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# Development of High Current Nb<sub>3</sub>Sn Rutherford Cables for NED and LARP

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WAMSDO, May 2008



# Outline

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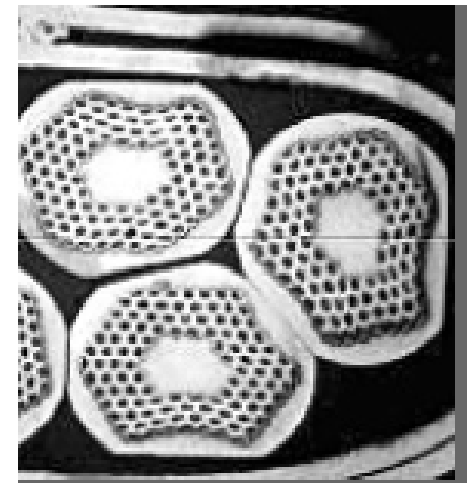
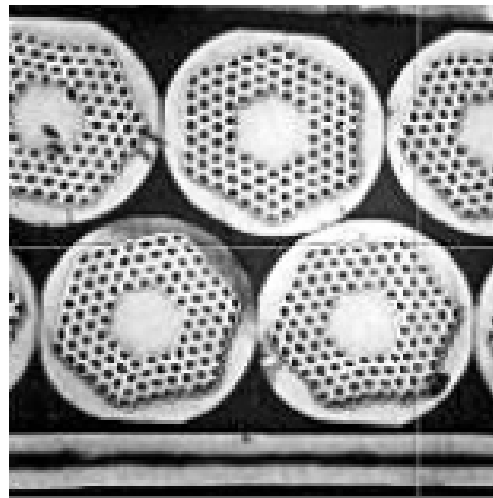
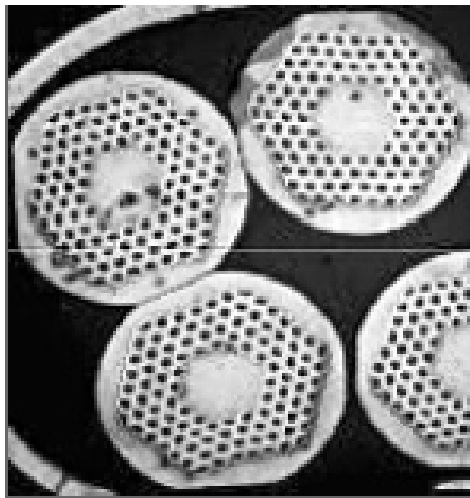
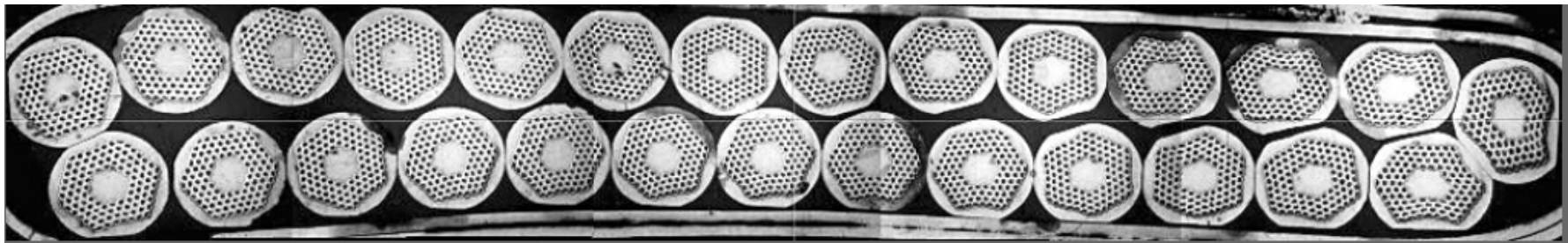
- Rutherford cables
- Cabling objective:
  - Damage free strand
  - Mechanically stable for winding a magnet
- Review cabling history for LBNL
  - Dipole D-20 (13.5/14.5T)
  - Recent rectangular cable fabrication for LBNL magnets
    - RD-3 series (14.7 T)
    - HD-1 series (16 T)
- Cables for LARP Technology Quadrupoles (TQ)
- Proto-type cables for Next European Dipole (NED)

