

WAMSDO 2008

Workshop on Accelerator Magnet, Superconductor, Design and Optimization

Irradiation Effects in Low T_c Superconductors

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Outline

Introduction

Radiation damage in solids

Behavior of various superconductors under irradiation

Radiation Effects in A15 type superconductors

- * Change of atomic ordering
- * Homogeneity after Irradiation
- * Irradiation temperature and recovery

Irradiated binary and alloyed Nb₃Sn wires

- * Critical field, Critical current
- * J_c under stress

Expected Radiation Spectrum in LHC

Conclusions

Introduction

Compound	T_c (K)	$B_{c2}(0)$ (T)	λ (nm)
NbTi	10	14	6.3
Nb ₃ Sn	18	28	4.2
Nb ₃ Al	19	33	
MgB ₂	39	35 - 65	5
V ₃ Ga	15	24	
(Hf,Zr)V ₂ Laves phases	10	20	
PbMo ₆ S ₈ Chevrel phases	15	50	2.2



Radiation damage in solids

The collision cascade

High energy particle: Energy transfer

Along the particle trajectory: local melting or continuous amorphous zone : **columnar track**.

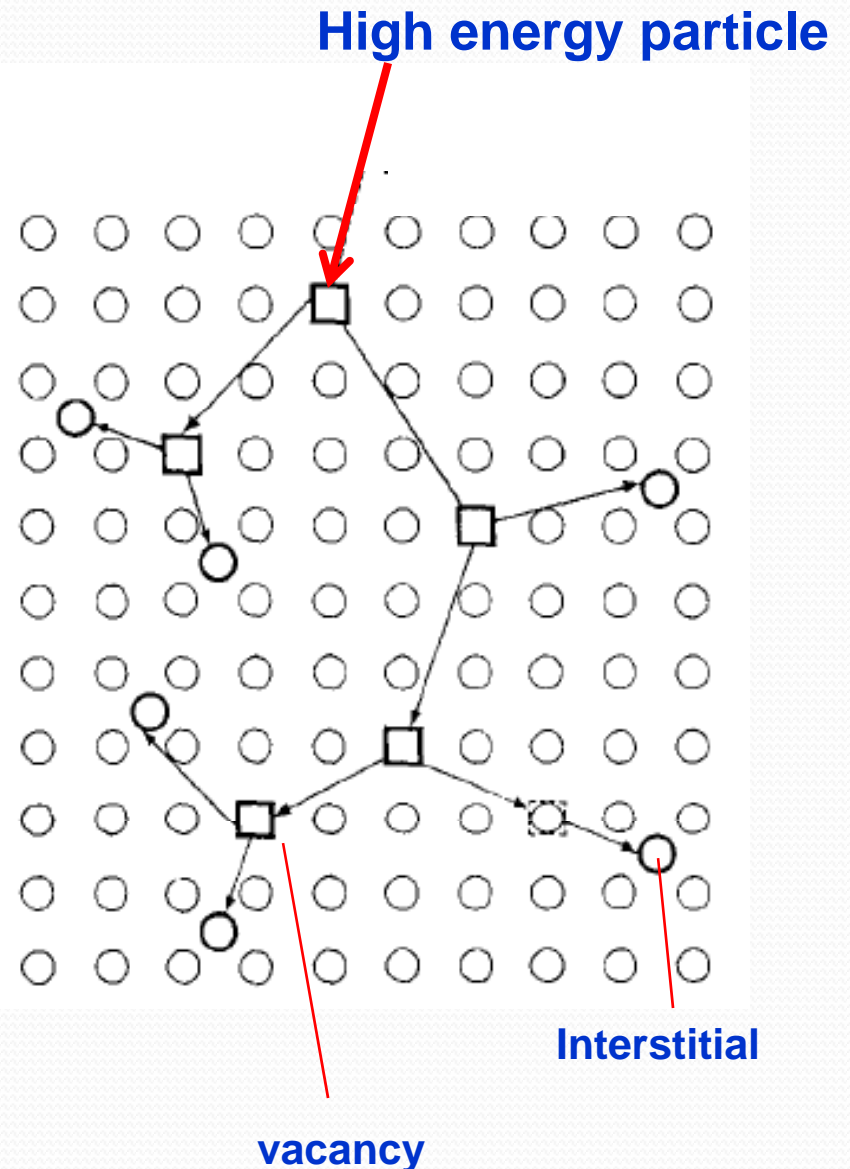
Displacement energy : E_d

$E_d = 10 - 40$ eV for most metals

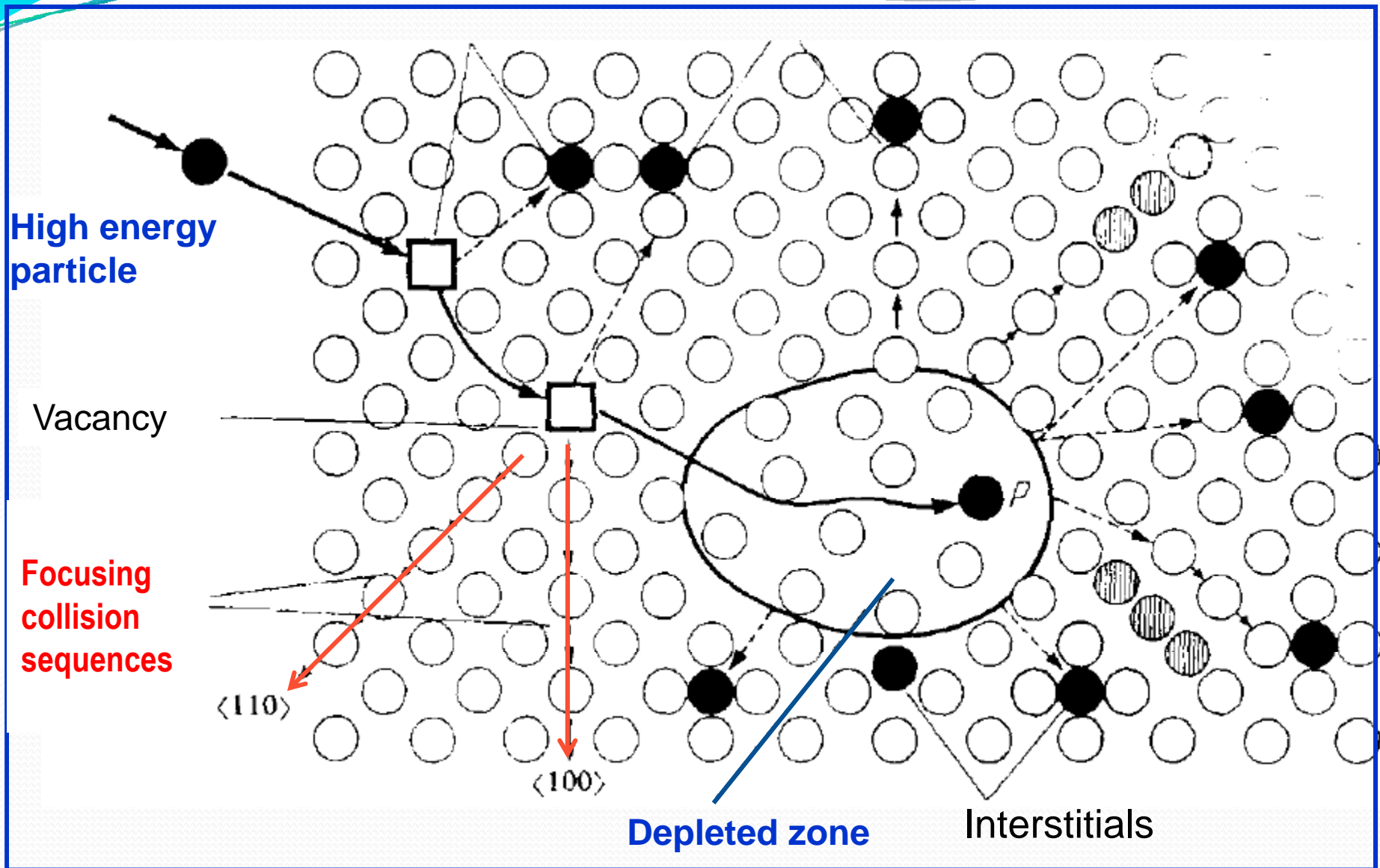
Number of displaced atoms:

