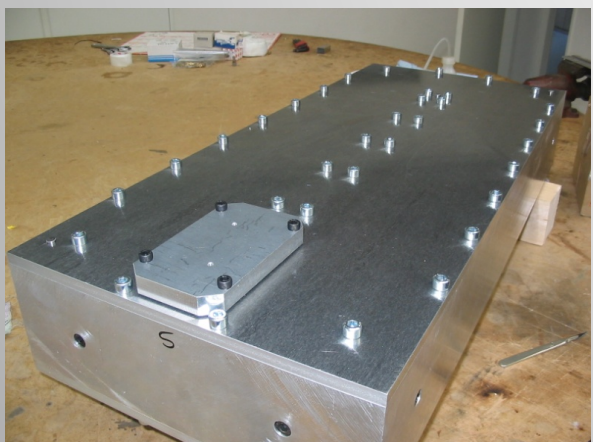
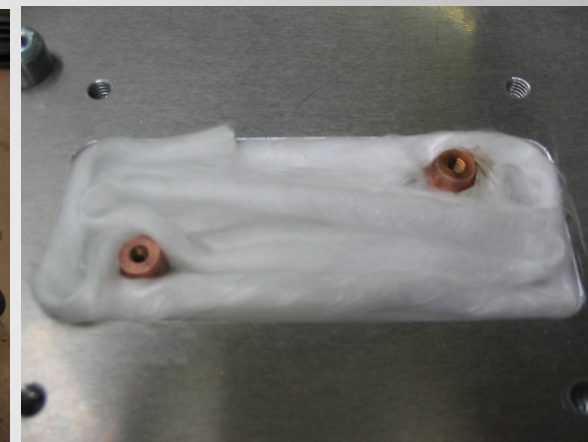
- Good results in accelerator magnets are being obtained with bisphenol-A + anhydride hardener + amine accelerator





Coil impregnation

heating and evacuating mold and coil (auto-clave or vacuum mold) → mixing resing →
heating and degassing resin → injecting resin → curing cycle → cooling





Coil impregnation



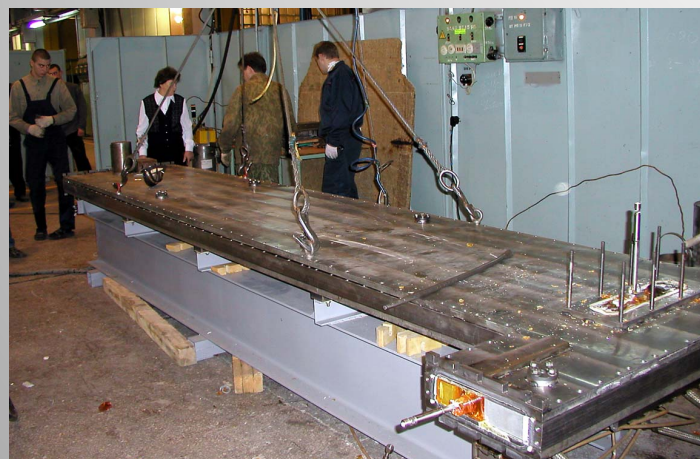
We can distinguish between two different impregnation techniques:

Precise mold

- + very good surface finish
- + moderate resin consumption
- requires release agent
- difficult to avoid resin rich areas
- expensive tooling (mold)
- ejection more difficult

Release tape

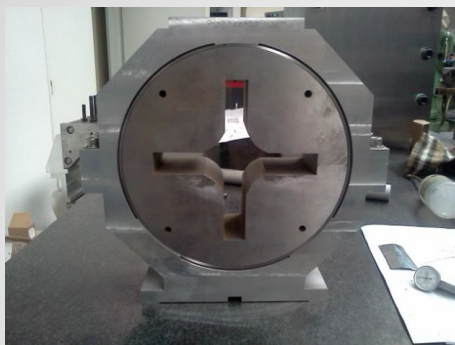
- + no excess of resin on the finished coil
- + inexpensive mold
- + easy de-molding
- poor surface finish
- higher resin consumption





Magnet assembly

By hand....



