CORPUSCULAR OPTICS

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Scope

- Beam transport in long, ~periodic machines (linacs, storage rings…) $\rightarrow$ general beam dynamics, beta functions etc $\rightarrow$ not here
- Beam transport in a short line
  - Beta functions not relevant (they suppose a quasi-harmonic motion) or unuseful
  - Geometrical optics is needed (ex: spectrometers)
- Programme
  - General matricial optics for accelerators
  - Description/matrix for standard focusing elements
  - Beam description (emittance) and transport
  - Basic properties (achromatic systems, spectrometers)
  - Exercises

Lorentz force

- General case

$$\boxed{\frac{dm\vec{v}}{dt} = q\left(\vec{E} + \vec{v} \wedge \vec{B}\right)}$$

- Non relativistic case only

$$\boxed{\vec{F} = q\left(\vec{E} + \vec{v} \wedge \vec{B}\right)}$$

- Remark: If no acceleration, you can often do as for non-relativistic case with (see later)

$$m = \gamma \cdot m_0$$

$$\beta = {}^{v}/_{c}$$

$$\gamma = \frac{1}{\sqrt{1-\beta^2}}$$

- Electric field: focusing, bending and energy change (“ acceleration”)
- Magnetic field: focusing and bending only

Magnetic rigidity

- T=neV is the kinetic energy
- n is the charge number and V the acceleration voltage
- We consider the energy at rest V_0 and compute the Lorentz factors
- We get the radius of curvature in a magnetic field B

$$\boxed{m_0c^2 = eV_0}$$

$$E = \gamma m_0 c^2 = \gamma e V_0 = T + m_0 c^2 = neV + eV_0$$
$$\Rightarrow \gamma = \frac{nV + V_0}{V_0}$$
$$\Rightarrow \beta = \frac{\sqrt{n^2V^2 + 2nVV_0}}{nV + V_0}$$

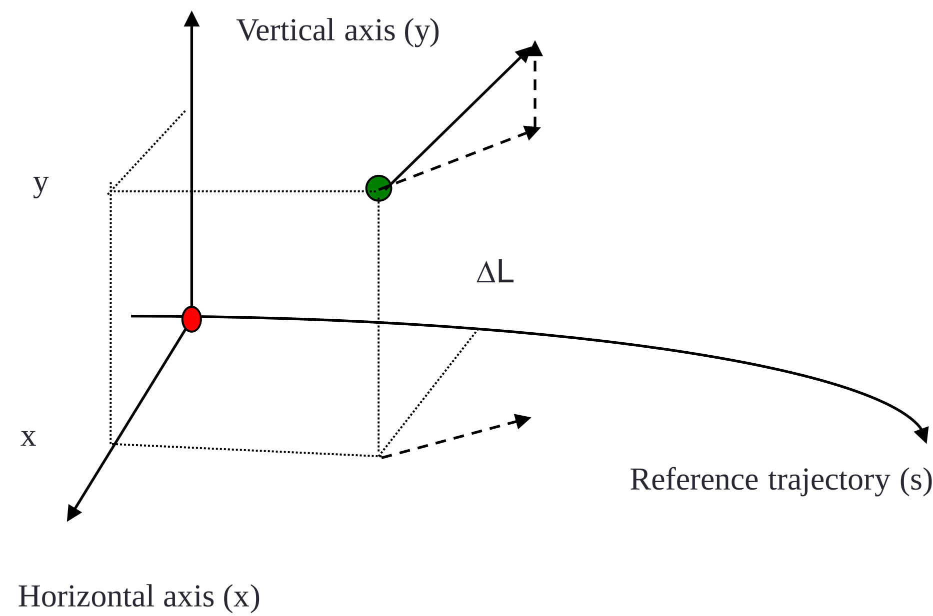
$$B\rho = \frac{mv}{q} = \frac{\gamma m_0 \beta c}{ne} = \frac{\sqrt{n^2V^2 + 2nVV_0}}{nc} = \frac{\sqrt{T^2 + 2TV_0}}{nc}$$

General frame – Gauss conditions

- Coordinates relative to a reference particle

$$\boxed{x' = \frac{dx}{ds} = \frac{p_x}{p_s} \qquad y' = \frac{dy}{ds} = \frac{p_y}{p_s}}$$

- Gauss conditions $\rightarrow$x,x',y,y' small
  - First order calculations
  - Linéarities
  - Non linearities = high order terms



- Phase space (x,x',y,y', ΔL, Δp/p0)
- Set of canonical <u>conjugate</u> coordinates

Please:

$$\frac{\Delta p}{p} \neq \frac{\Delta E}{E}$$

$$\frac{\Delta p}{p} \neq \frac{1}{2} \cdot \frac{\Delta E}{E}$$

We will work mainly with transverse coordinates

Equation of motion (illustration: one plane, non relativistic motion)

- Time→space transform

$$\boxed{\dot{x} = \frac{dx}{ds}\frac{ds}{dt} = vx' \Rightarrow x' = \frac{\dot{x}}{v}}$$

$$\boxed{\begin{aligned} &\frac{dx'}{dt} = \frac{dx'}{ds}\frac{ds}{dt} = vx'' = -\frac{1}{v^2}\frac{dv}{dt}\dot{x} + \frac{1}{v}x'' = -\frac{1}{v}\frac{dv}{dt}x' + \frac{1}{v}\ddot{x} \\ &\frac{dv}{dt} = \frac{dv}{ds}\frac{ds}{dt} = v\frac{dv}{ds} \end{aligned}}$$

- « acceleration »

$$\boxed{\begin{aligned} &vx'' = -\frac{dv}{ds}x' + \frac{1}{v}\ddot{x} \\ &\ddot{x} = v^2 x'' + vv'x' \end{aligned}} \longrightarrow \boxed{x'' = \frac{\ddot{x}}{v^2} - \frac{v'}{v}x'}$$

We suppose $v_s \sim v$

With a magnetic force (illustration, again)

- More generally:

$$\boxed{x'' = \frac{\ddot{x}}{v^2} - \frac{v'}{v}x' \Rightarrow x'' = \frac{\ddot{x}}{v^2} - \frac{p'}{p}x'}$$

- The « force term » $\frac{\ddot{x}}{v^2}$ is linearized

$$\boxed{x'' + \frac{p'}{p}x' = F(x) \Rightarrow x'' + \frac{p'}{p}x' \approx a + bx + cx'}$$

- The equation of motion is always the same
  - Damping term related to acceleration
  - The force term

→ Calculation rather easy

➢ Relativistic equation

$$\boxed{x'' + \frac{p'}{p}x' + k(s)x = \frac{1}{\rho_0}\frac{\Delta p}{p_0}}$$

Keywords: damping, focussing, dispersion

General 2D solution

$$\boxed{x'' + \frac{p'}{p} x' + k(s) x = \frac{1}{\rho_0} \frac{\Delta p}{p_0}}$$

$$\boxed{x'' + \frac{p'}{p} x' + k(s) x = 0}$$

$$x(s) = x_0 \cdot C(s) + x'_0 \cdot S(s)$$
$$x'(s) = x_0 \cdot C'(s) + x'_0 \cdot S'(s)$$

With C(0)=1, C'(0)=0, S(0)=0. S'(0)=1

$$X(s) = \begin{bmatrix} x(s) \\ x'(s) \end{bmatrix} = \begin{bmatrix} C(s) & S(s) \\ C'(s) & S'(s) \end{bmatrix} \cdot X_0$$

$$X(s) = M_{s \leftarrow 0} \cdot X_0$$

$$\boxed{x'' + \frac{p'}{p} x' + k(s) x = \frac{1}{\rho_0} \frac{\Delta p}{p_0}}$$

$$x(s) = x_0 \cdot C(s) + x'_0 \cdot S(s) + \frac{\Delta p}{p_0} \cdot D(s)$$

General conclusion

- We suppose the equation of motion to be linearized with a good enough approximation
- So, the general (first order) solution in 6D phase space is
$$X(s) = M_{s\leftarrow 0} \cdot X_0$$
M is the transfer (transport matrix) for abscissa 0 to abscissa s
- Transport to higher orders is much more complicated
- Composition: $M_{3\leftarrow 1} = M_{3\leftarrow 2} \cdot M_{2\leftarrow 1}$
- We will often work in lower dimensions (2 or 4)
- Particular case: horizontal motion with magnetic dispersion
$$x(s) = x_0 \cdot C(s) + x'_0 \cdot S(s) + \frac{\Delta p}{p_0} \cdot D(s)$$
- D is the dispersion function
- Beam transport is a LEGO play: assembly on transfer matrixes
  - Calculation of elementary matrixes (lenses, drift space, bending magnet, edge focusing)
  - General properties of systems versus the properties of matrixes (point to point imaging…)
- It can be shown from hamiltonian mechanics that this is equivalent to geometrical optics (non only an analogy)

Magnetic force versus electric force

- $x''_M = \frac{qvB}{mv^2}$
- $x''_E = \frac{qE}{mv^2}$
- $\frac{x_M}{x_E} = \frac{B}{E} \cdot v$
- For B=1T and E=1MV/m $\frac{x_M}{x_E} = 10^{-6} \cdot v$
- Limit for $v = 10^6 \rightarrow \beta = 0.0033 \rightarrow \sim 10\ keV\ protons$
- Electrostatic focusing is used for low energy beams (~100 keV protons –order of magnitude, please do the appropriate design-)
- $x''_E = \frac{qE}{mv^2} = \frac{qE}{qV} = \frac{E}{V}$: no charge separation (ex: solenoids at source exit)

GENERAL OPTICAL PROPERTIES OF MATRIXES

Goal:

- *Express a transport (optical property) in terms of matrix properties (coefficients)*
- *Choose and tune the optical elements to get these matrix properties (coefficients)*
- *Provide you the useful formulas*

Basic elements

Convention

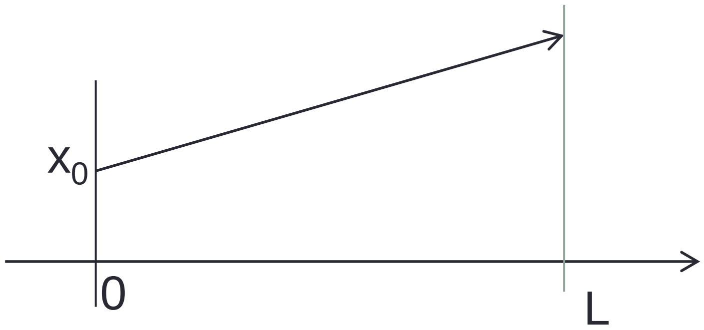
- Distances are positive from left to right
- Focusing lengths are positive (with the appropriate sign for focussing/defocussing

Fundamental property (2D case)

$$\det(M_{s\leftarrow 0}) = \frac{p_0}{p_s} = \Delta$$

Drift space

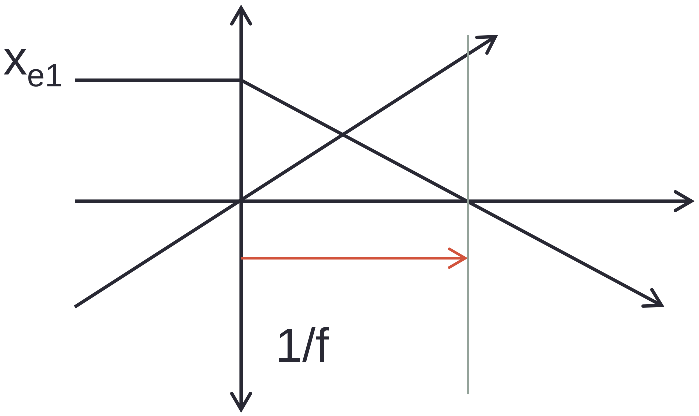
- $x(L) = x_0 + L \cdot x'_0$
- $x'(L) = x'_0$
- $M = \begin{bmatrix} 1 & L \\ 0 & 1 \end{bmatrix}$



Thin lenses

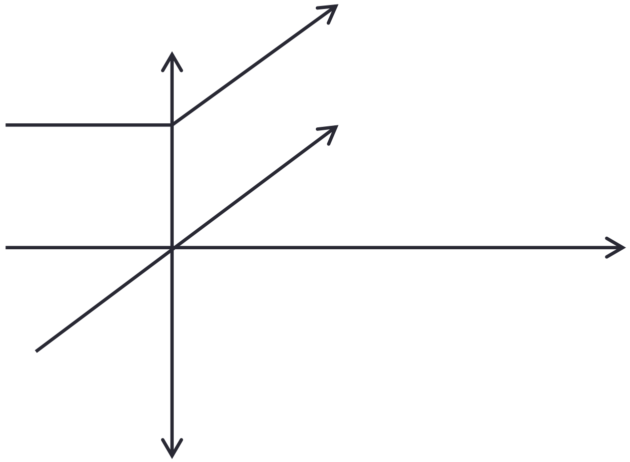
Focusing thin lens

- Superposition (linear) of two elementary beams
- $x_s = x_e$
- $x'_s = x'_e - \frac{x_e}{f}$
- $M = \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix}$



Defocusing thin lens

- $x_s = x_e$
- $x'_s = x'_e - \frac{x_e}{f}$
- $M = \begin{bmatrix} 1 & 0 \\ \frac{1}{f} & 1 \end{bmatrix}$