# 60 Strand Machine for Fabricating Rutherford Cables



# Typical Rutherford Cable

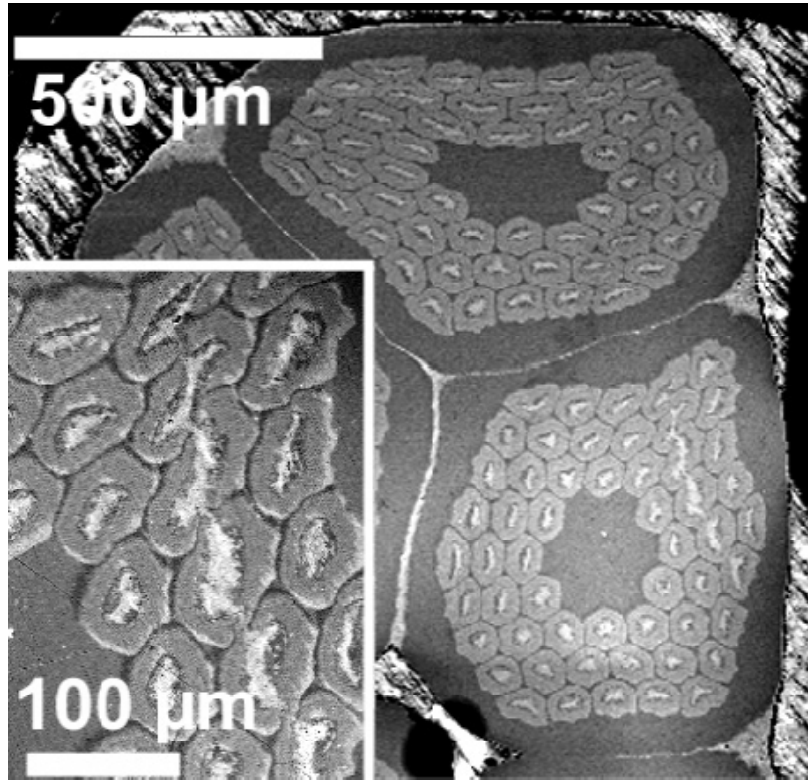
Cable 961



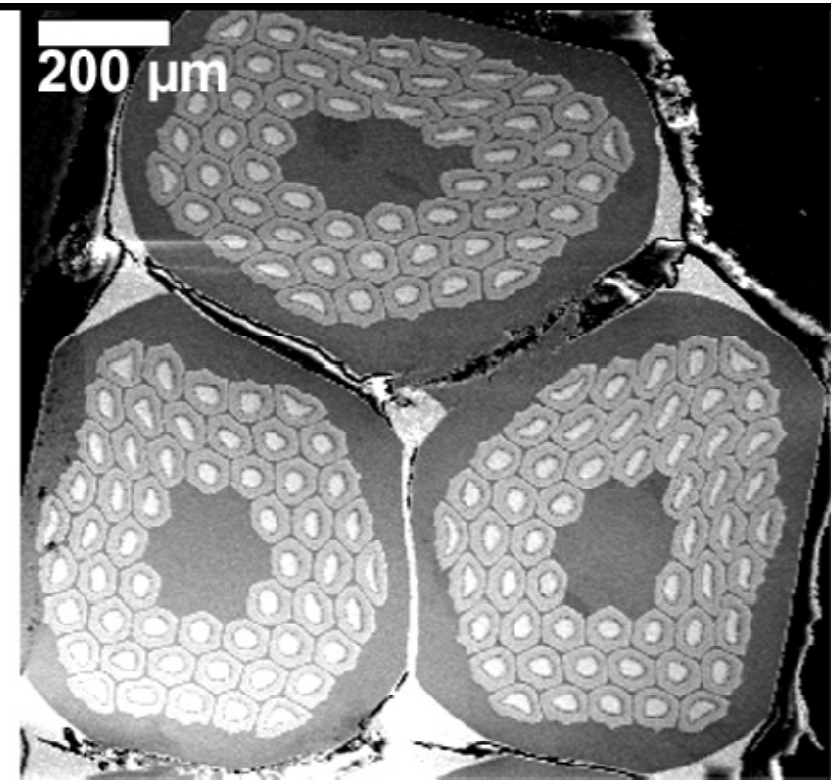
Edge deformations are important

# Good and bad cable edge deformation

- Bad



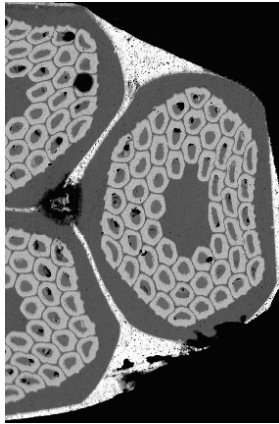
- Good



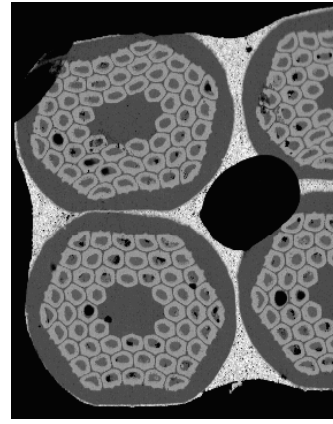
Main difference is different width of the cable

# Managing edge deformation

Decoupling of Thickness & Width  
as opposed to Packing Factor



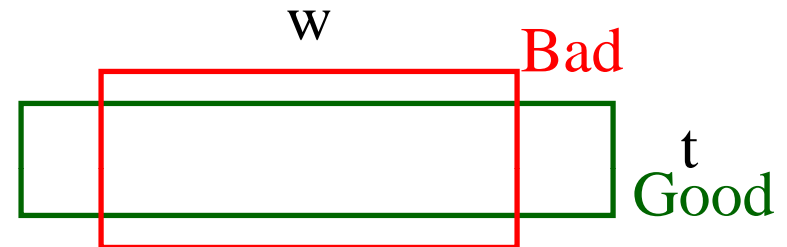
Design for this  
strand configuration  
at edge of cable



NOT this strand  
Configuration

0.8 mm strand diameter  
40 Strand cable  
Cable Area = 24.40 mm<sup>2</sup>  
87% Packing Factor

Problem with Packing Factor  
Two Cables have equal area but are  
NOT the same



2 Cables: Same compaction or  
Packing Factor

$$17.4 \text{ mm} \times 1.400 \text{ mm} = 24.4 \text{ mm}^2$$

$$17.0 \text{ mm} \times 1.435 \text{ mm} = 24.4 \text{ mm}^2$$

0.4 is mm half a strand diameter  
This difference can be fatal



# Deformation Parameters $t$ and $w$

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- Thickness deformation  $t$  ( $\sim$ strain)

$$t = (\text{cable thickness} / 2 \times \text{strand diameter}) - 1$$

- Width deformation  $w$  ( $\sim$ strain)

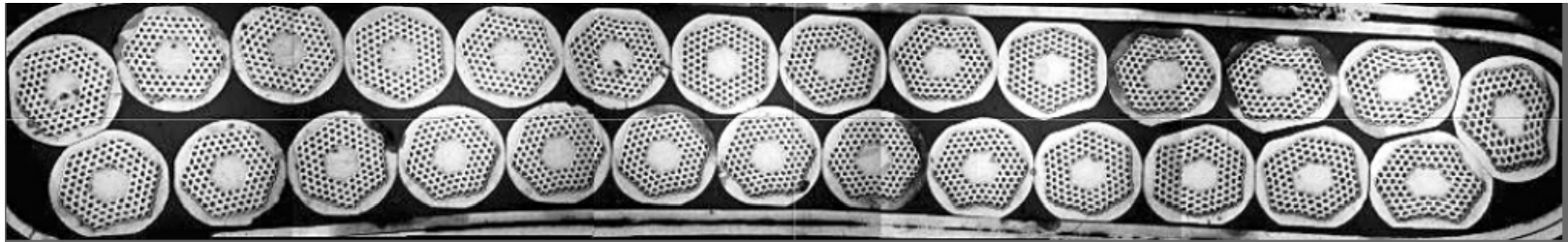
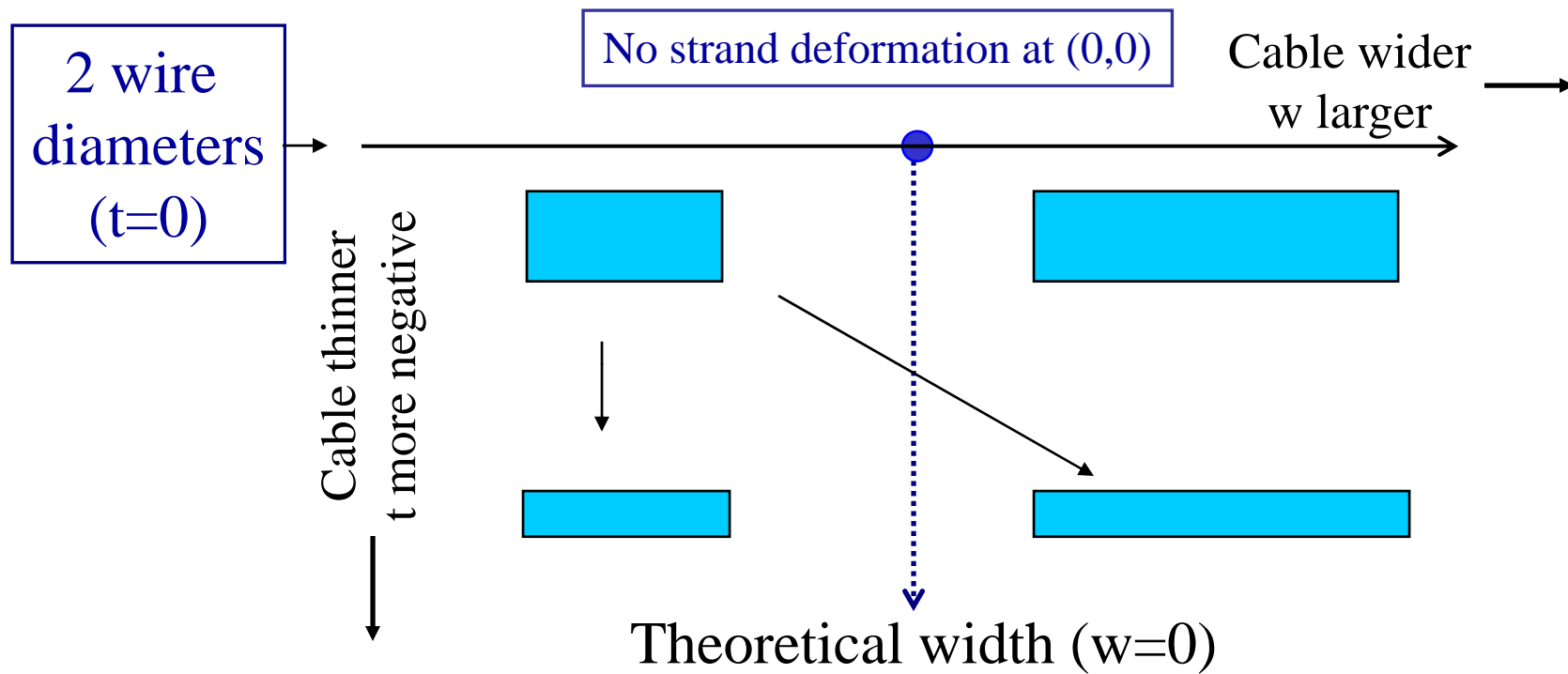
$$w = (\text{cable width} - \text{theoretical width}) / (\text{th. width})$$