$$v = T / 2E_d$$

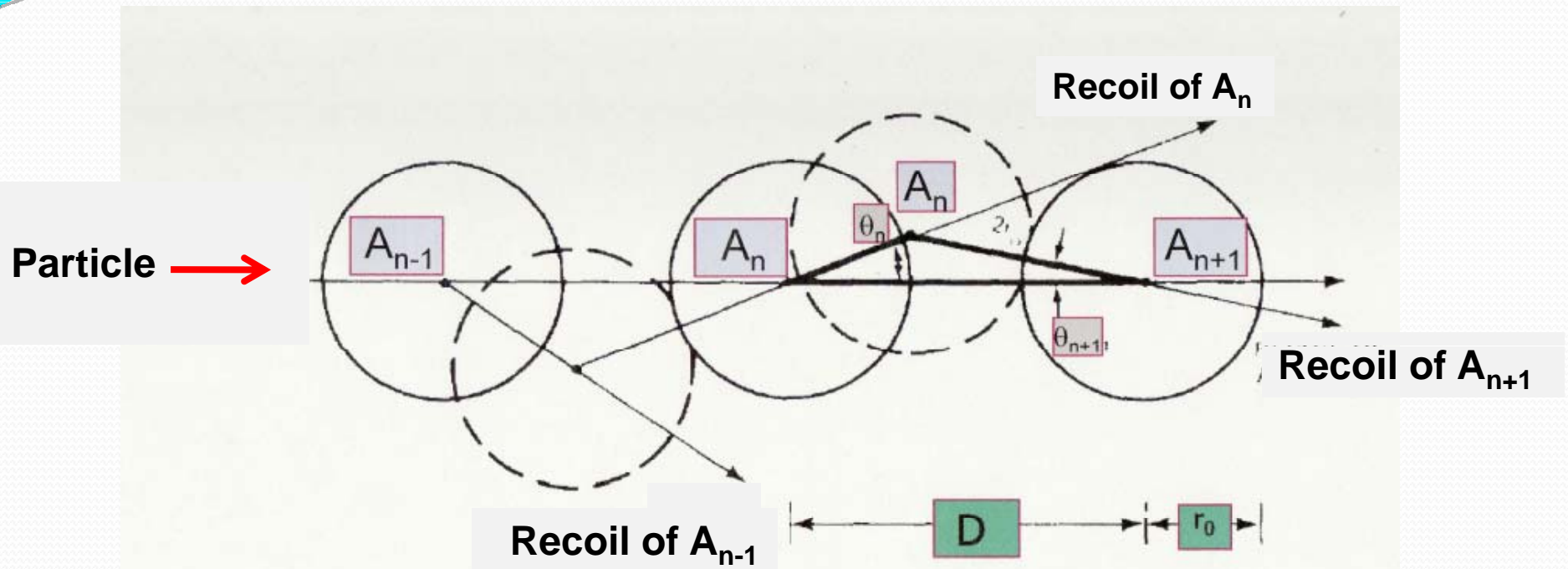
At the end of the path of the irradiating particle: **mean free path decreases, density of displaced atoms increases**



Formation of depleted (disordered) zones



Focusing energy transfer \longrightarrow Focusing Collision sequences



Angles must be small enough to keep collisions in a line

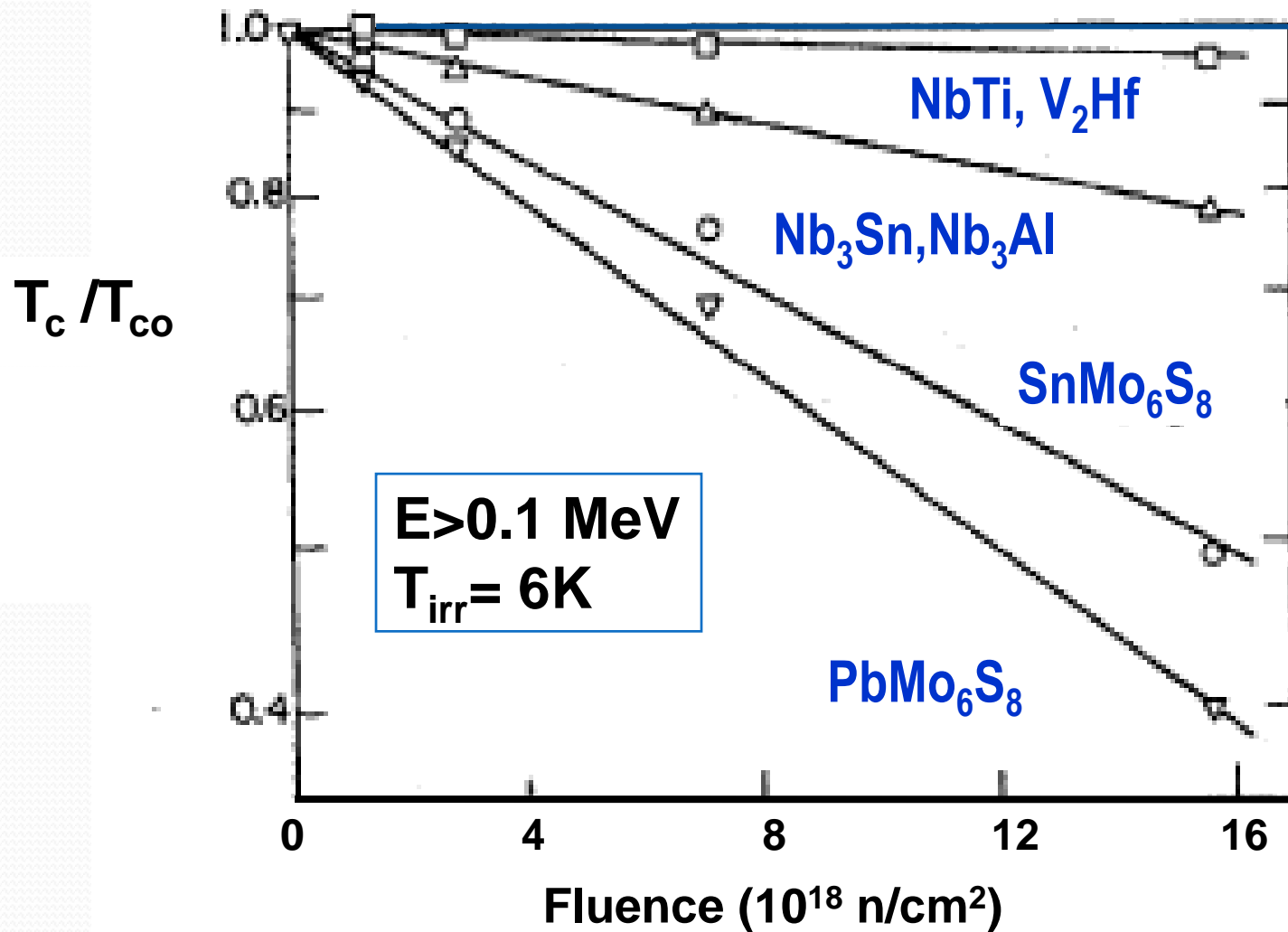
Collisions along a row of close-packed atoms