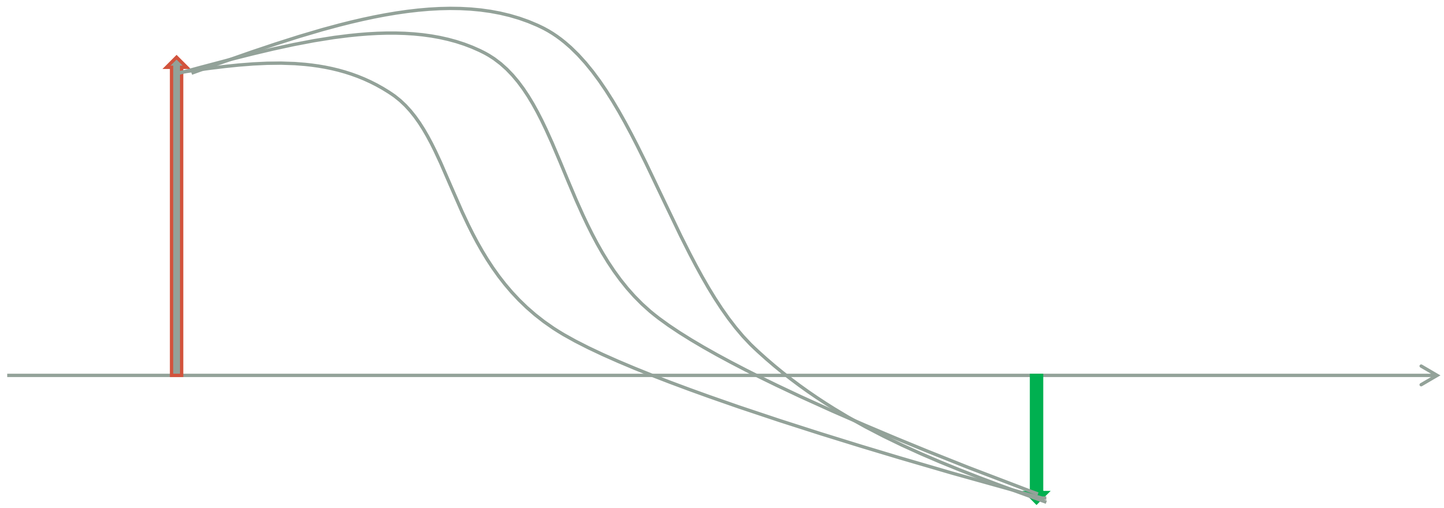


Point to point imaging

$$M_{s\leftarrow e} = \begin{bmatrix} M_{11} & 0 \\ M_{21} & M_{22} \end{bmatrix}$$

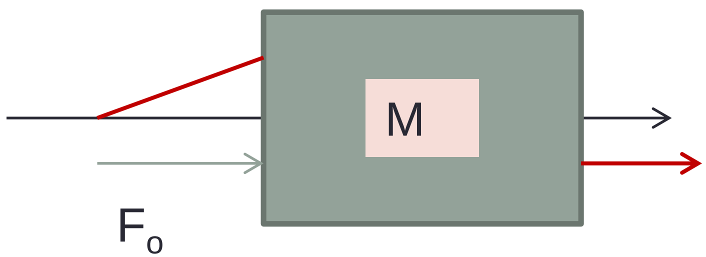
M_{11} is the magnification

$$M_{11} \cdot M_{22} = \frac{p_e}{p_s} = \Delta$$



Focal points

Object



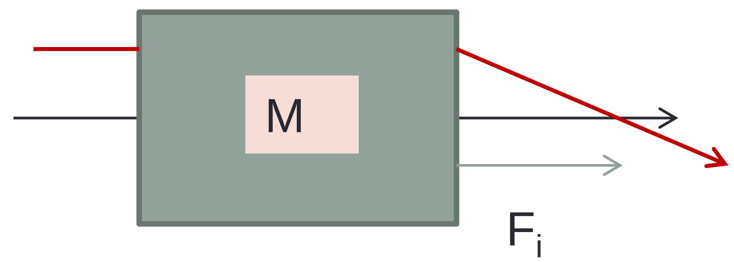
$$T = \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} \cdot \begin{bmatrix} 1 & F_0 \\ 0 & 1 \end{bmatrix}$$

$$\begin{bmatrix} x_s \\ 0 \end{bmatrix} = \mathrm{T} \cdot \begin{bmatrix} 0 \\ x'_e \end{bmatrix}$$

$$\rightarrow (M_{21} \cdot F_O + M_{22}) = 0$$

$$\rightarrow F_O = -\frac{M_{22}}{M_{21}}$$

Image



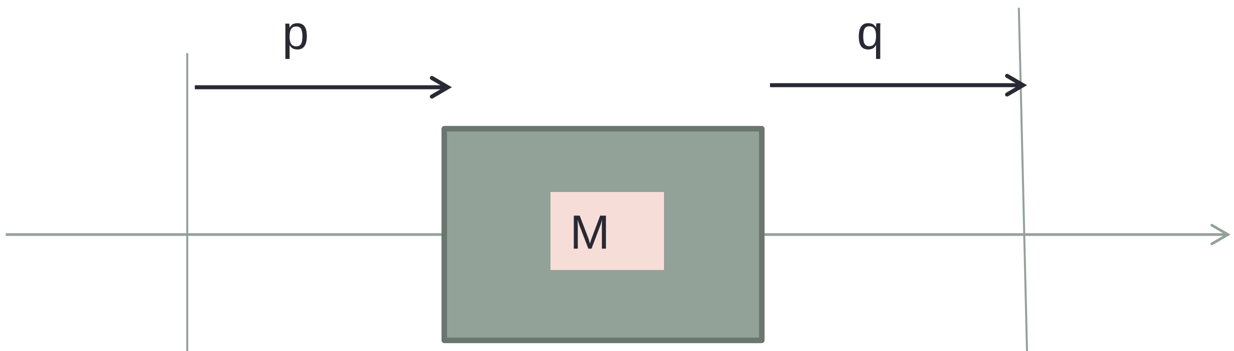
$$T = \begin{bmatrix} 1 & F_i \\ 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix}$$

$$\begin{bmatrix} 0 \\ x'_s \end{bmatrix} = \mathrm{T} \cdot \begin{bmatrix} x_e \\ 0 \end{bmatrix}$$

$$\rightarrow (M_{21} \cdot F_O + M_{11}) = 0$$

$$\rightarrow F_O = -\frac{M_{11}}{M_{21}}$$

A useful formula: drift/matrix/drift

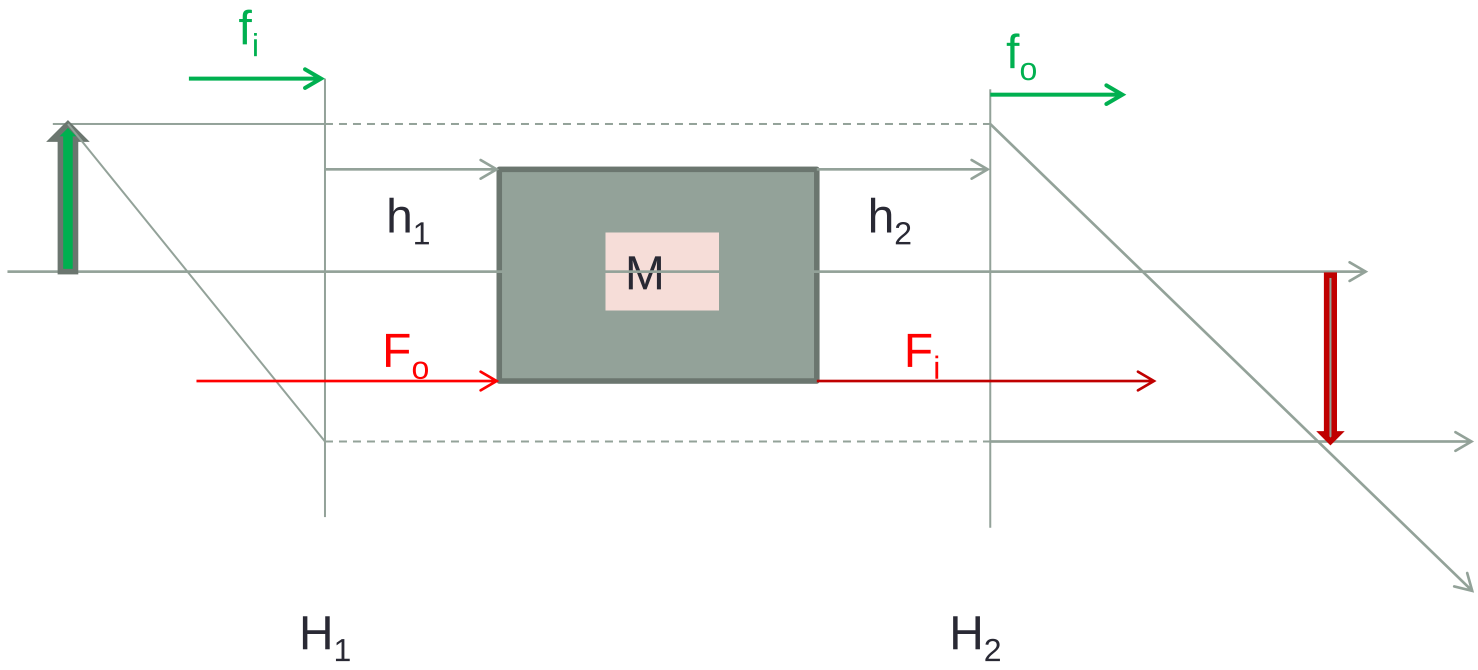


$$T = \begin{bmatrix} 1 & q \\ 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} \cdot \begin{bmatrix} 1 & p \\ 0 & 1 \end{bmatrix}$$

$$\begin{cases} T_{11} = M_{11} + qM_{21} \\ T_{12} = pqM_{21} + pM_{11} + qM_{22} + M_{12} \\ T_{21} = M_{21} \\ T_{22} = pM_{21} + M_{22} \end{cases}$$

Principal planes

- Position of the 2 planes H_1 and H_2 with
  - Point to point imaging from H_1 to H_2
  - Magnification equal to 1
  - → any incoming beam exits with the same position (x_s=x_e)



Position

- $$\begin{cases} T_{11} = M_{11} + h_2 M_{21} = 1 \\ T_{12} = h_1 \cdot h_2 M_{21} + h_1 \cdot M_{11} + h_2 \cdot M_{22} + M_{12} = 0 \end{cases}$$

- $h_2 = \frac{1 - M_{11}}{M_{21}}$
- $h_1 = \frac{\Delta - M_{22}}{M_{21}}$

Warning: h_1 is positive upstream, h_2 is positive downstream

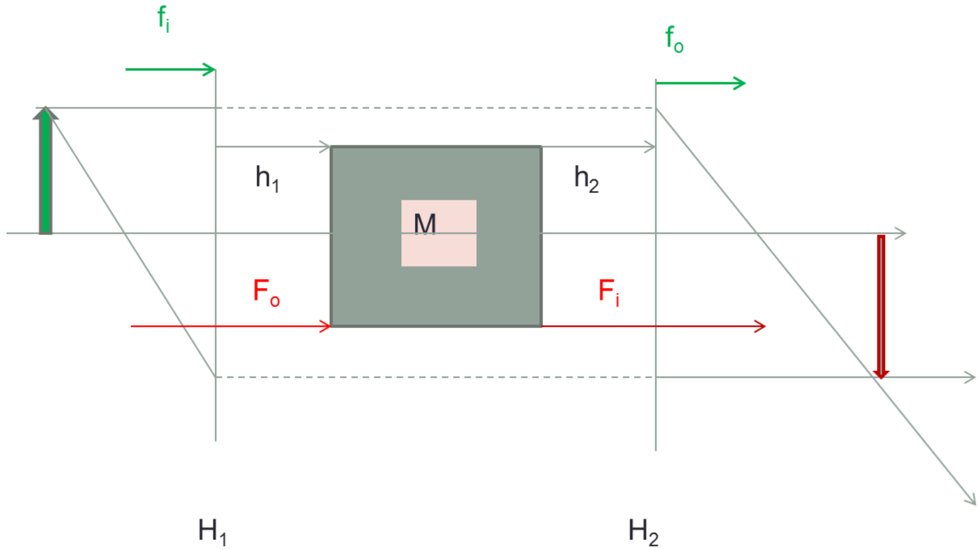
Foci vs principal planes

- We consider the T matrix instead of the M matrix
- $f_o = -\frac{T_{22}}{T_{21}} = -\frac{h_1 \cdot M_{21} + M_{22}}{M_{21}} = -\frac{\Delta}{M_{21}}$
- $f_i = -\frac{T_{11}}{T_{21}} = -\frac{h_2 \cdot M_{21} + M_{11}}{M_{21}} = -\frac{1}{M_{21}}$

