

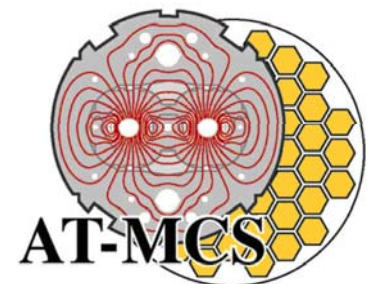
*Geneva – 20<sup>th</sup> May 2008*

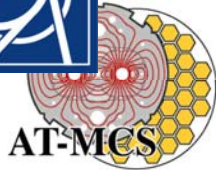


*WAMSDO 2008*

*Self-Field Instabilities in High- $J_c$  Nb<sub>3</sub>Sn Strands:  
the Effect of Copper RRR*

*Bernardo Bordini*





# OUTLINE



WAMSDO 2008

- ❑ INTRODUCTION
- ❑ LESSON LEARNED FROM WIRES WITH LOW RRR
- ❑ THE EFFECT OF RRR AT 4.2 K AND 1.9 K
- ❑ PRELIMINARY RESULTS ON
  - ❑ THE EFFECTS OF CHANGING THE STRAND'S THERMAL BOUNDARY CONDITIONS THROUGH A 'THICK' LAYER OF STYCAST
  - ❑ SENSITIVITY TO MECHANICAL PERTURBATION
  - ❑ THE EFFECTS OF LOCAL STRAND DAMAGES
- ❑ CONCLUSIONS



# *MAGNETO-THERMAL INSTABILITIES*



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- ❑ High- $J_c$  Nb<sub>3</sub>Sn wires is the best candidate for next generation High Field (>10 T) accelerator magnets.
- ❑ Although very promising, state of the art high- $J_c$  Nb<sub>3</sub>Sn wires suffer flux jumps.
- ❑ Flux jumps can quench the superconductor and severely limit the strand performance.
- ❑ Flux jumps are caused by magneto-thermal instabilities:
  - 1) 'Magnetization' instability depending on the  $J_c$  and  $D_{\text{eff}}$  ; at 4.2 K it can provoke premature magnet quenches in the very low field region (0 – 3 T) if the  $J_c$  and  $D_{\text{eff}}$  are not sufficiently low and the copper RRR is not sufficiently high;
  - 2) 'Self field' instability depending on  $J_c$  and the strand diameter; at 1.9 K this phenomenon is the dominant magneto-thermal instability in high- $J_c$  Nb<sub>3</sub>Sn wires and it might be the primary cause of premature quenches of HF magnets.



# SELF-FIELD INSTABILITY



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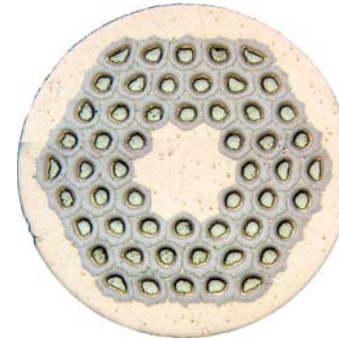
- ❑ Self field instability is caused by the uneven distribution of transport current ( $I$ ) within the wire.
- ❑ While ramping up  $I$  at a fixed  $B_a$ , the multifilamentary strand acts as a large monofilament with a radius equal to the composite radius:

The current only flows in the outermost sub-elements at the critical current density.

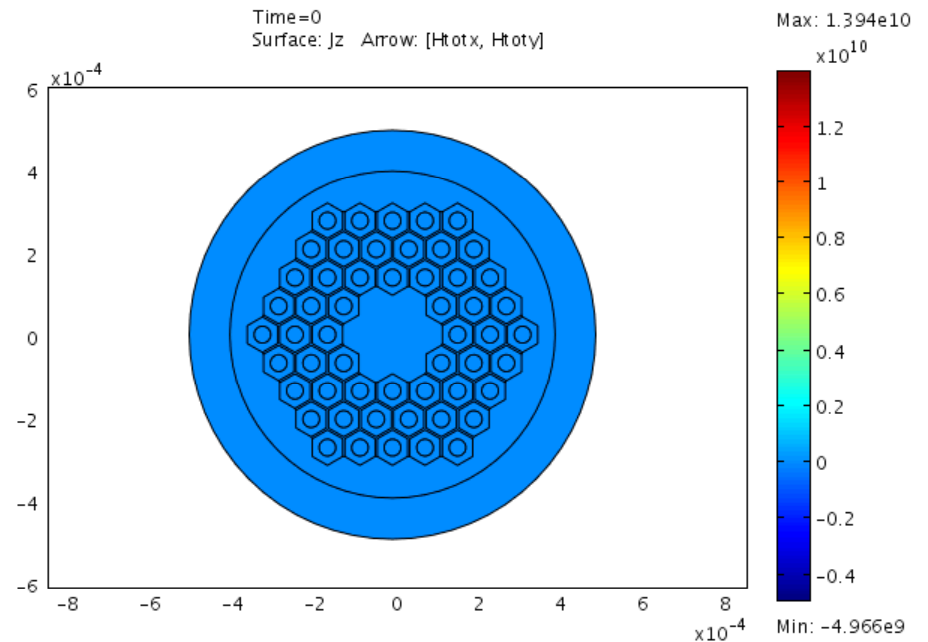
*Distribution of the transport current while increasing the current from 0 to 1200 A in a fixed applied field,  $B_a=6$  T*

20/May/2008

Bernardo Bordini



*0.8 mm RRP Nb<sub>3</sub>Sn strand*





# SELF-FIELD INSTABILITY : Simulation of Premature Quench



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The color represents  
the Transport Current  
distribution

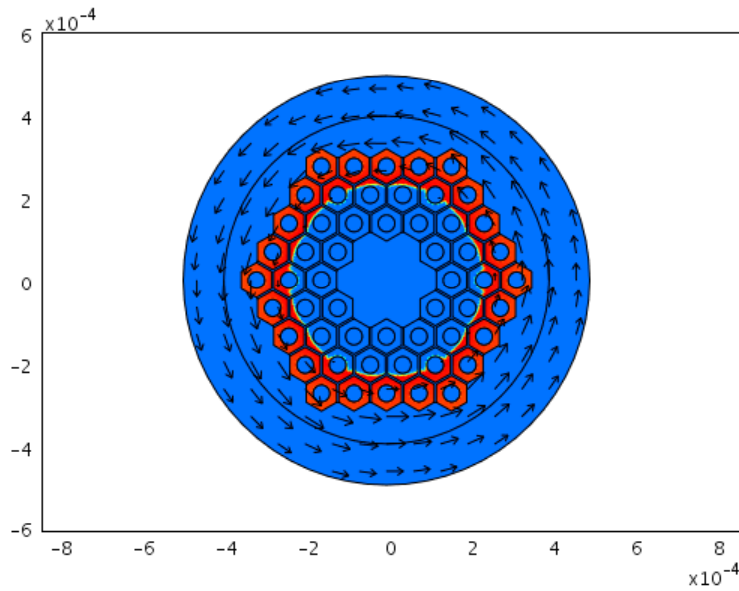
The color represents  
the Temperature  
distribution



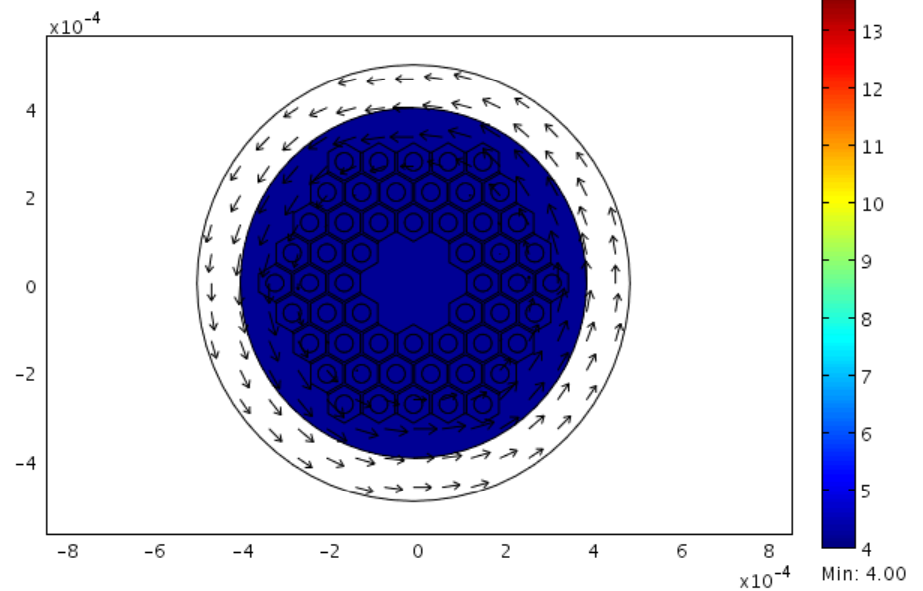
$B_a = 6 \text{ T}$  --  $I = 1200 \text{ A}$  --  $T_i = 4.2 \text{ K}$

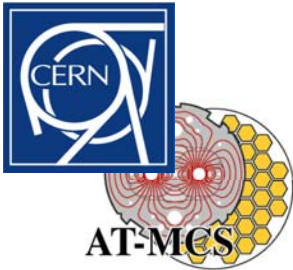


Time=60 (1)  
Surface: Jz Arrow: [Htotx, Htoty]



Time=60 (1)  
Surface:  $T^*((x^2+y^2)^{0.5} < 0.000400000001)$  [K] Arrow: [Htotx, Htoty]