- * Larger distances covered
- * More probable at low energies



Behavior of various superconductors submitted to high energy irradiation

Irradiation of various Low T_c superconductors



B.S. Brown, J.W. Hafstrom, T.E. Klippert, J. Appl. Phys., 48(1977)1759

Radiation Effects in A15 Type Compounds:

Change of Atomic Ordering

The Long Range Bragg-Williams Atomic Order Parameter

S: The degree of atomic ordering in an A15 type compound A_3B

S=1: perfect ordering

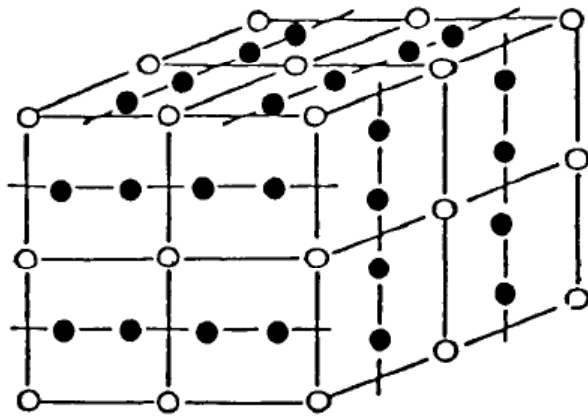
Probability to find atom A on 6c sites: 1

Probability to find atom B on 2a sites: 1

S = 0: complete disorder

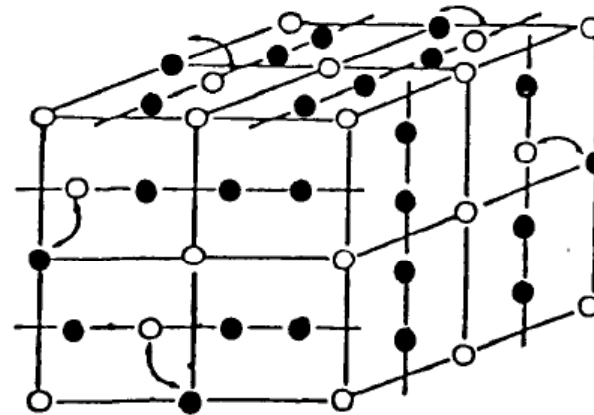
Probability to find atom A on 6c sites: 0.75

