

# Superferric rapidly cycling magnets Optimized field design and Measurement

P. Schnizer<sup>1</sup>, E. Fischer<sup>1</sup>, P. Akishin<sup>2</sup>, H. Kiesewetter<sup>1</sup>,  
T. Knapp<sup>1</sup>, F. Klos<sup>1</sup>, R. Kurnyshov<sup>3</sup>, T. Mack<sup>1</sup>,  
B. Schnizer<sup>4</sup>, P. Shcherbakov<sup>5</sup>

<sup>1</sup>Gesellschaft für Schwerionenforschung, Darmstadt, Germany

<sup>2</sup>Joint Institut for Nuclear Research, Dubna, Moscow Region, Russia

<sup>3</sup>Electroplant, Moscow, Russia

<sup>4</sup>Technische Universität Graz, Austria

<sup>5</sup>Institut for High Energy Physics, Protvino, Moscow Region, Russia

WAMSDO@CERN 19 – 23 May 2008 p.schnizer@gsi.de

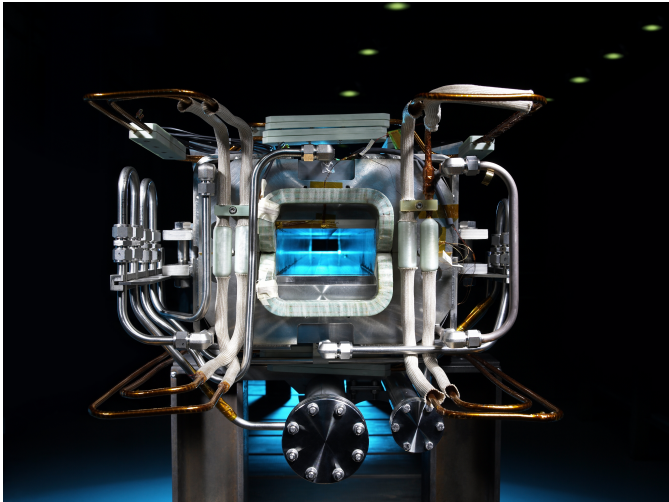
# Outline

- 1 Machine
- 2 Calculations
  - Field Description
  - DC Calculations
  - Calculations on the ramp
- 3 Measuring the Field Quality
  - Approach

# SIS 100: main parameters

- FAIR @ GSI → 2 synchrotrons with superconducting machines
- SIS 100 → core component
  - Nuclotron “father figure”
  - based on two phase cooled hollow cable
  - 2 T , 4 T / s,
  - 3.5 m long dipoles
  - 1 m long quadrupole in 5 m long SSS
  - elliptic vacuum chamber  $115 \times 60$  mm

# SIS 100: Prototype Dipole



Courtesy of Babcock Noell GmbH

# Circular Multipoles for Elliptic Apertures

Standard field description: Circular Multipoles

$$\mathbf{B}(\mathbf{z}) = B_y + iB_x = \sum_{m=0}^{\infty} \mathbf{C}_m \left( \frac{\mathbf{z}}{R_{ref}} \right)^m. \quad (1)$$

- convergent also outside  $R_{ref}$
- satisfactory field description **only for analytical data**
- coefficients  $\rightarrow$  FT on data on  $R_{ref}$  (FEM, measurement)  
 $\rightarrow$  thus with artifacts

# Multipoles Scale Factors

# for SIS 100

Aperture width  $w \dots 115 \text{ mm}$

Aperture height  $h \dots 60 \text{ mm}$

Coil diameter  $d \dots 46 \text{ mm}$

$$\left(\frac{w}{h}\right)^n = (\approx 1.9)^n$$

$$\left(\frac{w}{r}\right)^n = (2.5)^n$$

Single rotating coil measurement, single expansion on numerical data  $\rightarrow$  not sufficient

n	w / d	w / h
1	1.00	1.00
3	6.25	3.67
5	39.06	13.50
7	244.14	49.58
9	1525.88	182.13
11	9536.74	669.06
13	59604.64	2457.87

# Elliptic Multipoles for Complex Magnetic Field I/II

Field expansion:

$$\mathbf{w} = \eta + i\psi$$

$$\mathbf{B}(\mathbf{w}) = \frac{\mathbf{e}_0}{2} + \sum_{n=1}^{\infty} \mathbf{e}_n \frac{\cosh[n(\eta + i\psi)]}{\cosh(n\eta_0)}$$