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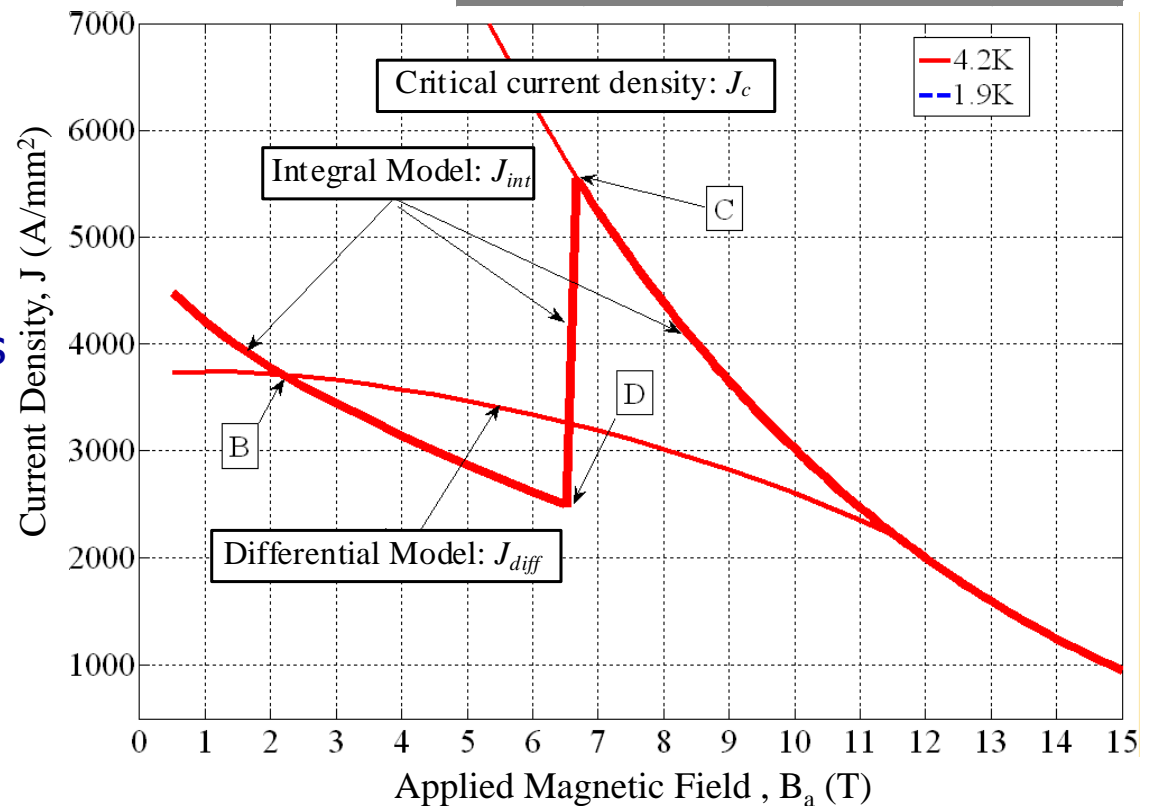
# MODEL SF INSTABILITY: a semi-analytical approach



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- ❑ A semi-analytical 'Integral' model was developed [1] to predict the minimum quench current due to magneto-thermal instability
- ❑ The model, based on the adiabatic hypothesis, is well adapted to round wires with a low RRR
- ❑ In the plot the current densities are averaged over the non-Cu area and the curves represent:
  1. the intrinsic  $J_c$  values
  2. the 'integral' model
  3. the 'differential' adiabatic stability model of self-filed [2] adapted to our strand.

Strand diam. [mm]	Strand type	$J_c$ @ 4.2 K-12 T [ $A/mm^2$ ]	$B_{c2}$ @ 4.2 K [T]
0.7	MJR 54/61	2000	22.73



[1] B. Bordini, E. Barzi, S. Feher, L.Rossi, A.V. Zlobin, to be published in *IEEE Trans. Appl. Supercond.* 2008 20/May/2008

[2] R. G. Mints, A. L. Rakhmanov, *Sov. Tech. Phys. Lett.*, vol 2, no. 6, Jun. 1976





# V-I DATA AND SF INSTABILITY



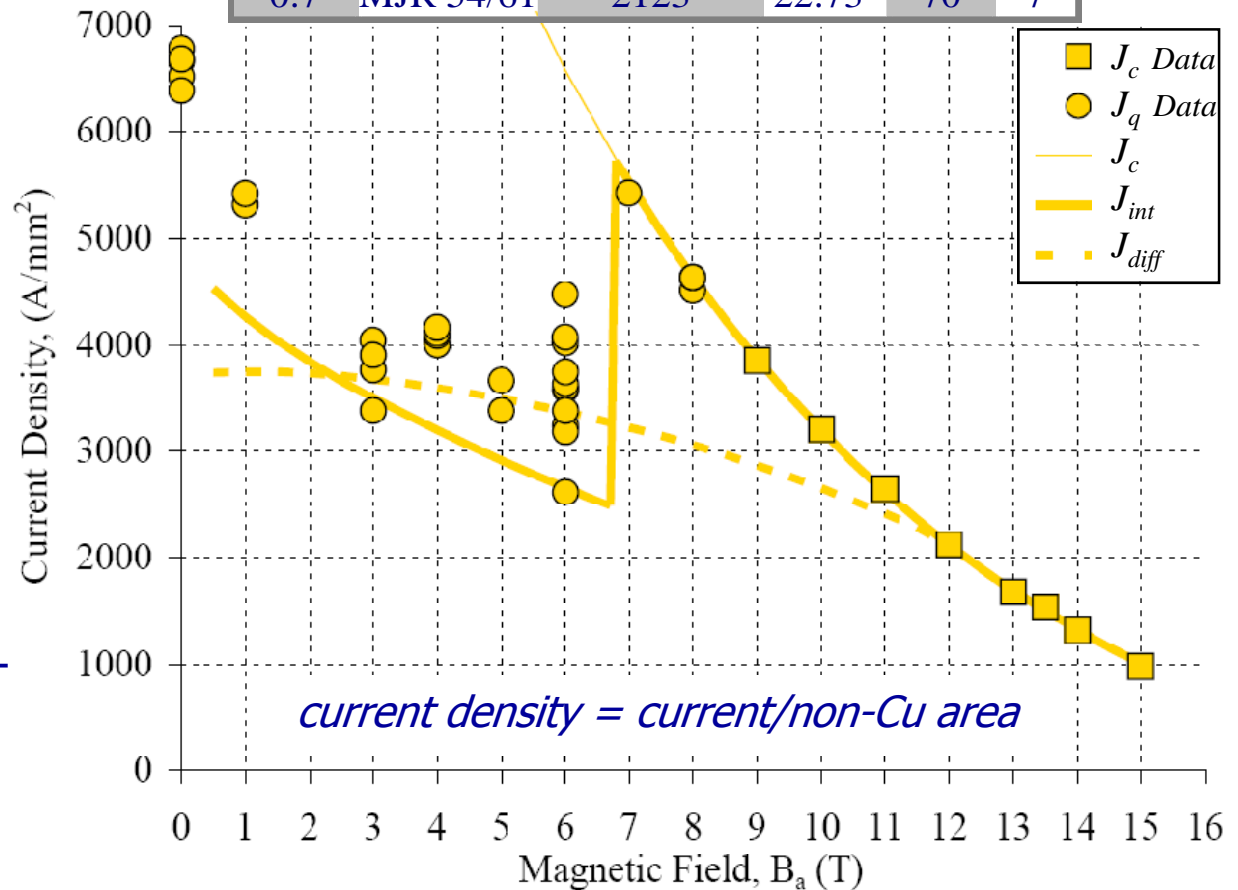
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□  $J_q$  data → V-I tests where premature quenches occurred .

□ 3 stability regions:

1. a high field stable region  $B_a \geq 7$  T
2. an intermediate field region  $2$  T  $< B_a < 7$  T where the min  $J_q$  follow the integral model
3. a low field region  $B_a < 2$  T where min  $J_q$  data increases decreasing  $B_a$ .

Strand diam. [mm]	Strand type	$J_c$ @ 4.2 K-12 T [A/mm <sup>2</sup> ]	$B_{c2}$ @ 4.2 K [T]	$D_{eff}$ [ $\mu$ m]	RRR
0.7	MJR 54/61	2123	22.73*	70	7







# V-I DATA AND SF INSTABILITY



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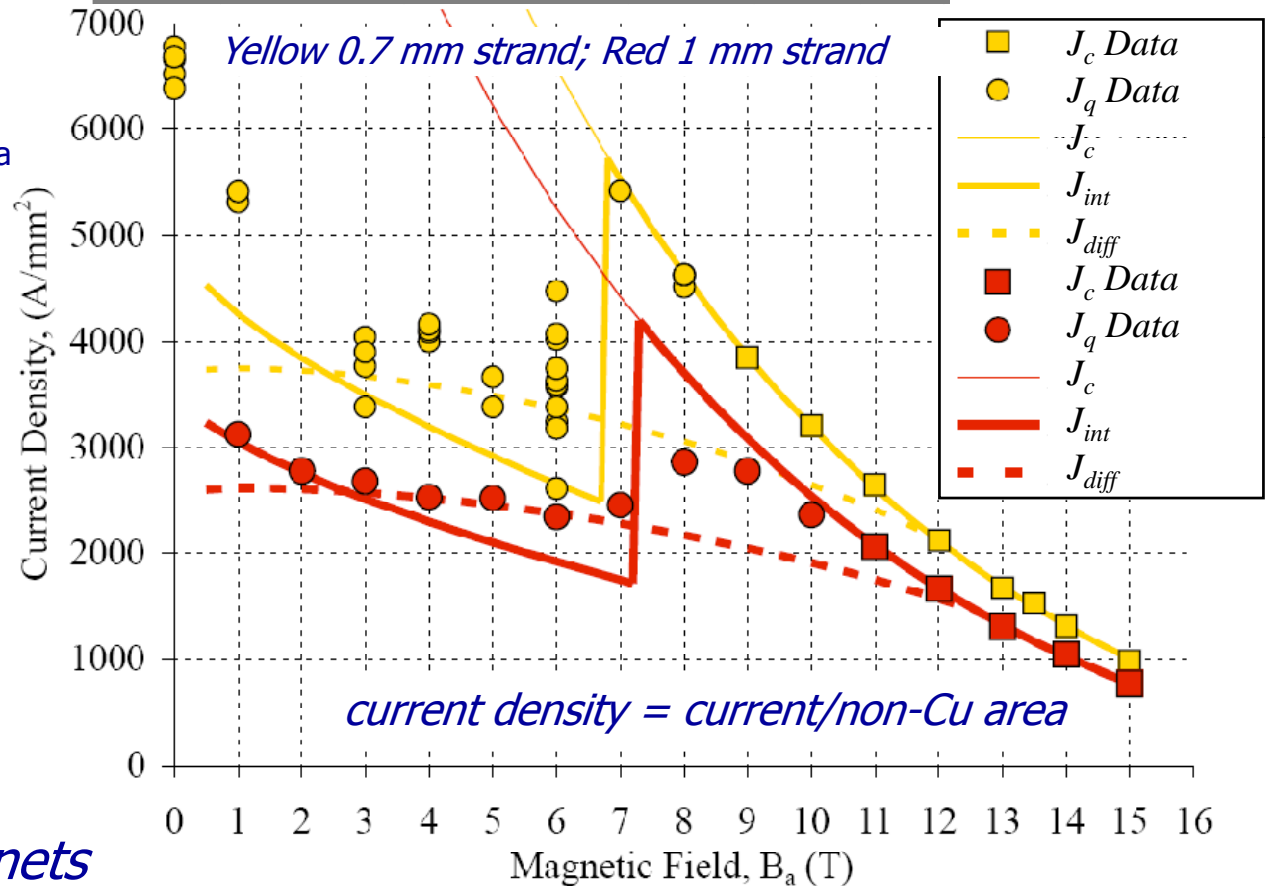
□ Increasing the strand diameter:

1. the premature quench current density at a certain  $B_a$  significantly decreases
2. the intermediate field region extends towards larger  $B_a$ .



*Increasing the strand diameter the self field instability gets more dangerous for  $Nb_3Sn$  magnets*

Strand diam. [mm]	Strand type	$J_c$ @ 4.2 K-12 T [ $A/mm^2$ ]	$B_{c2}$ @ 4.2 K [T]	$D_{eff}$ [ $\mu m$ ]	RRR
0.7	MJR 54/61	2123	22.73	70	7
1	MJR 54/61	1671	22.33	100	7





# V-I DATA: 4.2 K Vs. 1.9 K

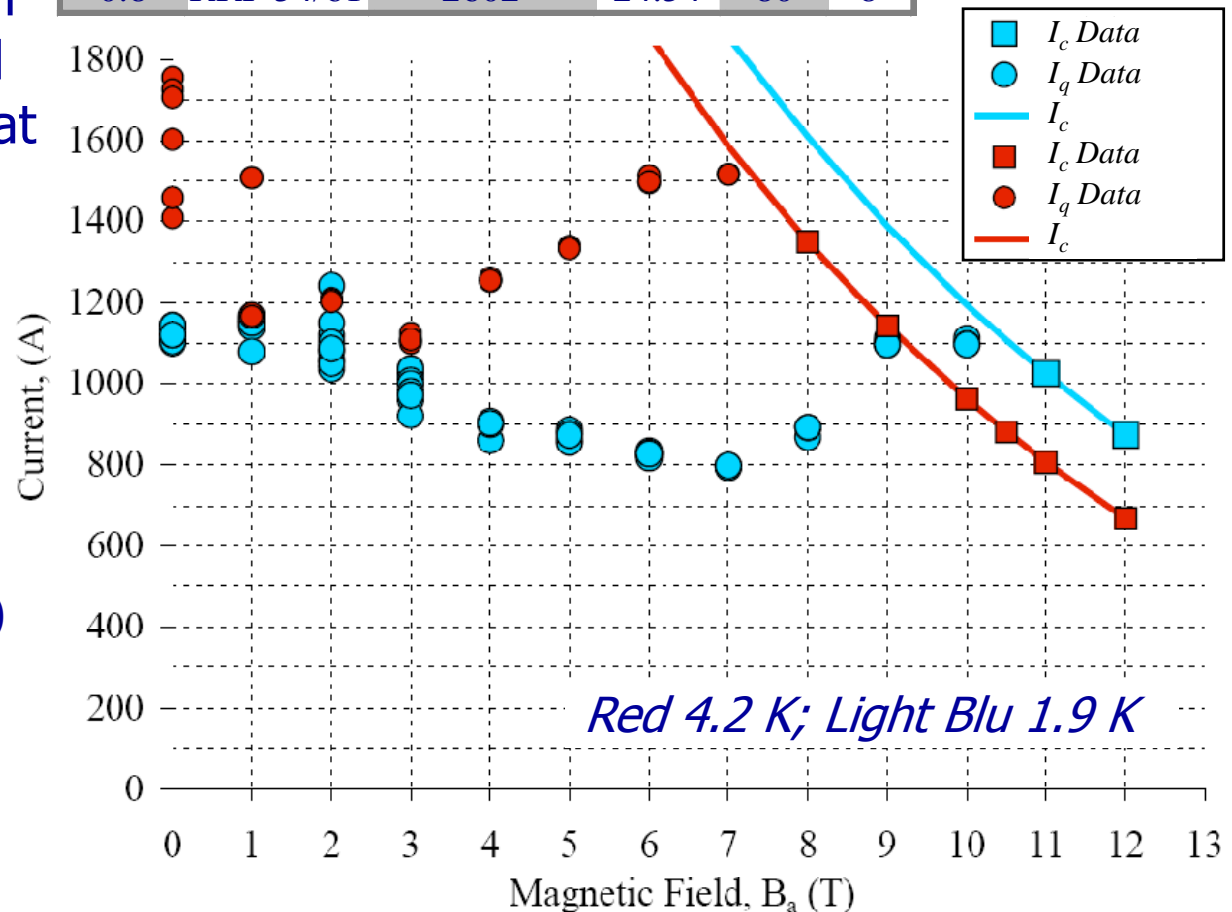


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Comparing V-I tests at 4.2 K and 1.9 K, one can notice that, as predicted by our self field model, at the lower temperature:

Strand diam. [mm]	Strand type	$J_c @ 4.2 K-12 T$ [ $A/mm^2$ ]	$B_{c2} @ 4.2 K$ [T]	$D_{eff}$ [ $\mu m$ ]	RRR
0.8	RRP 54/61	2602	24.54	80	8

- $I_c$  can only be attained at higher field values (11 T instead of 8 T);
- the minimum premature  $I_q$  moves towards higher fields (7 T instead of 3 T)
- the minimum premature  $I_q$  is lower (800 A instead of 1100 A).





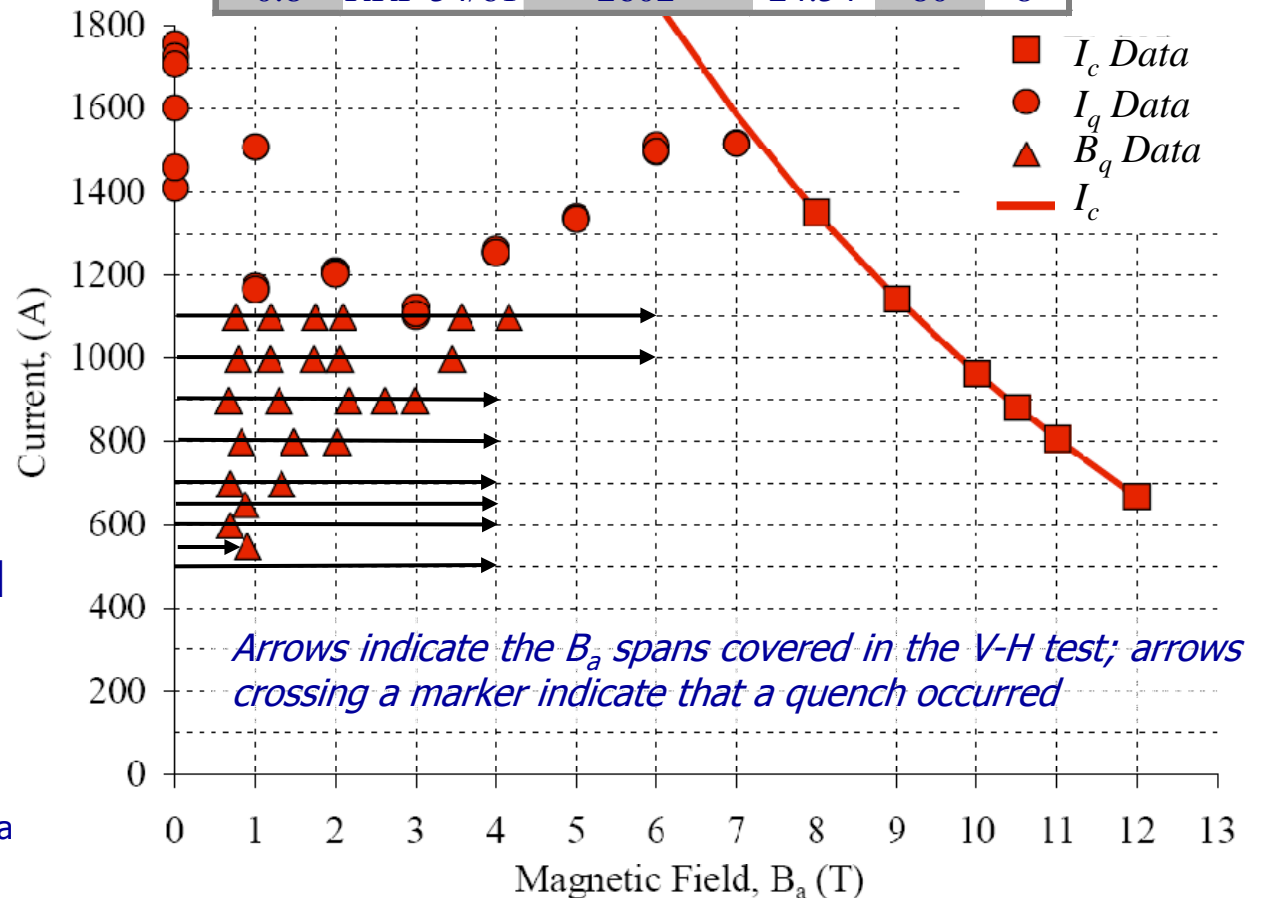
# V-I vs. V-H AT 4.2 K



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- ❑ The strand reached  $I_c$  for  $B_a \geq 8$  T.
- ❑ The minimum premature quench current values were:
  1.  $\sim 1100$  A at 3 T in  $J_q$  test (V-I)
  2. 550 A at  $\sim 0.9$  T in  $B_q$  test (V-H).
- ❑ During V-H test when a quench occurred the power supply was tripped and the  $B_a$  ramp was stopped, then the same current value was restored and finally the  $B_a$  was ramped up again.