Probability to find atom B on 2a sites: 0.25



$S = 1$

perfect order

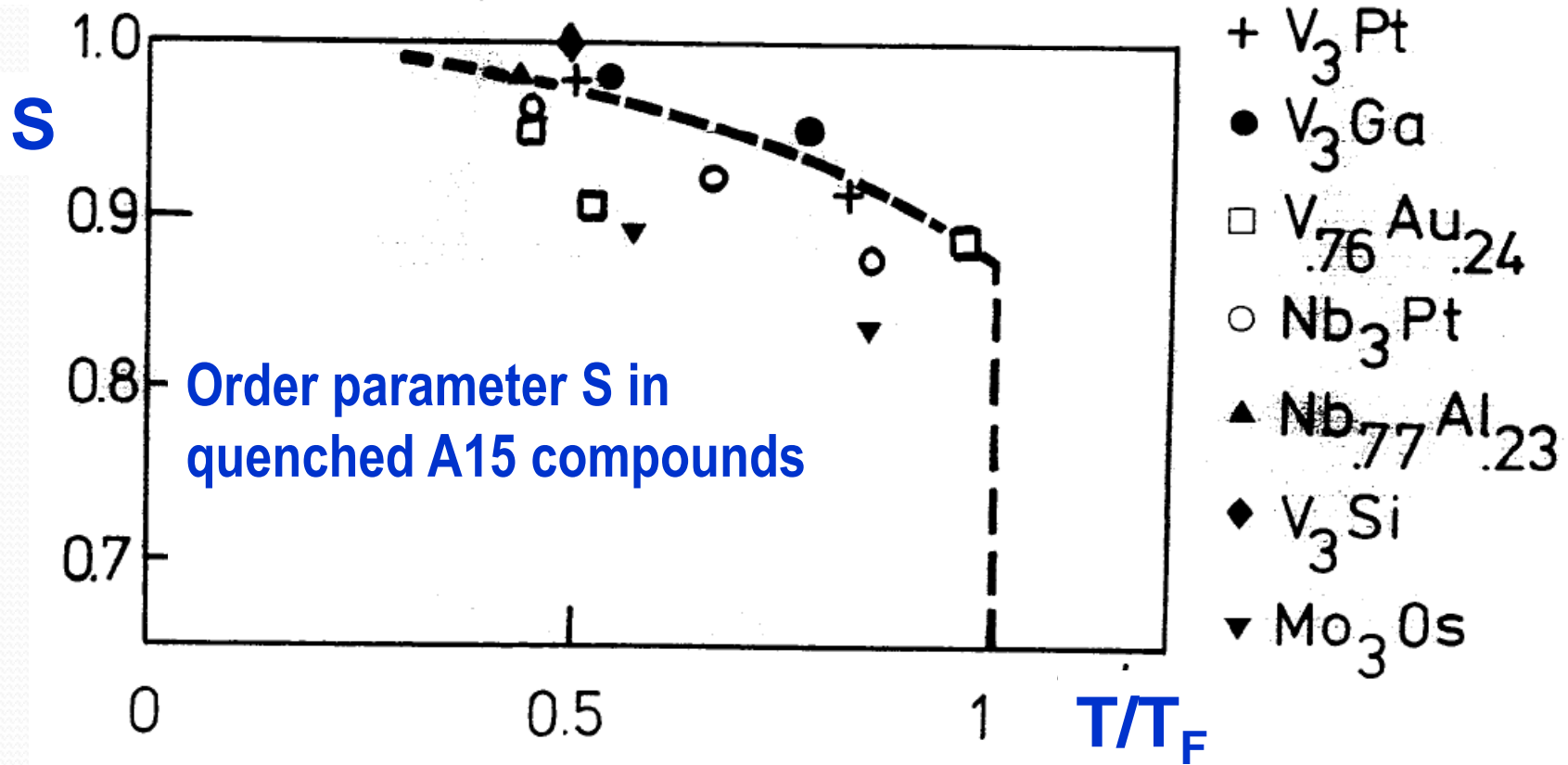


$S \neq 1$

partial disorder

Irradiation has **the same effect** as quenching from high temperatures:

→ **Reduction of the Bragg Williams order Parameter**



Order parameter S in quenched A15 compounds

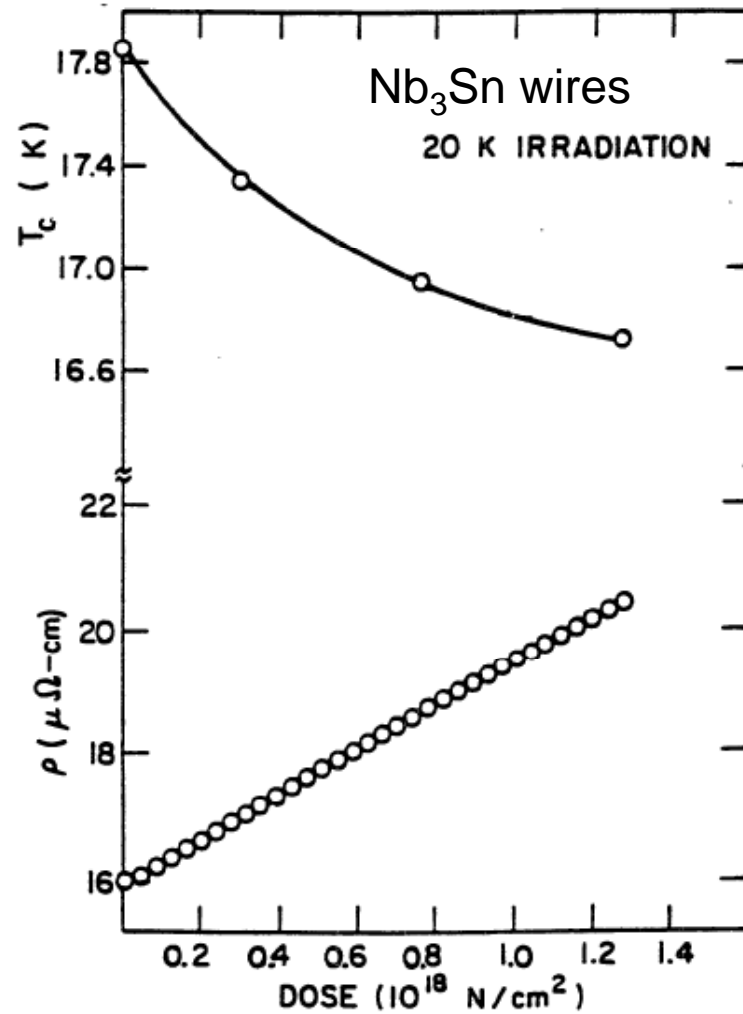
R. Flükiger, 1989

T_F : fusion temperature



Effects observed after High Energy Irradiation

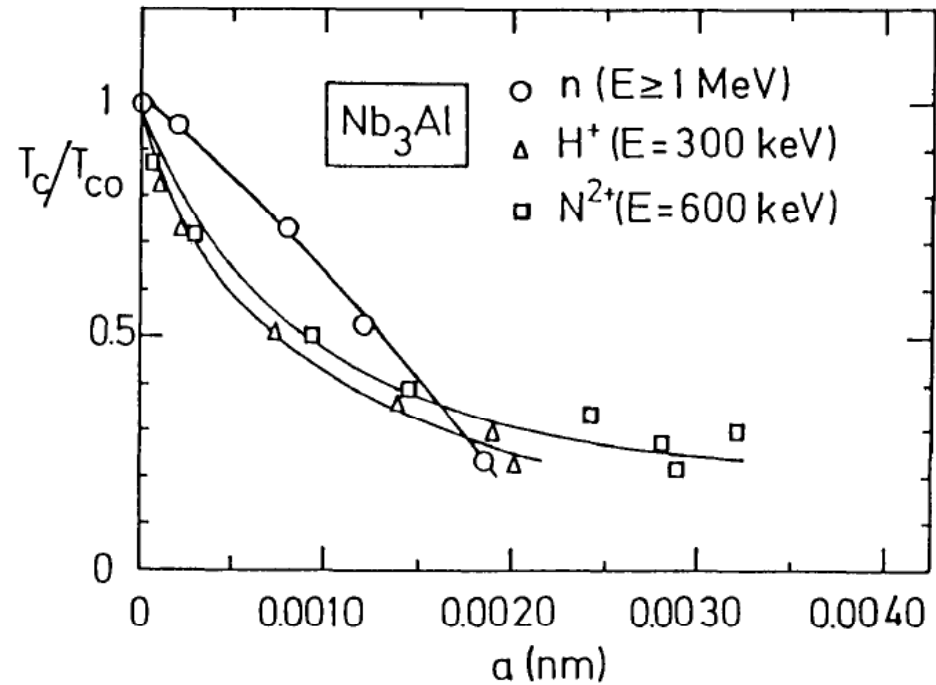
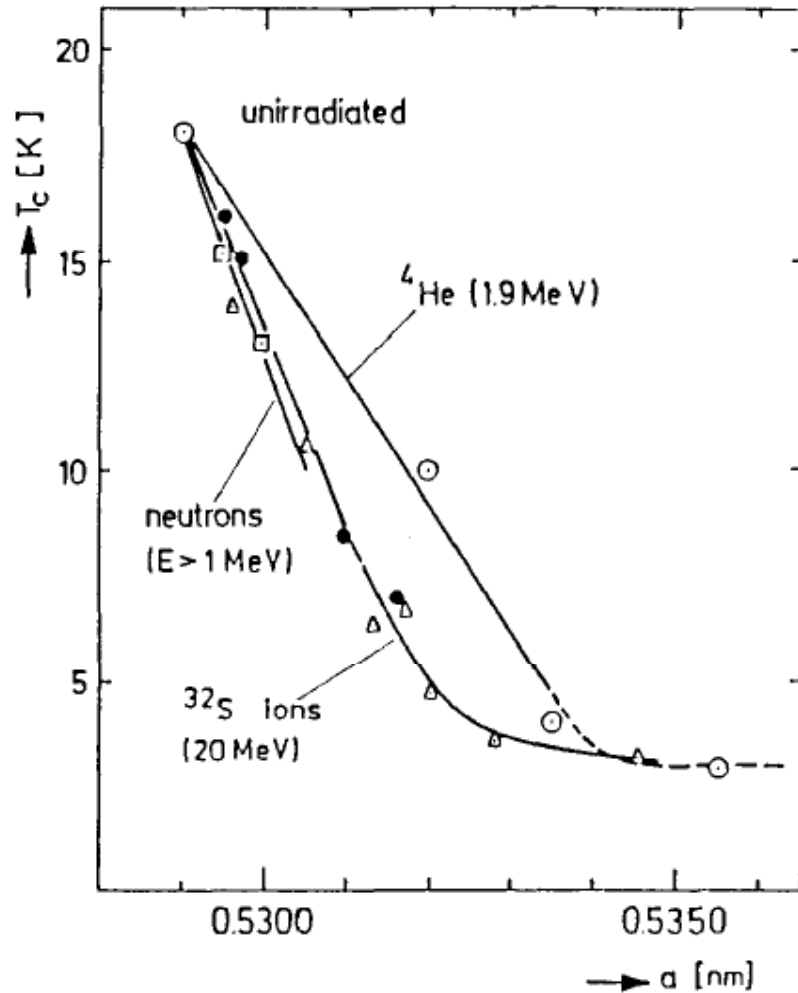
Enhancement of normal state electrical resistivity ρ_0