$\eta = \text{const.} \dots$  hyperbola

$\psi = \text{const.} \dots$  ellipse

Expansion coefficients:

$$\mathbf{e}_n = \frac{1}{2\pi} \int_{-\pi}^{\pi} \mathbf{B}(\mathbf{w} = e \cosh(\eta_0 + i\psi)) \times \cos(m\psi) d\psi.$$

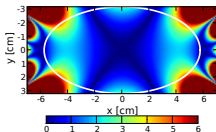
## Linear Analytic Transformation to Circular Ones

P. Schnizer, B. Schnizer, P. Akishin, and E. Fischer

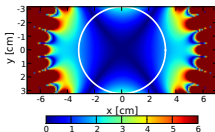
Field representation for elliptic apertures. Technical report, Feb. 2007, Jan. 2008

MT20: Magnetic field analysis for superferric accelerator magnets using elliptic multipoles and its advantages, 3L06

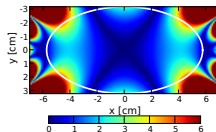
# Elliptic Multipoles $\Leftrightarrow$ Circular Multipoles



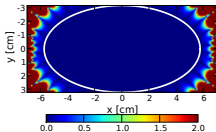
elliptic  $\mathcal{C}_e$



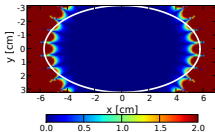
cyclic  $\mathcal{C}$



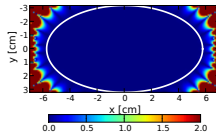
ell.  $\rightarrow$  cyclic in  $\mathcal{C}_e$



$\Delta$  elliptic  $\mathcal{C}_e$



$\Delta$  cyclic  $\mathcal{C}$



$\Delta$  ell.  $\rightarrow$  cyclic in  $\mathcal{C}_e$

Illustrated for CSLD at Injection Field ( $\approx 0.25 T$ )



# Literature

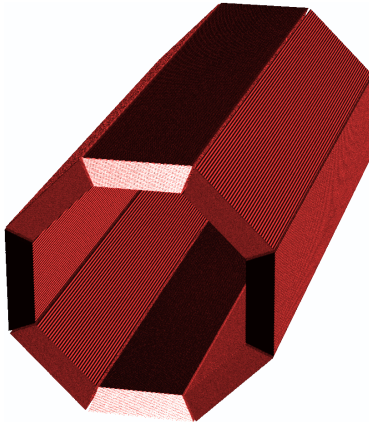
-  P. Schnizer, B. Schnizer, P. Akishin, and E. Fischer.  
Field representation for elliptic apertures.  
Technical report, Gesellschaft für Schwerionenforschung mbH, Planckstraße 1, D-64291 Darmstadt, February 2007.
-  P. Schnizer, B. Schnizer, P. Akishin, and E. Fischer.  
Magnetic field analysis for superferric accelerator magnets using elliptic multipoles and its advantages.  
*In The 20<sup>th</sup> international conference on magnet technology.* IEEE, August 2007.
-  P. Schnizer, B. Schnizer, P. Akishin, and E. Fischer.  
Field representation for elliptic apertures.  
Technical report, Gesellschaft für Schwerionenforschung mbH, Planckstraße 1, D-64291 Darmstadt, January 2008.

# Static calculations: Challenges

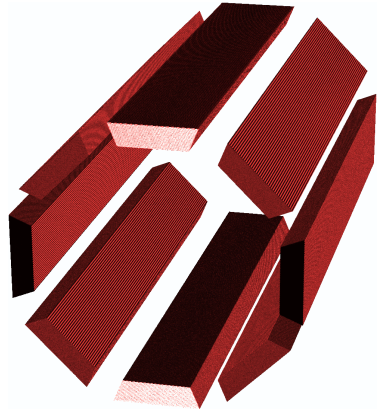
- SIS 100 magnets → superferric → iron dominated
- Nuclotron cable
  - superconducting wires wound around tube
  - small current carrying layer
  - not directly supported by TOSCA 3D
  - → modelling required
- influence of the coil not negligible

# Modelling the Nuclotron Conductor

I/II



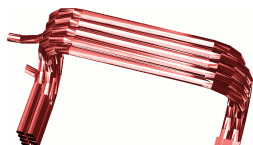
model



exploded

round shape modelled as bricks → many elements → careful  
selection of longitudinal length

