

# 2D wall impedance theory

Nicolas Mounet & Elias Métral

Acknowledgments: N. Biancacci, G. Rumolo, B. Salvant, C. Zannini, B. Zotter.

# 2D wall impedance theory

- Motivation
- Outline of the theory
- Examples of impedance results
- Computation of wake functions
- Possible extensions
- Conclusions

# Motivations for 2D analytical impedance models

- 3D simulation tools can nowadays solve EM problems taking into account **material electromagnetic properties**, BUT:
  - difficult to have in single simulation both low and high frequency content,
  - usually difficult to mix small and large scale features (e.g. thin coating on top of thick jaw),
  - always useful to compare with analytical formulas for benchmark and/or better understanding,

# Motivations for 2D analytical impedance models

- 3D simulation tools can nowadays solve EM problems taking into account **material electromagnetic properties**, BUT:
  - difficult to have in single simulation both low and high frequency content,
  - usually difficult to mix small and large scale features (e.g. thin coating on top of thick jaw),
  - always useful to compare with analytical formulas for benchmark and/or better understanding,
- **analytical approaches** are useful in particular for **resistive** effects,
- but can handle only **simple geometries**.

# Motivations for 2D analytical impedance models

- 3D simulation tools can nowadays solve EM problems taking into account **material electromagnetic properties**, BUT:
  - difficult to have in single simulation both low and high frequency content,
  - usually difficult to mix small and large scale features (e.g. thin coating on top of thick jaw),
  - always useful to compare with analytical formulas for benchmark and/or better understanding,
- **analytical approaches** are useful in particular for **resistive** effects,
- but can handle only **simple geometries**.
- In **2D axisymmetric**, **Zotter's** theory (CERN-AB-2005-043) is the most general theory to date, but it's **numerical implementation** was still an issue.

# Motivations for 2D analytical impedance models

- 3D simulation tools can nowadays solve EM problems taking into account **material electromagnetic properties**, BUT:
  - difficult to have in single simulation both low and high frequency content,
  - usually difficult to mix small and large scale features (e.g. thin coating on top of thick jaw),
  - always useful to compare with analytical formulas for benchmark and/or better understanding,
- **analytical approaches** are useful in particular for **resistive** effects,
- but can handle only **simple geometries**.
- In **2D axisymmetric**, **Zotter's** theory (CERN-AB-2005-043) is the most general theory to date, but it's **numerical implementation** was still an issue.
- For **flat infinite plates** (~collimator jaws), several formalisms exist (**Piwinski** *DESY* 84-097 & *DESY-HERA* 92-04, **Henke-Napoly** *EPAC'90* p.1046, **Gluckstern** et al *Phys. Rev. E* 47:656, **Yokoya** *Part. Acc.* 41:221, **Burov-Lebedev** *EPAC'02* p. 1455), all with **limitations** in number of layers, materials properties or frequency range.

# Motivations for 2D analytical impedance models

- 3D simulation tools can nowadays solve EM problems taking into account **material electromagnetic properties**, BUT:
  - difficult to have in single simulation both low and high frequency content,
  - usually difficult to mix small and large scale features (e.g. thin coating on top of thick jaw),
  - always useful to compare with analytical formulas for benchmark and/or better understanding,
- **analytical approaches** are useful in particular for **resistive** effects,
- but can handle only **simple geometries**.
- In **2D axisymmetric**, Zotter's theory (CERN-AB-2005-043) is the most general theory to date, but its **numerical implementation** was still an issue.
- For **flat infinite plates** (~collimator jaws), several formalisms exist (Piwinski *DESY* 84-097 & *DESY-HERA* 92-04, Henke-Napoly *EPAC'90* p.1046, Gluckstern et al *Phys. Rev. E* 47:656, Yokoya *Part. Acc.* 41:221, Burov-Lebedev *EPAC'02* p. 1455), all with **limitations** in number of layers, materials properties or frequency range.
- ⇒ develop here **axisym. and flat 2D theories** based on Zotter's formalism (details in EPFL PhD thesis 5305, 2012).

# 2D wall impedance theory

- 2D models: consider a **longitudinally smooth** element in the ring, of infinite length, and integrate the EM force from the source particle to the test particle, over a finite length.  
⇒ Neglect thus all **edge** effects.



# 2D wall impedance theory

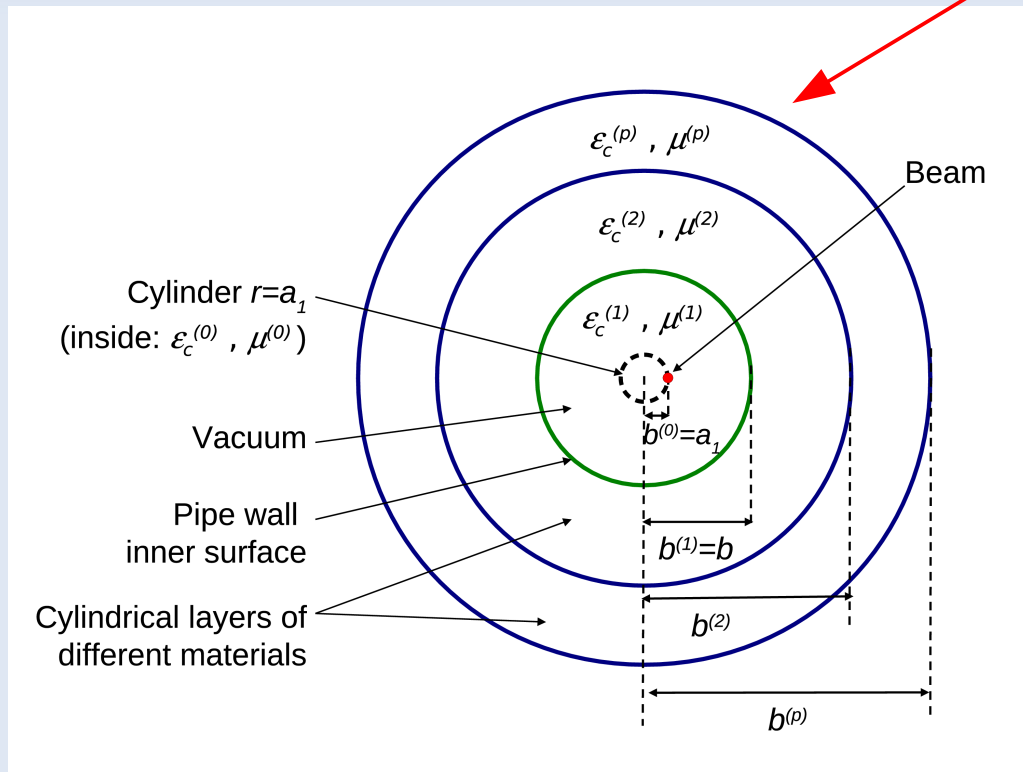
- 2D models: consider a **longitudinally smooth** element in the ring, of infinite length, and integrate the EM force from the source particle to the test particle, over a finite length.  
⇒ Neglect thus all **edge** effects.
- Main advantage: for simple geometries, EM fields obtained (semi-) **analytically** without any other assumptions (except **linearity**, **isotropy** and **homogeneity**).

# 2D wall impedance theory

- 2D models: consider a **longitudinally smooth** element in the ring, of infinite length, and integrate the EM force from the source particle to the test particle, over a finite length.  
⇒ Neglect thus all **edge** effects.
- Main advantage: for simple geometries, EM fields obtained (semi-) **analytically** without any other assumptions (except **linearity**, **isotropy** and **homogeneity**).
- Cross sections studied here: **multilayer** axisymmetric and flat chambers

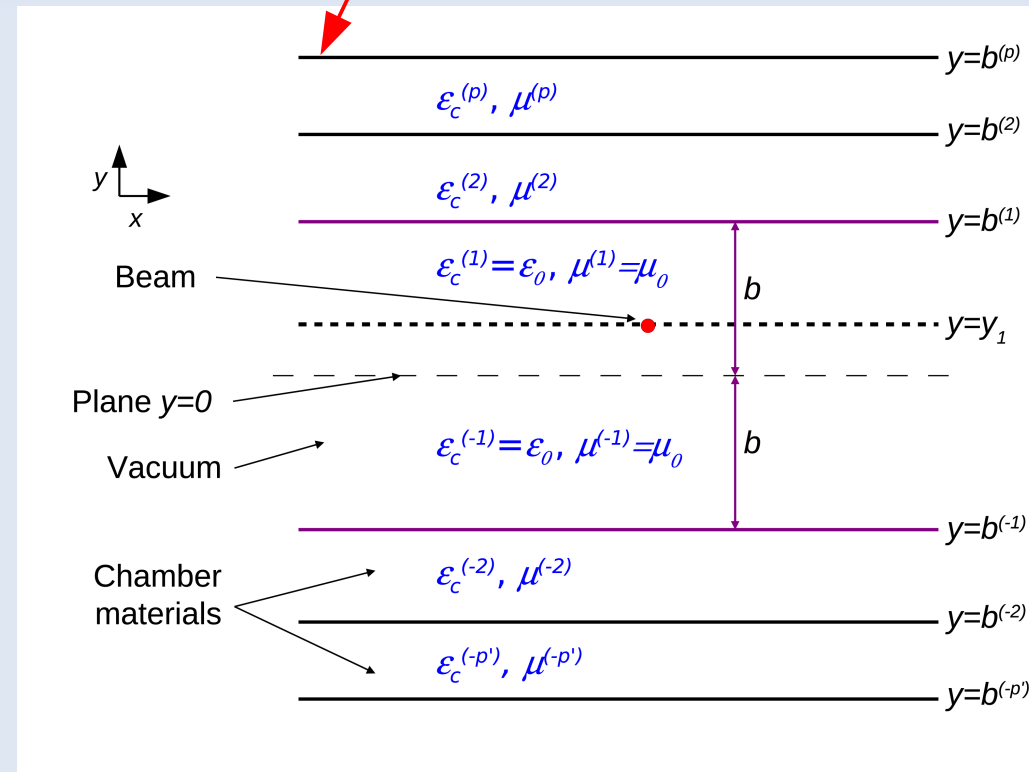
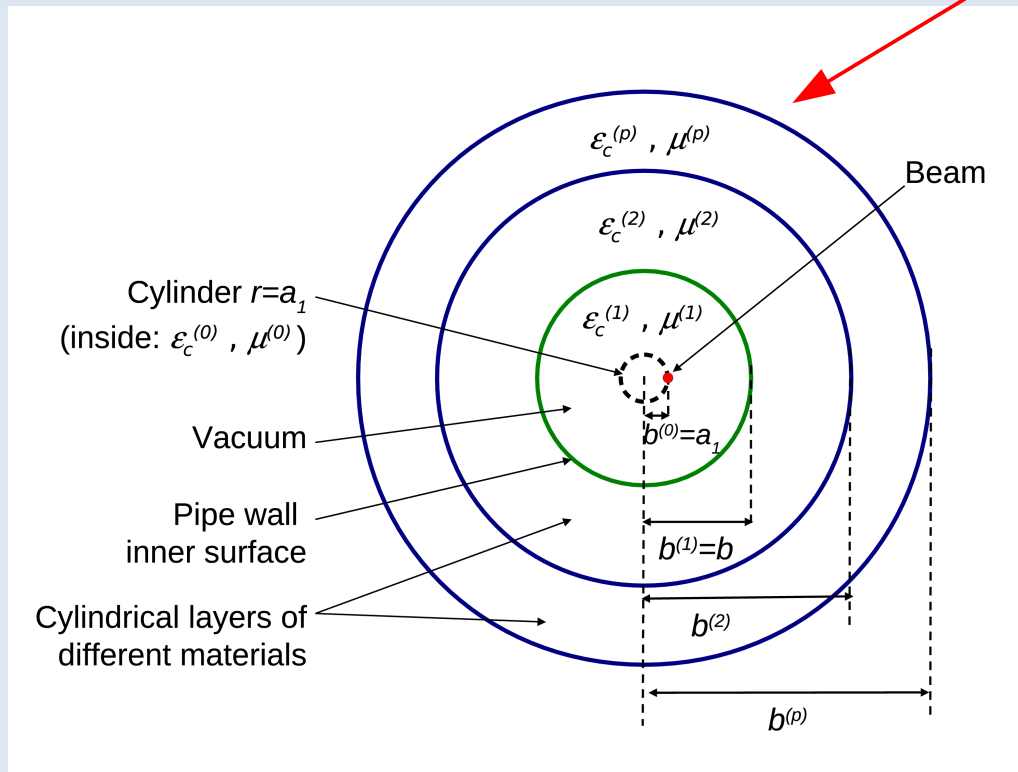
# 2D wall impedance theory

- 2D models: consider a **longitudinally smooth** element in the ring, of infinite length, and integrate the EM force from the source particle to the test particle, over a finite length.  
⇒ Neglect thus all **edge** effects.
- Main advantage: for simple geometries, EM fields obtained (semi-) **analytically** without any other assumptions (except **linearity**, **isotropy** and **homogeneity**).
- Cross sections studied here: **multilayer axisymmetric** and flat chambers



# 2D wall impedance theory

- 2D models: consider a **longitudinally smooth** element in the ring, of infinite length, and integrate the EM force from the source particle to the test particle, over a finite length.  
 ⇒ Neglect thus all **edge** effects.
- Main advantage: for simple geometries, EM fields obtained (semi-) **analytically** without any other assumptions (except **linearity**, **isotropy** and **homogeneity**).
- Cross sections studied here: **multilayer axisymmetric** and **flat** chambers



# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

$$\begin{aligned}\operatorname{div} \vec{D} &= \rho, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0,\end{aligned}$$

# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

$$\begin{aligned} \operatorname{div} \vec{D} &= \rho, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0, \end{aligned} \quad \text{with} \quad \begin{aligned} \vec{D} &= \varepsilon_c(\omega) \vec{E} = \varepsilon_0 \varepsilon_1(\omega) \vec{E}, \\ \vec{B} &= \mu(\omega) \vec{H} = \mu_0 \mu_1(\omega) \vec{H}, \end{aligned}$$

# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

$$\begin{aligned}\operatorname{div} \vec{D} &= \rho, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0,\end{aligned}$$

with

$$\begin{aligned}\vec{D} &= \varepsilon_c(\omega) \vec{E} = \varepsilon_0 \varepsilon_1(\omega) \vec{E}, \\ \vec{B} &= \mu(\omega) \vec{H} = \mu_0 \mu_1(\omega) \vec{H},\end{aligned}$$

Complex permittivity

Complex permeability



# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

$$\begin{aligned}\operatorname{div} \vec{D} &= \rho, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0,\end{aligned}$$

with

$$\begin{aligned}\vec{D} &= \varepsilon_c(\omega) \vec{E} = \varepsilon_0 \varepsilon_1(\omega) \vec{E}, \\ \vec{B} &= \mu(\omega) \vec{H} = \mu_0 \mu_1(\omega) \vec{H},\end{aligned}$$

Complex permittivity

Complex permeability

and  $\rho(r, \theta, s; \omega) = \frac{Q}{a_1} \delta(r - a_1) \delta_p(\theta - \theta_1) e^{-jks}$ . (point-like source)

# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

$$\begin{aligned} \operatorname{div} \vec{D} &= \rho, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0, \end{aligned}$$

with

$$\begin{aligned} \vec{D} &= \varepsilon_c(\omega) \vec{E} = \varepsilon_0 \varepsilon_1(\omega) \vec{E}, \\ \vec{B} &= \mu(\omega) \vec{H} = \mu_0 \mu_1(\omega) \vec{H}, \end{aligned}$$

Complex permittivity

Complex permeability

and  $\rho(r, \theta, s; \omega) = \frac{Q}{a_1} \delta(r - a_1) \delta_p(\theta - \theta_1) e^{-jk_s}$ . (point-like source)

- Playing with vector operations, get **wave equations**: e.g. for  $E$

$$\nabla^2 \vec{E} + \omega^2 \varepsilon_c \mu \vec{E} = \frac{1}{\varepsilon_c} \operatorname{grad} \rho + j\omega \mu \rho v \vec{e}_s.$$

# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

$$\begin{aligned} \operatorname{div} \vec{D} &= \rho, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0, \end{aligned}$$

with

$$\begin{aligned} \vec{D} &= \varepsilon_c(\omega) \vec{E} = \varepsilon_0 \varepsilon_1(\omega) \vec{E}, \\ \vec{B} &= \mu(\omega) \vec{H} = \mu_0 \mu_1(\omega) \vec{H}, \end{aligned}$$

Complex permittivity

Complex permeability

and  $\rho(r, \theta, s; \omega) = \frac{Q}{a_1} \delta(r - a_1) \delta_p(\theta - \theta_1) e^{-jk_s s}$ . (point-like source)

- Playing with vector operations, get **wave equations**: e.g. for  $E$

$$\nabla^2 \vec{E} + \omega^2 \varepsilon_c \mu \vec{E} = \frac{1}{\varepsilon_c} \operatorname{grad} \rho + j\omega \mu \rho v \vec{e}_s.$$

- Idea: **decompose** fields and source charge density thanks to **Fourier transforms**

# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

$$\begin{aligned} \operatorname{div} \vec{D} &= \rho, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0, \end{aligned}$$

with

$$\begin{aligned} \vec{D} &= \varepsilon_c(\omega) \vec{E} = \varepsilon_0 \varepsilon_1(\omega) \vec{E}, \\ \vec{B} &= \mu(\omega) \vec{H} = \mu_0 \mu_1(\omega) \vec{H}, \end{aligned}$$

Complex permittivity

Complex permeability

and  $\rho(r, \theta, s; \omega) = \frac{Q}{a_1} \delta(r - a_1) \delta_p(\theta - \theta_1) e^{-jk_s}$ . (point-like source)

- Playing with vector operations, get **wave equations**: e.g. for  $E$

$$\nabla^2 \vec{E} + \omega^2 \varepsilon_c \mu \vec{E} = \frac{1}{\varepsilon_c} \operatorname{grad} \rho + j\omega \mu \rho v \vec{e}_s.$$

- Idea: **decompose** fields and source charge density thanks to **Fourier transforms**

axisymmetric  $\rho(r, \theta, s; \omega) = \int_{-\infty}^{\infty} dk' e^{-jk' s} \delta(k' - k) \sum_{m=0}^{\infty} \frac{Q \cos(m\theta)}{\pi v a_1 (1 + \delta_{m0})} \delta(r - a_1),$

# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

$$\begin{aligned}
 \operatorname{div} \vec{D} &= \rho, & \text{with} & \quad \vec{D} = \varepsilon_c(\omega) \vec{E} = \varepsilon_0 \varepsilon_1(\omega) \vec{E}, \\
 \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}, & & \quad \vec{B} = \mu(\omega) \vec{H} = \mu_0 \mu_1(\omega) \vec{H}, \\
 \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, & & \\
 \operatorname{div} \vec{B} &= 0, & \text{and} & \quad \rho(r, \theta, s; \omega) = \frac{Q}{a_1} \delta(r - a_1) \delta_p(\theta - \theta_1) e^{-jk_s}. \quad (\text{point-like source})
 \end{aligned}$$

→ Complex permittivity  
→ Complex permeability

- Playing with vector operations, get **wave equations**: e.g. for  $E$

$$\nabla^2 \vec{E} + \omega^2 \varepsilon_c \mu \vec{E} = \frac{1}{\varepsilon_c} \operatorname{grad} \rho + j\omega \mu \rho v \vec{e}_s.$$

- Idea: **decompose** fields and source charge density thanks to **Fourier transforms**

**axisymmetric**  $\rho(r, \theta, s; \omega) = \int_{-\infty}^{\infty} dk' e^{-jk' s} \delta(k' - k) \sum_{m=0}^{\infty} \frac{Q \cos(m\theta)}{\pi v a_1 (1 + \delta_{m0})} \delta(r - a_1),$

**flat**  $\rho(x, y, s; \omega) = \int_{-\infty}^{\infty} dk' e^{-jk' s} \delta(k' - k) \frac{Q}{\pi v} \int_0^{\infty} dk_x \cos(k_x x) \delta(y - y_1),$

# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

$$\begin{aligned} \operatorname{div} \vec{D} &= \rho, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0, \end{aligned} \quad \text{with} \quad \begin{aligned} \vec{D} &= \varepsilon_c(\omega) \vec{E} = \varepsilon_0 \varepsilon_1(\omega) \vec{E}, \\ \vec{B} &= \mu(\omega) \vec{H} = \mu_0 \mu_1(\omega) \vec{H}, \end{aligned}$$

Complex permittivity

Complex permeability

and  $\rho(r, \theta, s; \omega) = \frac{Q}{a_1} \delta(r - a_1) \delta_p(\theta - \theta_1) e^{-jk_s}$ . (point-like source)

- Playing with vector operations, get **wave equations**: e.g. for  $E$

$$\nabla^2 \vec{E} + \omega^2 \varepsilon_c \mu \vec{E} = \frac{1}{\varepsilon_c} \operatorname{grad} \rho + j\omega \mu \rho v \vec{e}_s.$$

- Idea: **decompose** fields and source charge density thanks to **Fourier transforms**

axisymmetric  $\rho(r, \theta, s; \omega) = \int_{-\infty}^{\infty} dk' e^{-jk' s} \delta(k' - k) \sum_{m=0}^{\infty} \frac{Q \cos(m\theta)}{\pi v a_1 (1 + \delta_{m0})} \delta(r - a_1),$

Fourier series decomposition

flat  $\rho(x, y, s; \omega) = \int_{-\infty}^{\infty} dk' e^{-jk' s} \delta(k' - k) \frac{Q}{\pi v} \int_0^{\infty} dk_x \cos(k_x x) \delta(y - y_1),$

# Outline of the theory

- Essence of the formalism initially from **B. Zotter** (1969), in axisymmetric only.
- Start from Maxwell equations **in frequency domain**:

$$\begin{aligned} \operatorname{div} \vec{D} &= \rho, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0, \end{aligned}$$

with

$$\begin{aligned} \vec{D} &= \varepsilon_c(\omega) \vec{E} = \varepsilon_0 \varepsilon_1(\omega) \vec{E}, \\ \vec{B} &= \mu(\omega) \vec{H} = \mu_0 \mu_1(\omega) \vec{H}, \end{aligned}$$

Complex permittivity

Complex permeability

and  $\rho(r, \theta, s; \omega) = \frac{Q}{a_1} \delta(r - a_1) \delta_p(\theta - \theta_1) e^{-jk_s s}$ . (point-like source)

- Playing with vector operations, get **wave equations**: e.g. for  $E$

$$\nabla^2 \vec{E} + \omega^2 \varepsilon_c \mu \vec{E} = \frac{1}{\varepsilon_c} \operatorname{grad} \rho + j\omega \mu \rho v \vec{e}_s.$$

- Idea: **decompose** fields and source charge density thanks to **Fourier transforms**

axisymmetric

$$\rho(r, \theta, s; \omega) = \int_{-\infty}^{\infty} dk' e^{-jk' s} \delta(k' - k) \sum_{m=0}^{\infty} \frac{Q \cos(m\theta)}{\pi v a_1 (1 + \delta_{m0})} \delta(r - a_1),$$

Fourier series decomposition

flat

$$\rho(x, y, s; \omega) = \int_{-\infty}^{\infty} dk' e^{-jk' s} \delta(k' - k) \frac{Q}{\pi v} \int_0^{\infty} dk_x \cos(k_x x) \delta(y - y_1),$$

Continuous Fourier transforms

# Outline of the theory

- Write wave equations for the **longitudinal components  $E_s$  and  $H_s$** , then identify the terms (drop integrals and sums), obtaining (outside source) **homogeneous second order differential equations**:



# Outline of the theory

- Write wave equations for the longitudinal components  $E_s$  and  $H_s$ , then identify the terms (drop integrals and sums), obtaining (outside source) homogeneous second order differential equations:

axisym. (radial dependency  $R$ )  $r^2 \frac{d^2 R}{dr^2} + r \frac{dR}{dr} - [m^2 + r^2 (k^2 - \omega^2 \epsilon_c \mu)] R = 0,$   $\rightarrow$  modified Bessel functions

# Outline of the theory

- Write wave equations for the **longitudinal components  $E_s$  and  $H_s$** , then identify the terms (drop integrals and sums), obtaining (outside source) **homogeneous second order differential equations**:

axisym. (radial dependency  $R$ )  $r^2 \frac{d^2 R}{dr^2} + r \frac{dR}{dr} - [m^2 + r^2 (k^2 - \omega^2 \epsilon_c \mu)] R = 0,$   $\rightarrow$  modified Bessel functions

flat (vertical dependency  $Y$ )  $\frac{d^2 Y}{dy^2} - [k_x^2 + k^2 - \omega^2 \epsilon_c \mu] Y = 0,$   $\rightarrow$  exponentials

# Outline of the theory

- Write wave equations for the **longitudinal components  $E_s$  and  $H_s$** , then identify the terms (drop integrals and sums), obtaining (outside source) **homogeneous second order differential equations**:

axisym. (radial dependency  $R$ )  $r^2 \frac{d^2 R}{dr^2} + r \frac{dR}{dr} - [m^2 + r^2 (k^2 - \omega^2 \epsilon_c \mu)] R = 0,$   $\rightarrow$  modified Bessel functions

flat (vertical dependency  $Y$ )  $\frac{d^2 Y}{dy^2} - [k_x^2 + k^2 - \omega^2 \epsilon_c \mu] Y = 0,$   $\rightarrow$  exponentials

- Transverse components obtained from the longitudinal ones**, thanks to Maxwell eqs.

# Outline of the theory

- Write wave equations for the **longitudinal components  $E_s$  and  $H_s$** , then identify the terms (drop integrals and sums), obtaining (outside source) **homogeneous second order differential equations**:

axisym. (radial dependency  $R$ )  $r^2 \frac{d^2 R}{dr^2} + r \frac{dR}{dr} - [m^2 + r^2 (k^2 - \omega^2 \epsilon_c \mu)] R = 0$ ,  $\rightarrow$  modified Bessel functions

flat (vertical dependency  $Y$ )  $\frac{d^2 Y}{dy^2} - [k_x^2 + k^2 - \omega^2 \epsilon_c \mu] Y = 0$ ,  $\rightarrow$  exponentials

- Transverse components obtained from the longitudinal ones**, thanks to Maxwell eqs.
- Integration constants** determined from **field matching** (continuity of tangential field components) between adjacent layers. Instead of solving the full system by "brute force", use analytical trick: relate constants between adjacent layers by 4 x 4 matrices:

$$\text{Constants (layer } p+1) = M_p^{p+1} \cdot \text{constants (layer } p)$$

# Outline of the theory

- Write wave equations for the **longitudinal components  $E_s$  and  $H_s$** , then identify the terms (drop integrals and sums), obtaining (outside source) **homogeneous second order differential equations**:

axisym. (radial dependency  $R$ )  $r^2 \frac{d^2 R}{dr^2} + r \frac{dR}{dr} - [m^2 + r^2 (k^2 - \omega^2 \epsilon_c \mu)] R = 0$ ,  $\rightarrow$  modified Bessel functions

flat (vertical dependency  $Y$ )  $\frac{d^2 Y}{dy^2} - [k_x^2 + k^2 - \omega^2 \epsilon_c \mu] Y = 0$ ,  $\rightarrow$  exponentials

- Transverse components obtained from the longitudinal ones**, thanks to Maxwell eqs.
- Integration constants** determined from **field matching** (continuity of tangential field components) between adjacent layers. Instead of solving the full system by "brute force", use analytical trick: relate constants between adjacent layers by 4 x 4 matrices:

$$\text{Constants (layer } p+1) = M_p^{p+1} \cdot \text{constants (layer } p)$$

In the end:

$$\text{Constants (last layer)} = M \cdot \text{constants (first layer)}.$$

$\Rightarrow$  Only need to multiply 4x4 matrices and do a final inversion, to get all the constants.