$$\text{Theoretical width} = \frac{Nd}{2 \cos(PA)} + 0.72d$$

PA = Cable pitch angle

(factor 0.72  $d$  not included in plots in this presentation)

# Rutherford Cable Parameter Space

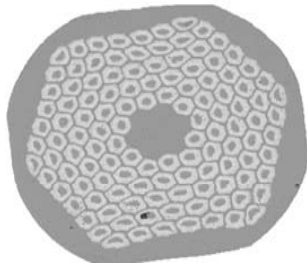




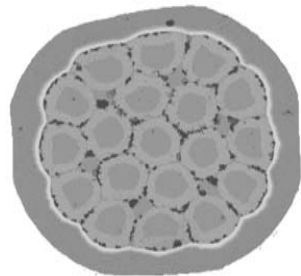
# Parameter space cables for D-20, RD-3, and HD-1

D-20 is Cosine Theta Dipole (14.7T), RD-3 is Racetrack Dipole, and HD-1 is High Field Dipole (16T)

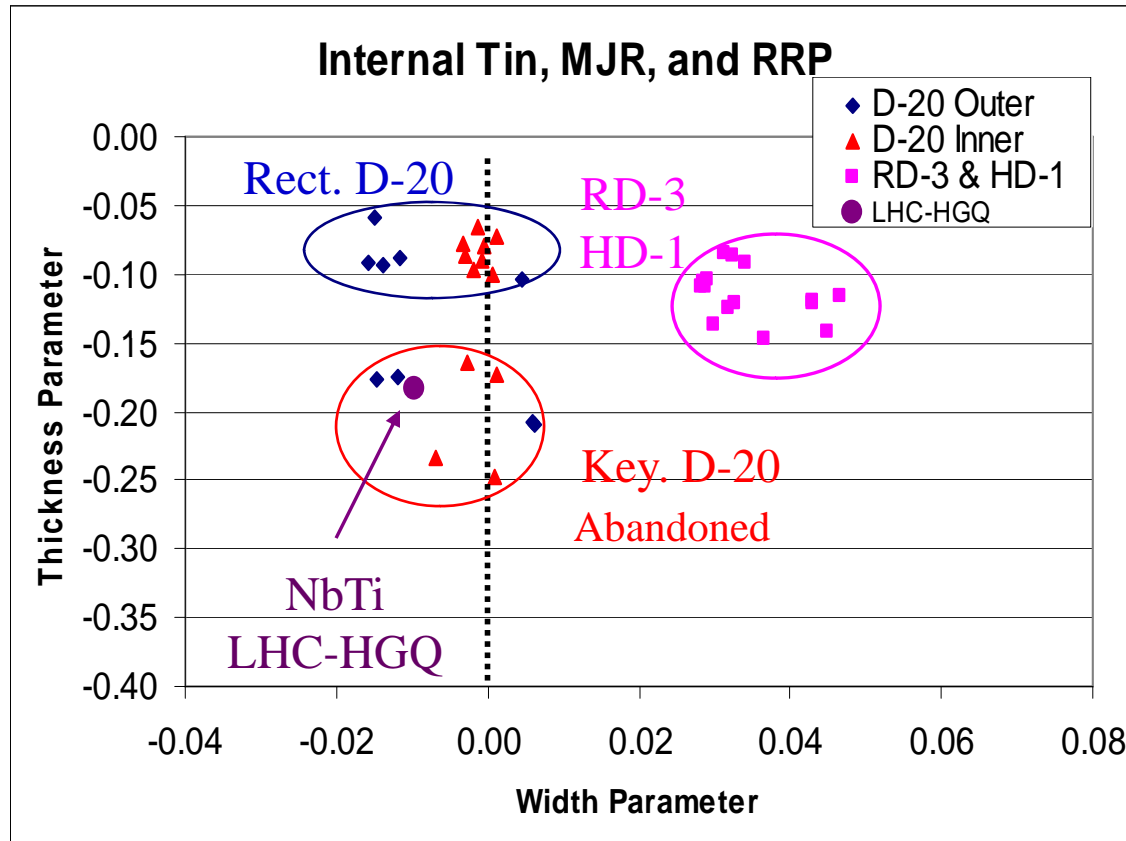
D-20



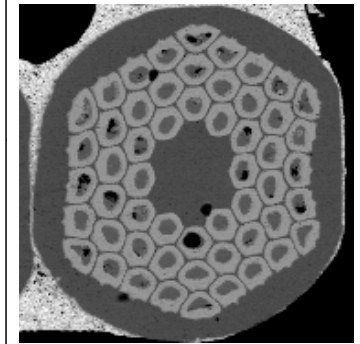
LBL Cable # 523  
MJR-TWCA



LBL Cable # 522  
IGC-Int. Tin



RD-3



LBL Cable # 805R  
Oxford-ORe

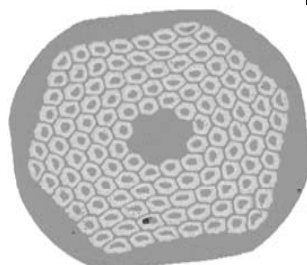
Keystoned D20 cables had ~20% loss in  $I_c$  and were more sensitive to transverse stress