# Modelling the Nuclotron Conductor



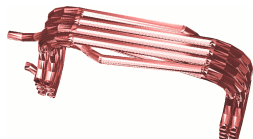
3D BNN



top BNN



bottom BNN



3D JNIR



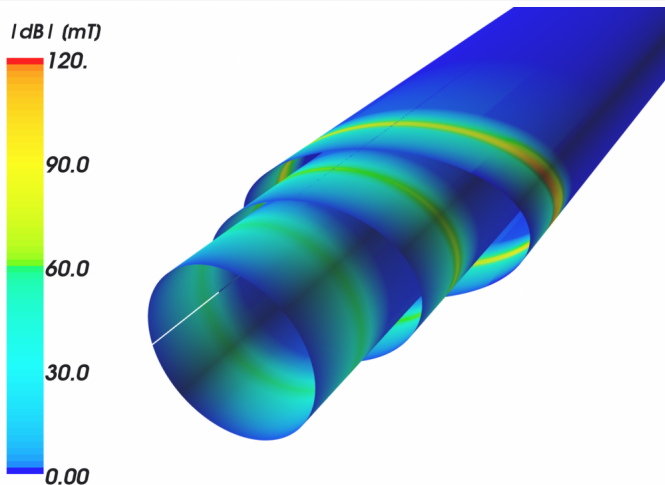
top JNIR



bottom JNIR

SIS 100 coil ends → embedded in G10 → original interlayer connection too complicated → field change acceptable?

# Interlayer connection: Field difference



maximum difference 0.1  $T$  at a small spot; acceptable

# Calculation on the ramp

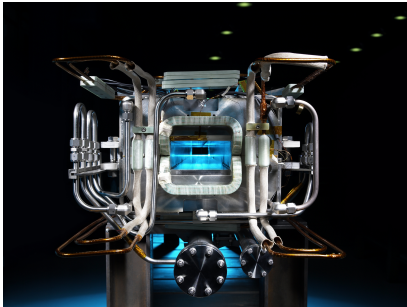
- SIS 100 magnets  $\rightarrow$  nominal ramp rate 4 T / s
- eddy currents
  - in the yoke
  - in the vacuum chamber
  - in the eddy currents

based on R&D presented in:

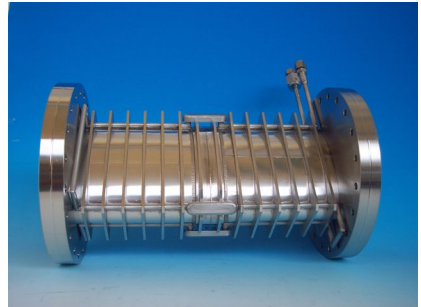
Cryogenics 2007: E. Fischer, R. Kurnishov, and P. Shcherbakov; Finite element calculations on detailed 3D models for the superferric main magnets of the FAIR SIS100 synchrotron.

# Prototype Magnet: To be tested

magnet



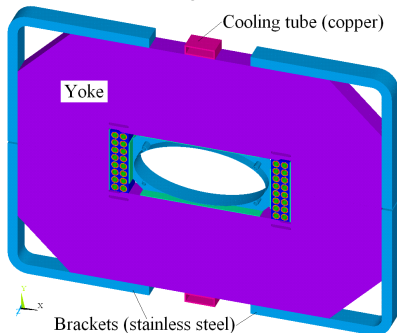
vacuum chamber model  
consists of: beam pipe  
ribs, cooling tubes



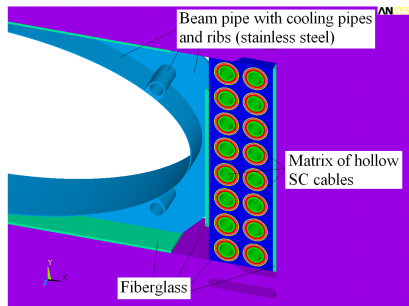
Courtesy of Babcock Noell GmbH

# Magnet Design

3D modell of a period in the magnet



total



zoom

EUCAS 2007: E. Fischer, R. Kurnyshov, and P. Shcherbakov;  
Analysis of Coupled Electromagnetic-Thermal Effects in  
Superconducting Accelerator Magnets