# Outline of the theory

- Write wave equations for the **longitudinal components  $E_s$  and  $H_s$** , then identify the terms (drop integrals and sums), obtaining (outside source) **homogeneous second order differential equations**:

axisym. (radial dependency  $R$ )  $r^2 \frac{d^2 R}{dr^2} + r \frac{dR}{dr} - [m^2 + r^2 (k^2 - \omega^2 \varepsilon_c \mu)] R = 0$ ,  $\rightarrow$  modified Bessel functions

flat (vertical dependency  $Y$ )  $\frac{d^2 Y}{dy^2} - [k_x^2 + k^2 - \omega^2 \varepsilon_c \mu] Y = 0$ ,  $\rightarrow$  exponentials

- Transverse components obtained from the longitudinal ones**, thanks to Maxwell eqs.
- Integration constants** determined from **field matching** (continuity of tangential field components) between adjacent layers. Instead of solving the full system by "brute force", use analytical trick: relate constants between adjacent layers by 4 x 4 matrices:

$$\text{Constants (layer } p+1) = M_p^{p+1} \cdot \text{constants (layer } p)$$

In the end:

$$\text{Constants (last layer)} = M \cdot \text{constants (first layer)}.$$

$\Rightarrow$  Only need to multiply 4x4 matrices and do a final inversion, to get all the constants.

- Finally, **put back the Fourier transforms and/or series**. In **flat** case, additional algebra to get a simpler form.

# Outline of the theory

- Electric field longitudinal component in the vacuum:

# Outline of the theory

- Electric field longitudinal component in the vacuum:

axisym.  $E_s^{vac} = \mathcal{C} e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1 r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{\text{TM}}^m \cos(m\theta)}{1 + \delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$



# Outline of the theory

- Electric field longitudinal component in the vacuum:

axisym.  $E_s^{vac} = \mathcal{C}e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{\text{TM}}^m \cos(m\theta)}{1+\delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$

flat  $E_s^{vac} = \mathcal{C}e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{x^2 + (y - y_1)^2} \right) - 4 \sum_{m,n=0}^{\infty} \frac{\alpha_{mn} \cos[n(\theta - \frac{\pi}{2})]}{(1+\delta_{m0})(1+\delta_{n0})} I_m \left( \frac{ky_1}{\gamma} \right) I_n \left( \frac{kr}{\gamma} \right) \right],$

# Outline of the theory

- Electric field longitudinal component in the vacuum:

axisym.  $E_s^{vac} = \mathcal{C}e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{TM}^m \cos(m\theta)}{1+\delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$

Direct space-charge term

flat  $E_s^{vac} = \mathcal{C}e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{x^2 + (y - y_1)^2} \right) - 4 \sum_{m,n=0}^{\infty} \frac{\alpha_{mn} \cos[n(\theta - \frac{\pi}{2})]}{(1+\delta_{m0})(1+\delta_{n0})} I_m \left( \frac{ky_1}{\gamma} \right) I_n \left( \frac{kr}{\gamma} \right) \right],$

# Outline of the theory

- Electric field longitudinal component in the vacuum:

**axisym.**  $E_s^{vac} = \mathcal{C}e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{TM}^m \cos(m\theta)}{1+\delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$

Direct space-charge term

Wall term

**flat**  $E_s^{vac} = \mathcal{C}e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{x^2 + (y - y_1)^2} \right) - 4 \sum_{m,n=0}^{\infty} \frac{\alpha_{mn} \cos[n(\theta - \frac{\pi}{2})]}{(1+\delta_{m0})(1+\delta_{n0})} I_m \left( \frac{ky_1}{\gamma} \right) I_n \left( \frac{kr}{\gamma} \right) \right],$

# Outline of the theory

- Electric field longitudinal component in the vacuum:

**axisym.**  $E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1 r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{TM}^m \cos(m\theta)}{1 + \delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$

**flat**  $E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{x^2 + (y - y_1)^2} \right) - 4 \sum_{m,n=0}^{\infty} \frac{\alpha_{mn} \cos[n(\theta - \frac{\pi}{2})]}{(1 + \delta_{m0})(1 + \delta_{n0})} I_m \left( \frac{ky_1}{\gamma} \right) I_n \left( \frac{kr}{\gamma} \right) \right],$

Direct space-charge term    Constants    Wall term

# Outline of the theory

- Electric field longitudinal component in the vacuum:

**axisym.**  $E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1 r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{TM}^m \cos(m\theta)}{1 + \delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$

**flat**  $E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{x^2 + (y - y_1)^2} \right) - 4 \sum_{m,n=0}^{\infty} \frac{\alpha_{mn} \cos[n(\theta - \frac{\pi}{2})]}{(1 + \delta_{m0})(1 + \delta_{n0})} I_m \left( \frac{ky_1}{\gamma} \right) I_n \left( \frac{kr}{\gamma} \right) \right],$

Diagram annotations:  
 - Red ovals highlight the  $K_0$  terms in both equations, with a red arrow pointing to the label "Direct space-charge term".  
 - Blue ovals highlight the infinite sums in both equations, with a blue arrow pointing to the label "Wall term".  
 - Green dotted ovals highlight the  $\alpha_{TM}^m$  and  $\alpha_{mn}$  terms, with a green arrow pointing to the label "Constants".

In the "wall term": only first terms of the sums are relevant when sufficiently close to the orbit → linear terms ( $m \leq 1, n \leq 2$ ).

# Outline of the theory

- Electric field longitudinal component in the vacuum:

**axisym.**  $E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1 r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{TM}^m \cos(m\theta)}{1 + \delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$

**flat**  $E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{x^2 + (y - y_1)^2} \right) - 4 \sum_{m,n=0}^{\infty} \frac{\alpha_{mn} \cos[n(\theta - \frac{\pi}{2})]}{(1 + \delta_{m0})(1 + \delta_{n0})} I_m \left( \frac{ky_1}{\gamma} \right) I_n \left( \frac{kr}{\gamma} \right) \right],$

Diagram annotations:  
 - Red ovals highlight the  $K_0$  terms in both equations, with a red arrow pointing to the text "Direct space-charge term".  
 - Blue ovals highlight the infinite sums in both equations, with a blue arrow pointing to the text "Wall term".  
 - Green dotted ovals highlight the coefficients  $\alpha_{TM}^m$  and  $\alpha_{mn}$  in the sums, with a green arrow pointing to the text "Constants".

In the "wall term": only first terms of the sums are relevant when sufficiently close to the orbit  $\rightarrow$  linear terms ( $m \leq 1, n \leq 2$ ).

- From  $E_s$  alone we can get the EM force in the vacuum:

# Outline of the theory

- Electric field longitudinal component in the vacuum:

**axisym.**  $E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1 r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{TM}^m \cos(m\theta)}{1 + \delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$

**flat**  $E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{x^2 + (y - y_1)^2} \right) - 4 \sum_{m,n=0}^{\infty} \frac{\alpha_{mn} \cos[n(\theta - \frac{\pi}{2})]}{(1 + \delta_{m0})(1 + \delta_{n0})} I_m \left( \frac{ky_1}{\gamma} \right) I_n \left( \frac{kr}{\gamma} \right) \right],$

Diagram annotations:  
 - Red ovals highlight the  $K_0$  terms in both equations, with a red arrow pointing to the text "Direct space-charge term".  
 - Blue ovals highlight the infinite sums in both equations, with a blue arrow pointing to the text "Wall term".  
 - Green dotted ovals highlight the coefficients  $\alpha_{TM}^m$  and  $\alpha_{mn}$ , with a green arrow pointing to the text "Constants".

In the "wall term": only first terms of the sums are relevant when sufficiently close to the orbit  $\rightarrow$  linear terms ( $m \leq 1, n \leq 2$ ).

- From  $E_s$  alone we can get the EM force in the vacuum:

longitudinal  $F_s = qE_s,$

# Outline of the theory

- Electric field longitudinal component in the vacuum:

axisym.

$$E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1 r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{TM}^m \cos(m\theta)}{1 + \delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$$

Direct space-charge term

Constants

Wall term

flat

$$E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{x^2 + (y - y_1)^2} \right) - 4 \sum_{m,n=0}^{\infty} \frac{\alpha_{mn} \cos[n(\theta - \frac{\pi}{2})]}{(1 + \delta_{m0})(1 + \delta_{n0})} I_m \left( \frac{ky_1}{\gamma} \right) I_n \left( \frac{kr}{\gamma} \right) \right],$$

In the "wall term": only first terms of the sums are relevant when sufficiently close to the orbit → linear terms ( $m \leq 1, n \leq 2$ ).

- From  $E_s$  alone we can get the EM force in the vacuum:

longitudinal  $F_s = qE_s,$

transverse (cyl. coordinates)

$$F_r = q(E_r - v\mu_0 H_\theta) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial r} = \frac{jq}{k} \frac{\partial E_s}{\partial r},$$

$$F_\theta = q(E_\theta + v\mu_0 H_r) = \frac{jq\gamma^2}{k} \frac{1 - \beta^2}{r} \frac{\partial E_s}{\partial \theta} = \frac{jq}{kr} \frac{\partial E_s}{\partial \theta}.$$



# Outline of the theory

- Electric field longitudinal component in the vacuum:

axisym.

$$E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1 r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{TM}^m \cos(m\theta)}{1 + \delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$$

Direct space-charge term

Constants

Wall term

flat

$$E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{x^2 + (y - y_1)^2} \right) - 4 \sum_{m,n=0}^{\infty} \frac{\alpha_{mn} \cos[n(\theta - \frac{\pi}{2})]}{(1 + \delta_{m0})(1 + \delta_{n0})} I_m \left( \frac{ky_1}{\gamma} \right) I_n \left( \frac{kr}{\gamma} \right) \right],$$

In the "wall term": only first terms of the sums are relevant when sufficiently close to the orbit → linear terms ( $m \leq 1, n \leq 2$ ).

- From  $E_s$  alone we can get the EM force in the vacuum:

longitudinal

$$F_s = q E_s,$$

transverse (cyl. coordinates)

$$F_r = q (E_r - v \mu_0 H_\theta) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial r} = \frac{jq}{k} \frac{\partial E_s}{\partial r},$$

$$F_\theta = q (E_\theta + v \mu_0 H_r) = \frac{jq\gamma^2}{k} \frac{1 - \beta^2}{r} \frac{\partial E_s}{\partial \theta} = \frac{jq}{kr} \frac{\partial E_s}{\partial \theta}.$$

transverse (cartesian coordinates)

$$F_x = q (E_x - v \mu_0 H_y) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial x} = \frac{jq}{k} \frac{\partial E_s}{\partial x},$$

$$F_y = q (E_y + v \mu_0 H_x) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial y} = \frac{jq}{k} \frac{\partial E_s}{\partial y},$$

# Outline of the theory

- Electric field longitudinal component in the vacuum:

axisym.

$$E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{a_1^2 + r^2 - 2a_1 r \cos \theta} \right) - 2 \sum_{m=0}^{\infty} \frac{\alpha_{TM}^m \cos(m\theta)}{1 + \delta_{m0}} I_m \left( \frac{ka_1}{\gamma} \right) I_m \left( \frac{kr}{\gamma} \right) \right],$$

Direct space-charge term

Constants

Wall term

flat

$$E_s^{vac} = C e^{-jks} \left[ K_0 \left( \frac{k}{\gamma} \sqrt{x^2 + (y - y_1)^2} \right) - 4 \sum_{m,n=0}^{\infty} \frac{\alpha_{mn} \cos[n(\theta - \frac{\pi}{2})]}{(1 + \delta_{m0})(1 + \delta_{n0})} I_m \left( \frac{ky_1}{\gamma} \right) I_n \left( \frac{kr}{\gamma} \right) \right],$$

In the "wall term": only first terms of the sums are relevant when sufficiently close to the orbit → linear terms ( $m \leq 1, n \leq 2$ ).

- From  $E_s$  alone we can get the EM force in the vacuum:

longitudinal

$$F_s = q E_s,$$

transverse (cyl. coordinates)

$$F_r = q (E_r - v \mu_0 H_\theta) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial r} = \frac{jq}{k} \frac{\partial E_s}{\partial r},$$

$$F_\theta = q (E_\theta + v \mu_0 H_r) = \frac{jq\gamma^2}{k} \frac{1 - \beta^2}{r} \frac{\partial E_s}{\partial \theta} = \frac{jq}{kr} \frac{\partial E_s}{\partial \theta}.$$

transverse (cartesian coordinates)

$$F_x = q (E_x - v \mu_0 H_y) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial x} = \frac{jq}{k} \frac{\partial E_s}{\partial x},$$

$$F_y = q (E_y + v \mu_0 H_x) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial y} = \frac{jq}{k} \frac{\partial E_s}{\partial y}.$$

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

Axisymmetric  
case

$$Z_{\parallel}^{Wall} \approx \frac{j\omega\mu_0 L}{2\pi\beta^2\gamma^2} \alpha_{TM}^0(\omega),$$
$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} (\alpha_{TM}^1(\omega)x_1 + \alpha_{TM}^0(\omega)x_2),$$

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

Axisymmetric  
case

$$Z_{\parallel}^{Wall} \approx \frac{j\omega\mu_0 L}{2\pi\beta^2\gamma^2} \alpha_{TM}^0(\omega),$$
$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} (\alpha_{TM}^1(\omega)x_1 + \alpha_{TM}^0(\omega)x_2),$$

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

Axisymmetric  
case

$$Z_{\parallel}^{Wall} \approx \frac{j\omega\mu_0 L}{2\pi\beta^2\gamma^2} \alpha_{TM}^0(\omega),$$
$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} (\alpha_{TM}^1(\omega)x_1 + \alpha_{TM}^0(\omega)x_2),$$

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

Axisymmetric case

$$Z_{\parallel}^{Wall} \approx \frac{j\omega\mu_0 L}{2\pi\beta^2\gamma^2} \alpha_{TM}^0(\omega),$$
$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} (\alpha_{TM}^1(\omega)x_1 + \alpha_{TM}^0(\omega)x_2),$$

Quadrupolar term also in axisymmetric !



# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

Axisymmetric case

$$Z_{\parallel}^{Wall} \approx \frac{j\omega\mu_0 L}{2\pi\beta^2\gamma^2} \alpha_{TM}^0(\omega),$$
$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} (\alpha_{TM}^1(\omega)x_1 + \alpha_{TM}^0(\omega)x_2),$$

Flat case

$$Z_{\parallel}^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^2} \alpha_{00}(\omega),$$
$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} [ -(\alpha_{00}(\omega) - \alpha_{02}(\omega))x_1 + (\alpha_{00}(\omega) - \alpha_{02}(\omega))x_2 ],$$
$$Z_y^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^3} \left[ \alpha_{01}(\omega) + \frac{\alpha_{11}(\omega)k}{\gamma}y_1 + k\frac{\alpha_{00}(\omega) + \alpha_{02}(\omega)}{2\gamma}y_2 \right].$$

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

Axisymmetric case

$$Z_{\parallel}^{Wall} \approx \frac{j\omega\mu_0 L}{2\pi\beta^2\gamma^2} \alpha_{TM}^0(\omega),$$

$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} (\alpha_{TM}^1(\omega)x_1 + \alpha_{TM}^0(\omega)x_2),$$

Flat case

$$Z_{\parallel}^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^2} \alpha_{00}(\omega),$$

$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} [ -(\alpha_{00}(\omega) - \alpha_{02}(\omega))x_1 + (\alpha_{00}(\omega) - \alpha_{02}(\omega))x_2 ],$$

$$Z_y^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^3} \left[ \alpha_{01}(\omega) + \frac{\alpha_{11}(\omega)k}{\gamma}y_1 + k\frac{\alpha_{00}(\omega) + \alpha_{02}(\omega)}{2\gamma}y_2 \right].$$

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

Axisymmetric case

$$Z_{\parallel}^{Wall} \approx \frac{j\omega\mu_0 L}{2\pi\beta^2\gamma^2} \alpha_{TM}^0(\omega),$$

$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} (\alpha_{TM}^1(\omega)x_1 + \alpha_{TM}^0(\omega)x_2),$$

Flat case

$$Z_{\parallel}^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^2} \alpha_{00}(\omega), \quad \text{Constant term in vertical when no top-bottom symmetry}$$

$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} [ -(\alpha_{00}(\omega) - \alpha_{02}(\omega))x_1 + (\alpha_{00}(\omega) - \alpha_{02}(\omega))x_2 ],$$

$$Z_y^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^3} \left[ \alpha_{01}(\omega) + \frac{\alpha_{11}(\omega)k}{\gamma}y_1 + k\frac{\alpha_{00}(\omega) + \alpha_{02}(\omega)}{2\gamma}y_2 \right].$$

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

Axisymmetric case

$$Z_{\parallel}^{Wall} \approx \frac{j\omega\mu_0 L}{2\pi\beta^2\gamma^2} \alpha_{TM}^0(\omega),$$

$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} (\alpha_{TM}^1(\omega)x_1 + \alpha_{TM}^0(\omega)x_2),$$

Flat case

$$Z_{\parallel}^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^2} \alpha_{00}(\omega),$$

$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} [ -(\alpha_{00}(\omega) - \alpha_{02}(\omega)) x_1 + (\alpha_{00}(\omega) - \alpha_{02}(\omega)) x_2 ],$$

$$Z_y^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^3} \left[ \alpha_{01}(\omega) + \frac{\alpha_{11}(\omega)k}{\gamma} y_1 + k \frac{\alpha_{00}(\omega) + \alpha_{02}(\omega)}{2\gamma} y_2 \right].$$

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

Axisymmetric case

$$Z_{\parallel}^{Wall} \approx \frac{j\omega\mu_0 L}{2\pi\beta^2\gamma^2} \alpha_{TM}^0(\omega),$$

$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} (\alpha_{TM}^1(\omega)x_1 + \alpha_{TM}^0(\omega)x_2),$$

Flat case: **quadrupolar terms not exactly opposite to one another** ( $\neq$  A. Burov – V. Danilov, PRL 1999, ultrarelativistic case)

Flat case

$$Z_{\parallel}^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^2} \alpha_{00}(\omega),$$

$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} [ -(\alpha_{00}(\omega) - \alpha_{02}(\omega)) x_1 + (\alpha_{00}(\omega) - \alpha_{02}(\omega)) x_2 ],$$

$$Z_y^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^3} \left[ \alpha_{01}(\omega) + \frac{\alpha_{11}(\omega)k}{\gamma} y_1 + k \frac{\alpha_{00}(\omega) + \alpha_{02}(\omega)}{2\gamma} y_2 \right].$$

# Final wall impedances

- From EM force in vacuum, upon integration over a finite length  $L$  and normalization (by the test and sources charges) we obtain the **beam-coupling impedances** as simple functions of the first few  $\alpha_{TM}^m$  (**axisymmetric**) or  $\alpha_{mn}$  (**flat**) (**freq. dependent**).
- Keeping only **constant** & **linear terms** (**dipolar** terms proportional to **source** coordinates  $x_1$  &  $y_1$ , **quadrupolar** ones to **test** coordinates  $x_2$  &  $y_2$ ):

Axisymmetric case

$$Z_{\parallel}^{Wall} \approx \frac{j\omega\mu_0 L}{2\pi\beta^2\gamma^2} \alpha_{TM}^0(\omega),$$

$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} (\alpha_{TM}^1(\omega)x_1 + \alpha_{TM}^0(\omega)x_2),$$

Flat case

$$Z_{\parallel}^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^2} \alpha_{00}(\omega),$$

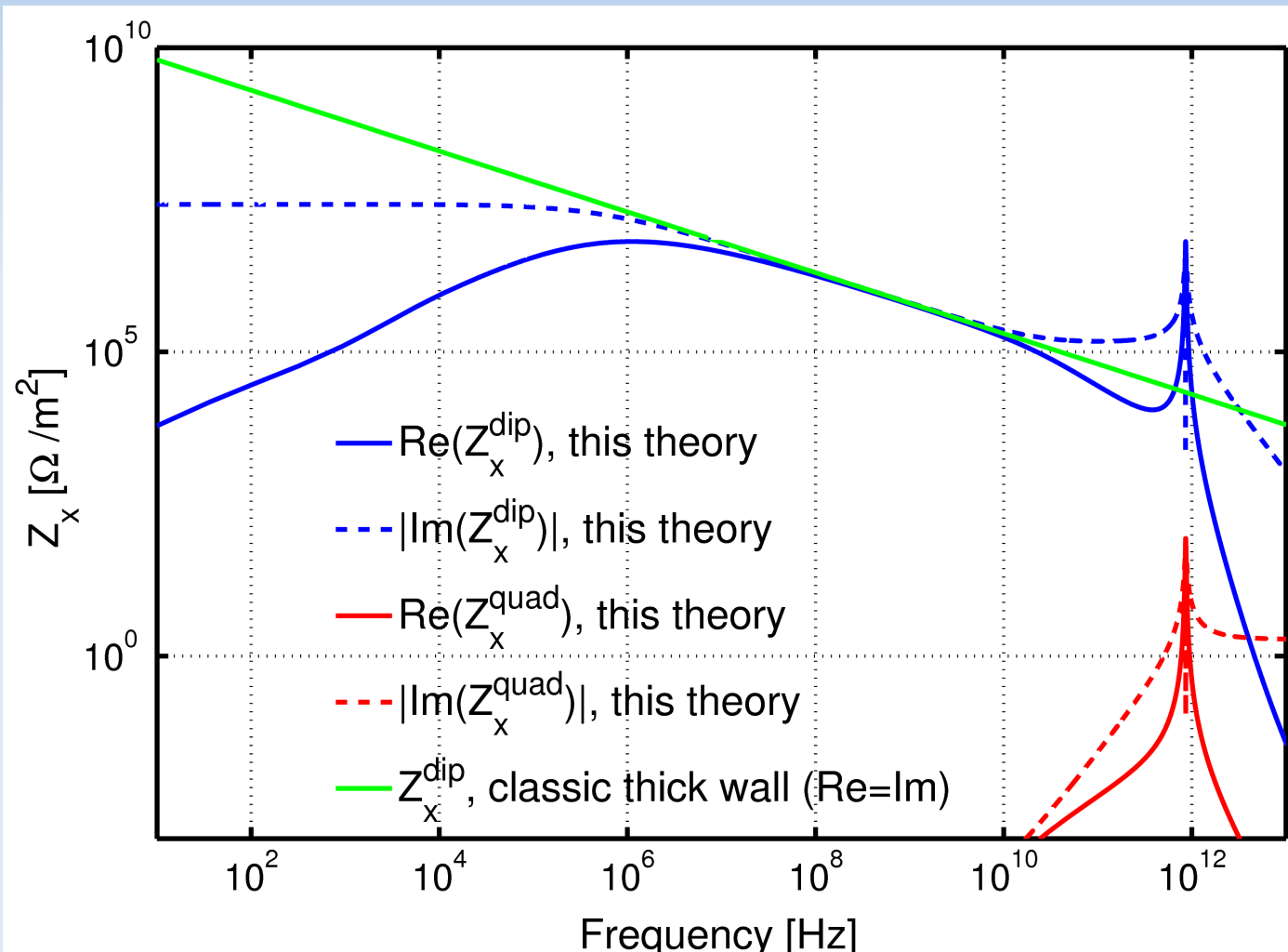
$$Z_x^{Wall} \approx \frac{jk^2 Z_0 L}{4\pi\beta\gamma^4} [ -(\alpha_{00}(\omega) - \alpha_{02}(\omega))x_1 + (\alpha_{00}(\omega) - \alpha_{02}(\omega))x_2 ],$$

$$Z_y^{Wall} \approx \frac{jkZ_0 L}{2\pi\beta\gamma^3} \left[ \alpha_{01}(\omega) + \frac{\alpha_{11}(\omega)k}{\gamma}y_1 + k\frac{\alpha_{00}(\omega) + \alpha_{02}(\omega)}{2\gamma}y_2 \right].$$

**Note: it is easy to go to higher order than linear !**

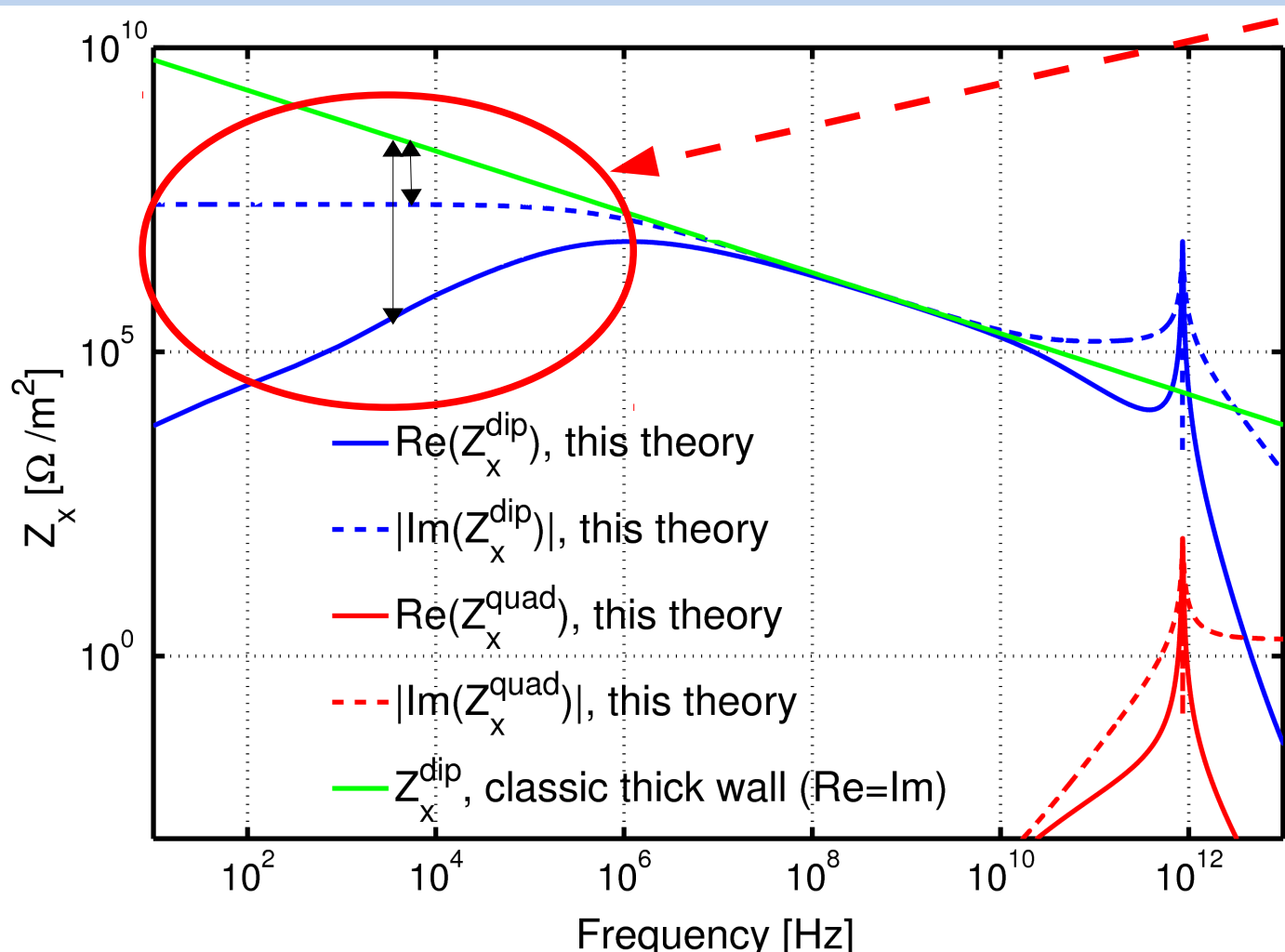
# Results in axisymmetric

- 25mm-thick graphite of radius 1.5 mm (surrounded by stainless steel), compared to classic formula:



# Results in axisymmetric

- 25mm-thick graphite of radius 1.5 mm (surrounded by stainless steel), compared to classic formula:

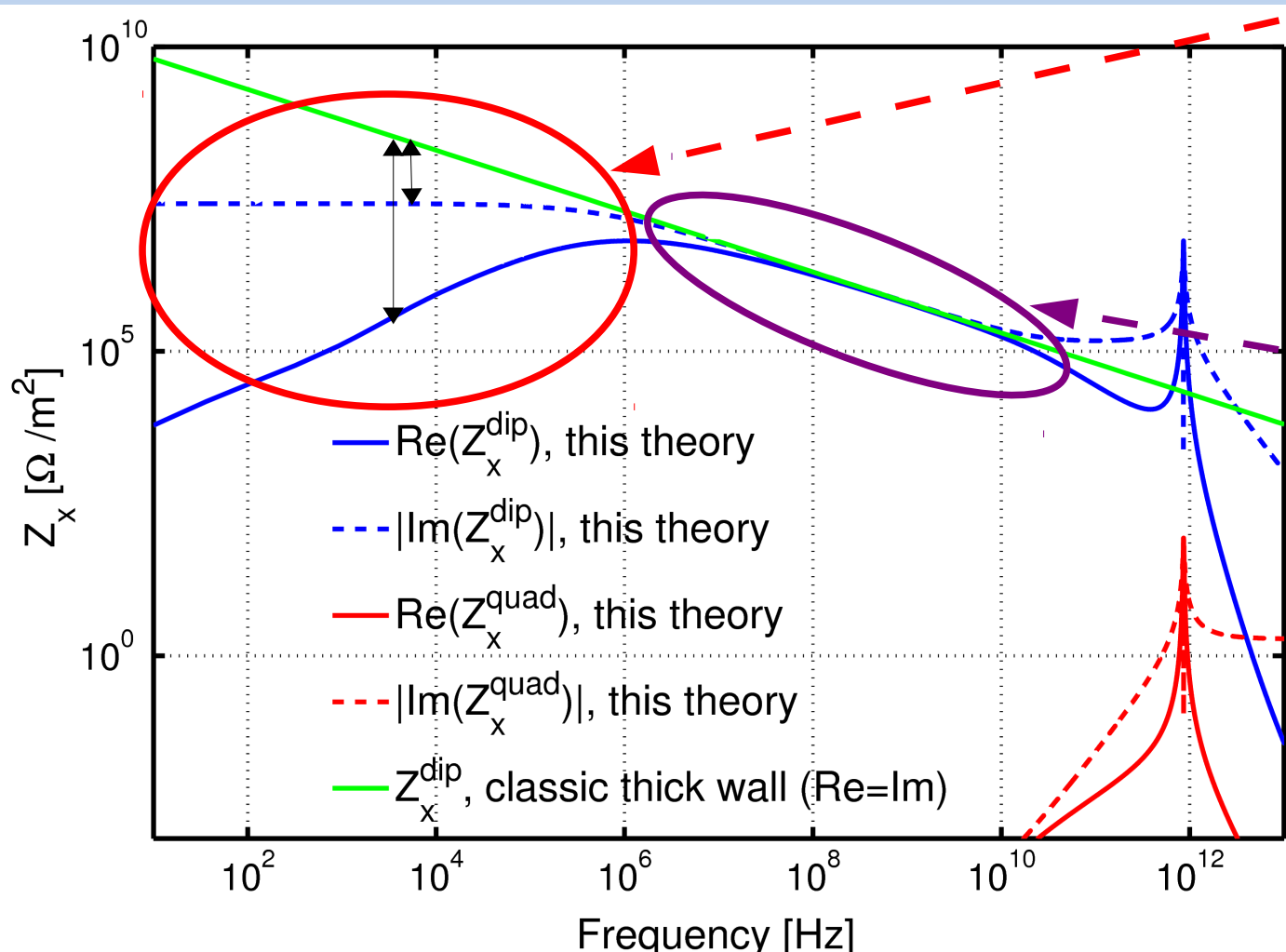


Low frequencies:  
importance of general  
theory w.r.t classic  
formula (factor  $\sim 10$  for  
imag. part,  $>100$  for real  
part)



# Results in axisymmetric

- 25mm-thick graphite of radius 1.5 mm (surrounded by stainless steel), compared to classic formula:

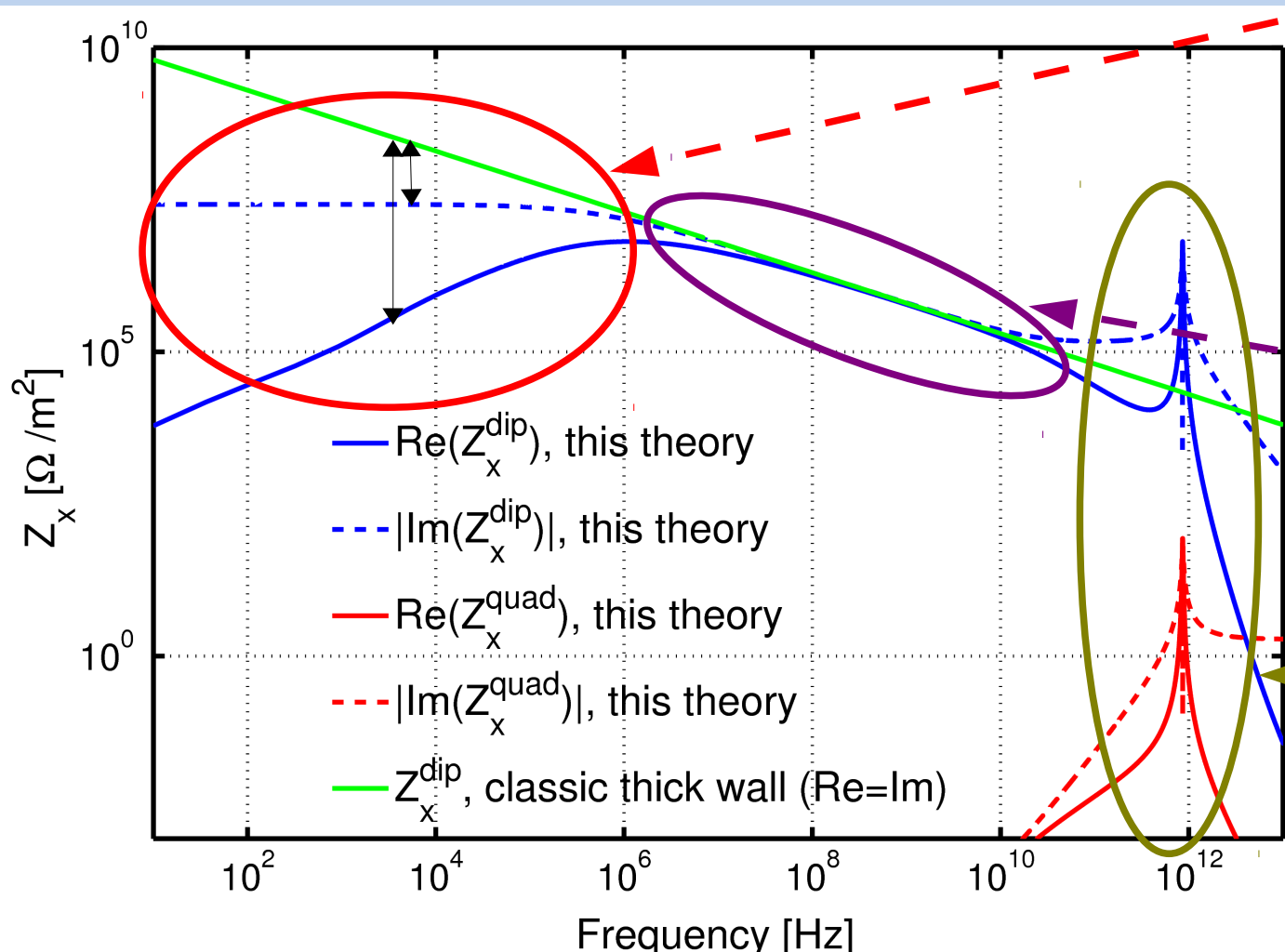


Low frequencies: importance of general theory w.r.t classic formula (factor  $\sim 10$  for imag. part,  $>100$  for real part)

Intermediate frequencies: classic formula valid (skin depth approximation).

# Results in axisymmetric

- 25mm-thick graphite of radius 1.5 mm (surrounded by stainless steel), compared to classic formula:



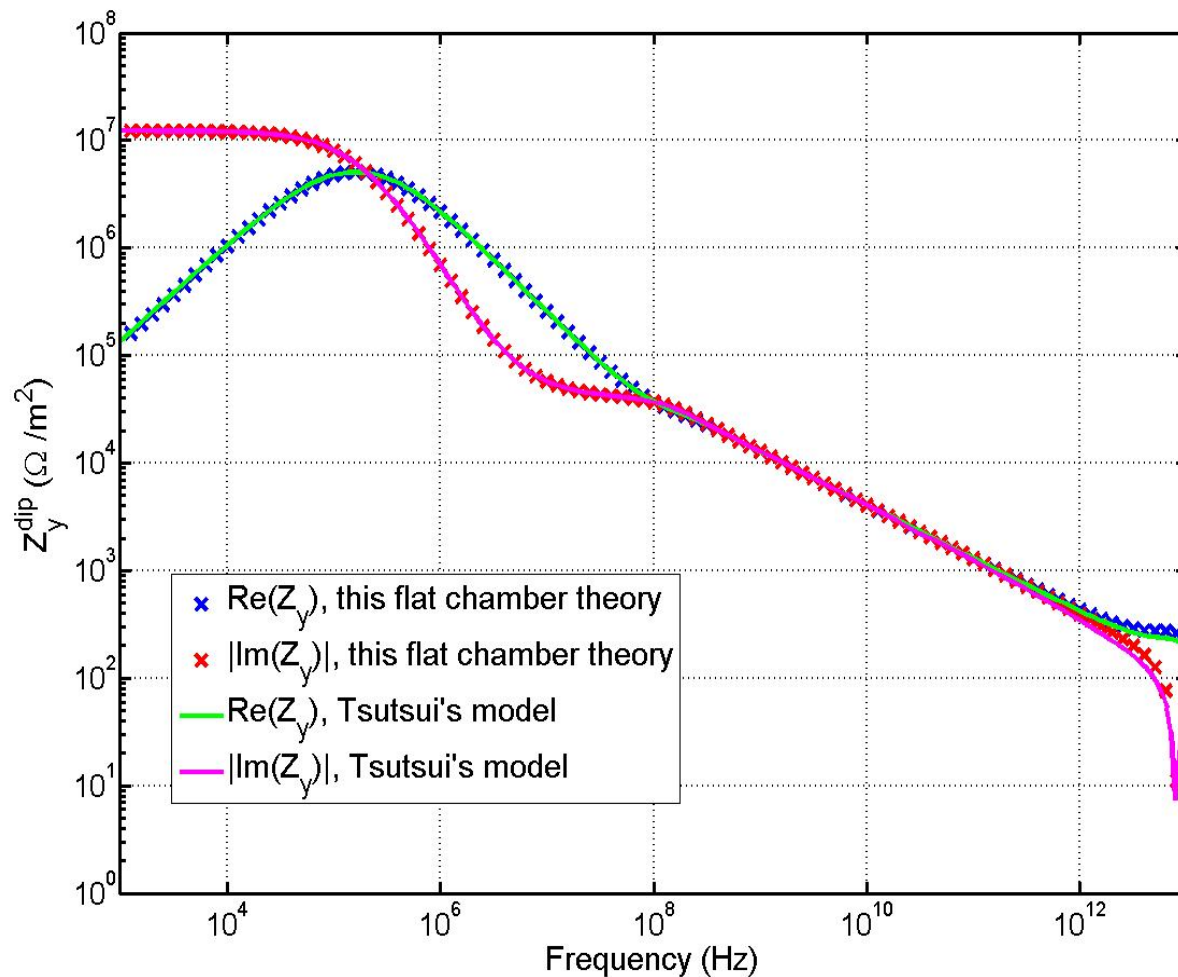
Low frequencies: importance of general theory w.r.t classic formula (factor  $\sim 10$  for imag. part,  $>100$  for real part)

Intermediate frequencies: classic formula valid (skin depth approximation).

High frequencies: resonance + new quadrupolar term (in this theory only).