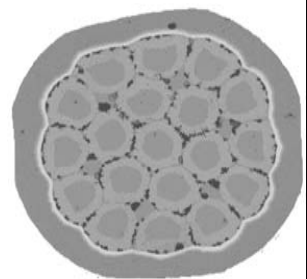
# Zones of interest from cables for D-20, RD-3, and HD-1

D-20 is Cosine Theta Dipole (14.7T), RD-3 is Racetrack Dipole, and HD-1 is High Field Dipole (16T)

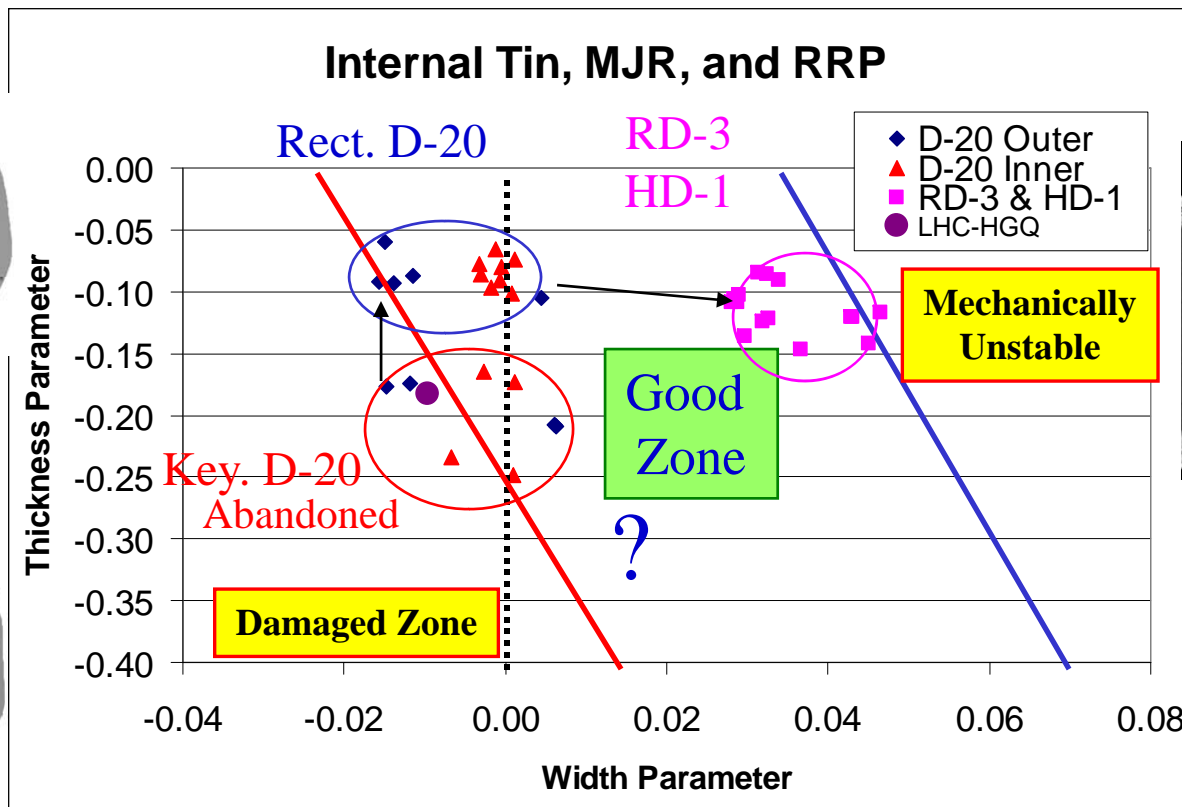
## D-20



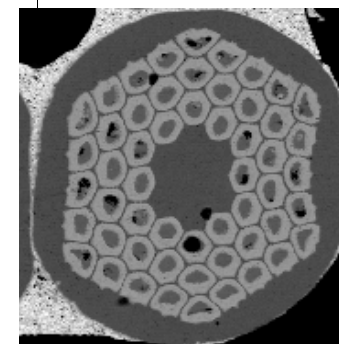
LBL Cable # 523  
MJR-TWCA



LBL Cable # 522  
IGC-Int. Tin



## RD-3



LBL Cable # 805R  
Oxford-ORe



# Technology Quad (TQ) – Cable Specifications & Production

- Spec

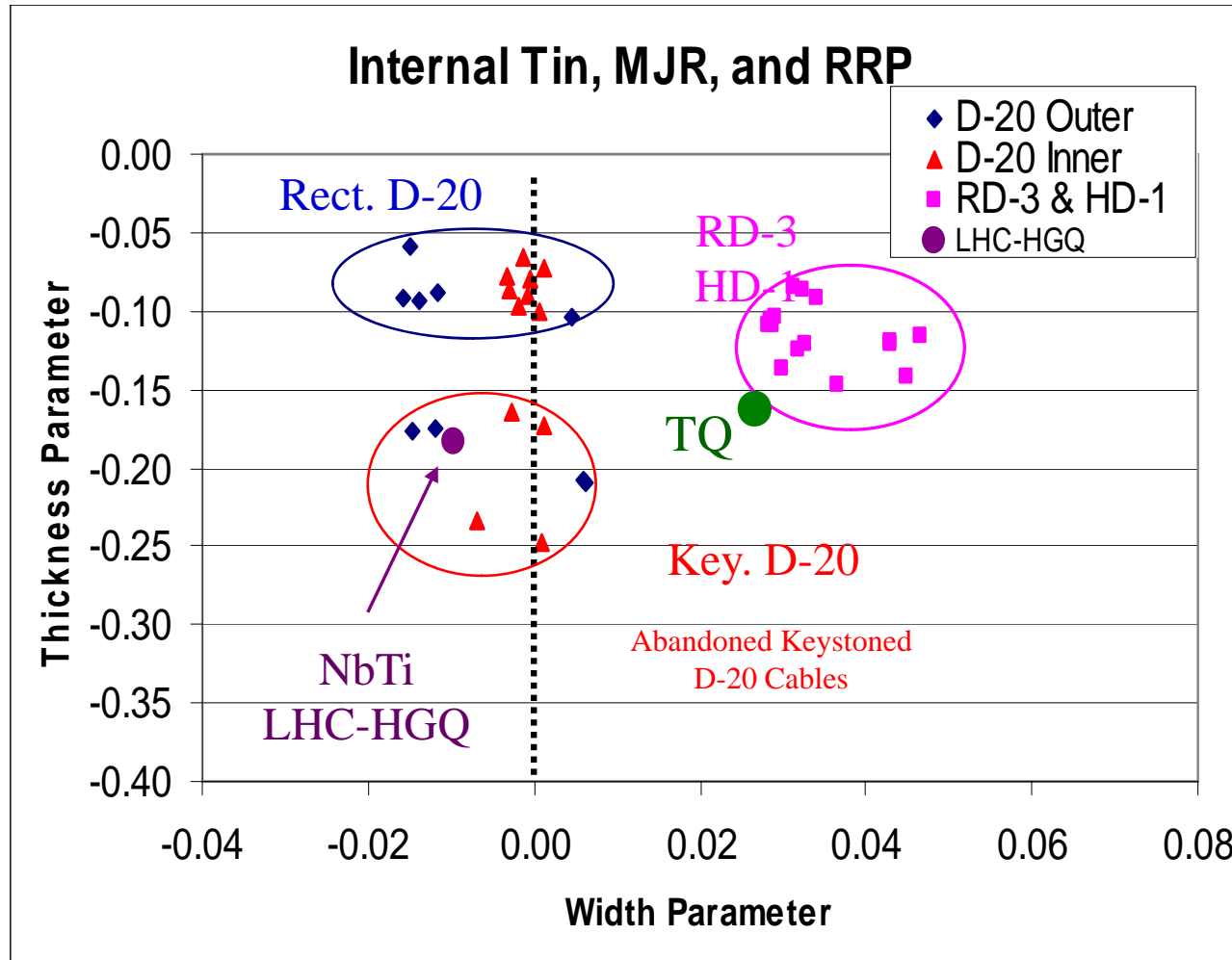
Parameters	Units	TQ Cable	Tolerance
Strands in cable	No.	27	NA
Strand diameter	mm	0.7	+/- 0.002
Width	mm	<u>10.077 max.</u>	+0.000, -0.100
Thickness	mm	1.26	+/- 0.010
Keystone angle	deg.	1.0	+/- 0.10