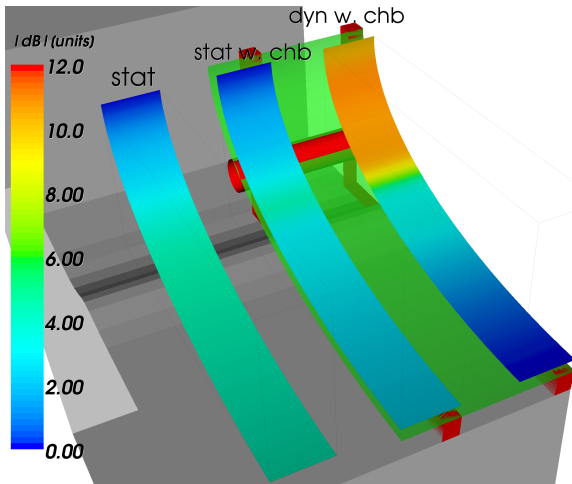


# Method of Calculation and Results

- calculated for triangular cycle ( $0T \rightarrow 2T \rightarrow 0T$ ,  $4T/s$ )
- time points at  $\approx 0.25T$ ,  $\approx 1.04T$ ,  $\approx 1.83T$ ,  $\approx 2.00T$
- data
  - field on ellipses (maximum errors at the border)
  - circular multipoles (calculated from elliptic ones)

# Impact on the field quality

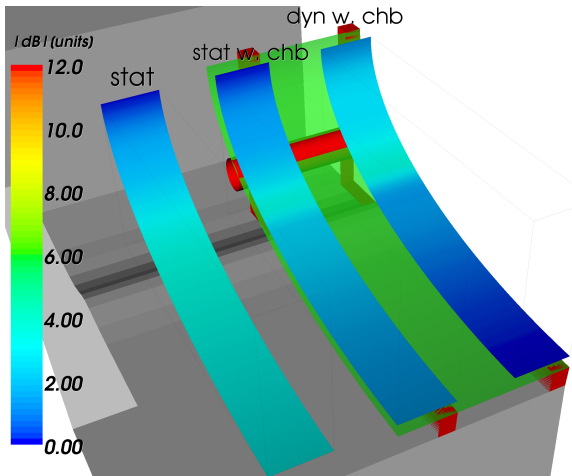
I/IV



Field to  $0.248T$   
(injection)  
field distortion  $\rightarrow$   
static 5 units,  
dynamic  $\times 3!$

# Impact on the field quality

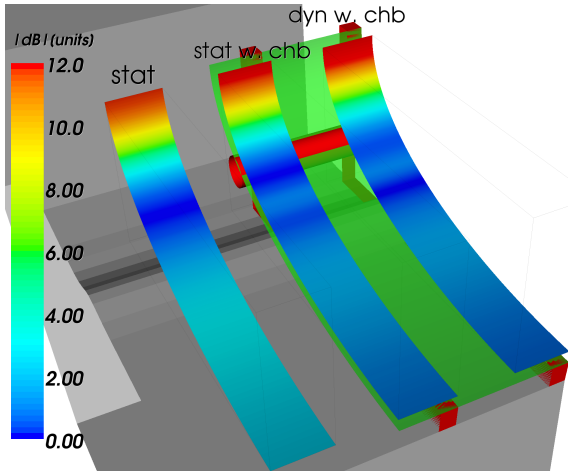
II/IV



Field to 1.04 T  
 $t = 0.25s$   
field distortion  $\rightarrow$   
4 units (= 400 ppm)  
dynamic to higher variation

# Impact on the field quality

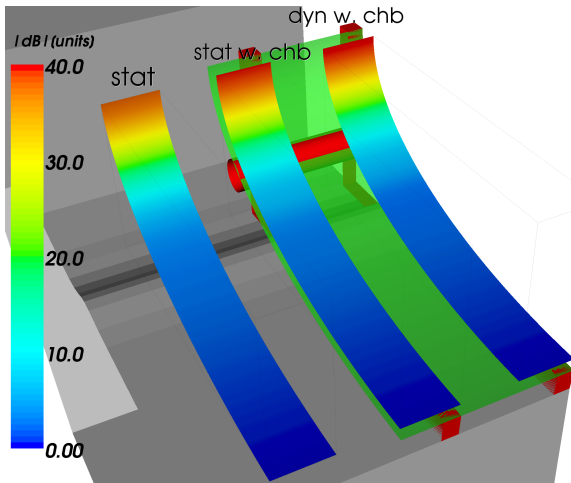
III/IV



Field to  $1.832 T$   
saturation  $\rightarrow$  field  
distortion  
dynamic to higher  
variation  
dynamic  $3\times$ ,  
static  $10\times$  higher  
than injection