... or with the help of tooling

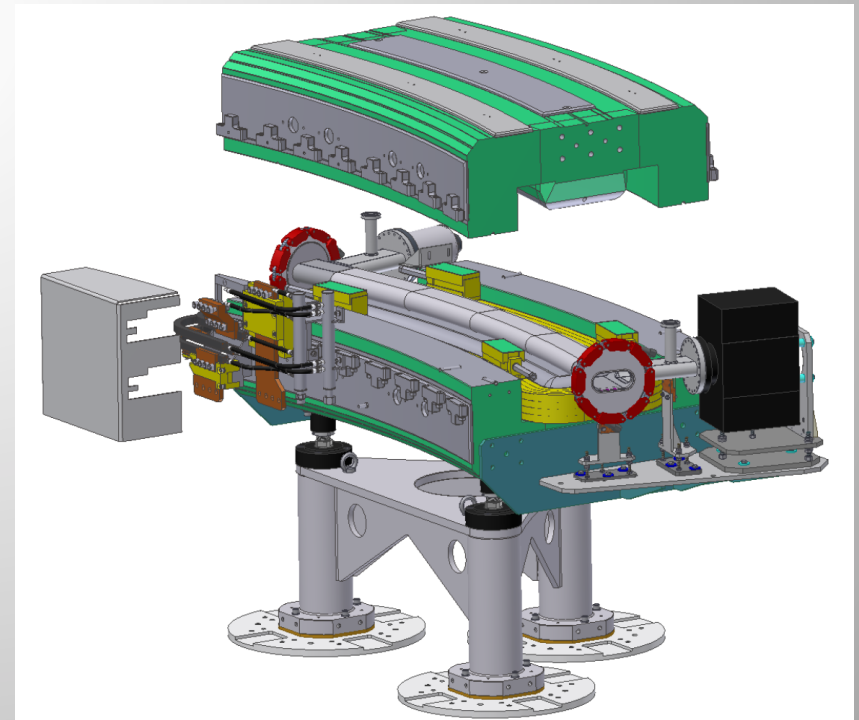
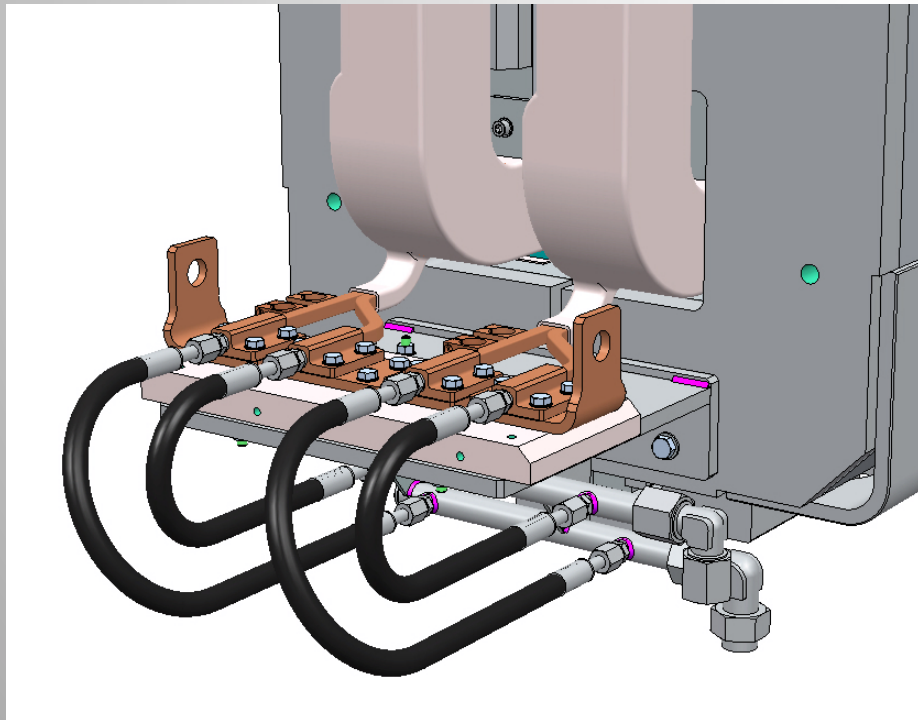




Auxiliary components



- Electrical connections
- Hydraulic connections
- Interlock system (temperature, pressure, water flow)
- Magnetic measurement devices (pick-up coils, hall probes)
- Alignment targets, adjustment tables and support jacks