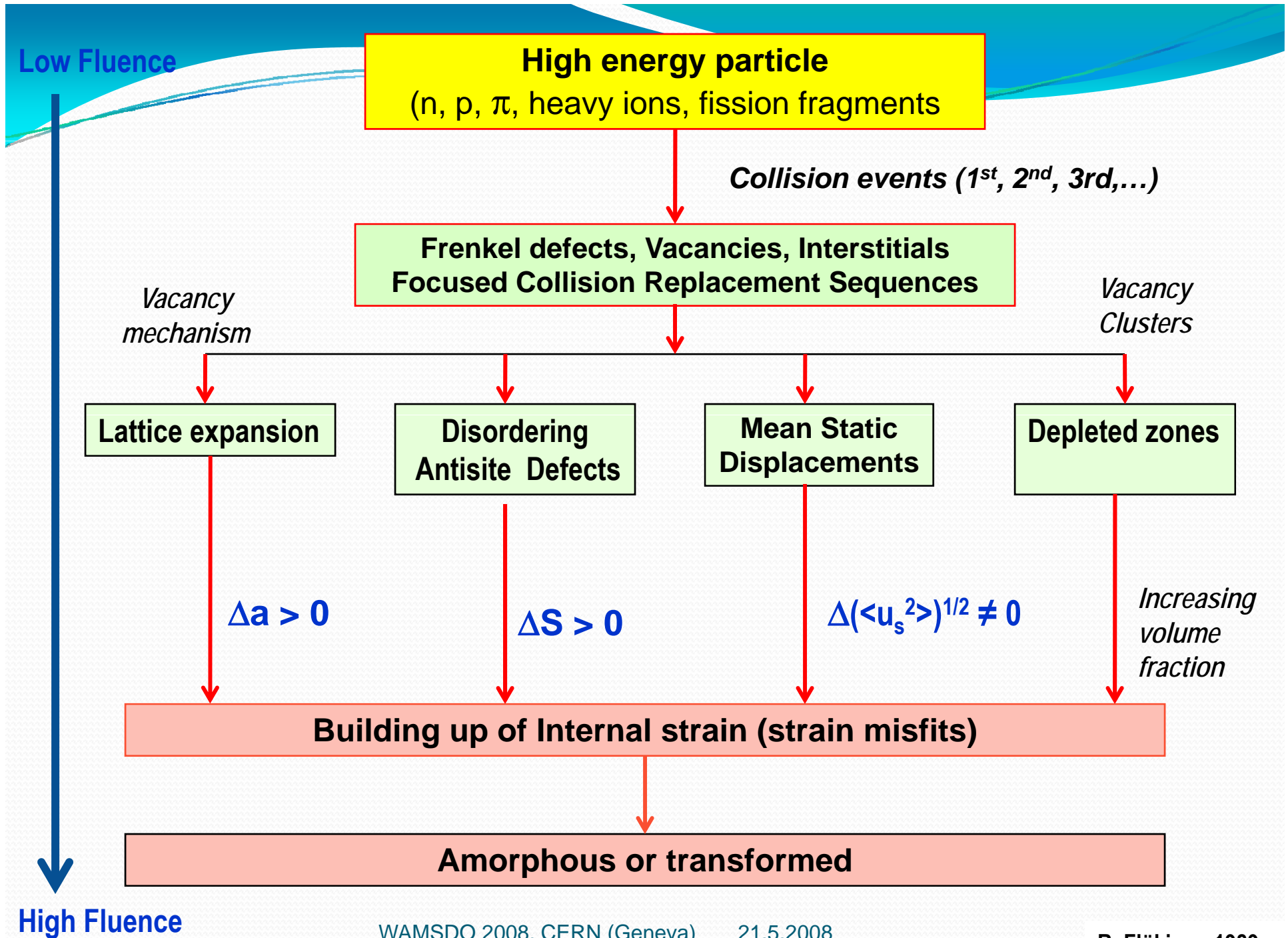
$$B_{c2} \sim T_c \gamma \rho_0$$

B.S. Brown, R.C. Birtcher, R.T. Kampwirth, T.M. Blewitt, J. Nucl. Materials 72(1978)76

Decrease of T_c and lattice expansion after irradiation with various particles



Neutrons: Sweedler, 1978, H^+ , N^{2+} : Schneider, 1982, ^4He : Burbank, 1979, ^{32}S : Nölscher, 1985.