# Impact on the field quality

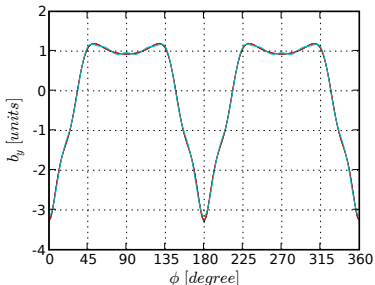
III/IV



Field to 2.00 T  
saturation  $\rightarrow$  field  
distortion (much  
larger than at 1.83  
T)  
eddy currents to  
not significant  
dynamic  $3\times$ ,  
static  $10\times$  higher  
than injection

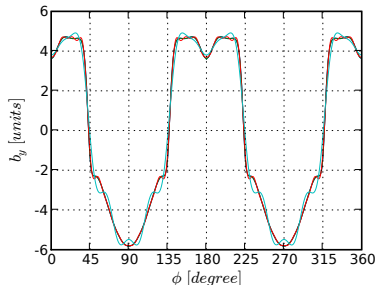
# Static to dynamic: Integral over one Period

Deviation of  $B_y$  in units once around the ellipse



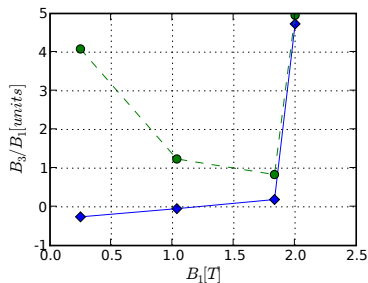
static

at injection: ramp effects factor of 2 - 3!



dynamic with vacuum chamber

# Expected Multipole Errors



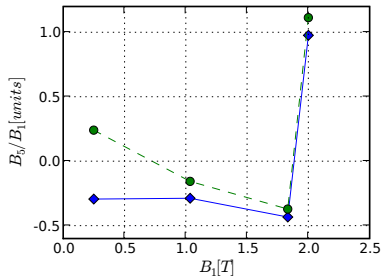
$b_3$ , sextupole ( $2^3 = 8$ )

$R_{Ref} = 40$  mm

blue ... static

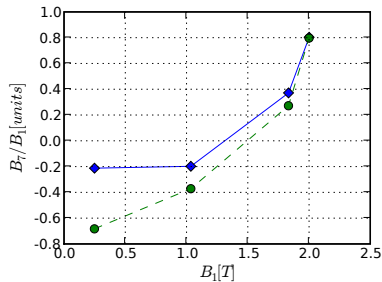
green... on the ramp

sextupole: at injection 10 times larger ...



$b_5$ , dekapole ( $2^3 = 32$ )

# Expected Multipole Errors

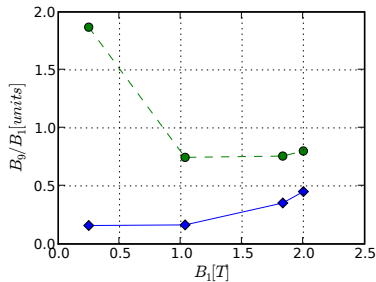


$$b_7, (2^7 = 128)$$

$$R_{Ref} = 40 \text{ mm}$$

blue ... static

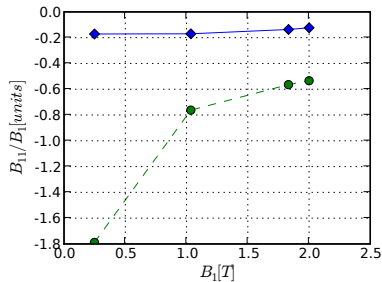
green... on the ramp



$$b_9, (2^7 = 512)$$



# Expected Multipole Errors

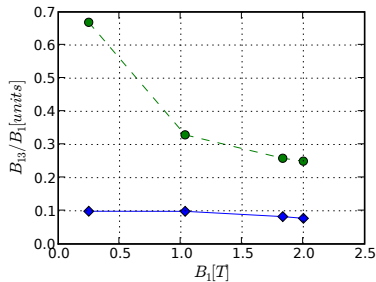


$$b_{11}, (2^{11} = 2048)$$

$$R_{Ref} = 40 \text{ mm}$$

blue ... static

green... on the ramp



$$b_{13}, (2^{13} = 8192)$$

# Magnetic Measurement: Accuracy Targets

- integral strength  $\rightarrow$  250 ppm
- field angle  $\rightarrow$  0.5 mrad
- field axis (quadrupole)  $\rightarrow$  0.25 mm
- higher order harmonics  $\rightarrow$  10ppm