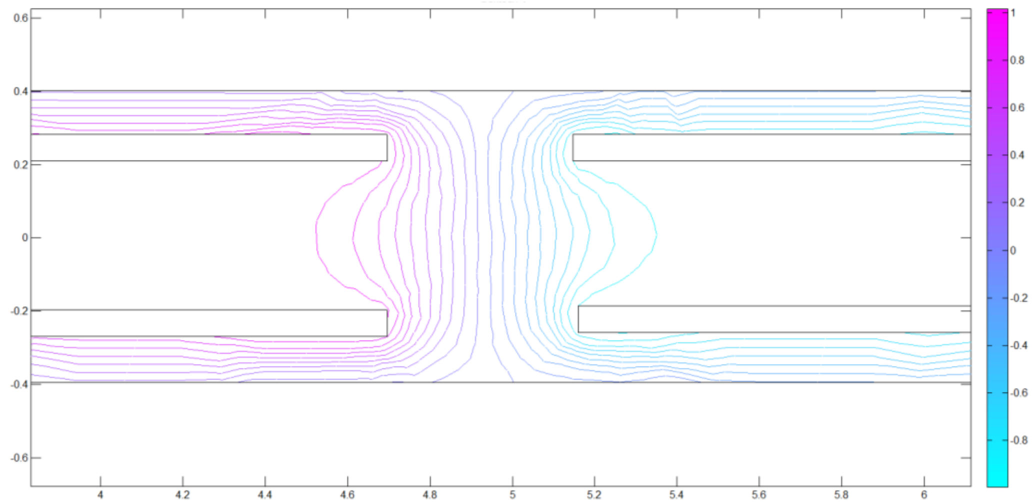
$$\frac{f_O}{f_i} = \Delta$$

Use

- This description is useful when using non sharp edge elements like electrostatic lenses and to construct easily trajectories.
- It tells you "where" and "how" the system is. Ex: $h_1=-h_2 \leftrightarrow$ thin lens
- A tracking code provides the transfer matrix M between given planes (far enough in a low field region).
- The values of F_o and F_i depend on the choice of the plane: not constant not a real lens characteristic
- The position of H_o and H_i, the values of f_o and f_i are constant
- The focal lengths given by codes are f_o and f_i



$$\frac{f_o}{f_i} = \Delta$$



Symetric system

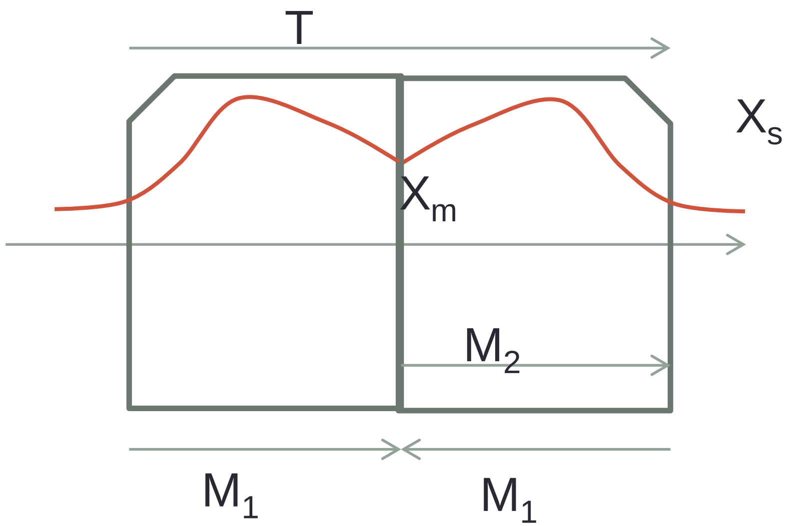
- Backward motion is obtained by changing x'→-x'

$$J = \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix} = J^{-1}$$

$$J \cdot X_m = M_1 \cdot J \cdot X_s = M_1 \cdot J \cdot M_2 \cdot X_m$$

$$M_2 = J \cdot M_1^{-1} \cdot J$$

$$T = J \cdot M_1^{-1} \cdot J \cdot M_1$$



Warning: structure is symetric, trajectory <u>may</u> be

- $T = \frac{1}{\det(M_1)} \begin{bmatrix} M_{11}M_{22} + M_{12}M_{21} & 2M_{22}M_{12} \\ 2M_{11}M_{21} & M_{11}M_{22} + M_{12}M_{21} \end{bmatrix}$

Two last properties

- General expression of the transfer matrix

$$M = \frac{1}{f_i} \cdot \begin{bmatrix} F_i & f_i \cdot f_O - F_i \cdot F_O \\ -1 & F_O \end{bmatrix}$$

- Point to point imaging for any system: an objet is at a distance p from an optical system. Where is the image?

$$T_{12} = pqM_{21} + pM_{11} + qM_{22} + M_{12} = 0$$

$$\rightarrow (p - F_o) \cdot (q - F_i) = f_i \cdot f_O$$

Classical thin lens $\frac{1}{p} + \frac{1}{q} = \frac{1}{f}$

FOCUSING ELEMENTS

Electrostatic lenses

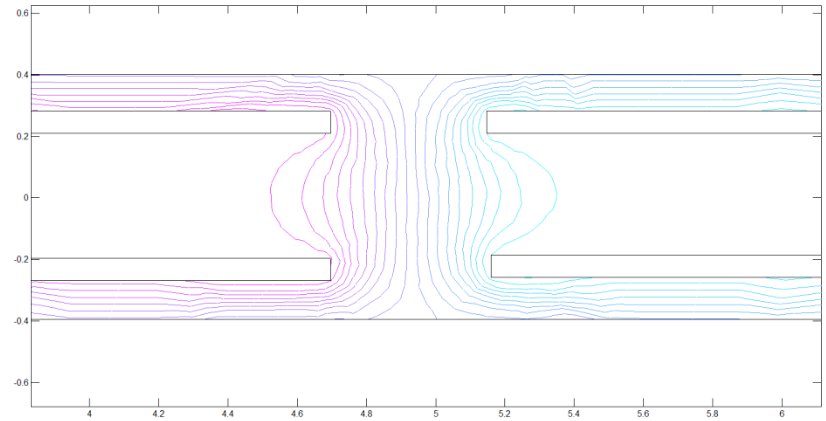
Electrostatic quadrupole

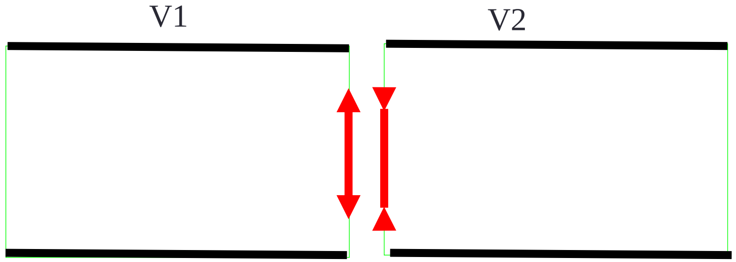
Magnetic quadrupole

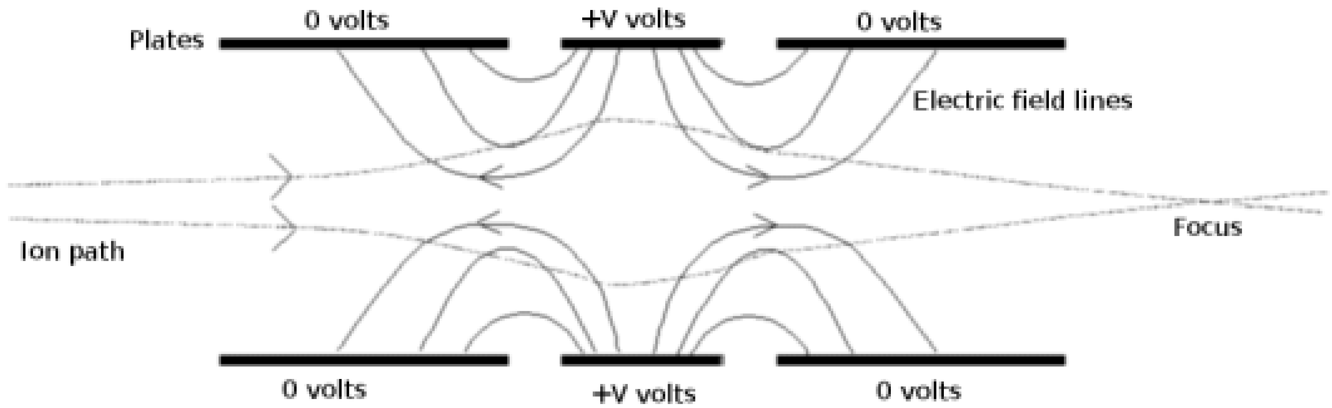
Solenoid

Electrostatic lenses

- Can be flat, round (cylindrical)…
- Can be accelerating or decelerating
- Always focusing







Equation of motion (non relativistic)

- Example on a cylindrical lens
  - Poisson
  - $A_0(s)$ = potential on axis
  - Paraxial equation of motion

$$\Delta V = \frac{\partial^2 V}{\partial s^2} + \frac{1}{r} \cdot \frac{\partial}{\partial r} \cdot \left(r \cdot \frac{\partial V}{\partial r} \right) = 0$$

$$V(r,s) = \sum_{n=0}^{+\infty} A_n(s) \cdot r^{2n}$$

- Same equation for another lens

$$V(r,s) = A_0(s) - \frac{A''_0}{2^2} r^2 + \sum_{n=2}^{+\infty} (-1)^n \frac{A_0^{(2n)}}{(2n!)^2} r^{2n}$$

- In practise:
  - No formula for transfer matrix
  - Tables with principal planes and associated focal lengths
  - Computer codes. Be careful with the numbers (meaning of the focal lengths, again)

$$\boldsymbol{r'' + \frac{A'_0}{2A_0} r' + \frac{A''_0}{4A_0} r = 0}$$

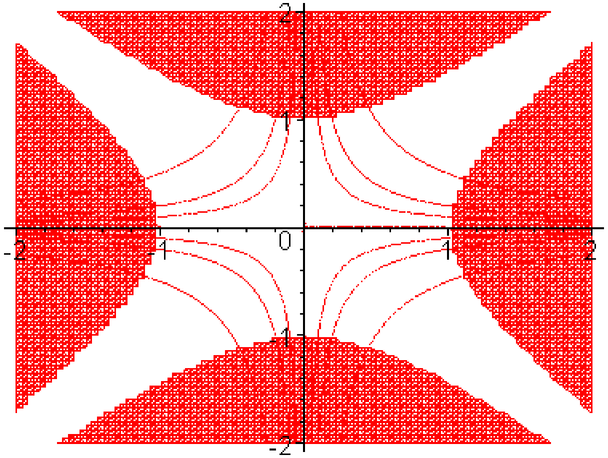
V=0 **MUST** be for v=0

Electrostatic quadrupole

- $\vec{F} = \begin{bmatrix} m\ddot{x} \\ m\ddot{y} \end{bmatrix} = -2q\frac{\Delta V}{R_0^2} \cdot \begin{bmatrix} x \\ -y \end{bmatrix}$
- $x'' = -\frac{g}{v \cdot (B\rho)} x \equiv -K^2 \cdot x$ (case of x-focusing)
- $y'' = \frac{g}{v \cdot (B\rho)} y = K^2 \cdot y$
- $x = x_0 \cdot cos(KL) + x'_0 \cdot \frac{1}{K} \cdot sin(KL)$
- $y = y_0 \cdot ch(KL) + x'_0 \cdot \frac{1}{K} \cdot sh(KL)$

$$V(x, y) = \frac{\Delta V}{R_0^2} \cdot (x^2 - y^2)$$

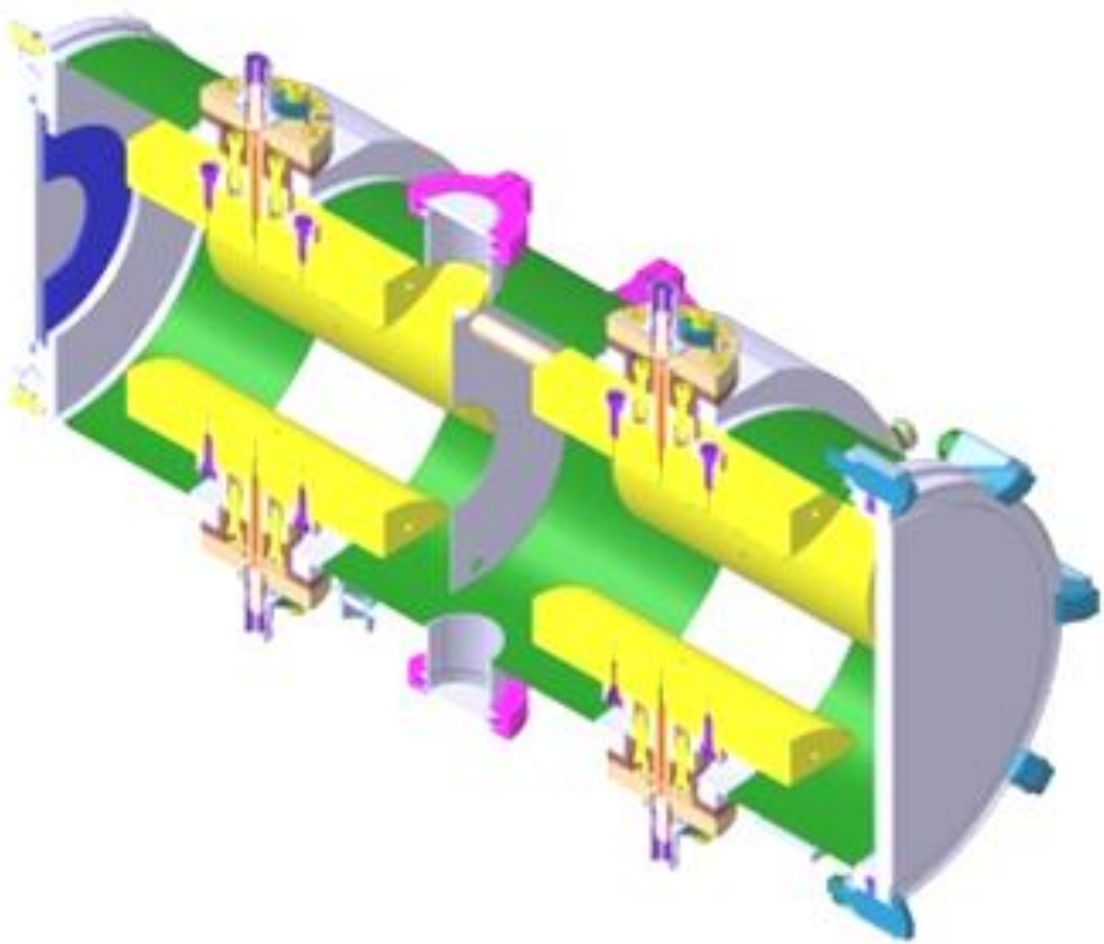
$$g = \frac{2\Delta V}{R_0^2}$$



$$\boxed{K^2 = \frac{g}{v \cdot (B\rho)}}$$

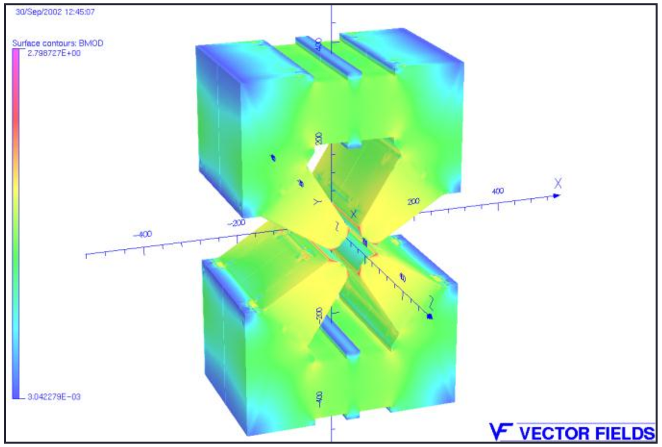
$$M = \begin{bmatrix} \cos(KL) & \sin(KL)/K & 0 & 0 \\ -K\sin(KL) & \cos(KL) & 0 & 0 \\ 0 & 0 & ch(KL) & sh(KL)/K \\ 0 & 0 & Ksh(KL) & ch(KL) \end{bmatrix}$$