Strand diam. [mm]	Strand type	$J_c$ @ 4.2 K-12 T [ $A/mm^2$ ]	$B_{c2}$ @ 4.2 K [T]	$D_{eff}$ [ $\mu m$ ]	RRR
0.8	RRP 54/61	2602	24.54	80	8





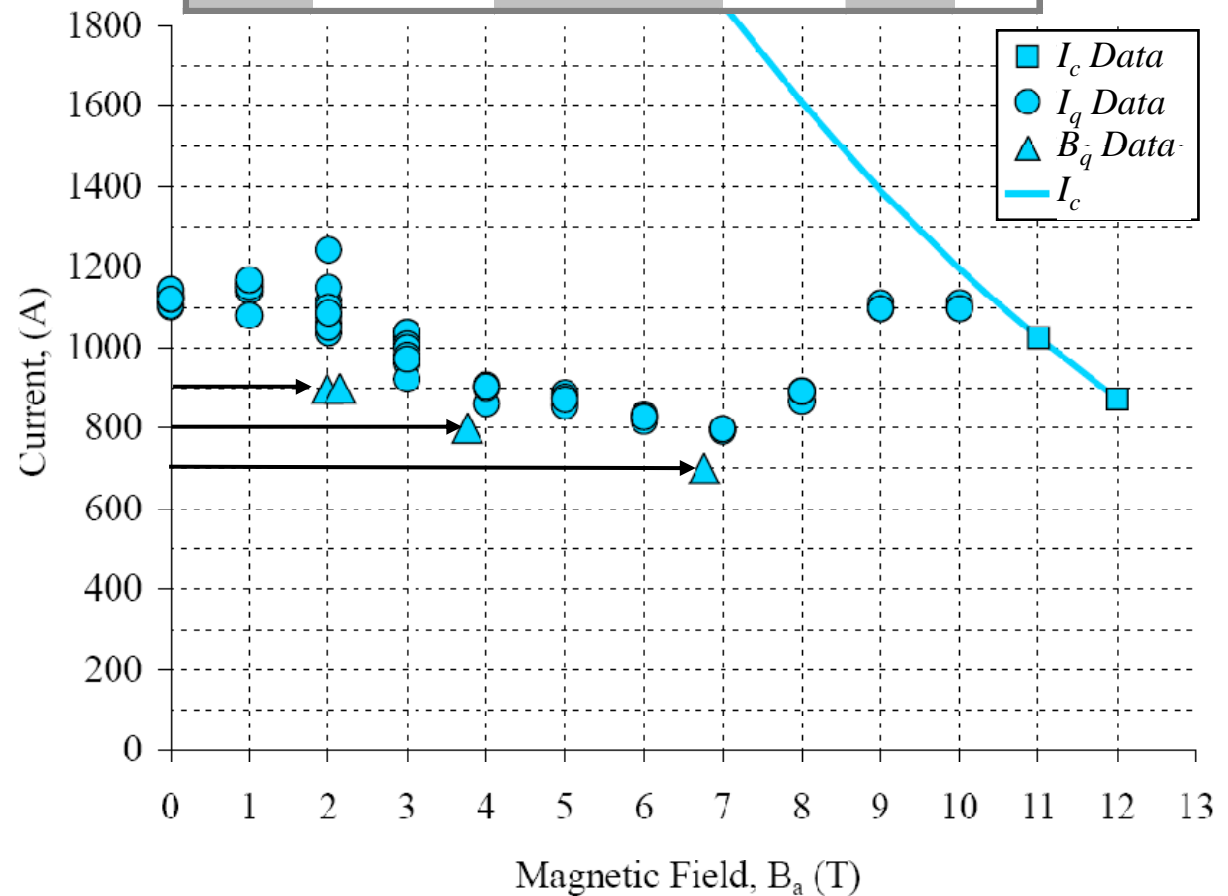
# V-I vs. V-H AT 1.9 K



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- In the V-H tests ( $B_q$ ) at 1.9 K an unexpected behavior was observed: the quench current was not significantly lower than during V-I ( $I_q$ ) tests.
- From this measurements one might conclude that the Self field instability is the predominant instability mechanism at 1.9 K.

Strand diam. [mm]	Strand type	$J_c$ @ 4.2 K-12 T [ $A/mm^2$ ]	$B_{c2}$ @ 4.2 K [T]	$D_{eff}$ [ $\mu m$ ]	RRR
0.8	RRP 54/61	2602	24.54	80	8





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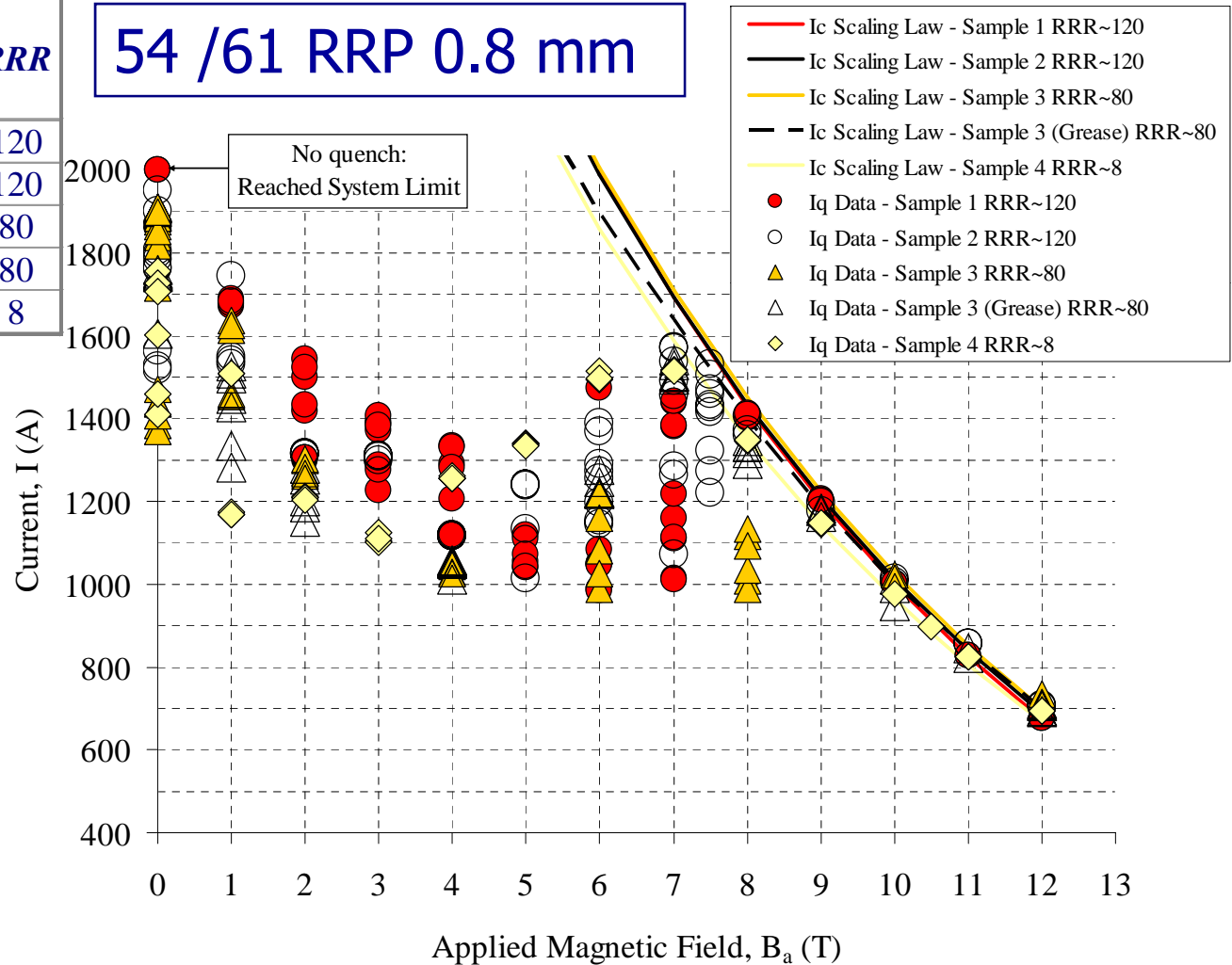
# STRAND TEST RESULTS @ 4.2 K: RRR ranging from 8 to 120



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Sample Number	$J_c @ 4.2 K$ [A/mm <sup>2</sup> ]	$B_{c2} @ 4.2 K$ [T]	$D_{eff}$ [μm]	RRR
1	2580	23.06	80	120
2	2645	23.56	80	120
3	2672	23.94	80	80
3 (Grease)	2683	24.72	80	80
4	2602	24.54	80	8

54 /61 RRP 0.8 mm



□ The current values of premature quenches due to the self field instability are not much dependent on the RRR value