Main Target  $\rightarrow$  strength, angle, axis

# Magnetic measurement: field quality

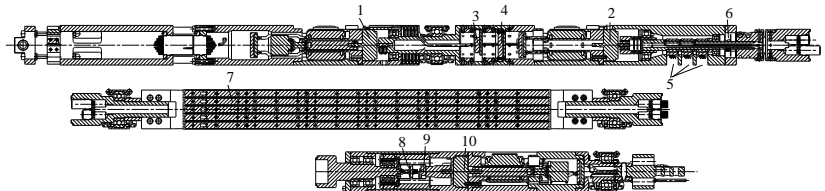
- superferric design: field formed by magnet poles
- deteriorated by the yoke
  - permeability of the iron
  - mechanical artifacts
  - manufacturing tolerances
  - eddy currents
- deteriorated by the vacuum chamber
  - geometry of the vacuum chamber
  - permeability of the steel
  - resistivity of the chamber
- Standard Magnetic Measurement **not** inside vacuum chamber → field mainly created by yoke
- vacuum chamber distortion → calculated → checked by special measurement

# Selected method

- series tests → measurement equipment @ 300 K → anticryostat
- moveable anti-cryostat → covers (nearly) whole ellipse, thus no extrapolation
- rotating coil probe for DC, step by step coil probe on the ramp → same equipment for both magnet operations
- based on “bucking coil probes” → requirements for field homogeneity reduced by  $\frac{1}{100}$

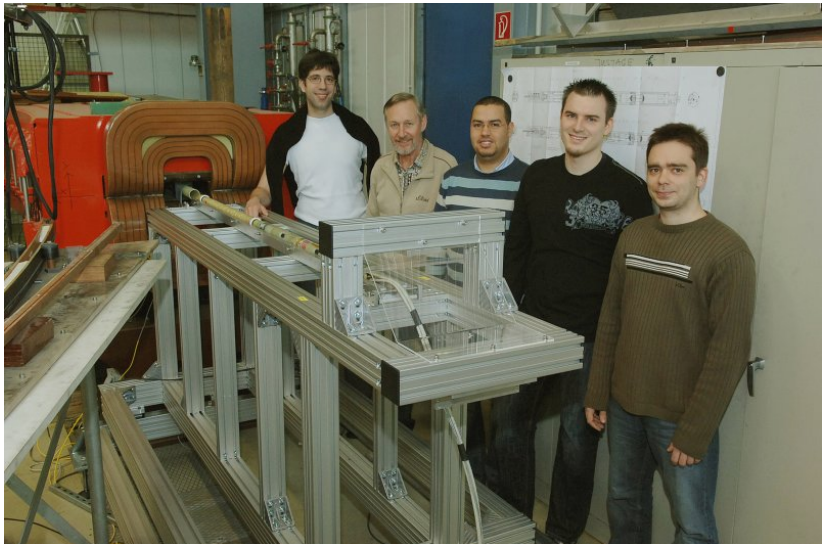
MT20: P. Schnizer et al. : A mole for measuring pulsed superconducting magnets, 4N10

# Sketch of the Mole



1 levelling piezo motor 2 coil rotation piezo motor 3, 4 inclinometers 5 slip rings 6 angular encoder with 512 ticks, 7 coil probes 8 angular encoder with 7500 counts 9 its inclinometer and 10 levelling motor

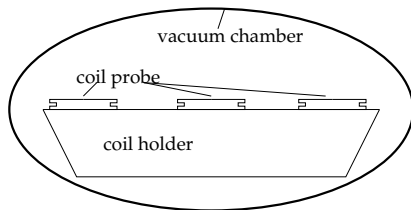
# The mole



# The mole



# Vacuum chamber artifacts: special measurement



- Vacuum chamber → elliptic vacuum chamber
- coil probes on a common support placed laterally separate
- allow to compare calculations to measurements



# Conclusion

- SIS 100 Dipoles: first prototype produced
- DC and ramp field quality calculated
- Vacuum chamber adds considerably to the field distortion
- Standard Magnetic Measurement **not** inside vacuum chamber → field mainly created by yoke
- vacuum chamber distortion → calculated → checked by special measurement