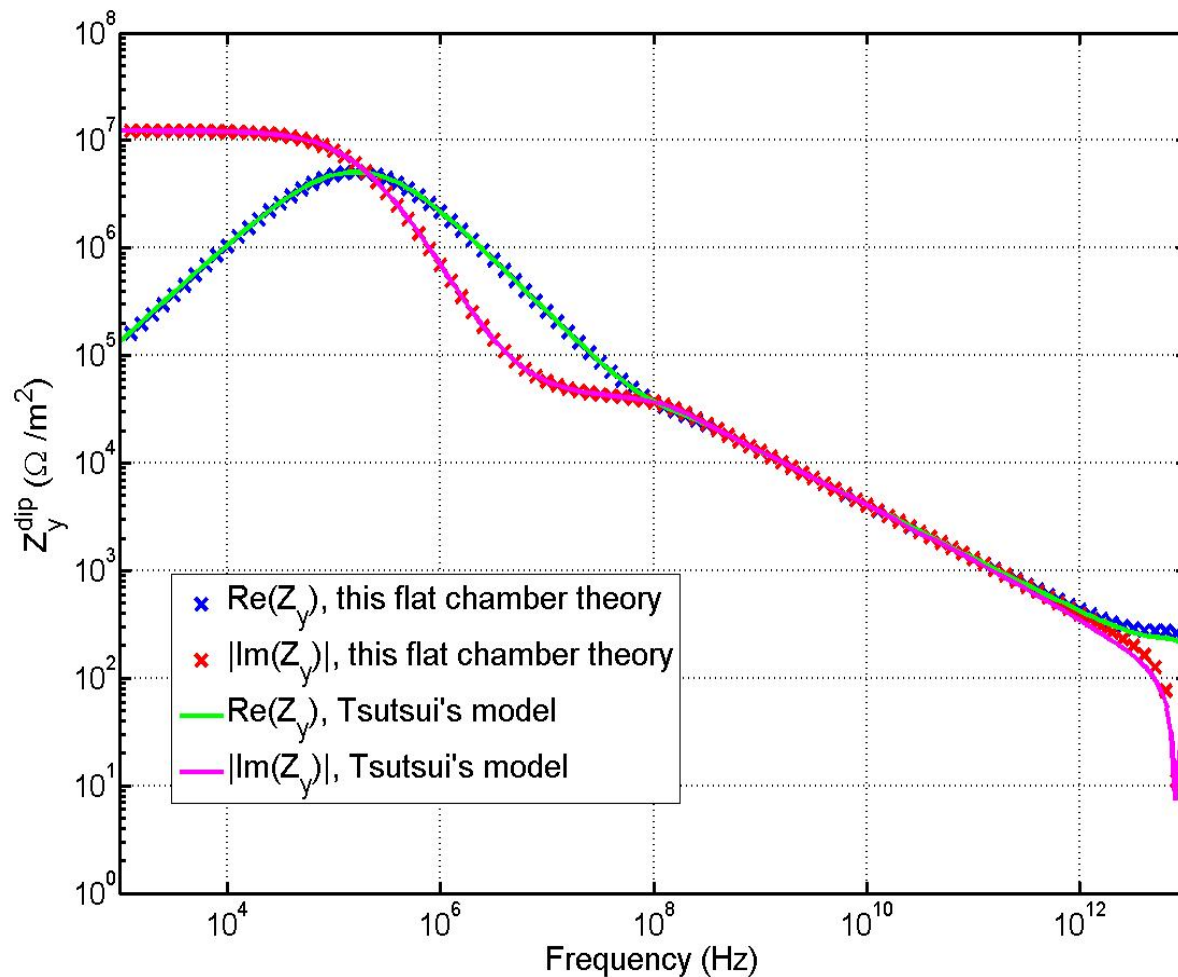
# Flat chamber results: comparison to Tsutsui's formalism

- For 3 layers (LHC copper-coated graphite collimator - 10 $\mu$ m Cu, half-gap 2mm), comparison with Tsutsui's model (LHC project note 318) on a rectangular geometry, the two other sides being taken far enough apart:



# Flat chamber results: comparison to Tsutsui's formalism

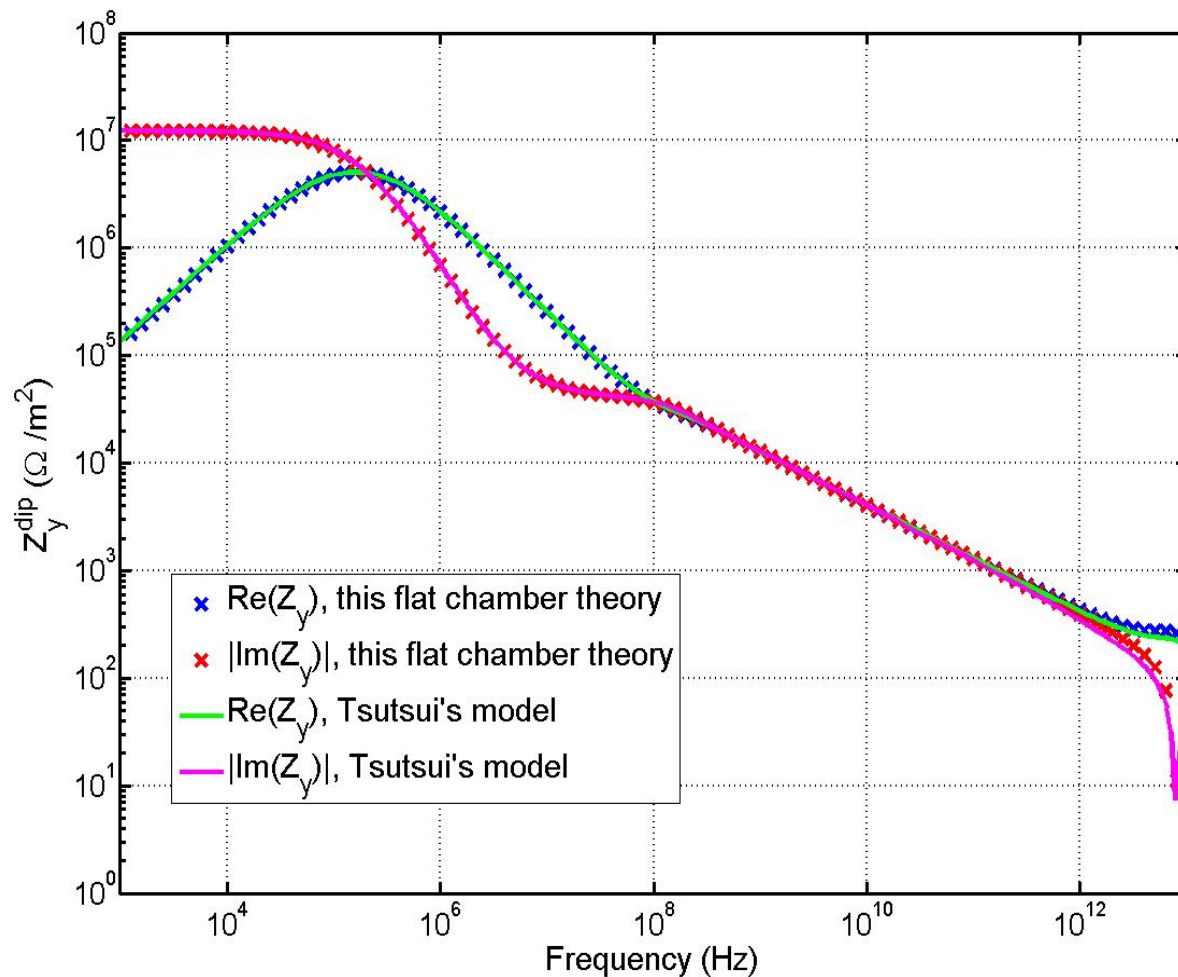
- For 3 layers (LHC copper-coated graphite collimator - 10 $\mu$ m Cu, half-gap 2mm), comparison with Tsutsui's model (LHC project note 318) on a rectangular geometry, the two other sides being taken far enough apart:



$\Rightarrow$  Very good agreement between the two approaches.

# Flat chamber results: comparison to Tsutsui's formalism

- For 3 layers (LHC copper-coated graphite collimator - 10 $\mu$ m Cu, half-gap 2mm), comparison with Tsutsui's model (LHC project note 318) on a rectangular geometry, the two other sides being taken far enough apart:

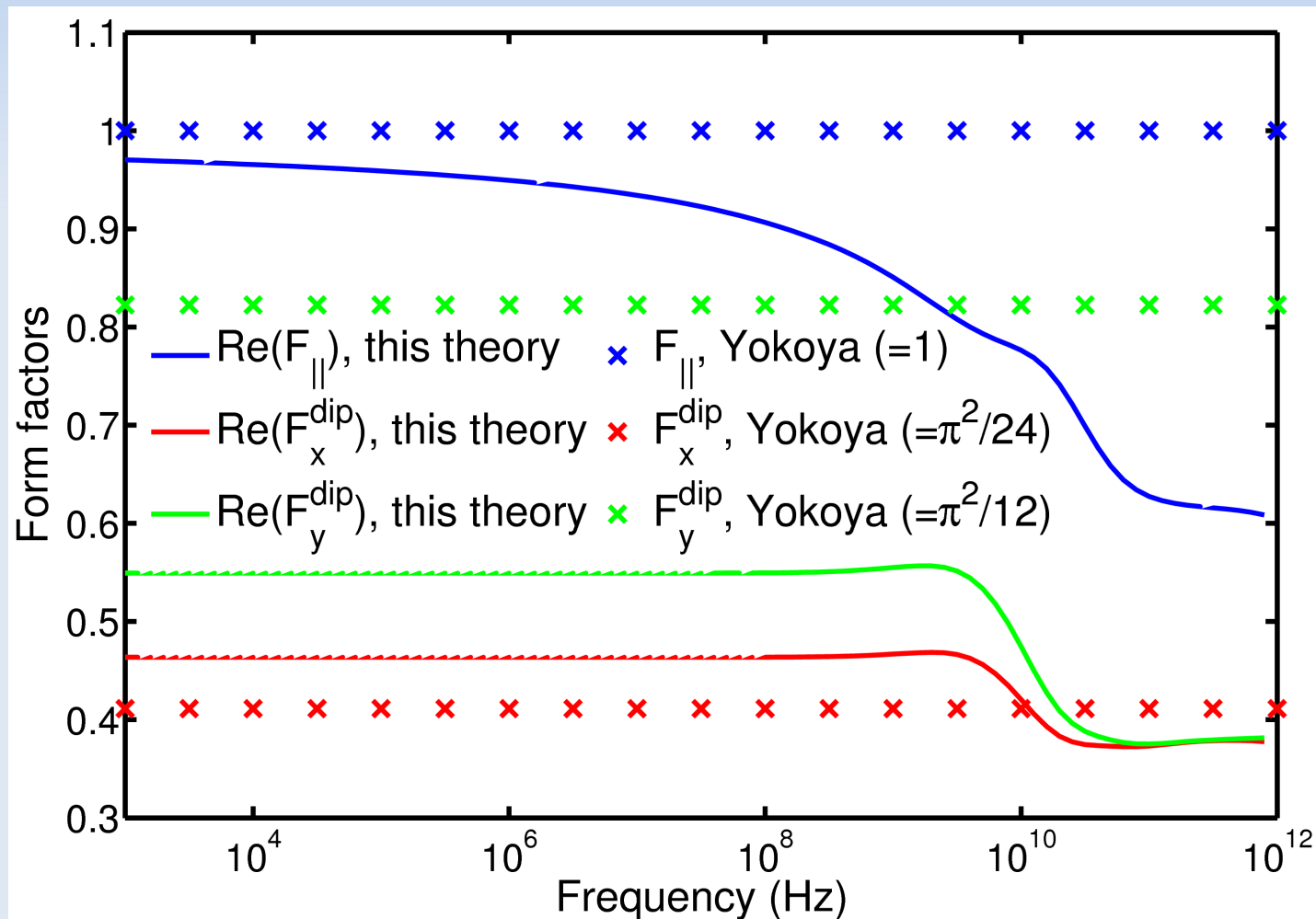


⇒ Very good agreement between the two approaches.

⇒ Can compute impedance for many layers (particularly interesting for coating – difficult to simulate in 3D EM codes)

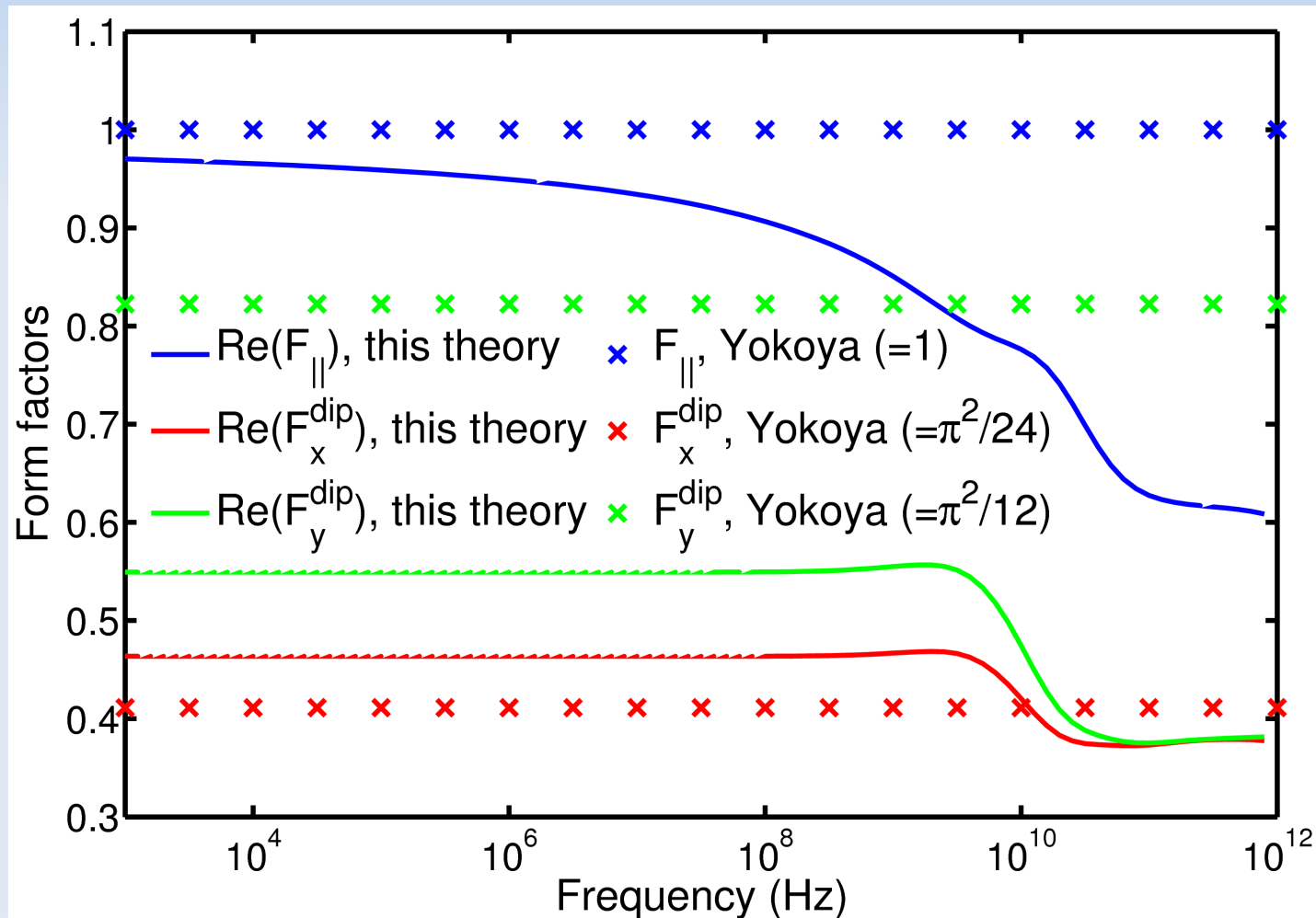
# Form factors flat / axisymmetric

- Ratio of **flat** chamber impedances w.r.t longitudinal and transverse dipolar **axisymmetric** ones → **generalize Yokoya factors** (Part. Acc., 1993, p. 511). In the case of a single-layer ceramic (hBN) at 450 GeV:



# Form factors flat / axisymmetric

- Ratio of **flat** chamber impedances w.r.t longitudinal and transverse dipolar **axisymmetric** ones → **generalize Yokoya factors** (Part. Acc., 1993, p. 511). In the case of a single-layer ceramic (hBN) at 450 GeV:



⇒ In this **particular case**, frequency dependent form factors quite  $\neq$  from the **Yokoya factors** (was first observed with other means by **B. Salvant et al IPAC'10**, p. 2054).