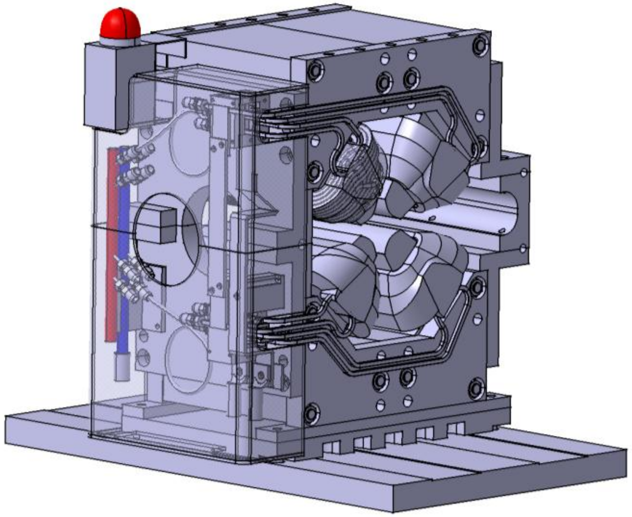
Courtesy Bernard Launé

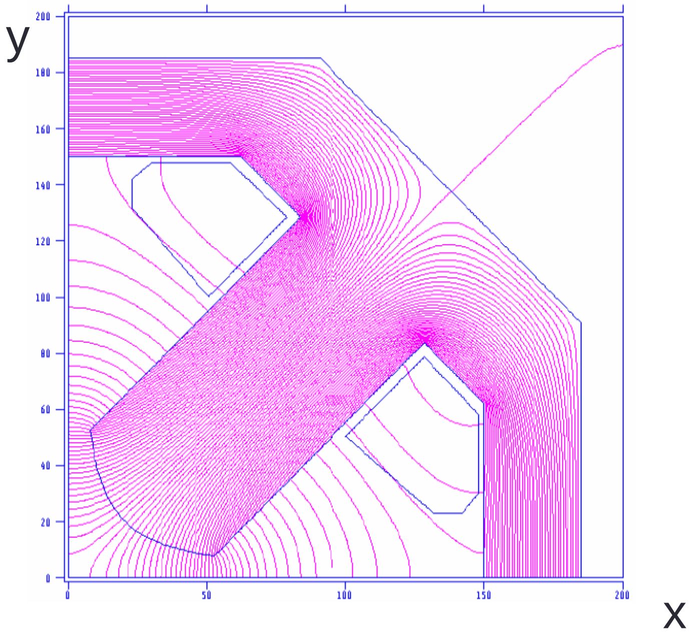


- Inside the vacuum chamber
- No power losses
- Insulators must be protected (collimators)

Magnetic quadrupoles



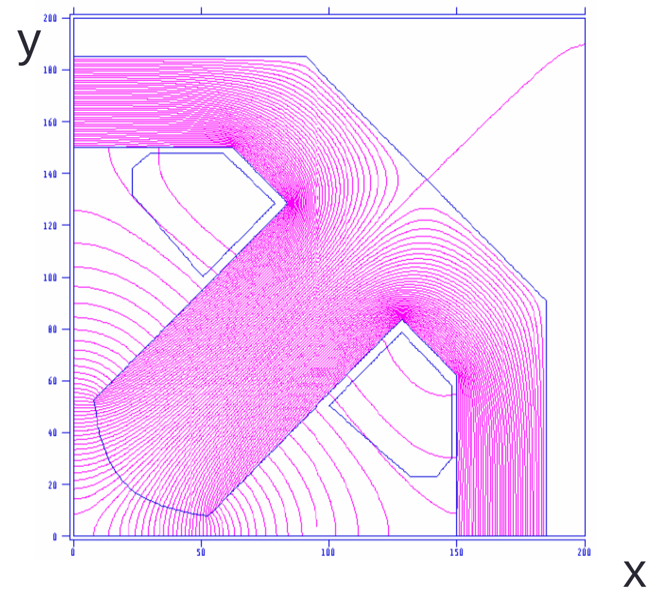




SOLEIL quadrupoles
Courtesy Bernard Launé

Magnetic quadrupole

- Scalar potential: $\phi = gxy$
- Field: $\vec{B} = grad\phi = \begin{bmatrix} gx \\ gy \end{bmatrix}$
- $g = {}^{B_0}/_{R_0}$
- Velocity: longitudinal
- $\vec{F} = q\vec{v} \wedge \vec{B}$
- $x" = -\frac{qvgx}{mv^2} = -\frac{g}{(B\rho)}x$
- $x" = -K^2 x$
- $y" = K^2 x$



$$K^2 = \frac{g}{(B\rho)}$$

$$M = \begin{bmatrix} \cos(KL) & \sin(KL)/K & 0 & 0 \\ -K\sin(KL) & \cos(KL) & 0 & 0 \\ 0 & 0 & ch(KL) & sh(KL)/K \\ 0 & 0 & Ksh(KL) & ch(KL) \end{bmatrix}$$

Optical properties of quadrupoles

- Principal planes (ex foc plane):
- $h_1 = h_2 = \frac{1-M_{11}}{M_{21}} = \frac{1-\cos(KL)}{-K sin(KL)} \sim -\frac{K^2L^2}{2K^2L} = -\frac{L}{2}$
- A quadrupole is equivalent (up to the validity of the approximation before) to a thin lens surrounded by two drift spaces of half-length
- The focal length of the lens is given by:
- $\frac{1}{f} = K^2L$ ie $\frac{2\Delta V \cdot L}{v(B\rho)R_0^2} \sim \frac{\Delta V \cdot L}{TR_0^2}$ (electrostatic, then non relativistic) and $\frac{gL}{(B\rho)} = \frac{B_0 L}{R_0(B\rho)}$ (magnetic)
- A quadrupole is not stigmatic: $|M_{21}| \neq |M_{34}|$

Doublet and triplet of identical quads

- Doublet: FOD (focusing, drift, defocusing)

$$M = \begin{bmatrix} 1 - L/f & L \\ -L/f^2 & 1 + L/f \end{bmatrix}$$

$$h_1 = -f \quad \text{and} \quad h_2 = f$$

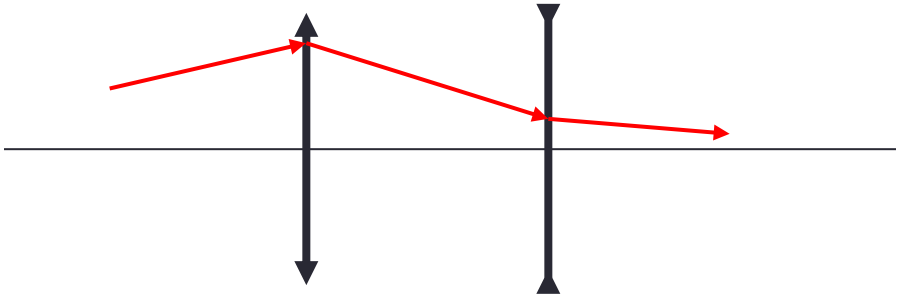
- A doublet is always convergent but never equivalent to a thin lens
- Symmetric triplet: FODOF

$$M = \begin{bmatrix} 1 - 2L^2/f^2 & 2L(1 + \frac{L}{f}) \\ -2L(1 - \frac{L}{f})/f^2 & 1 - 2L^2/f^2 \end{bmatrix}$$

$h_1 = h_2 = \frac{-L}{1-L/f} \sim -L$ if $f \gg L$ (thin lens)

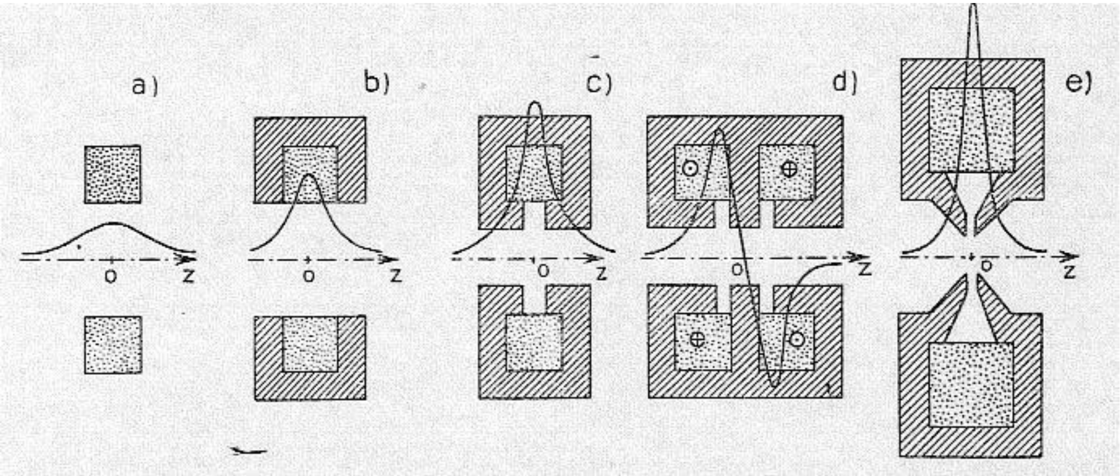
FODO structure

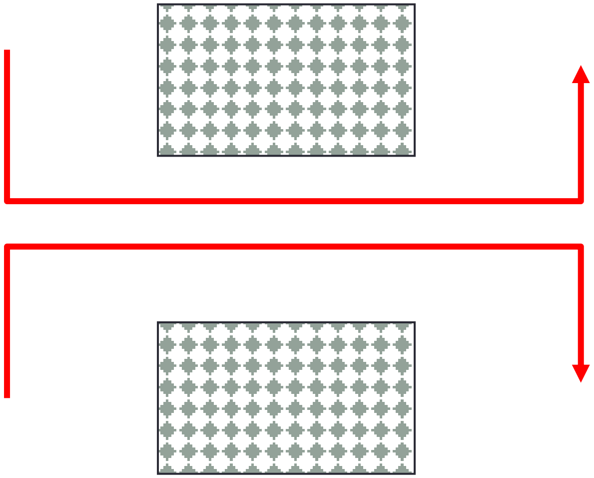
- A quadrupole focusing in one direction is defocusing in the other one
- The only way to have a stable system is to have an alternate gradient structure with identical quadrupoles : the FODO cell
- Exercise: show a FODO cell is always converging

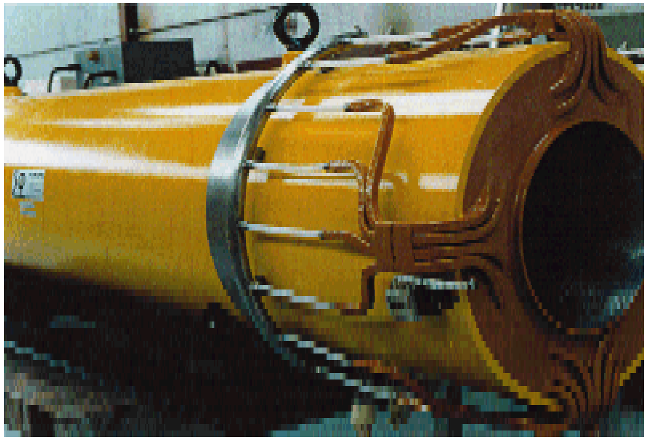


fodo1.xls

Solenoid – Glaser lenses







$$B_s \approx B_0\left(1+\frac{s^2}{a^2}\right)^{-1}$$

$$\frac{1}{f}=\frac{\pi a B_0^2}{8(B\rho)^2}$$

~equivalent to a thin lens

Transfer matrix

- Equation of radial motion

$$r'' + \left[\frac{B_s}{2(B\rho)}\right]^2 \cdot r = 0$$

- Radial focusing+rotation.