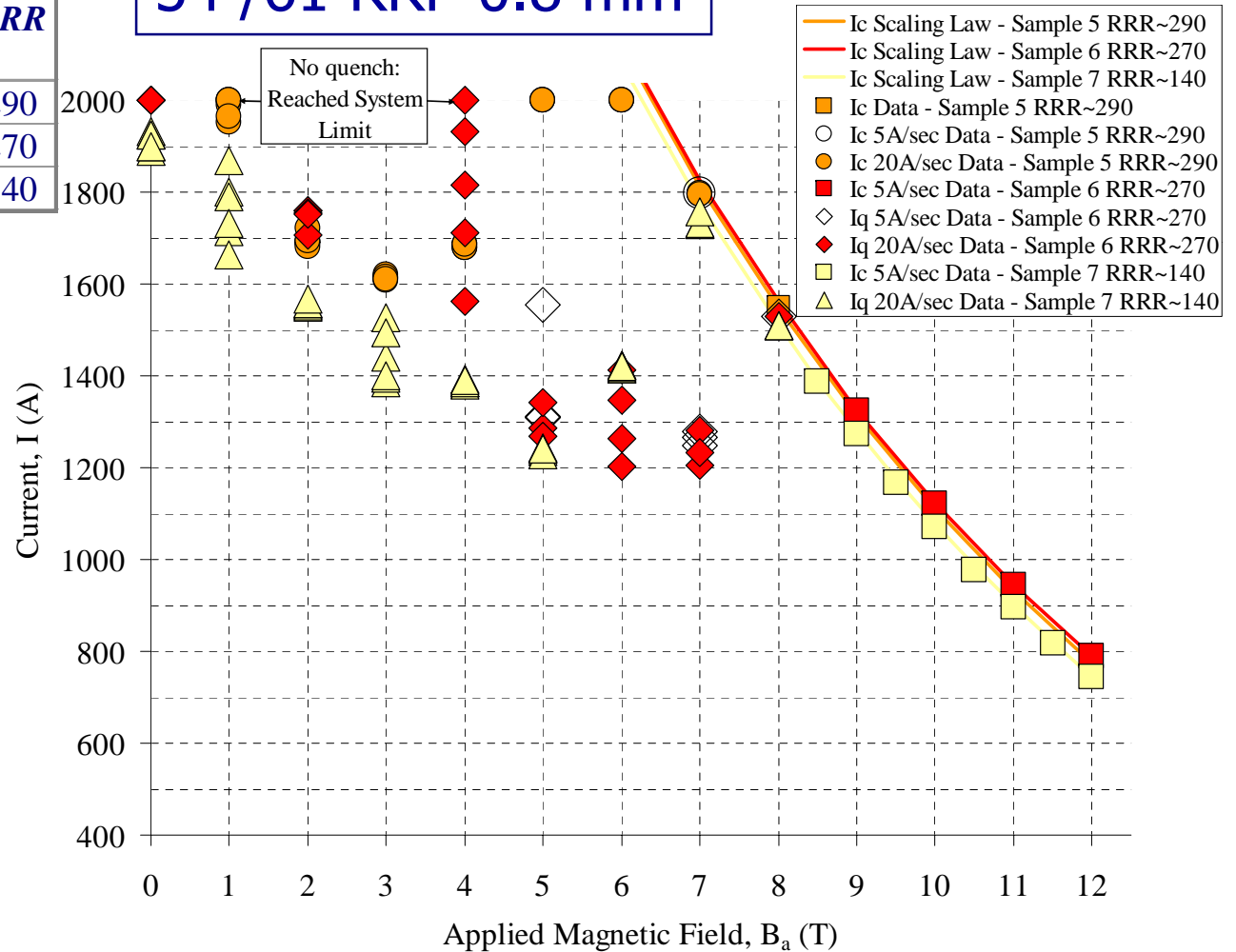
# STRAND TEST RESULTS @ 4.2 K: RRR ranging from 140 to 290



WAMSDO 2008

Sample Number	$J_c$ @ 4.2 K-12 T [A/mm <sup>2</sup> ]	$B_{c2}$ @ 4.2 K [T]	$D_{eff}$ [ $\mu$ m]	RRR
5	2978	24.5	80	290
6	3028	24.92	80	270
7	2852	24.13	80	140

54 /61 RRP 0.8 mm



□ The current values of premature quenches due to the self field instability are not much dependent on the RRR value





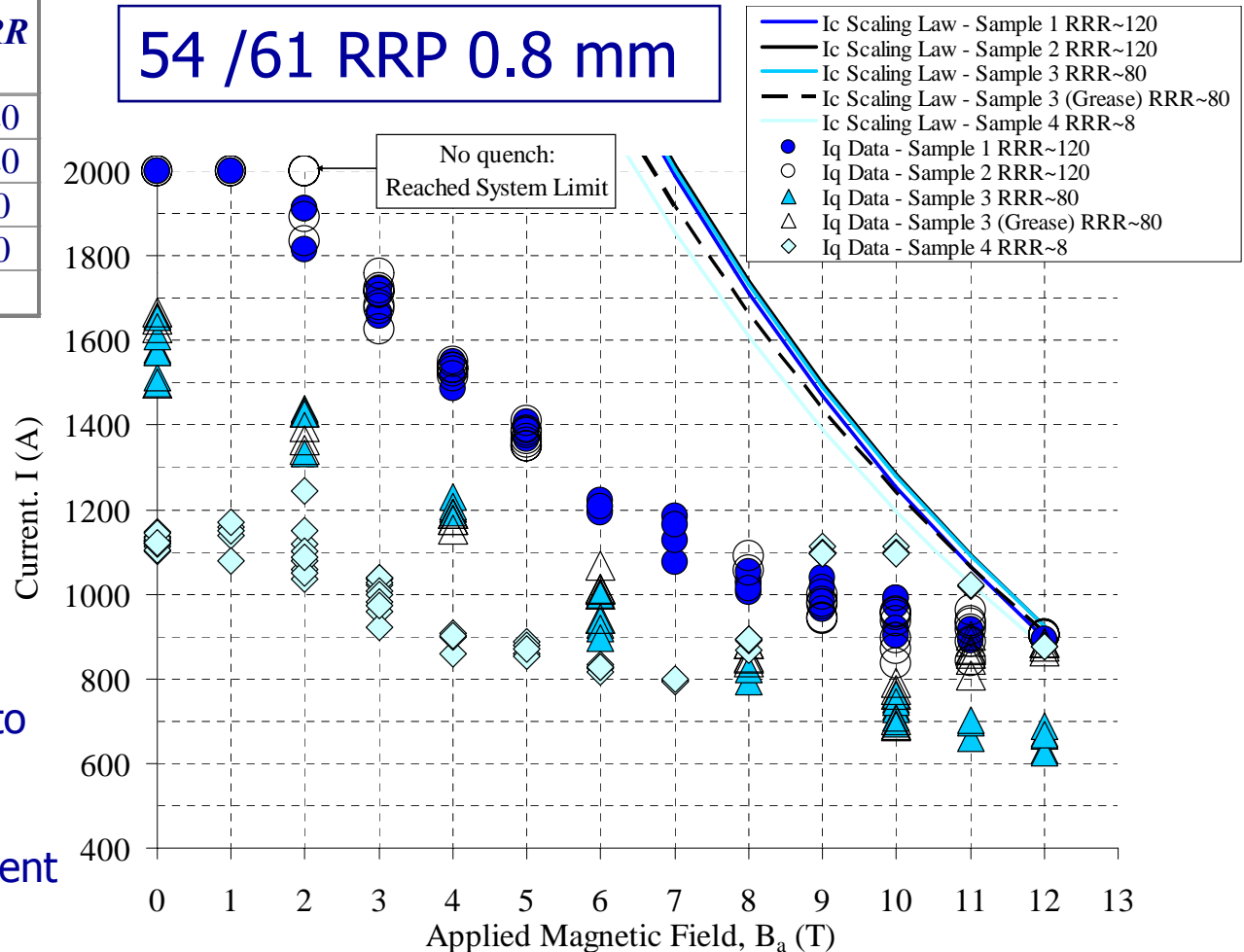
# STRAND TEST RESULTS @ 1.9 K: RRR ranging from 8 to 120



WAMSDO 2008

Sample Number	$J_c$ @ 4.2 K-12 T [A/mm <sup>2</sup> ]	$B_{c2}$ @ 4.2 K [T]	$D_{eff}$ [μm]	RRR
1	2580	23.06	80	120
2	2645	23.56	80	120
3	2672	23.94	80	80
3 (Grease)	2683	24.72	80	80
4	2602	24.54	80	8

- The current values of premature quenches due to the self field instability are dependent on the RRR value in the low field region (at 1.9 K ~ 0-7 T)
- At higher fields it is difficult to experimentally estimate the effect of RRR because the instability is strongly dependent on the initial perturbation