⇒ We can get such form factors for **any material** or material combination (i.e. several layers).

# Wake functions

- Wake functions are the **Fourier transforms** of the impedances, e.g.

$$W_x(\tau) = -\frac{j}{2\pi} \int_{-\infty}^{\infty} d\omega e^{j\omega\tau} Z_x(\omega), \text{ for a test particle at } \tau \text{ seconds behind the source}$$

In principle, straightforward to obtain from the impedances: "do an FFT".

In practice, usual method with discrete Fourier transform (DFT) with evenly spaced frequency mesh **not accurate enough** when dealing with **large frequency range**.



# Wake functions

- Wake functions are the **Fourier transforms** of the impedances, e.g.

$$W_x(\tau) = -\frac{j}{2\pi} \int_{-\infty}^{\infty} d\omega e^{j\omega\tau} Z_x(\omega), \text{ for a test particle at } \tau \text{ seconds behind the source}$$

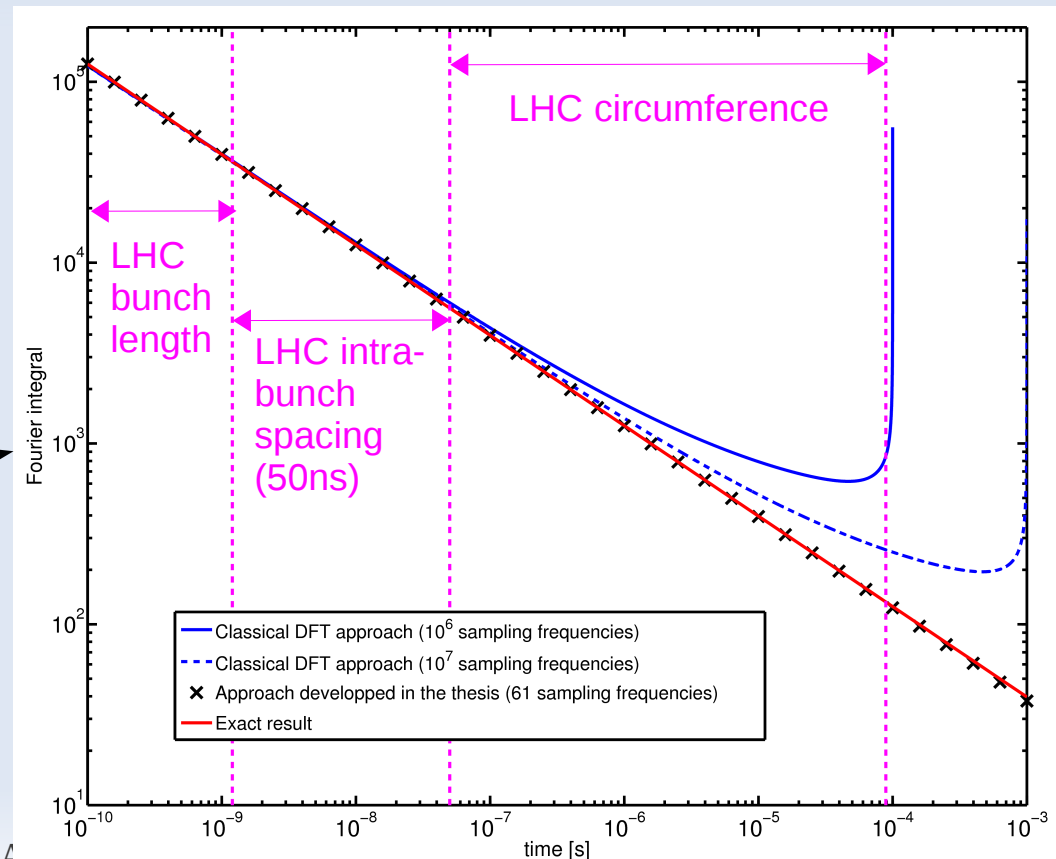
In principle, straightforward to obtain from the impedances: "do an FFT".

In practice, usual method with discrete Fourier transform (DFT) with evenly spaced frequency mesh **not accurate enough** when dealing with **large frequency range**.

⇒ developed a "new" method (based on idea from 1928): given **any frequency sampling**, on each subinterval replace the impedance by its cubic interpolation, and integrate it **analytically**.

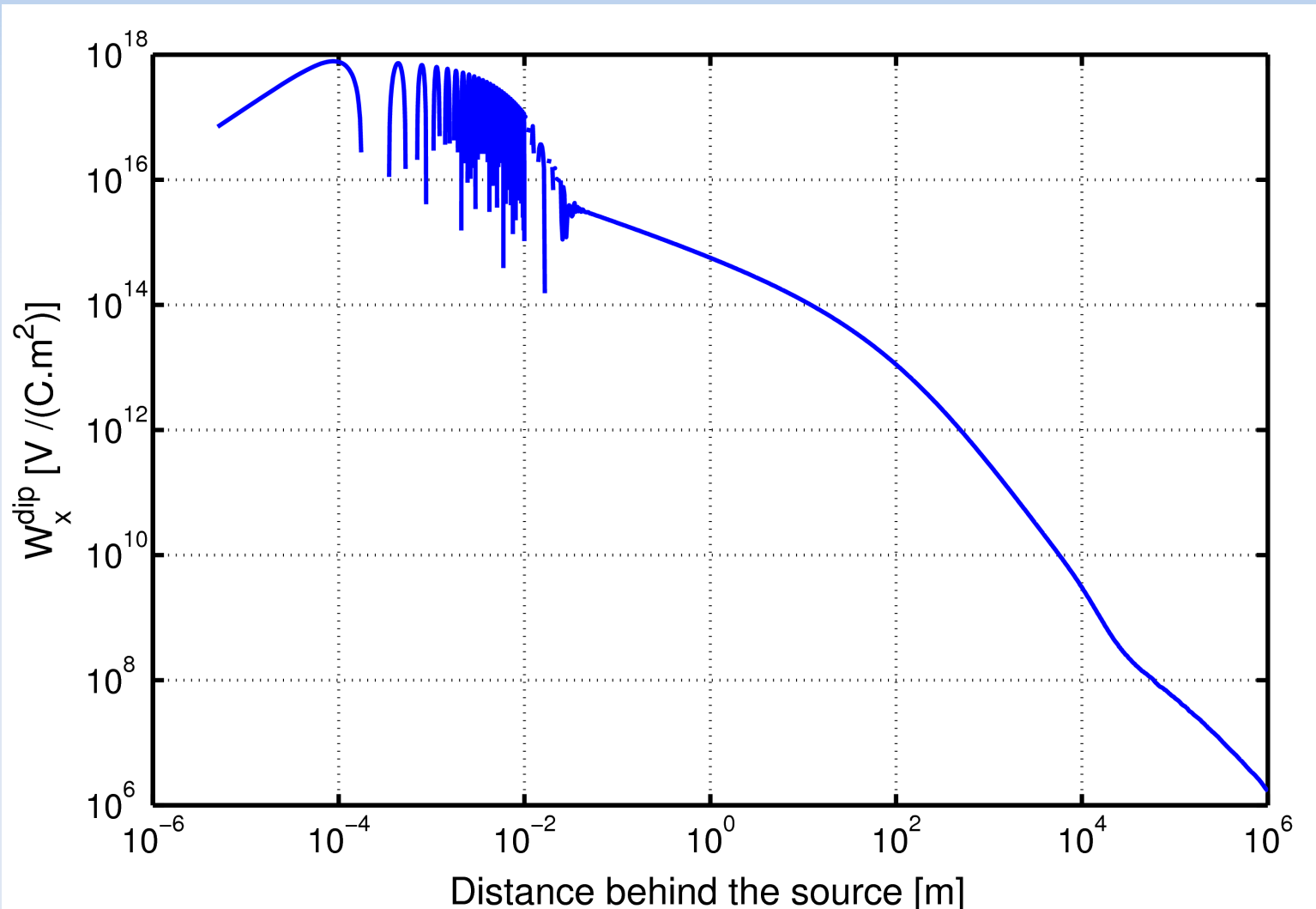
Example with  $Z_x = 1/\sqrt{|\omega|}$

→ **contrary to DFT, this method can correctly handle the different scales.**



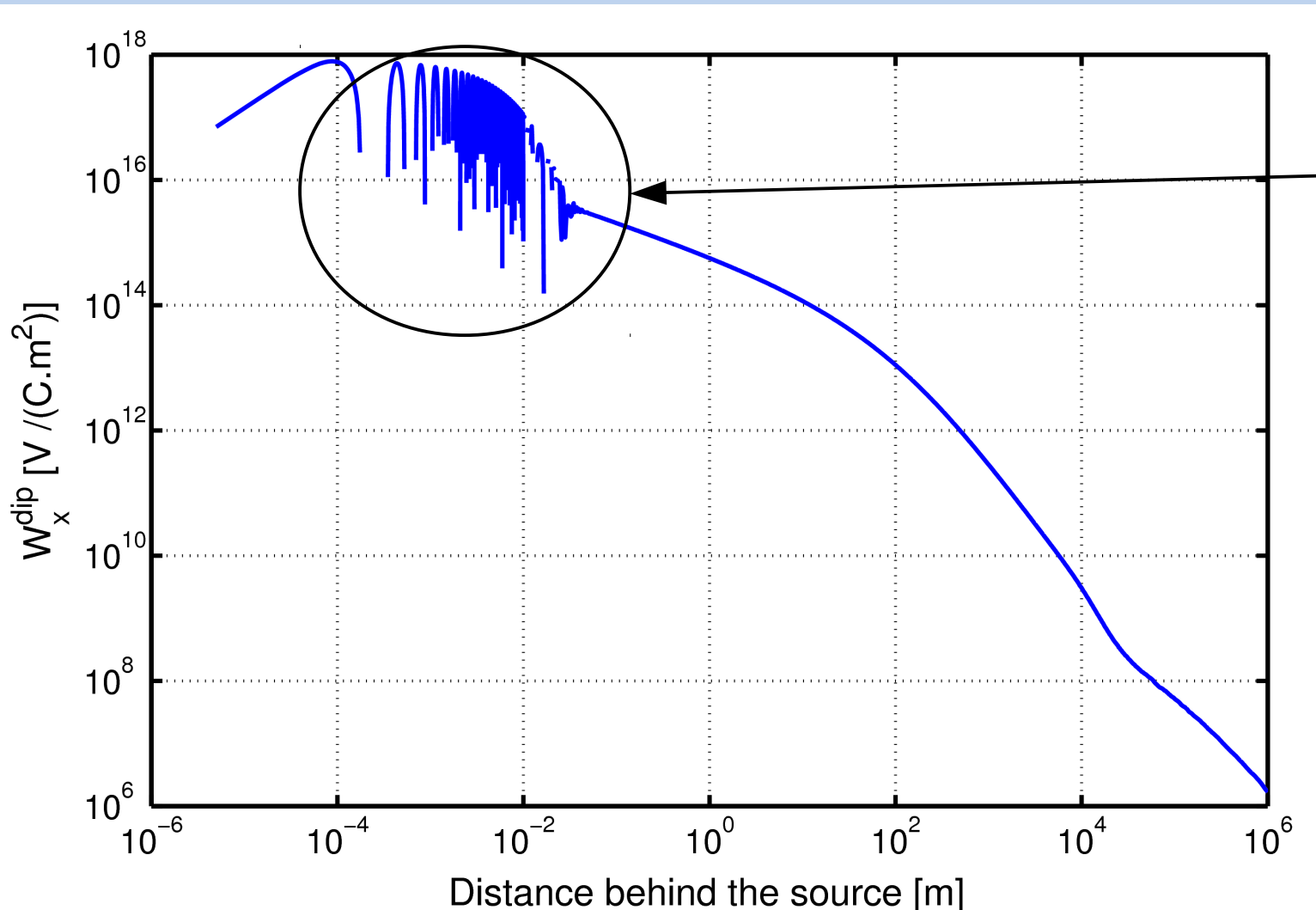
# Wake function: results (axisymmetric)

- 25mm-thick graphite of radius 1.5 mm (surrounded by stainless steel):