$$K = \frac{B_s}{2(B\rho)}$$

- The transfer matrix is the product of a rotation R_{KL} and a focusing matrix N

$$C = \cos(KL)\ and\ S = \sin(KL)$$

- Coupling H/V

$$M = \begin{bmatrix} C^2 & SC/K & SC & S^2/K \\ -KSC & C^2 & -KS^2 & SC \\ -SC & -S^2/K & C^2 & SC/K \\ KS^2 & -SC & -KSC & C^2 \end{bmatrix}$$

$$N = \begin{bmatrix} C & S/K & 0 & 0 \\ -KS & C & 0 & 0 \\ 0 & 0 & C & S/K \\ 0 & 0 & -KS & C \end{bmatrix}$$

$$M = N \cdot R_{KL}$$

MAGNETS

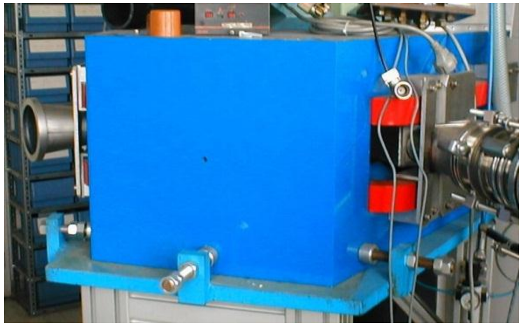
Sector magnet

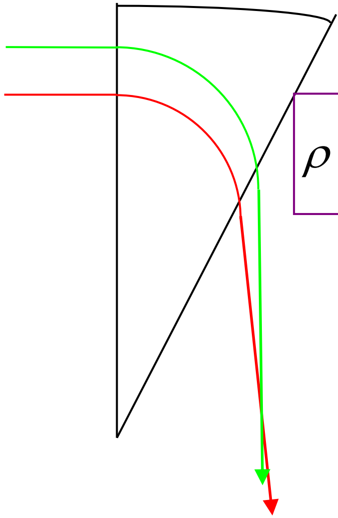
Field index

Edge focusing

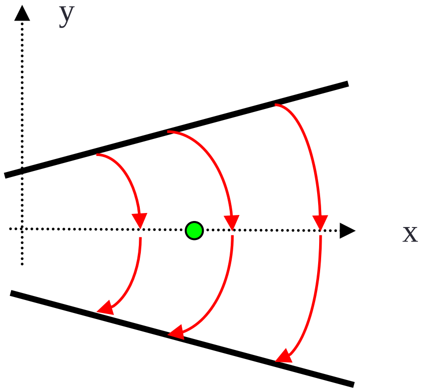
Achromatic systems

Dipole magnet: beam bending and focusing





$$\rho = \frac{(B\rho)}{B}$$



- Here: focusing in the deviation plane
- ***Field index*** : <u>horizontal</u> component out of the middle plane $\rightarrow$ <u>vertical</u> focusing
- The choice of the index allows any kind of focusing
- No index: focusing in the deviation plane, drift space in the other one

$$n = \frac{B_0}{R}\frac{\partial B_y}{\partial x} = -\frac{B_0}{R}\frac{\partial B_x}{\partial y}$$

$$B_y \sim B_0 + \frac{\partial B_y}{\partial x} x = B_0 \cdot \left[1 - \frac{n}{R} x\right]$$

$$B_x = -B_0 \cdot \frac{n}{R} y$$

$$x'' + \frac{1-n}{R^2} x = \frac{1}{R}\frac{\Delta p}{p_0}$$

$$y'' + \frac{n}{R^2} y = 0$$

$$x'' + \frac{1-n}{R^2}x = \frac{1}{R}\frac{\Delta p}{p_0}$$

$$y'' + \frac{n}{R^2}y = 0$$

$$1 - n > 0 \; and \; n > 0$$

$$K_x = \sqrt{\frac{1-n}{R^2}}, K_y = \sqrt{\frac{n}{R^2}}, \theta_x = K_x L, \; \theta_y = K_y L$$

$$C_x = \cos(\theta_x)\,, S_x = sin(\theta_x)\,, C_y = \cos(\theta_y)\,, S_y = sin(\theta_y)\,,$$

$$\begin{bmatrix} C_x & S_x/K_x & 0 & 0 & 0 & \dfrac{(1-C_x)}{RK_x^2} \\ -K_x S_x & C_x & 0 & 0 & 0 & \dfrac{S_x}{RK_x} \\ 0 & 0 & C_y & S_y/K_y & 0 & 0 \\ 0 & 0 & -K_y S_y & C_y & 0 & 0 \\ S_x/RK_x & -(1-C_x)/K_x^2 & 0 & 0 & 1 & -\dfrac{\theta_x - S_x}{R^2 K_x^3} \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$x'' + \frac{1-n}{R^2}x = \frac{1}{R}\frac{\Delta p}{p_0}$$

$$y'' + \frac{n}{R^2}y = 0$$

$$1 - n < 0 \; and \; n > 0$$

$$K_x = \sqrt{\frac{1-n}{R^2}}, K_y = \sqrt{\frac{n}{R^2}}, \theta_x = K_x L,\ \theta_y = K_y L$$

$$C_x = ch(\theta_x)\,,\ S_x = sh(\theta_x)\,,\ C_y = \cos(\theta_y)\,,\ S_y = sin(\theta_y)\,,$$

$$\begin{bmatrix} C_x & S_x/K_x & 0 & 0 & 0 & -\dfrac{(1-C_x)}{RK_x^2} \\ K_x S_x & C_x & 0 & 0 & 0 & \dfrac{S_x}{RK_x} \\ 0 & 0 & C_y & S_y/K_y & 0 & 0 \\ 0 & 0 & -K_y S_y & C_y & 0 & 0 \\ S_x/RK_x & (1-C_x)/K_x^2 & 0 & 0 & 1 & \dfrac{\theta_x - S_x}{R^2 K_x^3} \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$x'' + \frac{1-n}{R^2}x = \frac{1}{R}\frac{\Delta p}{p_0}$$

$$y'' + \frac{n}{R^2}y = 0$$

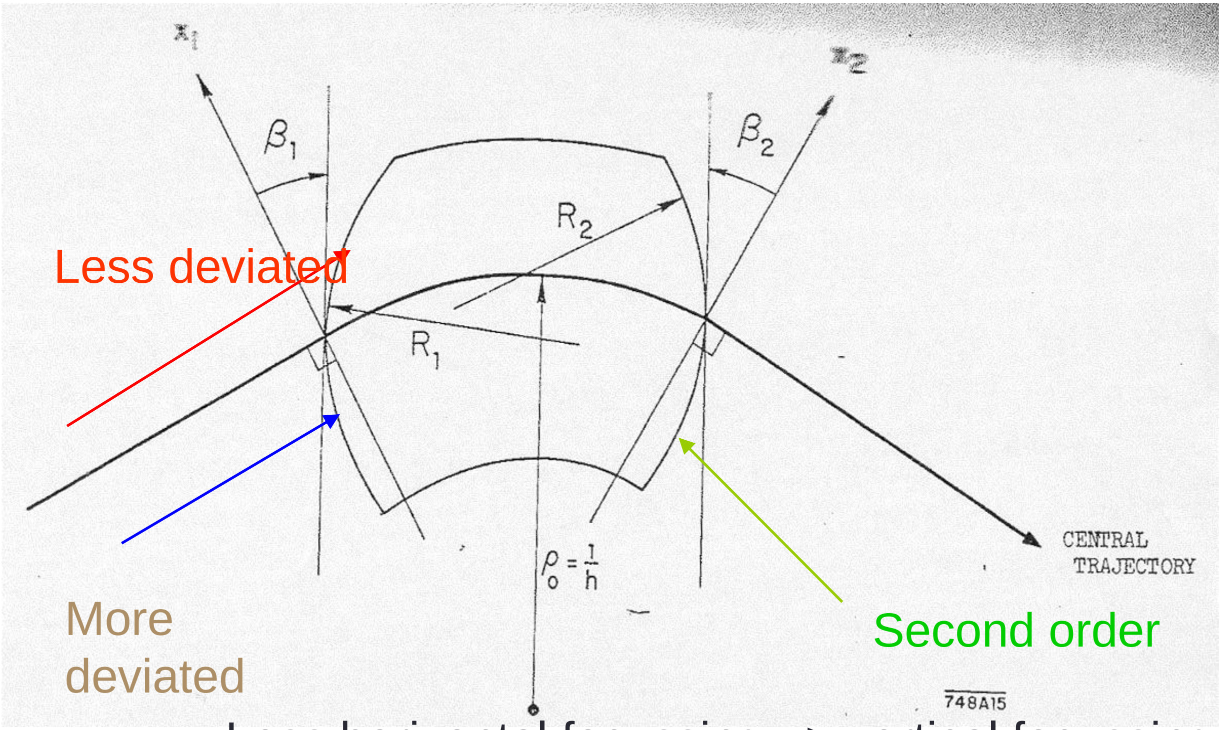
$$1 - n < 0 \; and \; n < 0$$

$$K_x = \sqrt{\frac{1-n}{R^2}}, K_y = \sqrt{\frac{n}{R^2}}, \theta_x = K_x L, \theta_y = K_y L$$

$$C_x = ch(\theta_x), S_x = sh(\theta_x), C_y = ch(\theta_y), S_y = sh(\theta_y),$$

$$\begin{bmatrix} C_x & S_x/K_x & 0 & 0 & 0 & -\frac{(1-C_x)}{RK_x^2} \\ K_x S_x & C_x & 0 & 0 & 0 & \frac{S_x}{RK_x} \\ 0 & 0 & C_y & S_y/K_y & 0 & 0 \\ 0 & 0 & K_y S_y & C_y & 0 & 0 \\ S_x/RK_x & (1-C_x)/K_x^2 & 0 & 0 & 1 & \frac{\theta_x - S_x}{R^2 K_x^3} \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

Edge focusing



Less horizontal focussing => vertical focussing

Edge focusing provides more focusing in one plane and the opposite (less focusing) in the other plane

$$\left|\frac{1}{f}\right| \approx \frac{1}{\rho} tan\beta$$

remark

- If the edge angle is defocusing in the deviation plane and equal to ¼ rotation angle, the global focusing is ~identical in each plane
- If the edge angle is defocusing in the deviation plane and equal to ½ rotation angle, there no longer focusing in the deviation plane (drift) : use of rectangular magnets

¼ angle sur chaque face: ~même focalisation x/y

$$\begin{bmatrix} 4\cos\left(\frac{\theta}{4}\right)^2-3 & ro\sin(\theta) & 0 & 0 \\ -\frac{2\sin\left(\frac{\theta}{4}\right)}{\cos\left(\frac{\theta}{4}\right)ro} & 4\cos\left(\frac{\theta}{4}\right)^2-3 & 0 & 0 \\ 0 & 0 & 1-\tan\left(\frac{\theta}{4}\right)\theta & ro\,\theta \\ 0 & 0 & \frac{\tan\left(\frac{\theta}{4}\right)\left(-2+\tan\left(\frac{\theta}{4}\right)\theta\right)}{ro} & 1-\tan\left(\frac{\theta}{4}\right)\theta \end{bmatrix}$$

Angle ½ on chaque face : espace deglissement dans le plan de déviation

$$\begin{bmatrix} 1 & ro\sin(\theta) & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1-\tan\left(\frac{\theta}{2}\right)\theta & ro\,\theta \\ 0 & 0 & \frac{\tan\left(\frac{\theta}{2}\right)\left(-2+\tan\left(\frac{\theta}{2}\right)\theta\right)}{ro} & 1-\tan\left(\frac{\theta}{2}\right)\theta \end{bmatrix}$$

Dispersion, achromats

- Let the system to be dispersive
- D = Dispersion function
- Separation versus <u>momentum</u>
- Spot size is increased

$$x'' + \frac{p'}{p} x' + k(s) x = \frac{1}{\rho} \frac{\Delta p}{p_0}$$

$$\begin{cases} x(s) = C(s) x_0 + S(s) x'_0 + D(s) \dfrac{\Delta p}{p_0} \\ x'(s) = C'(s) x_0 + S'(s) x'_0 + D'(s) \dfrac{\Delta p}{p_0} \end{cases}$$

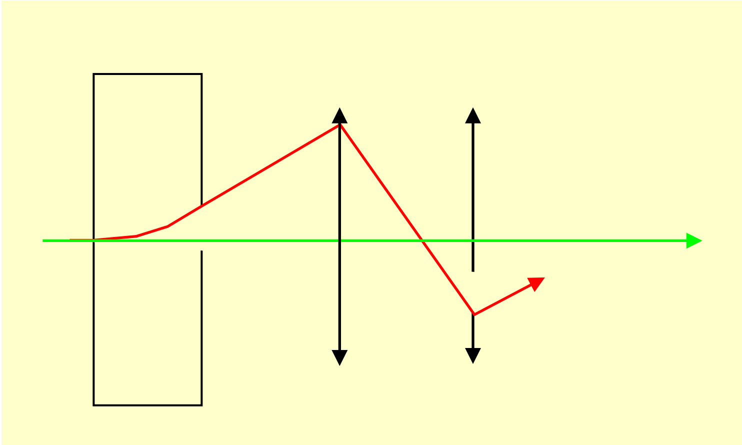
$$\sigma_x = \sqrt{\sigma_0^2 + D^2 \sigma_{\Delta p / p_0}^2}$$

- Make D=D'=0

→ Achromatic system

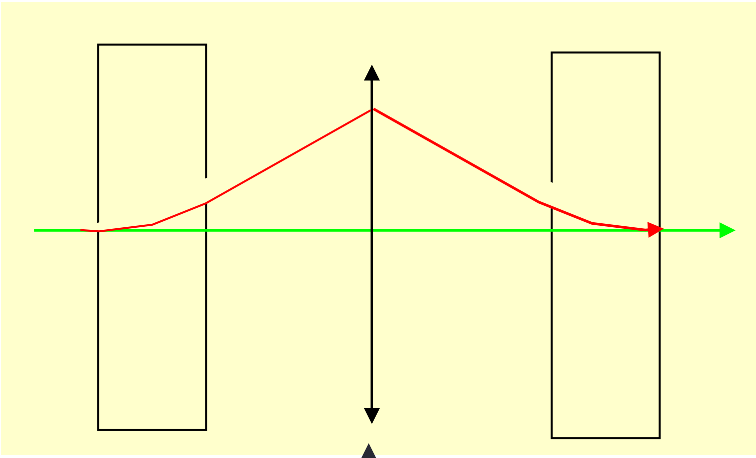
Achromats

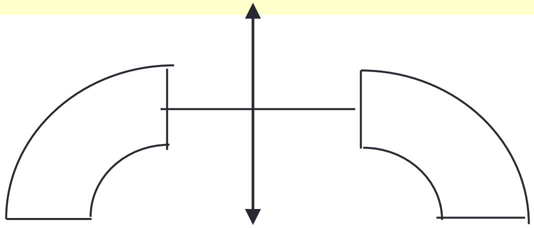
- Dispersive system



- One example

And for counterwise rotation?