- Made

Cable No.	Billet No.	Strand Dia. (mm)	Thick. (mm)	Width (mm)	P.L. (mm)	K.A. (deg.)
928R	205, 206, & 208	0.703	1.264	10.056	78.0	1.05
933R	8220	0.703	1.267	10.042	78.7	1.09
939R	8220	0.703	1.262	9.993	80.5	1.04
940R	8647	0.704	1.264	10.026	80.5	0.98
946R	8781	0.705	1.266	10.062	79.5	1.00



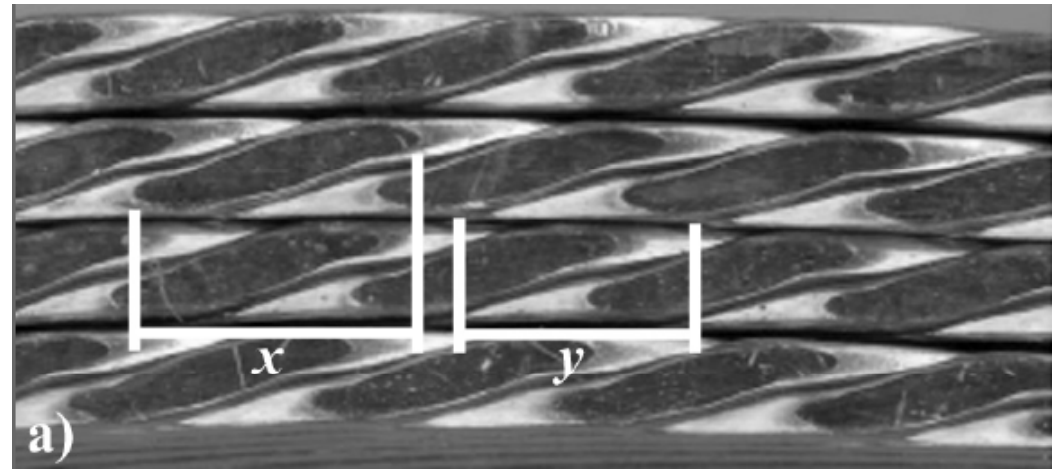
# TQ cable compared to past cables



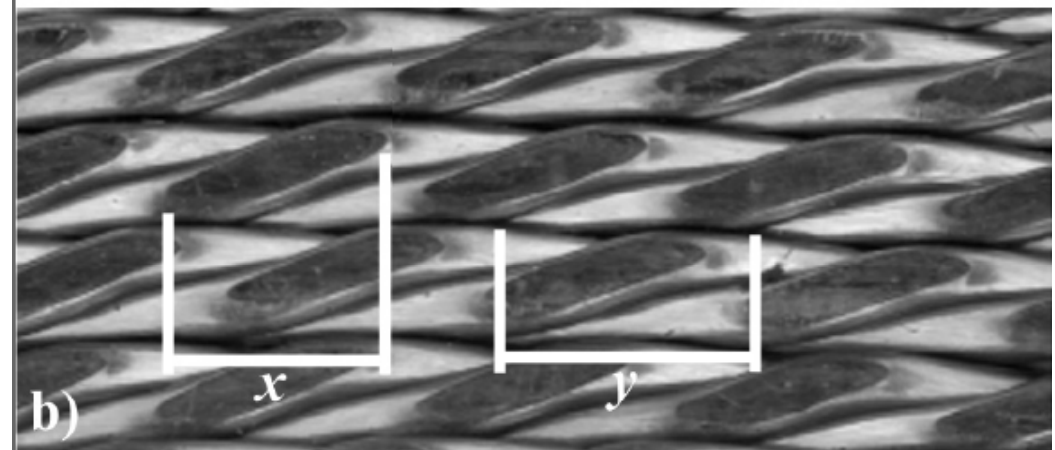
# Facet size as online probe

Bad

- Facet length ( $x$ ) should be less than Pitch Length/strand ( $y$ )
  - Minor axis