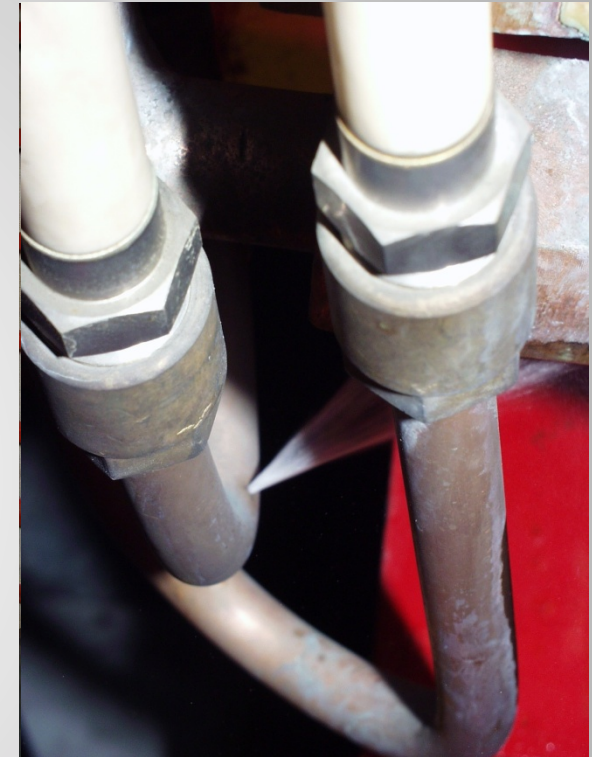




Hydraulic circuits



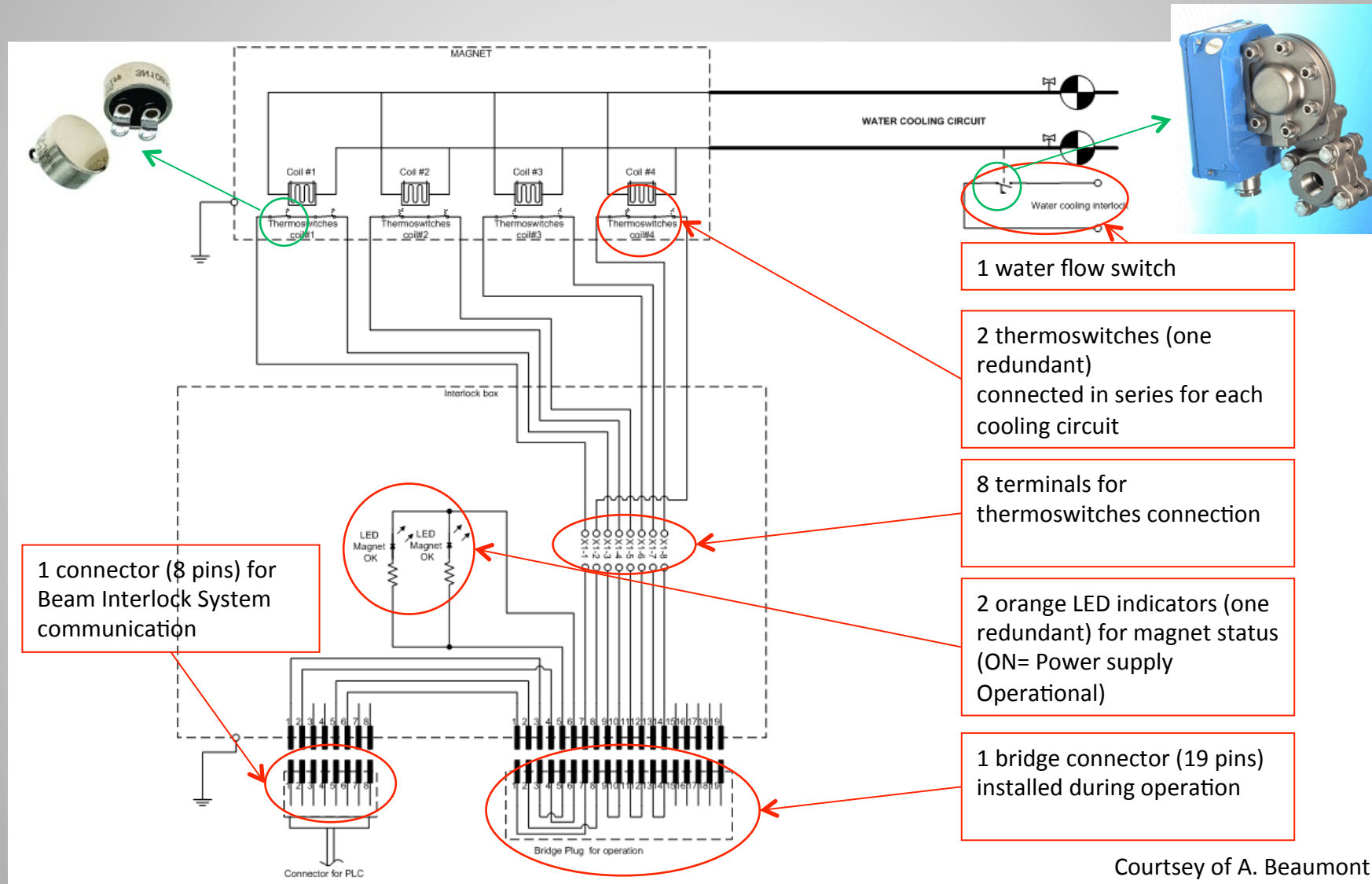
- Water circuits are most critical items
- 95% of all magnet failures due to water leaks:
 - Corrosion
 - Erosion
 - Poor brazing quality
 - Poor welding quality
 - Failure or aging of joints
 - Inadequate materials
 - Incorrect assembly
 - Radiation damage
 - Inadequate design