Example

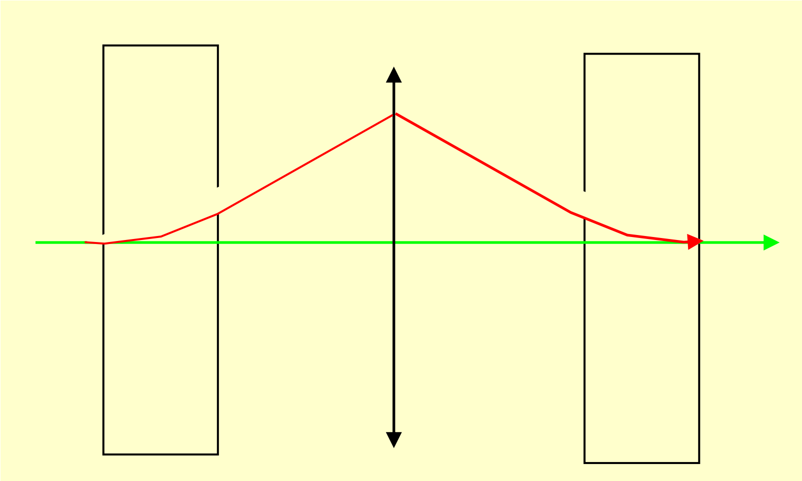
$$D_{dip} = \rho(1-\cos\theta)$$

$$D'_{dip} = \sin\theta$$

$$\Rightarrow \begin{cases} D_{in} = \rho(1-\cos\theta) + L\sin\theta \\ D'_{in} = \sin\theta \end{cases}$$

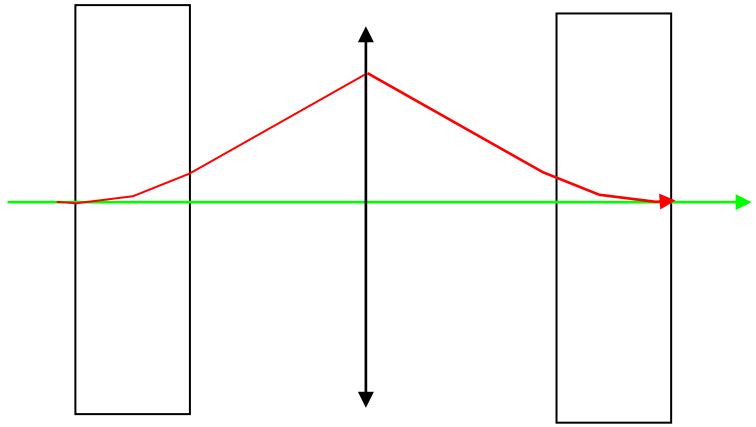
$$\Rightarrow \begin{cases} D_{out} = D_{in} \\ D'_{out} = D'_{in} - \dfrac{D_{in}}{f} \equiv -D'_{in} \end{cases}$$

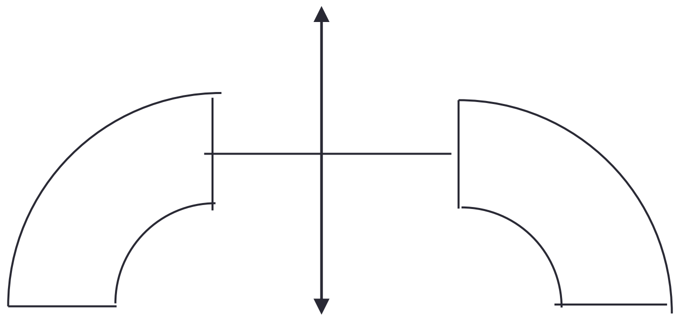
$$\Rightarrow f = \frac{D_{in}}{2D'_{in}} = \frac{\rho(1-\cos\theta) + L\sin\theta}{2\sin\theta}$$



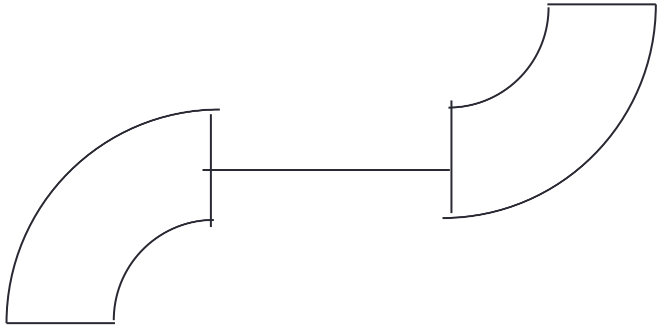
- One lens is needed
- In fact: one triplet
- Achromat+foc

The achromatic chicane





?



examples

The lens is converging for median-plane motion and diverging for vertical,

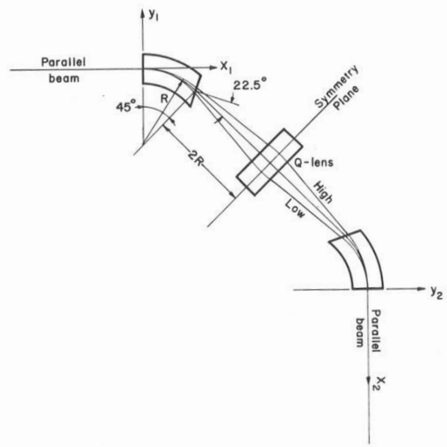
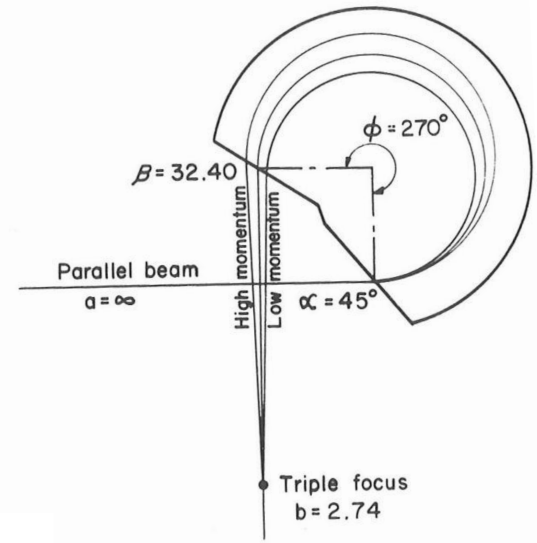


FIG. 12. Achromatic magnet system after K. L. Brown (Penner, 1961).

4.2 DEFLECTING MAGNETS



10. Nondispersive stigmatic right-angle magnet.

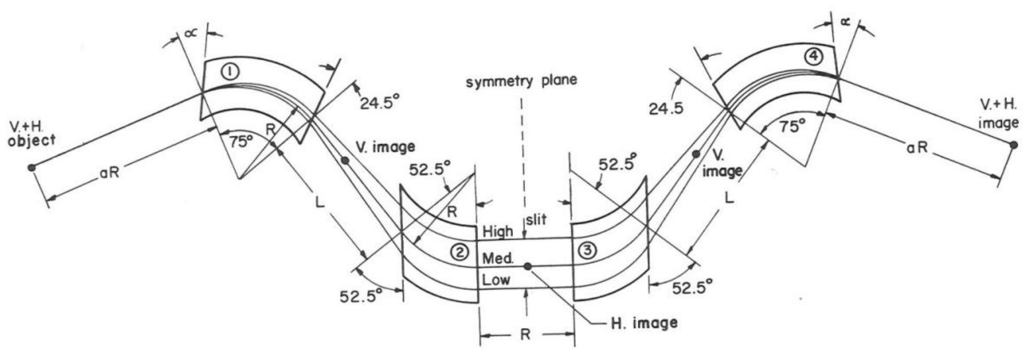


FIG. 13. Achromatic magnet system after H. A. Enge (1961).

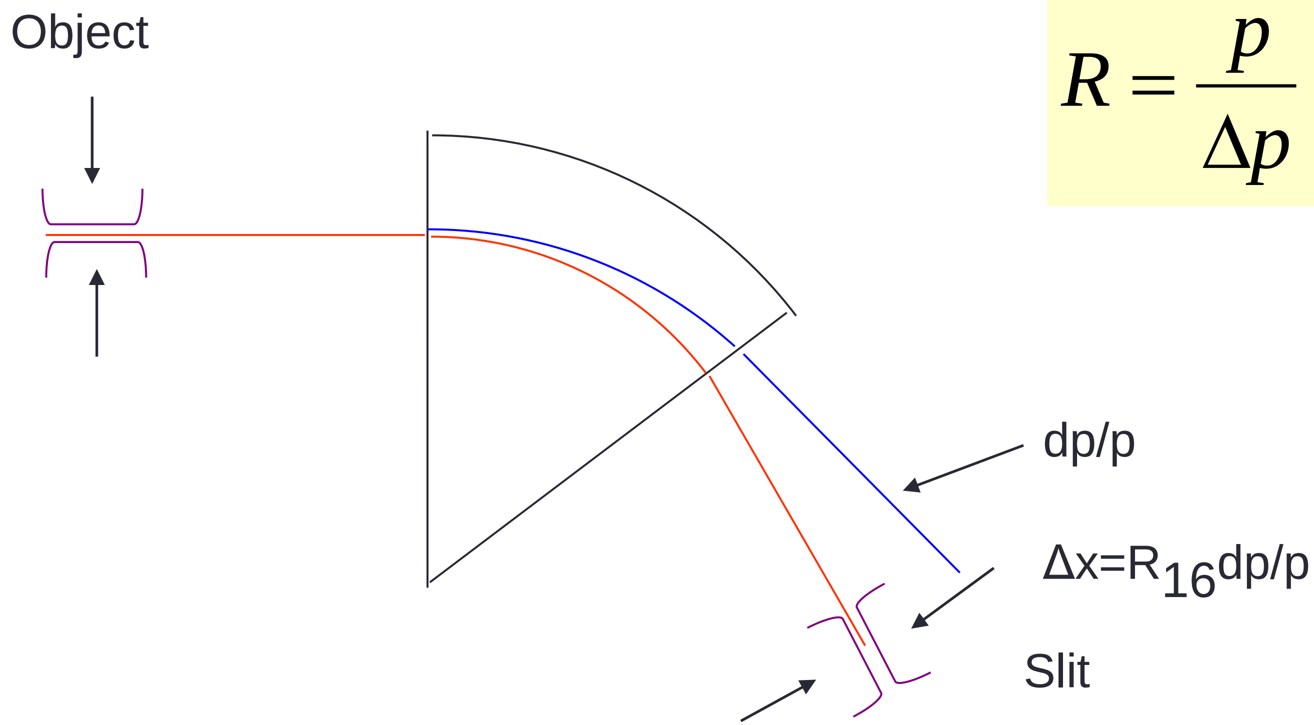
HARALD A. ENGE

Courtesy Bernard Launé

Spectrometer (magnetic separation only)

Résolution

$$R = \frac{p}{\Delta p} = \frac{D}{2Gx_e}$$

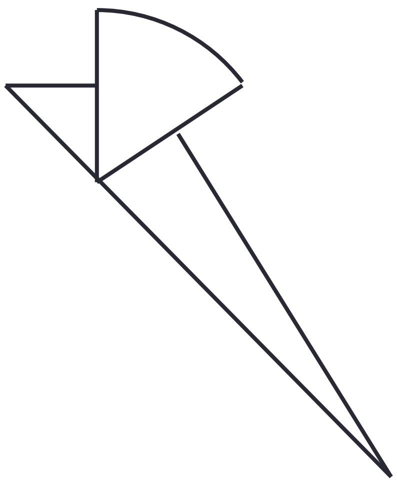


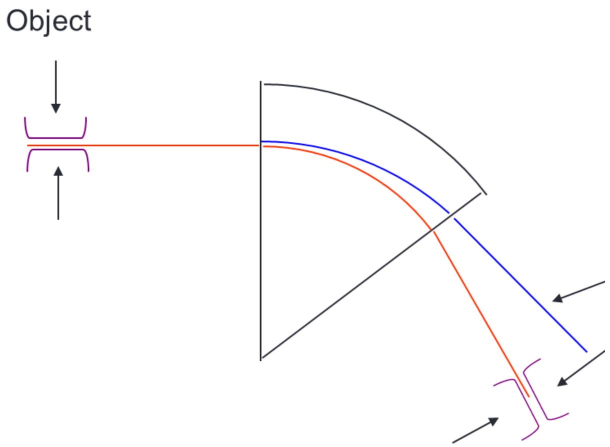
Spectrometer design

- Point to point imaging $\rightarrow$system size
- Waist to Waist imaging
- Beam size: $R_S = |M_{11}| \cdot R_E$
- Analysis if $D\frac{\Delta P}{P} = 2R_S$