Good



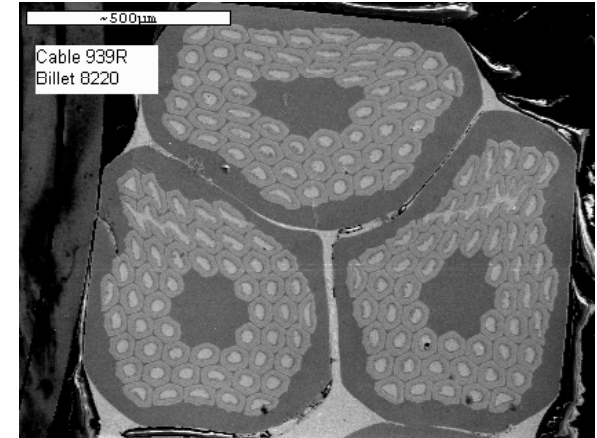
# Thin edge of cables as online probe

## Facets at cable edge



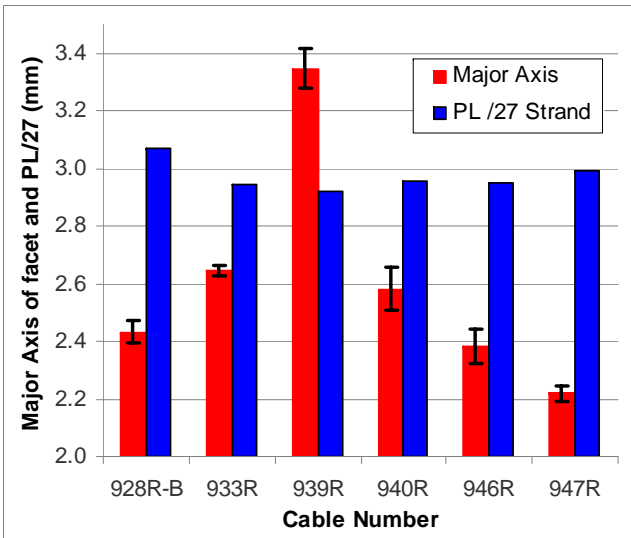
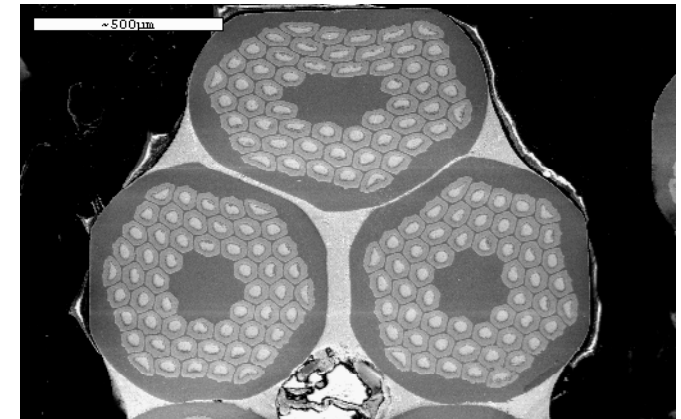
939R  
Bad

## SEM Images of Cross Section



946R

Good



Facets < Pitch length/strand



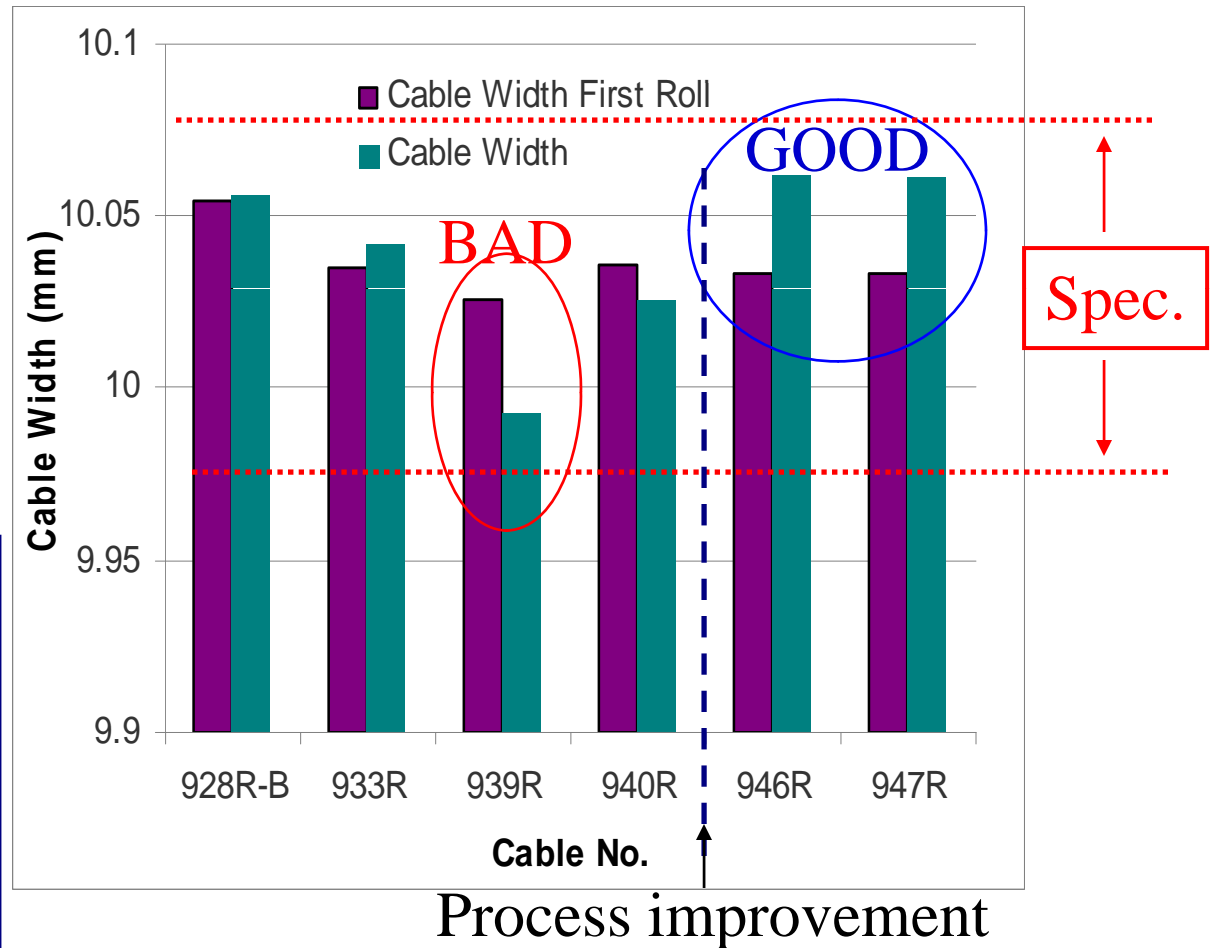
# TQ cable widths after re-rolling

- Do **NOT** re-roll cable to a smaller width

Re-rolling after anneal is used to provide final shape

- **Fabrication (first rolling)**
- **Anneal cable 200C for 4-6 h**
- **Re-roll (second rolling) – final cable**

After cable 940R the processing was changed  
From one set of rolls  
To 2 sets of rolls,  
One for the fabrication  
and one for re-rolling  
~ 50 micrometer wider





## Summary of Critical and Stability Currents for TQ Cables

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- All cables but 939R:
  - Reduced  $J_c(12T,4.2K)$  by about **0-3%**
  - Reduced stability current ( $I_s$ ) by **~10%**
- Cable 939R (bad example with sheared sub-elements):
  - Reduced  $J_c(12T,4.2K)$  by about **~5% (Only)**
  - Reduced stability current ( $I_s$ ) **by ~50% (RRR loss?)**
- Concern – Past  $J_c$  measurements on cables with edge damage has shown them to be more sensitive to transverse stress.