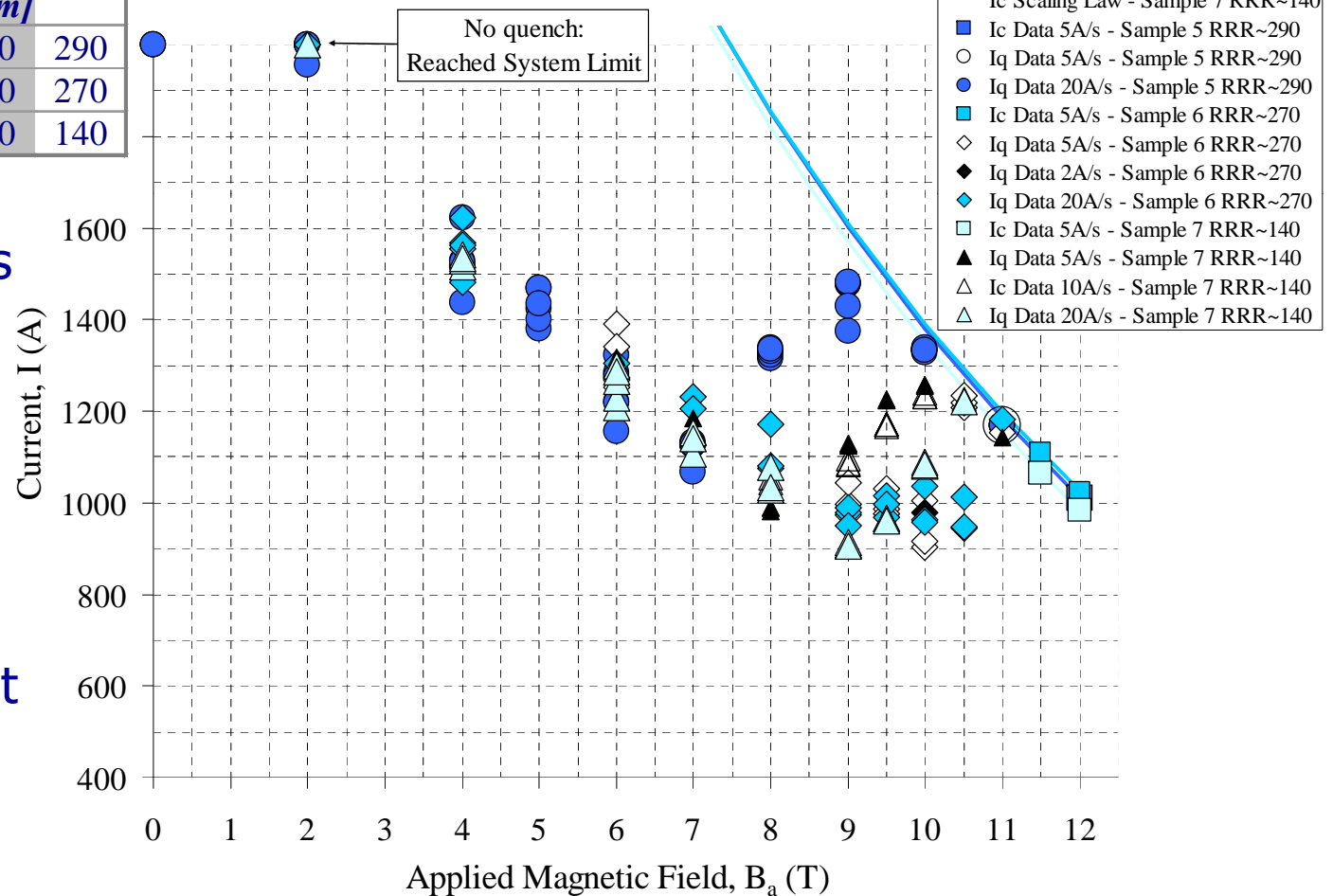
# STRAND TEST RESULTS @ 1.9 K: RRR ranging from 140 to 290



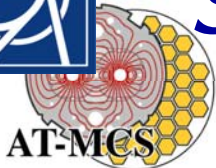
WAMSDO 2008

Sample Number	$J_c @ 4.2 \text{ K-12 T}$ [A/mm <sup>2</sup> ]	$B_{c2} @ 4.2 \text{ K}$ [T]	$D_{eff}$ [ $\mu\text{m}$ ]	RRR
5	2978	24.5	80	290
6	3028	24.92	80	270
7	2852	24.13	80	140

54 /61 RRP 0.8 mm



□ The current values of premature quenches due to the self field instability are not dependent on the RRR value in the low field region (at 1.9 K ~ 0-7 T)



# STRAND TEST RESULTS @ 1.9 K: PIT Vs. RRP

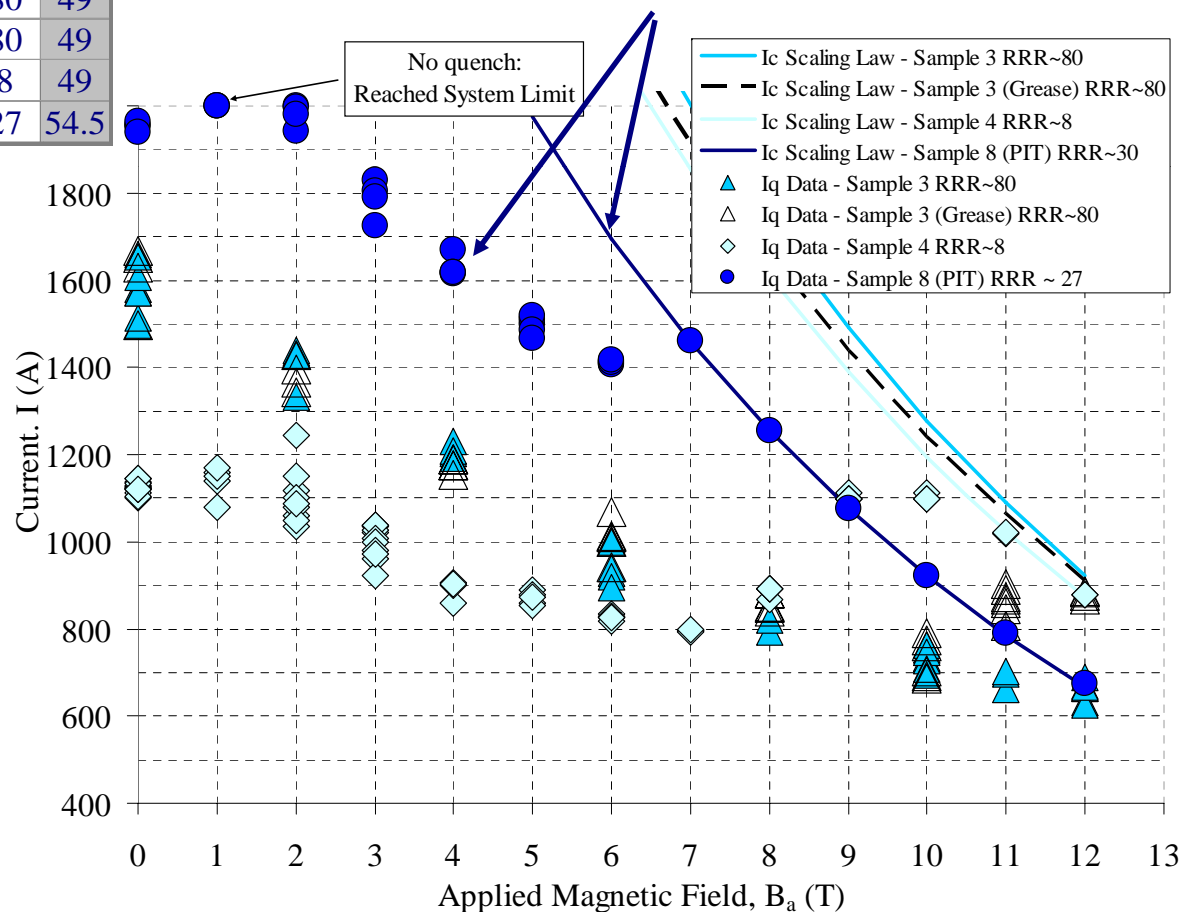


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Sample Number	Strand type	Strand Diam. [mm]	$J_c$ @ 4.2 K-12 T [ $A/mm^2$ ]	$B_{c2}$ @ 4.2 K [T]	$D_{eff}$ [ $\mu m$ ]	RRR	Cu %
3	RRP	0.8	2672	23.94	80	80	49
3 (Grease)	RRP	0.8	2683	24.72	80	80	49
4	RRP	0.8	2602	24.54	80	8	49
8	PIT	0.8	2224	24.27	30	27	54.5

0.8 mm PIT wire

- An high RRR is not sufficient to solve the problem of self field instability in record- $J_c$  RRP OST strands at 1.9 K
- A possible solution might be to increase the overall Cu content and the Cu in between the superconducting sub-elements; PIT strands adopted these solutions and preliminary results show that they are much more self-field stable



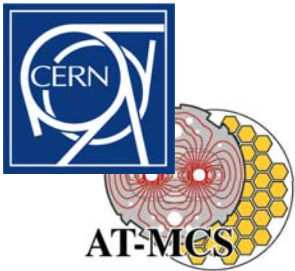


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# THE EFFECTS OF COVERING THE WIRE WITH 'THICK' LAYER OF STYCAST



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- ❑ At first the strand was tested in direct contact with helium
- ❑ Then the same strand was covered by  $\sim 1$  mm of stycast and retested
- ❑ The thermal diffusivity ( $D_{th}$ ) of epoxy at 4.2 K and 1.9 K is respectively  $\sim 2.3 \cdot 10^{-5} \text{ m}^2\text{s}$  and  $\sim 2.03 \cdot 10^{-4} \text{ m}^2\text{s}$  (Cryocomp)
- ❑ The thermal penetration thickness  $\delta_{th}$  is:  $\delta_{th} = 4\sqrt{D_{th} \cdot t}$
- ❑ The time scale for a local flux jump is generally  $< 10^{-4} \text{ s}$

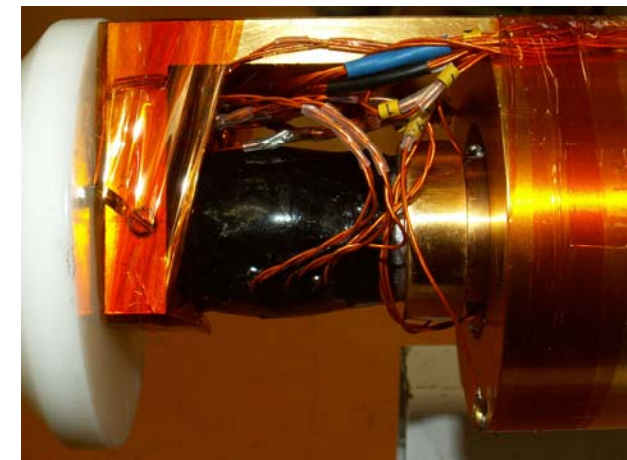


Sample holder diameter  $\sim 32$  mm

$$\delta_{th}(4.2 \text{ K}) < 0.19 \text{ mm}$$

$$\delta_{th}(1.9 \text{ K}) < 0.57 \text{ mm}$$

*Increasing the thickness of the stycast layer over 1 mm should not change the premature quench current values*