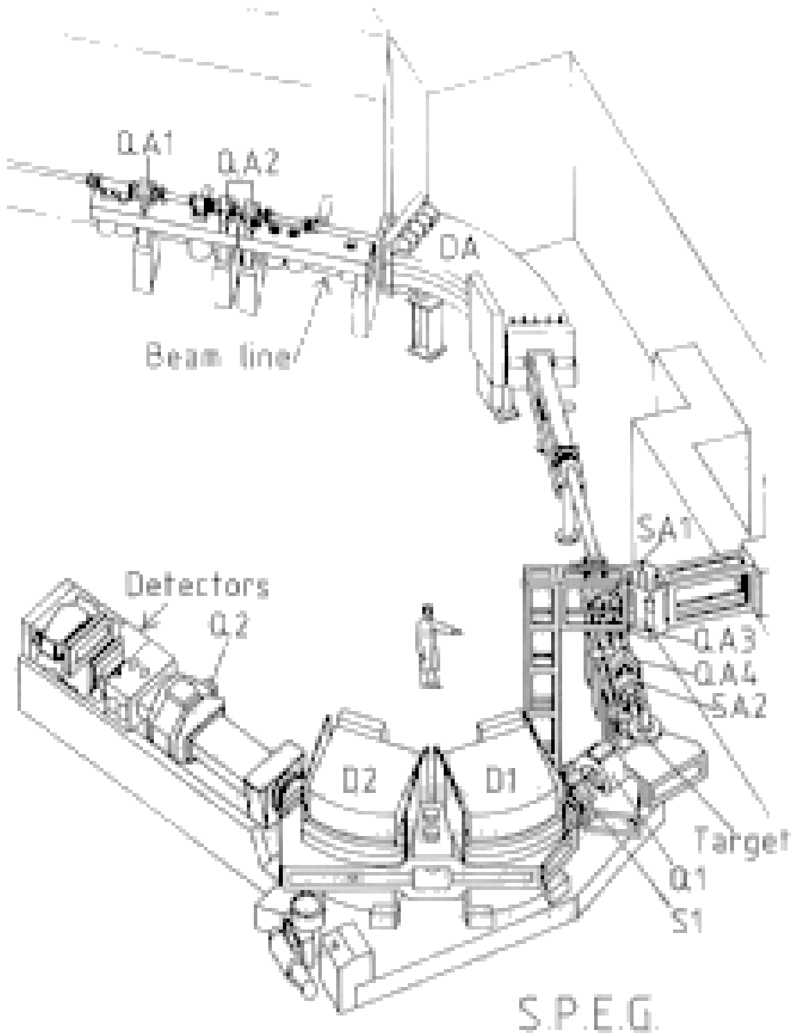
$$\frac{p}{\Delta p} = \frac{D}{2|M_{11}| \cdot R_E}$$

- Resolution is directly depending on the magnetic area covered by the beam, not by optics
- Optics has operational aspects (ex: achievable slit size) and low effect on resolution





SPEG spectrometer (GANIL)

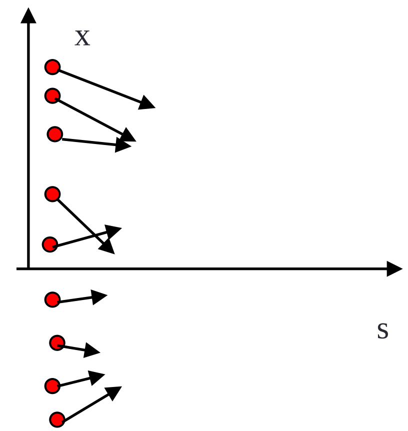


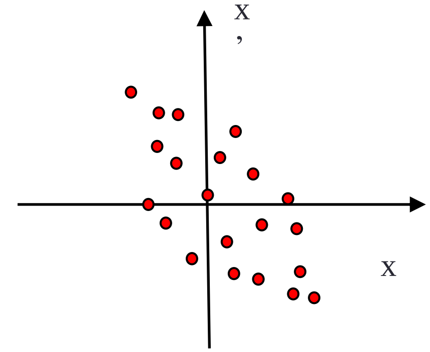
BEAM TRANSPORT

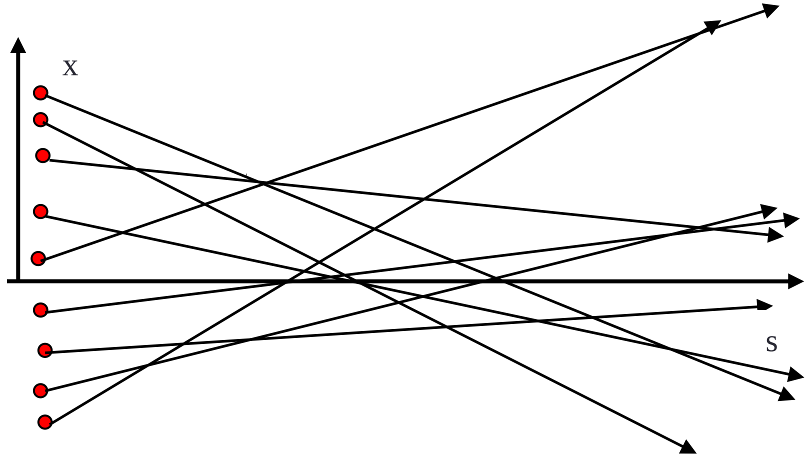
Beam description: emittance, RMS emittance
Emittance transport, Liouville theorem
Courant-Snyder invariant – Twiss matrix
Emittance matching
Emittance measurements(examples)
Collimators

Global description of a beam (2D case)

- Ex: trajectories of individual particles in a drift space
- Need of a global description
- Need to describe convergence, divergence, beam enveloppe
- Need to describe extrema beam enveloppe (“waist”)
- RMS description of the beam







Beam matrix

- Beam matrix
  - Covariance matrix in phase space
  - Here (x, x') only)
  - RMS beam extension in phase space (nD variance)

$$X = \begin{bmatrix} x \\ x' \end{bmatrix} \rightarrow \tilde{X} = \begin{bmatrix} x & x' \end{bmatrix}$$

$$X\tilde{X} = \begin{bmatrix} x^2 & xx' \\ xx' & x'^2 \end{bmatrix} \rightarrow < X\tilde{X} > = \begin{bmatrix} < x^2 > & < xx' > \\ < xx' > & < x'^2 > \end{bmatrix} \equiv \Sigma$$

- Linear transport easy

$$Y = MX \Rightarrow Y\tilde{Y} = MX\tilde{X}\tilde{M}$$

$$\Rightarrow < Y\tilde{Y} > = M < X\tilde{X} > \tilde{M}$$

$$\Rightarrow \Sigma_1 = M\Sigma_0\tilde{M}$$

- Transformation is a tensorial transform

→Not a matrix but a tensor

→Matrix: tranformation

→Tensor: property (here: RMS extent)

Emittance (Twiss) parameters

- From the beam matrix
- Defines the ellipses including n% of the beam in an RMS (intuitive) sense.
- The ellipse corresponding to ε_{RMS} is the concentration ellipse
- Warning; RMS emittance definition changes upon authors, by a factor ½, 2 or 4…

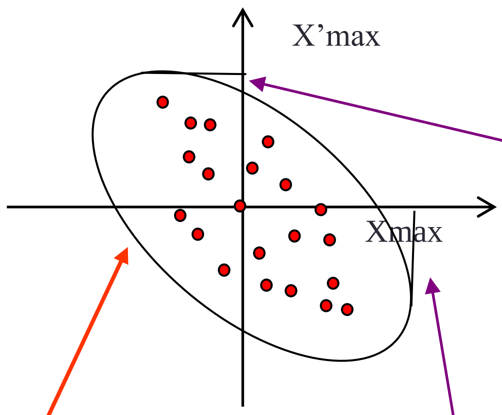
$$\Sigma = \begin{bmatrix} <x^2> & <xx'> \\ <xx'> & <x'^2> \end{bmatrix} \equiv \begin{bmatrix} \beta\varepsilon_{RMS} & -\alpha\varepsilon_{RMS} \\ -\alpha\varepsilon_{RMS} & \gamma\varepsilon_{RMS} \end{bmatrix}$$

$$\beta\gamma - \alpha^2 \equiv 1$$

$$\Rightarrow \begin{cases} \varepsilon_{RMS} = \sqrt{\det(\Sigma)} = \sqrt{<x^2><x'^2> - (<xx'>)^2} \\ \beta = \dfrac{<x^2>}{\varepsilon_{RMS}} \\ \alpha = -\dfrac{<xx'>}{\varepsilon_{RMS}} \end{cases}$$

Not to be confused with Lorentz factors

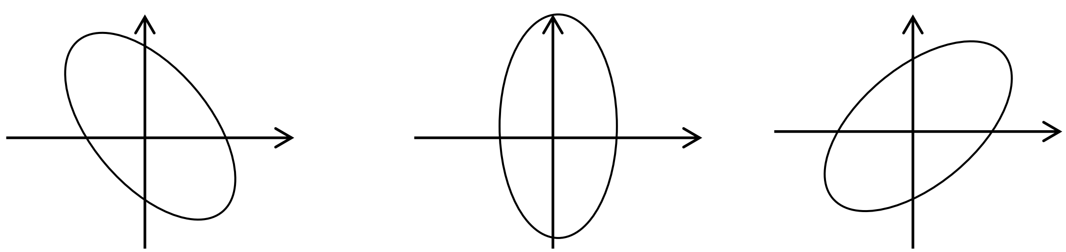
Ellipses



$$A = \pi\varepsilon$$

$$x_{\max} = \sqrt{\beta\varepsilon}$$
$$x'_{\max} = \sqrt{\gamma\varepsilon}$$

$$\beta x'^2 + 2\alpha x x' + \gamma x^2 = \varepsilon$$



α>0 (convergent) α=0 (waist) α<0 (divergent)

- RMS ellipses
- Include more or less (ex : 95%) particles.
- 4 paramèters (α,β,γ,ε) – in fact 3.

- Ex: if the beam is gaussian in two dimensions, the number of particles in the ellipse is $N_0 \cdot [1 - exp(-\varepsilon/2\varepsilon_{RMS})]$
- σ_ε =2ε_{RMS} is the emittance standard deviation
  - σ_ε includes 63%
  - 2 σ_ε includes 86%
  - 3 σ_ε includes 95%

Emittance transport

- Explicit formula

$$\boxed{\begin{bmatrix}\beta\\ \alpha\\ \gamma\end{bmatrix}_1=\frac{1}{\Delta}\begin{bmatrix}M_{11}^2 & -2M_{11}M_{12} & M_{12}^2\\ -M_{11}M_{21} & M_{12}M_{21}+M_{11}M_{22} & -M_{22}M_{12}\\ M_{21}^2 & -2M_{22}M_{21} & M_{22}^2\end{bmatrix}\begin{bmatrix}\beta\\ \alpha\\ \gamma\end{bmatrix}_0}$$

- Beam RMS enveloppe

$$\sqrt{<x^2>}=\sqrt{\beta\cdot\varepsilon_{rms}}$$

- α versus β

$$x(s+ds)=x(s)+x'(s)ds \rightarrow M_{ds}=\begin{bmatrix}1 & ds\\ \dots & \dots\end{bmatrix}$$

$$\beta(s+ds)=\beta(s)-2\alpha\cdot ds$$

$$\boldsymbol{\alpha=-\frac{\beta'}{2}}$$

- Enveloppe extremum if α=0 (waist)

Courant/Snyder invariant – Emittance matching

- Consider a periodic system made of identical cells (no acceleration). Let M be the matrix of each cell. M has 2 eigenvalues λ and $1/\lambda$ (determinant is 1)
- Suppose the motion to be stable, then λ^n and $1/\lambda^n$ must be bounded for any value of n (integer)
- The only way is $|\lambda| = 1 = |1/\lambda| \rightarrow \lambda = e^{i\mu}$
- $\rightarrow Tr(M) = \lambda + \frac{1}{\lambda} = 2\cos(\mu)$
- The motion is stable if and only if $0 \leq \frac{1}{2} Tr(M) < 1$

Courant/Snyder invariant – Emittance matching

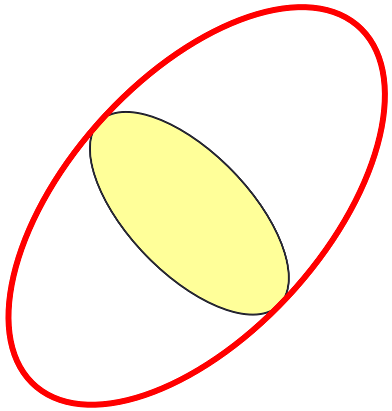
- Suppose the motion to be stable
- The following formulas are straighforward, with the transfer matrix TWISS parameters

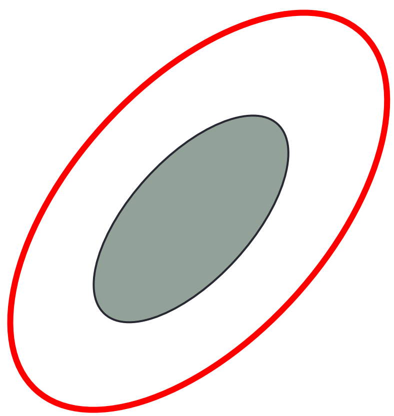
$$M = \begin{bmatrix} \cos\mu + \alpha^* \sin\mu & \beta^* \sin\mu \\ \gamma^* \sin\mu & \cos\mu - \alpha^* \sin\mu \end{bmatrix}$$

$$M = \cos\mu \cdot \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} + \sin\mu \cdot \begin{bmatrix} \alpha^* & \beta^* \\ \gamma^* & -\alpha^* \end{bmatrix} \equiv \cos\mu \cdot I + \sin\mu \cdot J$$