- Leaks can be detected and repaired during magnet acceptance tests and commissioning...
- ... but, many leaks occur only after years in operation
- Often not monitored → magnet damage (short circuits, corrosion of iron yoke) and collateral damages on other equipment possible



Magnet Interlock System

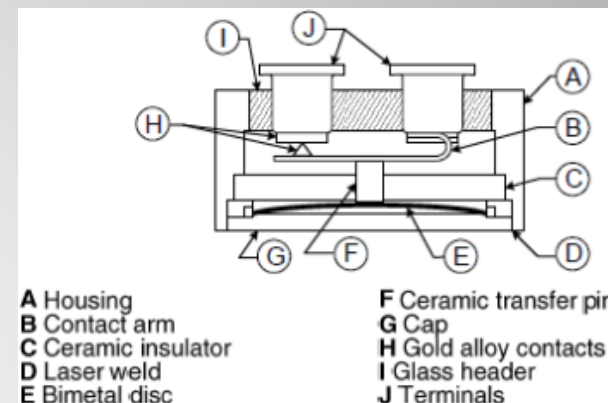


Courtesy of A. Beaumont

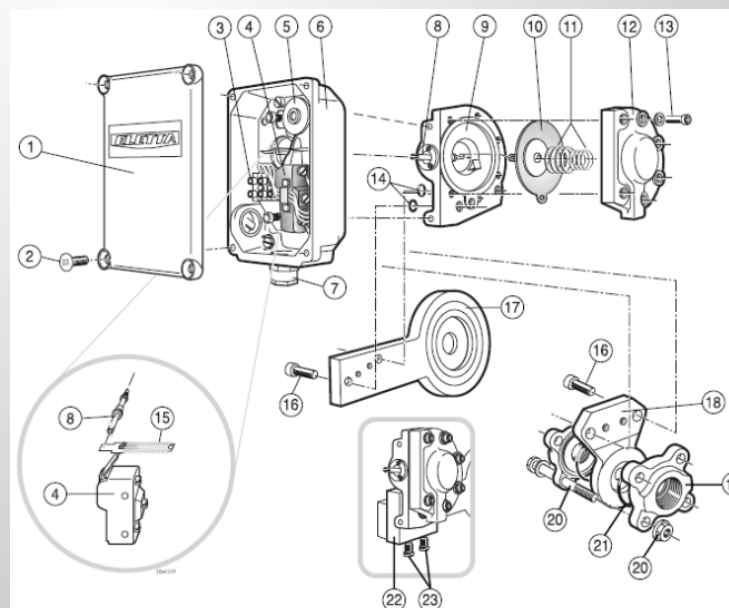


Interlock Sensors

Thermo-switch:



Flow-switch:





Summary



- Cost optimization is an important design aspect, in particular in view of future energy costs
- Engineers have a vast choice of materials and manufacturing techniques available influencing the performance of the magnet
- Selecting appropriate materials is not always trivial and requires specific know-how about the material properties
- The manufacturing techniques shall be adapted to meet the specified requirements of the final product in all respects
- The engineer has to make his choice about the foreseen manufacturing techniques in an early stage of the project since it has a significant impact on the magnet costs