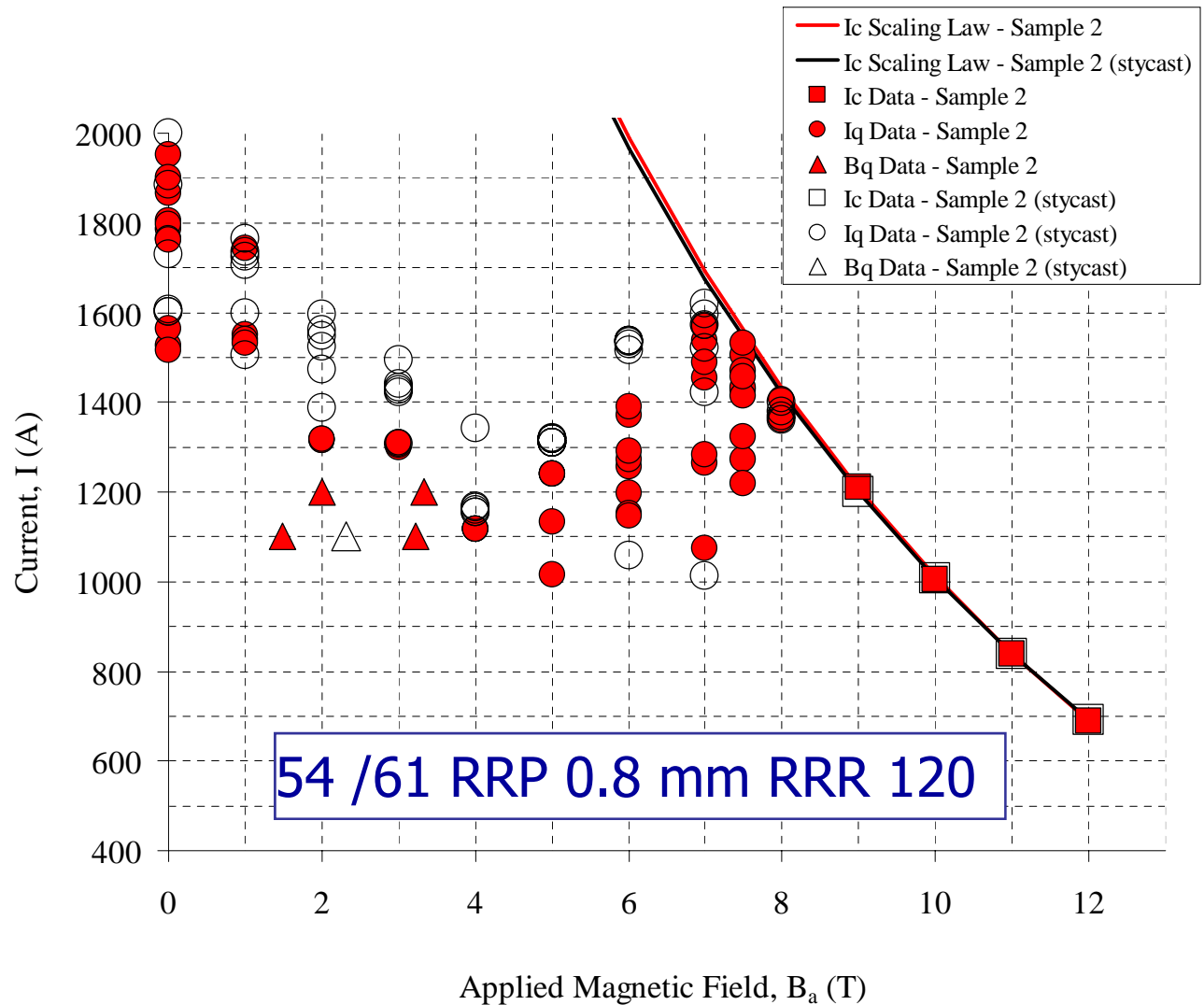


# THE EFFECTS @ 4.2 K OF COVERING THE WIRE WITH 'THICK' LAYER OF STYCAST



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- The thick layer of stycast did not change the critical current values and did not significantly change the premature quench current values



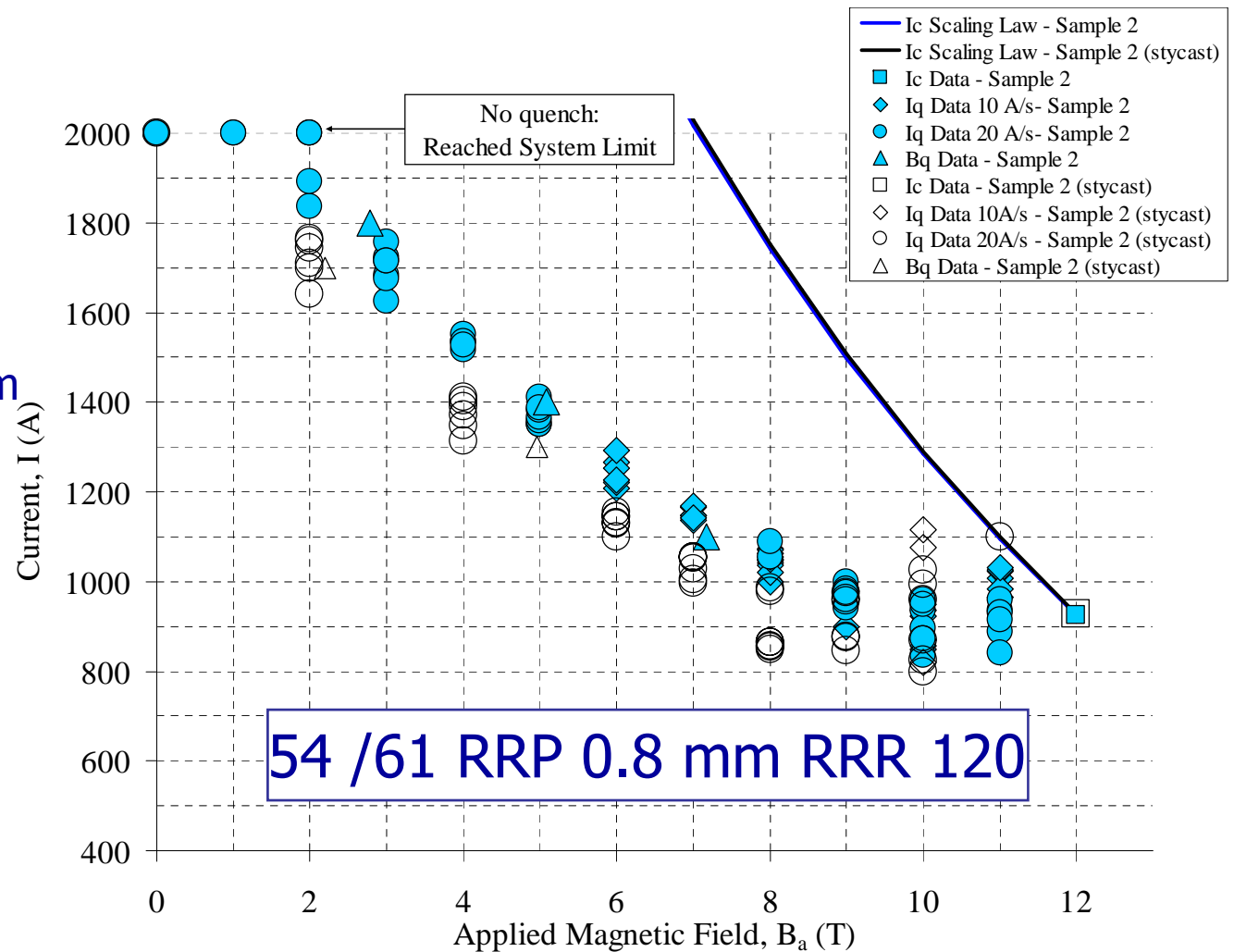


# THE EFFECTS @ 1.9 K OF COVERING THE WIRE WITH 'THICK' LAYER OF STYCAST



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- ❑ The thick layer of stycast did not change the critical current
- ❑ In the low field region ( $\sim 0-7$  T at 1.9K) it decreased the minimum quench current of  $\sim 10\%$
- ❑ Also for strand with high RRR, the Self field instability is predominant instability mechanism at 1.9 K.