$$J^2 = -1$$

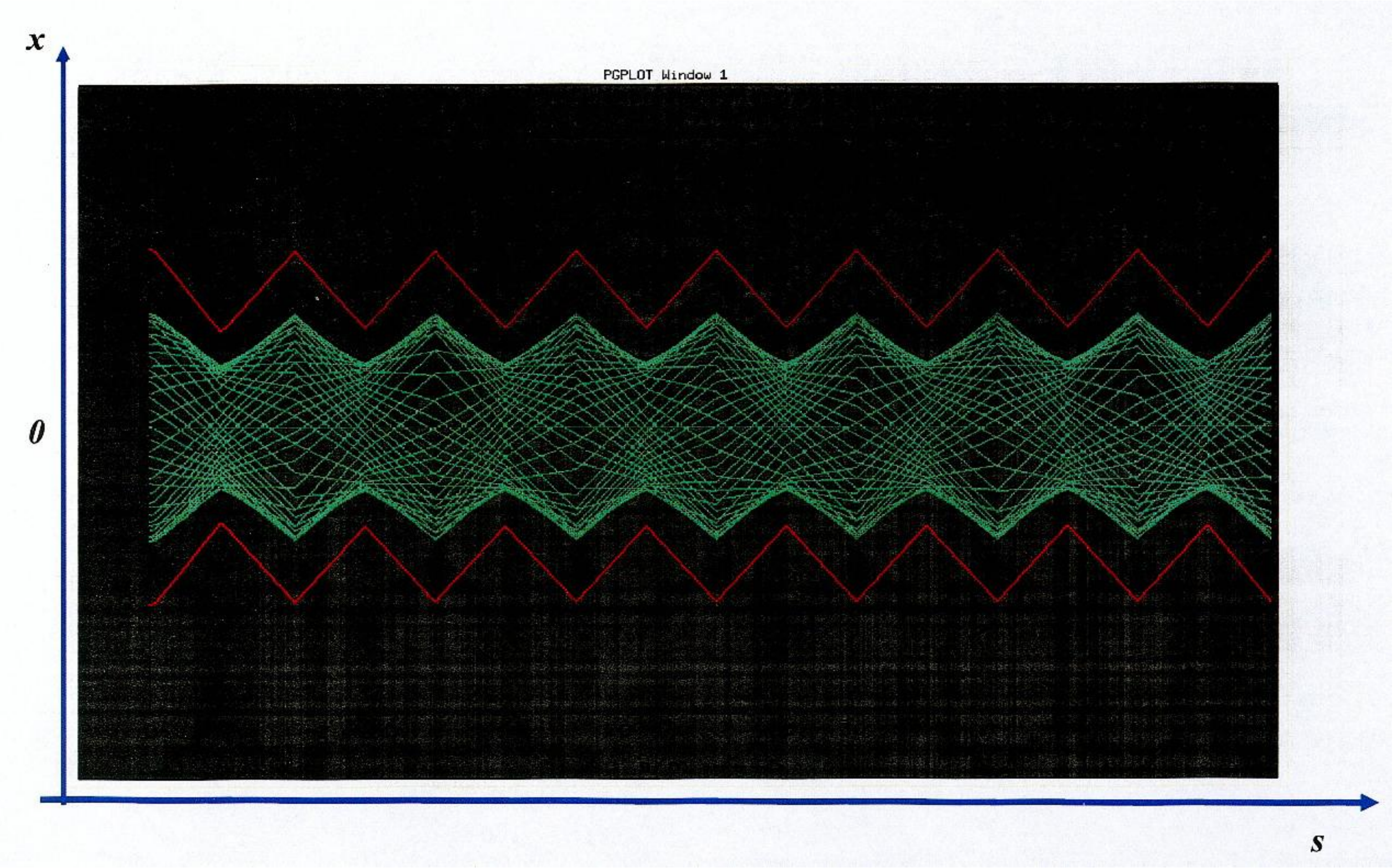
$$M \cdot \begin{bmatrix} \beta^* & -\alpha^* \\ -\alpha^* & \gamma^* \end{bmatrix} \cdot \tilde{M} = \begin{bmatrix} \beta^* & -\alpha^* \\ -\alpha^* & \gamma^* \end{bmatrix}$$





Emittance matching: if the injected emittance Twiss parameters are equal to the system Twiss parameters, the oscillations of the beam enveloppe are minimized, and the beam occupies less space in phase space.

Beam matching



Liouville Theorem (2D)

- Let X_1 and X_2 be to vectors in phase space

$$Y_1 = M \cdot X_1 \; and \; Y_2 = M \cdot X_2$$

$$det[Y_1 \quad Y_2] = \det(M) \cdot det[X_1 \quad X_2] = \frac{p_e}{p_s} \cdot det[X_1 \quad X_2]$$

- The area in phase space varies accordingly to momentum
- →the area is constant if there is no acceleration
- →$\beta_{Lorentz} \cdot \gamma_{Lorentz} \cdot \varepsilon$ is constant (normalized emittance)

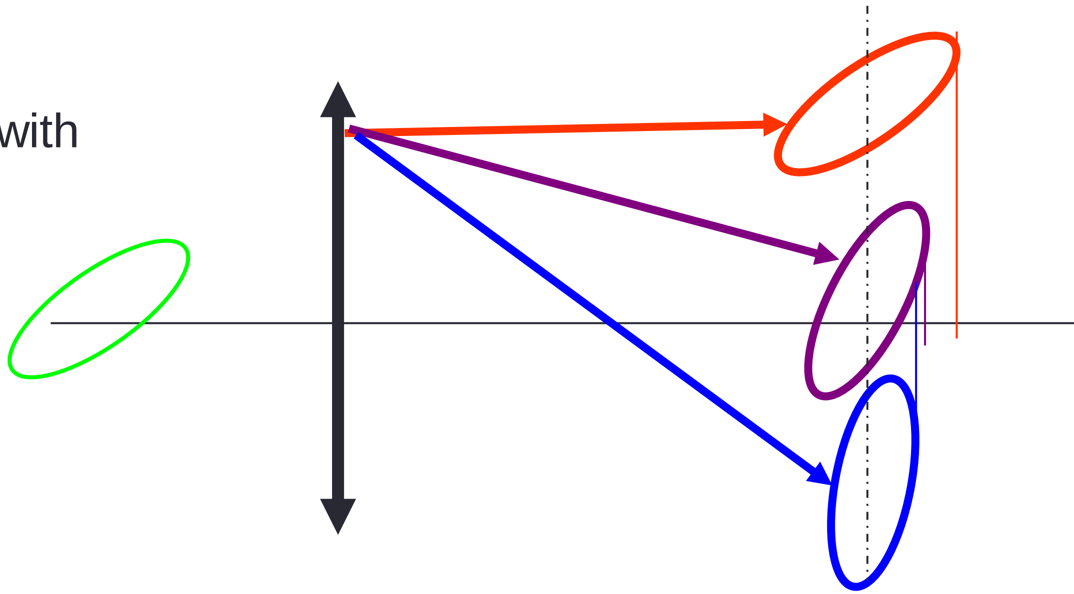
- Warning: if the motion is not linear, the “apparent” RMS emittance varies, even the surface in phase space is constant

A few words about emittance measurements

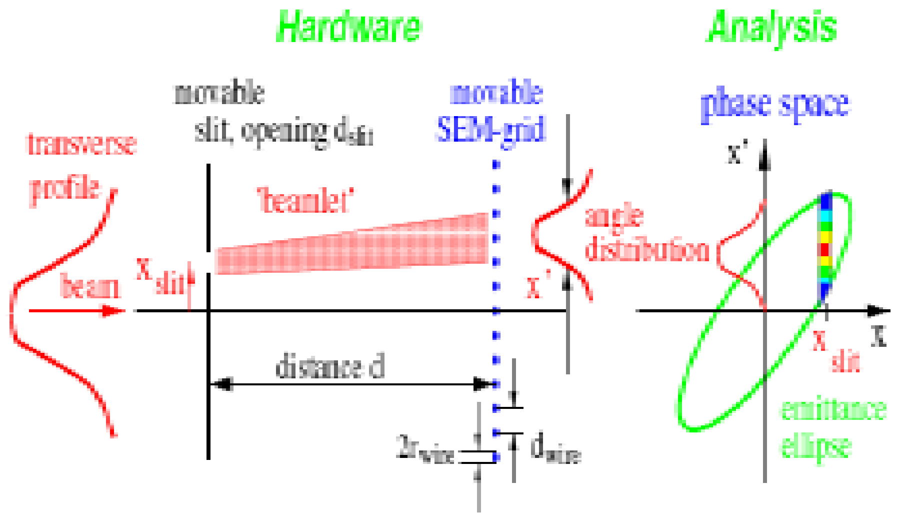
- The RMS enveloppe varies with focusing
- It is related to the initial emittance parameters
- A known lens (system) is used with differents tunings
- N profile (RMS) measurements are made
- N equation with 4 unknown are obtained
- Warning: numerically unstable with solenoids (even if a theoretical solution exists)

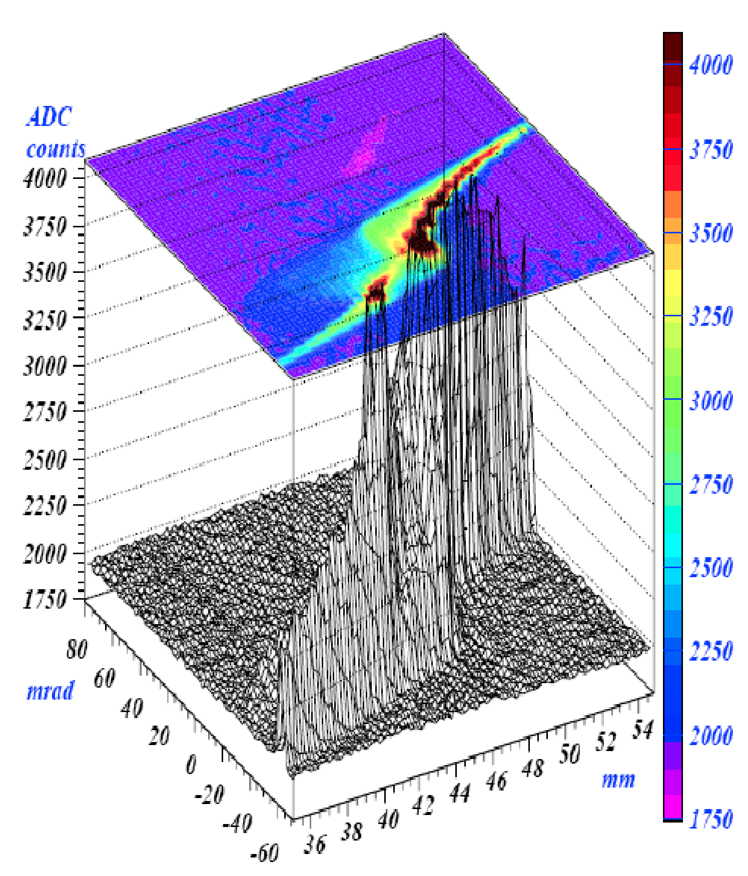
$$< x^2 >= \sigma_0^2 = \beta_0 \varepsilon_{RMS}$$

$$\sigma^2 = \left(A\beta + B\alpha + C\gamma\right)\varepsilon_{RMS}$$



Moving slit (real phase picture)

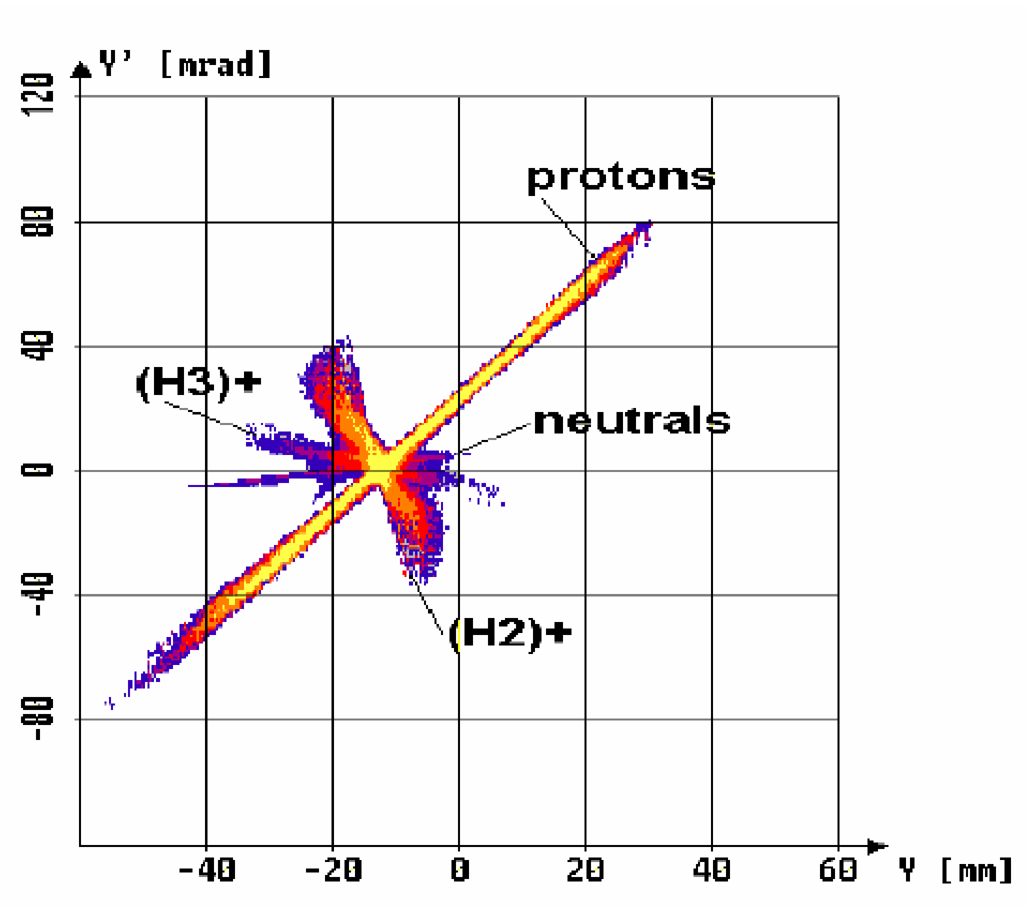




Elliptic shape might be far from reality at low energy

Courtesy Bernard Launé

The reality (SILHI source, Saclay)



Saclay source SILHI

Courtesy Bernard Launé

Collimators on some examples

- Collimator: $\begin{bmatrix} A \\ \lambda \end{bmatrix}$ (A=aperture, $\lambda \in \mathbb{R}$)
- M: transfer matrix from collimator to target
- Case 1:$M_{22} = 0$. A horizontal line is transformed to an horizontal one. No effect on beam size
- Case 2:$M_{12} = 0$. A vertical line is transformed to an vertical one. Effect is maximum. In this case $R_{target} = |M_{11}| \cdot A$