# NED Cable Parameters

No. of Strands =	40	Width > =	26.91		
Strand DIA. =	1.25	Cable MID Thk. =	2.5		
Pitch Angle =	16				
CALC Compacted Cable RESET		Pitch length =	181.398		
		PF @ Max Width =	0.7591		
		PF @ Min Width =	0.78539816		
Module: [B]		COMPACTED CABLE			
	INPUT B				
Cable Width Max. =	26.91		MIN.	MID	MAJ.
Cable Mid Thk. =	2.275				
Keystone angle. =	0.44	Cable Thickness =	2.17167	2.275	2.37833
Pitch length =	181.398	Packing Factor =	0.87586	0.83608	0.79976

- LBNL Cable-CALC
  - Should increase the width from 26 mm to 26.9 mm.
  - Note: Removal of 1 strand is only 2.5% Ic reduction but provides significantly more width margin



# NED Cable Prototype Fabrication

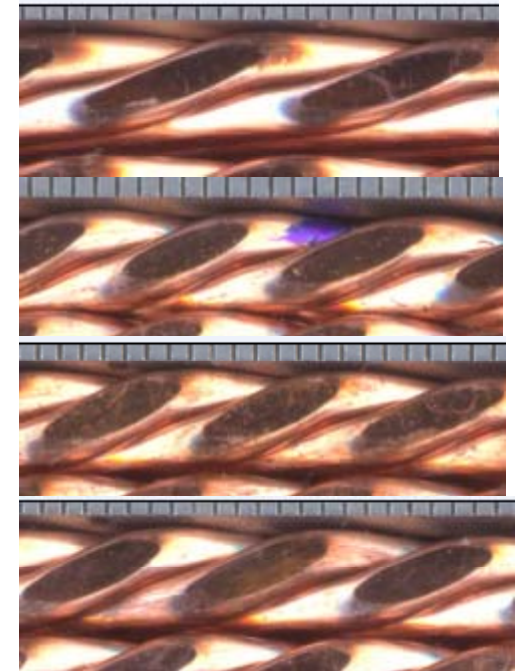
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- LBNL cabling machine was pushed to its limits due to the:
  - Large strand diameter
  - High stiffness of the strand
- Higher tension on the strands should make the cabling process easier.
  - It should permit fabrication of cables with a lower pitch angle ( $\sim 16^\circ$ )
  - Plus reduce the gaps between strands

# NED cable edge facet summary

## Four short prototype cable sections made

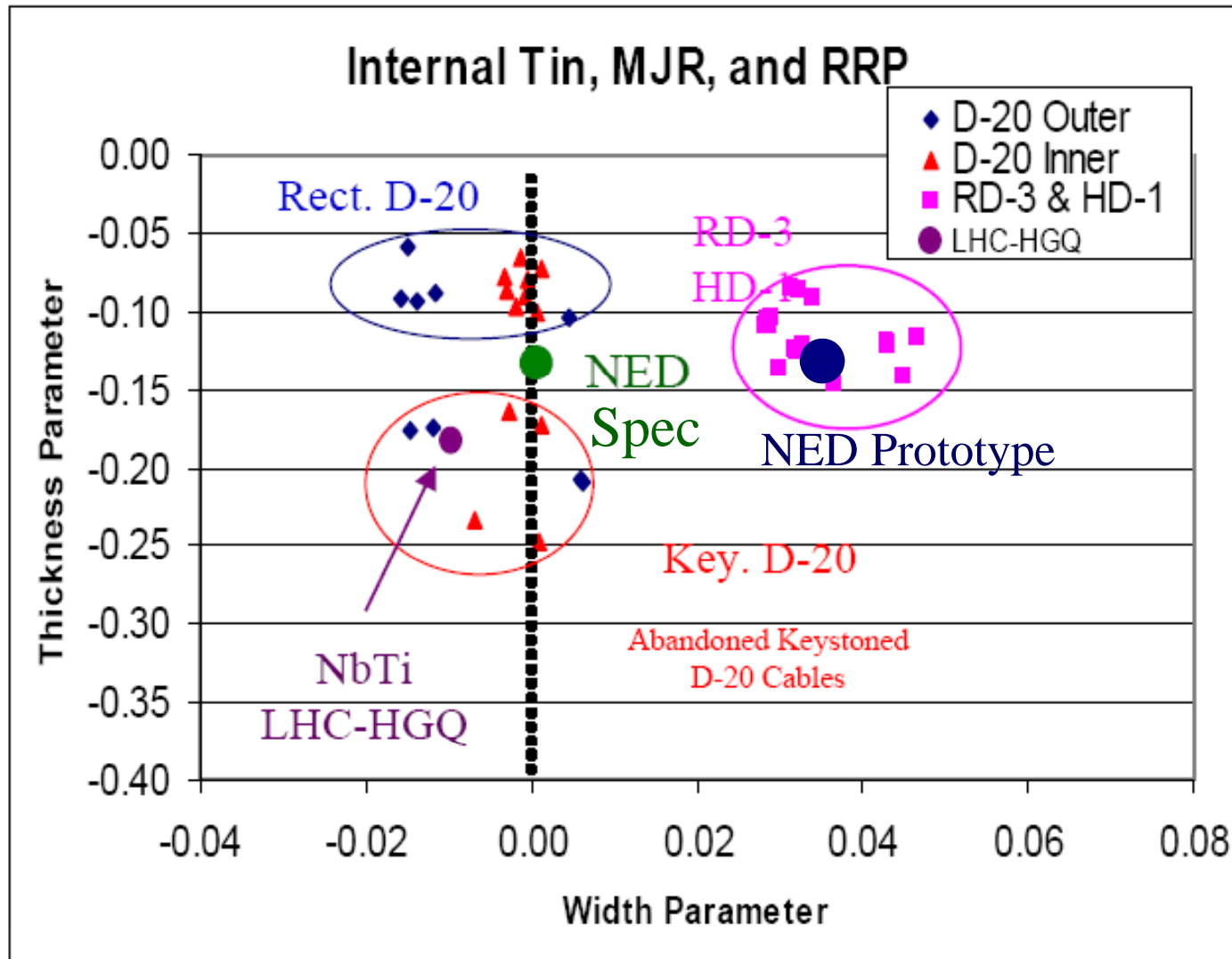
	Facet Length mm	Pitch Length mm	Facet/Pitch	Cable Pitch Length mm
965-A-Min	4.26	4.76	0.89	190.7
965-A-Maj	4.11	4.83	0.85	193.1
965-C-Min	3.17	3.76	0.84	150.5
965-C-Maj	3.45	3.76	0.92	150.5
965-D-Min	3.34	3.74	0.89	149.6
965-D-Maj	3.65	3.79	0.96	151.5
965-E-Min	3.33	3.75	0.89	150.1
965-E-Maj	3.57	3.77	0.95	150.9



- Facet/Pitch on the minor edge are similar
  - Section C has the smallest ratio
  - Section C has 4-8%  $I_c$  reduction (T. Boutboul, EUCAS-07 )