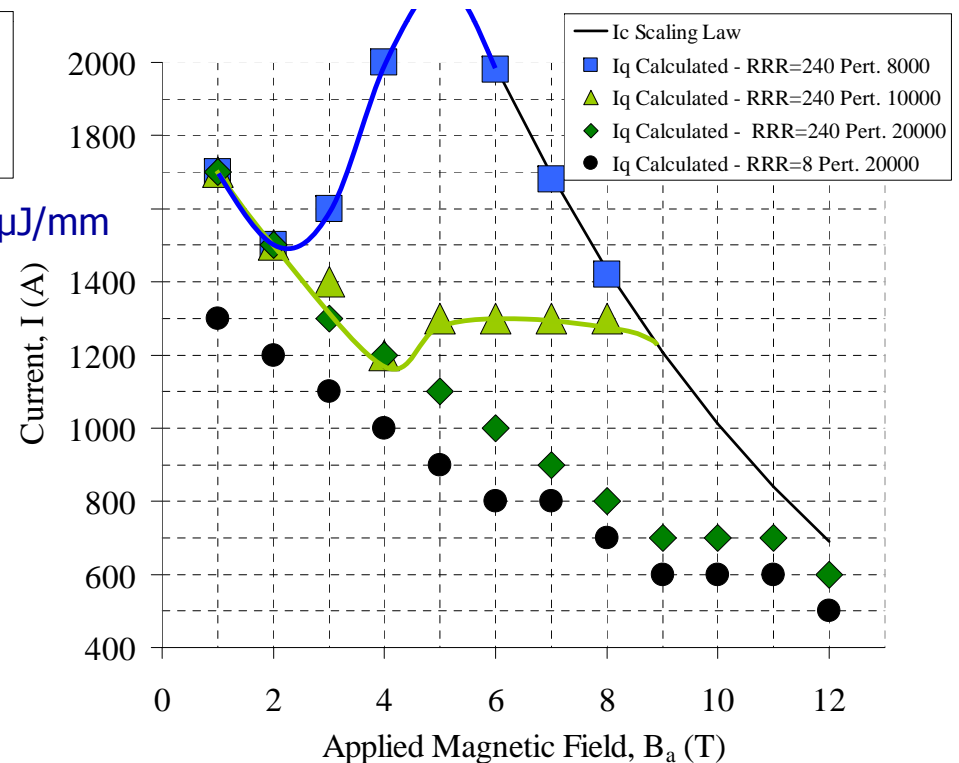
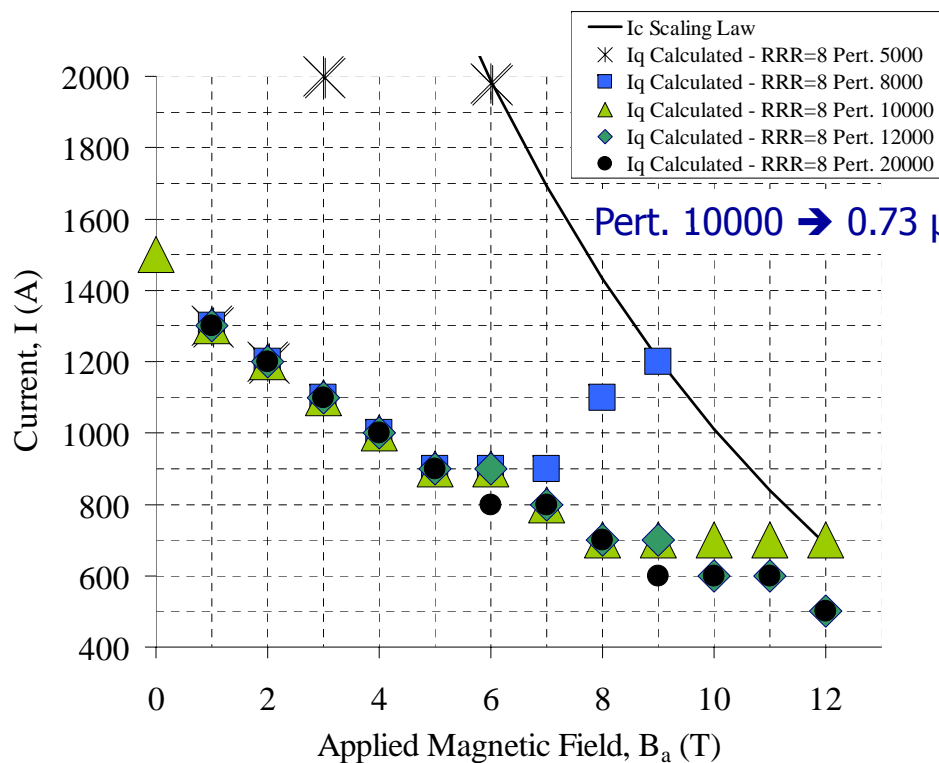
# DEPENDANCE ON THE ENERGY OF THE INITIAL PERTURBATION



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- The simulation of the self field instability by a Finite Element Model shows that the instability in the intermediate field region is sensitive to the amount of energy provided by the perturbation that initiates the flux-jump

Simulation of the quench current behavior at 4.2 K of a 0.8 mm 54 /61 RRP strand ( $J_c=2650 \text{ A/mm}^2@12 \text{ T}$ )





# EFFECTS OF LOCAL STRAND'S DAMAGES



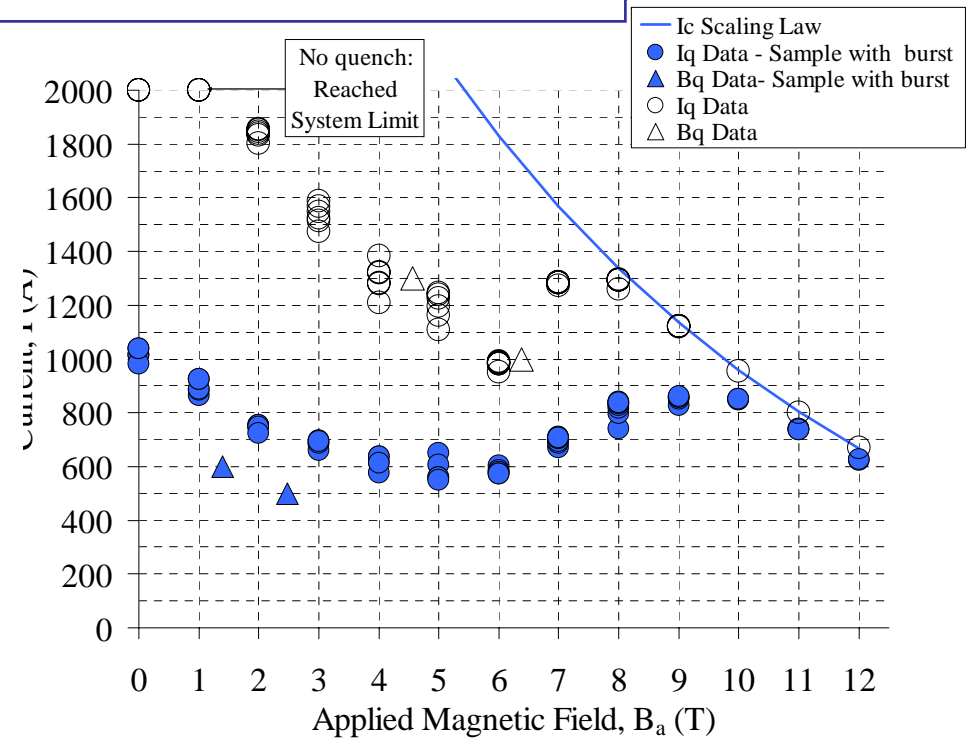
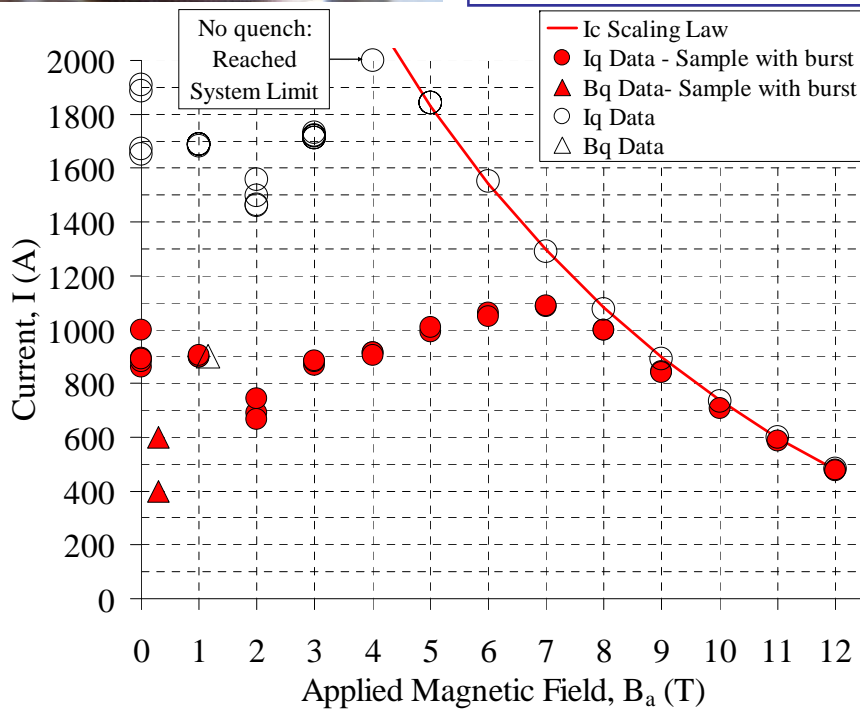
WAMSDO 2008

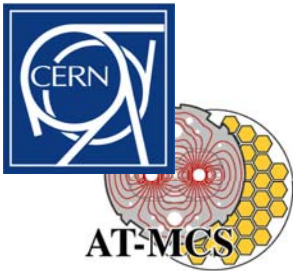


Sample holder diameter ~ 32 mm

□ A small local damage of the copper stabilizer can completely jeopardize the dynamic stabilization of a high  $J_c$  Nb<sub>3</sub>Sn strand

LARP 54 /61 RRP 0.7 mm RRR > 250





## CONCLUSIONS



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- ❑ The self field instability is the predominant instability mechanism at 1.9 K.
- ❑ At 1.9 K, in the low field region ( $\sim 0-7$  T):
  - 1) the stability is improved by increasing the RRR in the range 8-120 while it was not observed a significant improvement in the range 140-290
  - 2) covering the strand sample with a 'thick' layer of stycast reduced the values of the premature quench current of  $\sim 10$  %
- ❑ At 1.9 K, in the intermediate field region ( $\sim 7-11$  T) the quench current seems to be strongly dependent on the energy value of the perturbation that initiates the flux jump; in strand tests many times the minimum quench current was recorded in this field region and its value was lower than the critical current at 12 T
- ❑ An increase of the overall Cu content and the Cu in between the superconducting sub-elements might improve the self-field stability of record- $J_c$  RRP strands; PIT strands adopted these solutions (they also have a lower  $J_c$ ) and preliminary results show that they are much more self-field stable



## *ACKNOWLEDGMENTS*



*WAMSDO 2008*

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