# Wake function: results (axisymmetric)

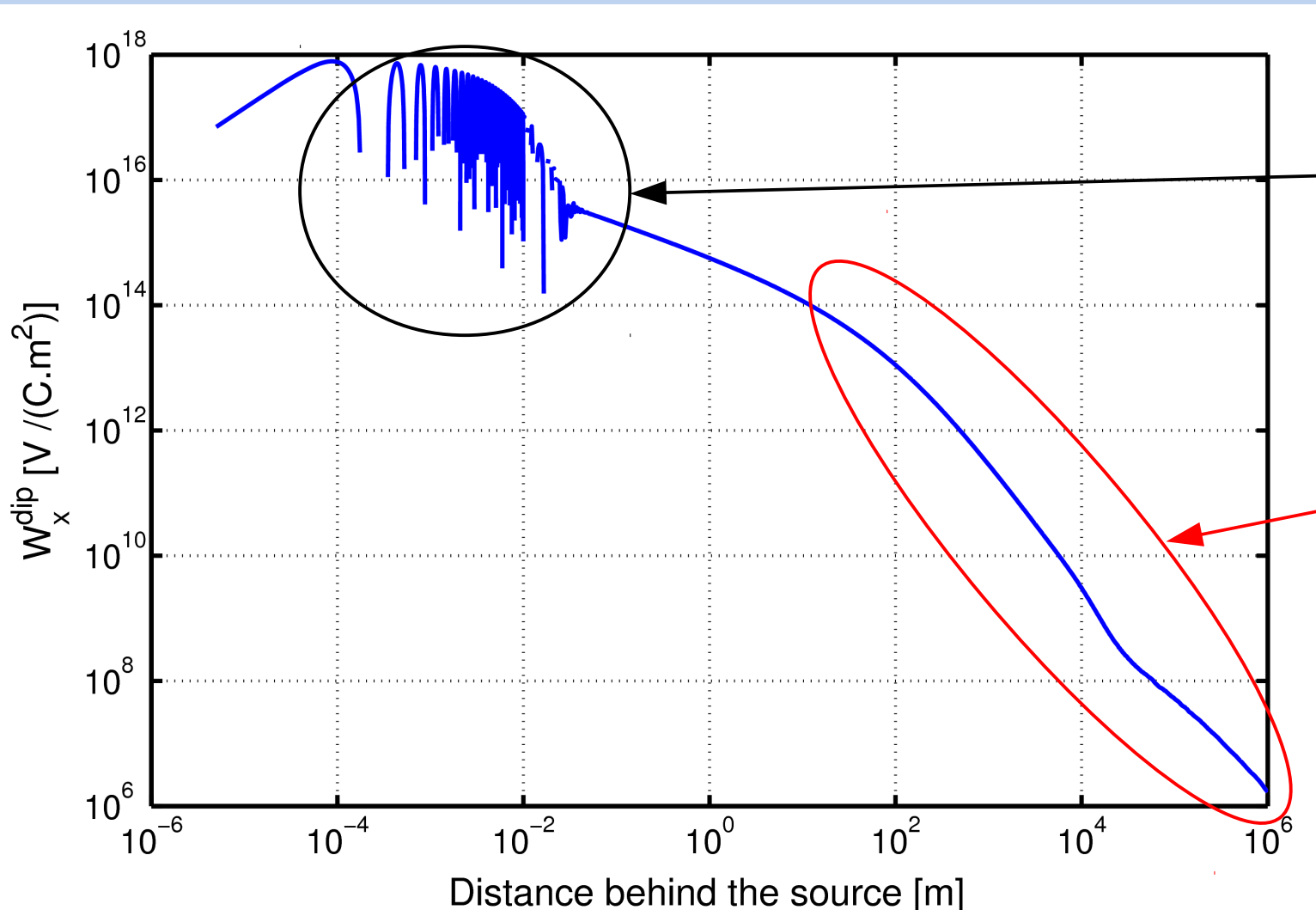
- 25mm-thick graphite of radius 1.5 mm (surrounded by stainless steel):



High frequency oscillations (due to the THz resonance).

# Wake function: results (axisymmetric)

- 25mm-thick graphite of radius 1.5 mm (surrounded by stainless steel):

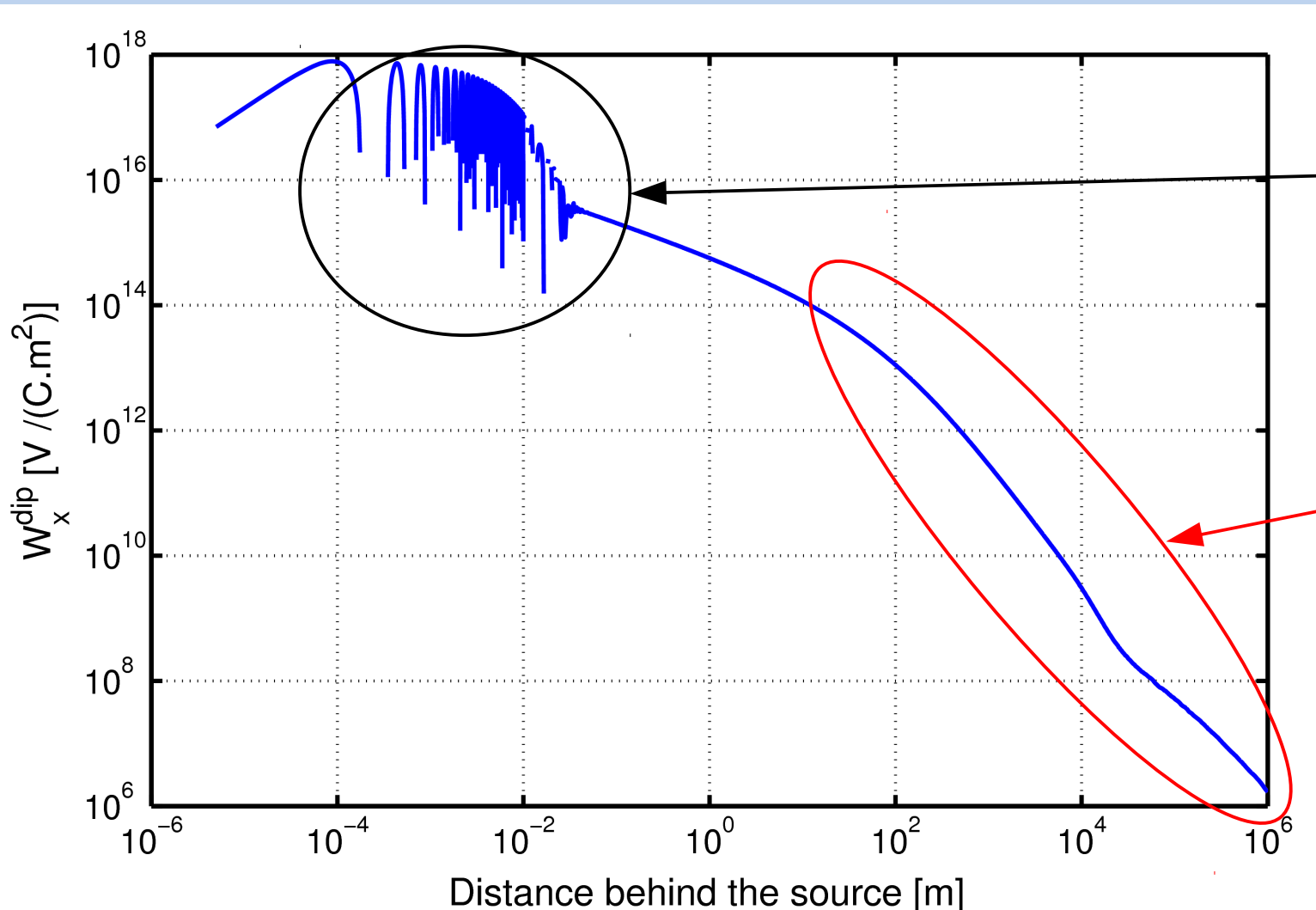


High frequency oscillations (due to the THz resonance).

Long-range behaviour (multibunch and multiturn)  
→ would be very difficult to get from EM "brute force" simulations.

# Wake function: results (axisymmetric)

- 25mm-thick graphite of radius 1.5 mm (surrounded by stainless steel):



High frequency oscillations (due to the THz resonance).

Long-range behaviour (multibunch and multiturn)  
→ would be very difficult to get from EM "brute force" simulations.

Wake in-front can also be computed.

# Possible extensions

- What happens when **source** and **test** particles have **different velocities** ?  
e.g. let's look at radial force in **axisymmetric** chamber:

$$F_r = q (E_r - v\mu_0 H_\theta) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial r} = \frac{jq}{k} \frac{\partial E_s}{\partial r},$$

# Possible extensions

- What happens when **source** and **test** particles have **different velocities** ?  
e.g. let's look at radial force in **axisymmetric** chamber:

$$F_r = q (E_r - v\mu_0 H_\theta) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial r} = \frac{jq}{k} \frac{\partial E_s}{\partial r}, \text{ Not valid anymore}$$

# Possible extensions

- What happens when **source** and **test** particles have **different velocities** ?  
e.g. let's look at radial force in **axisymmetric** chamber:

$$F_r = q (E_r - v\mu_0 H_\theta) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial r} = \frac{jq}{k} \frac{\partial E_s}{\partial r}, \text{ Not valid anymore}$$

→ instead we have:

$$F_r = q (E_r - v_{test}\mu_0 H_\theta) \\ = \frac{jq\gamma_{source}^2}{k} \left[ (1 - \beta_{test}\beta_{source}) \frac{\partial E_s}{\partial r} + (\beta_{source} - \beta_{test}) \frac{Z_0}{r} \frac{\partial H_s}{\partial \theta} \right],$$

Thanks to G. Rumolo



# Possible extensions

- What happens when **source** and **test** particles have **different velocities** ?  
e.g. let's look at radial force in **axisymmetric** chamber:

$$F_r = q (E_r - v\mu_0 H_\theta) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial r} = \frac{jq}{k} \frac{\partial E_s}{\partial r}, \text{ Not valid anymore}$$

→ instead we have:

$$F_r = q (E_r - v_{test}\mu_0 H_\theta) \\ = \frac{jq\gamma_{source}^2}{k} \left[ (1 - \beta_{test}\beta_{source}) \frac{\partial E_s}{\partial r} + (\beta_{source} - \beta_{test}) \frac{Z_0}{r} \frac{\partial H_s}{\partial \theta} \right]$$

Thanks to G. Rumolo

# Possible extensions

- What happens when **source** and **test** particles have **different velocities** ?  
e.g. let's look at radial force in **axisymmetric** chamber:

$$F_r = q (E_r - v\mu_0 H_\theta) = \frac{jq\gamma^2}{k} (1 - \beta^2) \frac{\partial E_s}{\partial r} = \frac{jq}{k} \frac{\partial E_s}{\partial r}, \text{ Not valid anymore}$$

→ instead we have:

$$F_r = q (E_r - v_{test}\mu_0 H_\theta) \\ = \frac{jq\gamma_{source}^2}{k} \left[ (1 - \beta_{test}\beta_{source}) \frac{\partial E_s}{\partial r} + (\beta_{source} - \beta_{test}) \frac{Z_0}{r} \frac{\partial H_s}{\partial \theta} \right]$$

Thanks to G. Rumolo

⇒ Radial force now also depends on  $H_s$  and can be very different.

Example: **AWAKE** experiment at CERN (electron beam circulating in same chamber as proton beam)

# Possible extensions

- What about **multilayer elliptic chambers** ?
  - in principle can be handled with the same ideas, using the following **change of variables** – or conformal map (Palumbo-Vaccaro *Il Nuovo Cimento* 89A:243, Gluckstern et al *Phys. Rev. E* 47:656, Piwinski *DESY* 94-068):

$$\begin{aligned}x &= c \cosh u \cos v, \\y &= c \sinh u \sin v.\end{aligned}$$

$c$  = ellipse **linear eccentricity** (or focal distance)

# Possible extensions

- What about **multilayer elliptic chambers** ?  
→ in principle can be handled with the same ideas, using the following **change of variables** – or conformal map (Palumbo-Vaccaro *Il Nuovo Cimento* 89A:243, Gluckstern et al *Phys. Rev. E* 47:656, Piwinski *DESY* 94-068):

$$\begin{aligned}x &= c \cosh u \cos v, \\y &= c \sinh u \sin v.\end{aligned}$$

$c$  = ellipse **linear eccentricity** (or focal distance)

- Separation of variables leads to **Mathieu differential equations**:

$$\begin{aligned}U''(u) + U(u) [K_u + c^2(k^2 - \omega^2 \varepsilon_c \mu) \cosh^2 u] &= 0, \\V''(v) + V(v) [K_v + c^2(k^2 - \omega^2 \varepsilon_c \mu) \cos^2 v] &= 0,\end{aligned}$$

# Possible extensions

- What about **multilayer elliptic chambers** ?
  - in principle can be handled with the same ideas, using the following **change of variables** – or conformal map (Palumbo-Vaccaro *Il Nuovo Cimento* 89A:243, Gluckstern et al *Phys. Rev. E* 47:656, Piwinski *DESY* 94-068):

$$\begin{aligned}x &= c \cosh u \cos v, \\y &= c \sinh u \sin v.\end{aligned}$$

$c$  = ellipse **linear eccentricity** (or focal distance)

- Separation of variables leads to **Mathieu differential equations**:

$$\begin{aligned}U''(u) + U(u) [K_u + c^2(k^2 - \omega^2 \varepsilon_c \mu) \cosh^2 u] &= 0, \\V''(v) + V(v) [K_v + c^2(k^2 - \omega^2 \varepsilon_c \mu) \cos^2 v] &= 0,\end{aligned}$$

⇒ provided all layer boundaries are **ellipses with same eccentricities** (confocal), we can in principle apply the same formalism as in cylindrical, replacing:

- cosines and sines by periodic Mathieu functions,
  - modified Bessel functions by modified Mathieu functions,
- and of course re-doing the decompositions & field matching accordingly...

# Conclusions

- For **multilayer axisymmetric chambers**, **Zotter formalism** has been extended to all orders of non-linearity, and its implementation improved thanks to the matrix formalism for the field matching → the number of layers is no longer an issue.
- For **multilayer flat chambers**, a **new theory** similar to Zotter's has been derived, giving also impedances without any assumptions on the materials conductivity, on the frequency or on the beam velocity.
- Both these theories were benchmarked.
- An **efficient algorithm** to compute **wake functions** from impedances spreading over a large frequency range, using a non-equidistant discretization, has been developed.

⇒ **Implemented in codes** (**Rewall**, **ImpedanceWake2D**, available at <http://impedance.web.cern.ch>), used for various machines (LHC, HL-LHC, PS, SPS, CLIC, FCC, TLEP).

- Possible extensions could be investigated:
  - case with **different source and test velocities** (relatively easy),
  - multilayer **elliptic** chamber (more difficult).

*Thank you for your attention !*