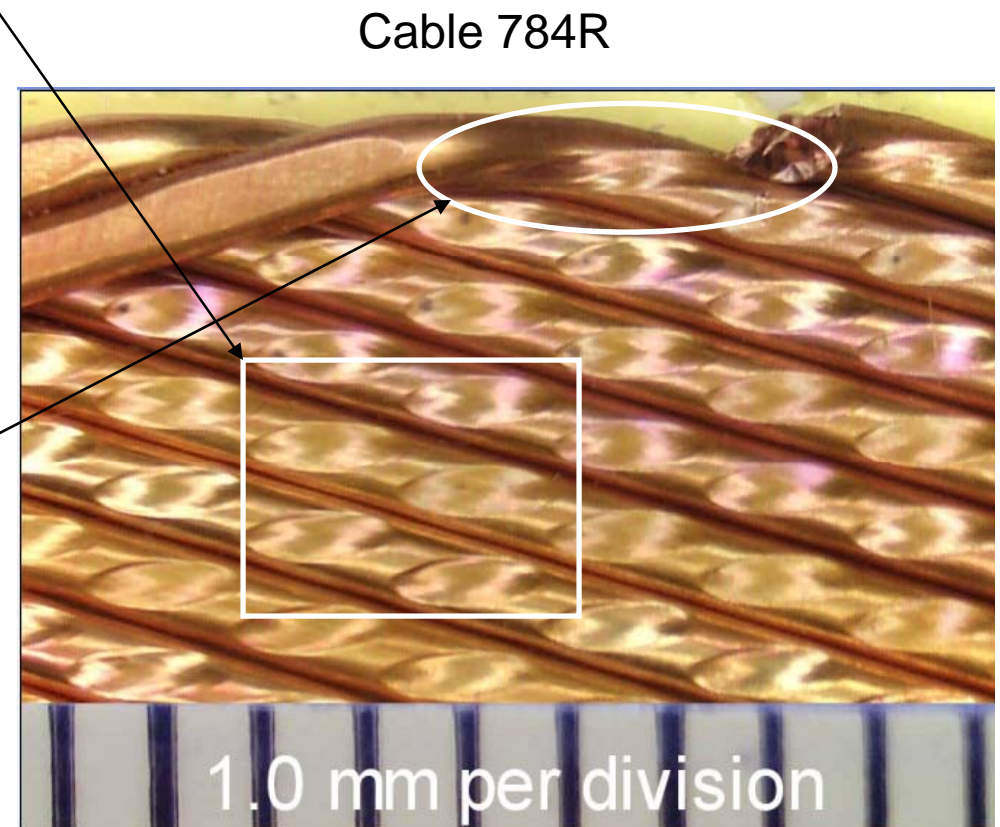


# NED spec and prototype



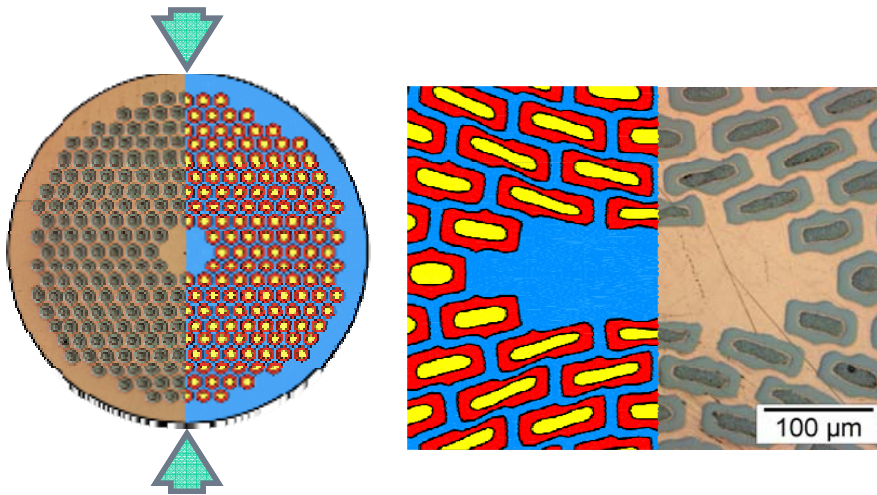
## Strand deformation inside a cable

- Dimples at strand cross over points (box)
  - Deformation not uniform along a strand
  - Making cables thinner has shown no significant impact on performance
  - Perhaps cables can be made thinner
- Strand deformation as it goes from the top of cable to bottom (oval)
  - Limits cable performance
- Need 3D modeling to understand strand deformation at the cable edge



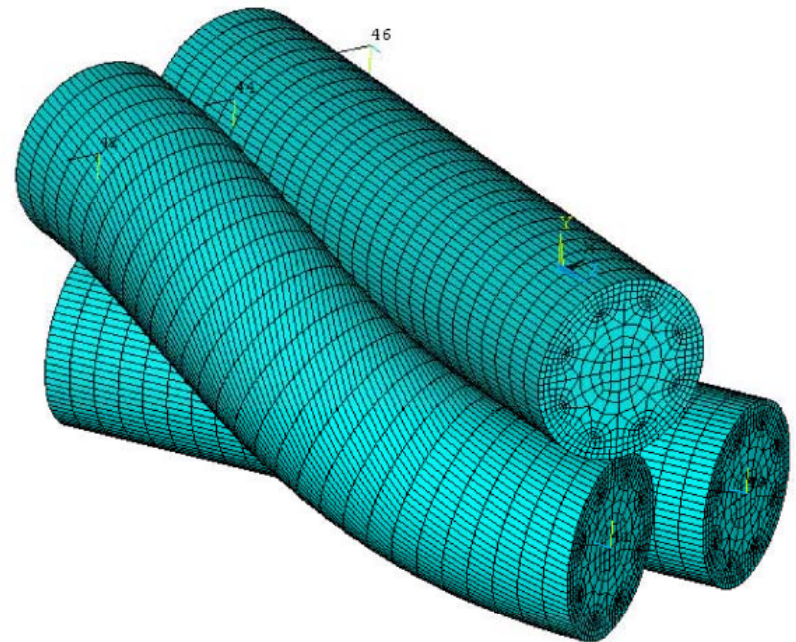
# Modeling 2D and 3D

## 2D Strand Modeling



- *S. Farinon, Presented at CHATS-AS 2006*

## 3D Modeling of Strand



*Marco La China*



# Summary

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- The facet size on the edge of the cable provides a direct measure of the amount of strand deformation.
  - Indicates the amount of sub-element distortion inside the strand.
- This work shows that a **nearly damage-free mechanically-stable cable** can be produced from:
  - MJR and RRP strands with reduction of **only 0-3%  $J_c$**  (12T, 4.2K).
  - PIT strand with reduction of 4-8%  $J_c$  (12, 4.2K)
- Cabling damage (i.e. sheared sub-elements) had minimal effect on  $J_c$  but it has a **significant** impact on strand stability.
  - The stability current ( $I_s$ ) **drops by ~50%** in a strand with only a ~5% drop in  $J_c$  at 12T and 4.2K