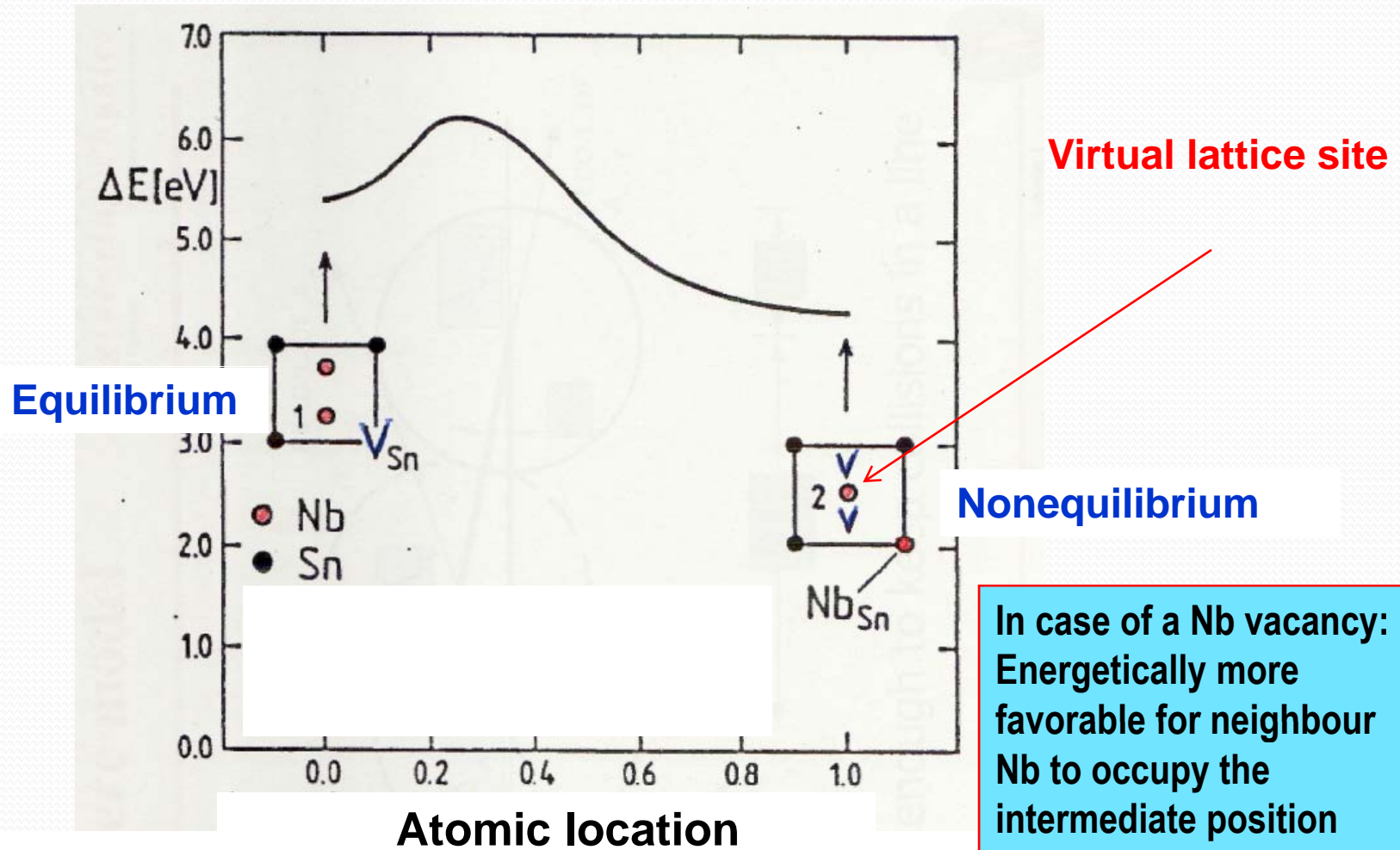
In A15 Compounds: Homogeneous Degree of Ordering after Irradiation

Consequence of the Vacancy Diffusion Mechanism

Arguments:

- Analogy between effects of irradiation and of fast quenching
- Correlation between radiation fluence and atomic order parameter
- Homogeneity of T_c , proven by **specific heat measurements**

Presence of vacancies: The “virtual” lattice site



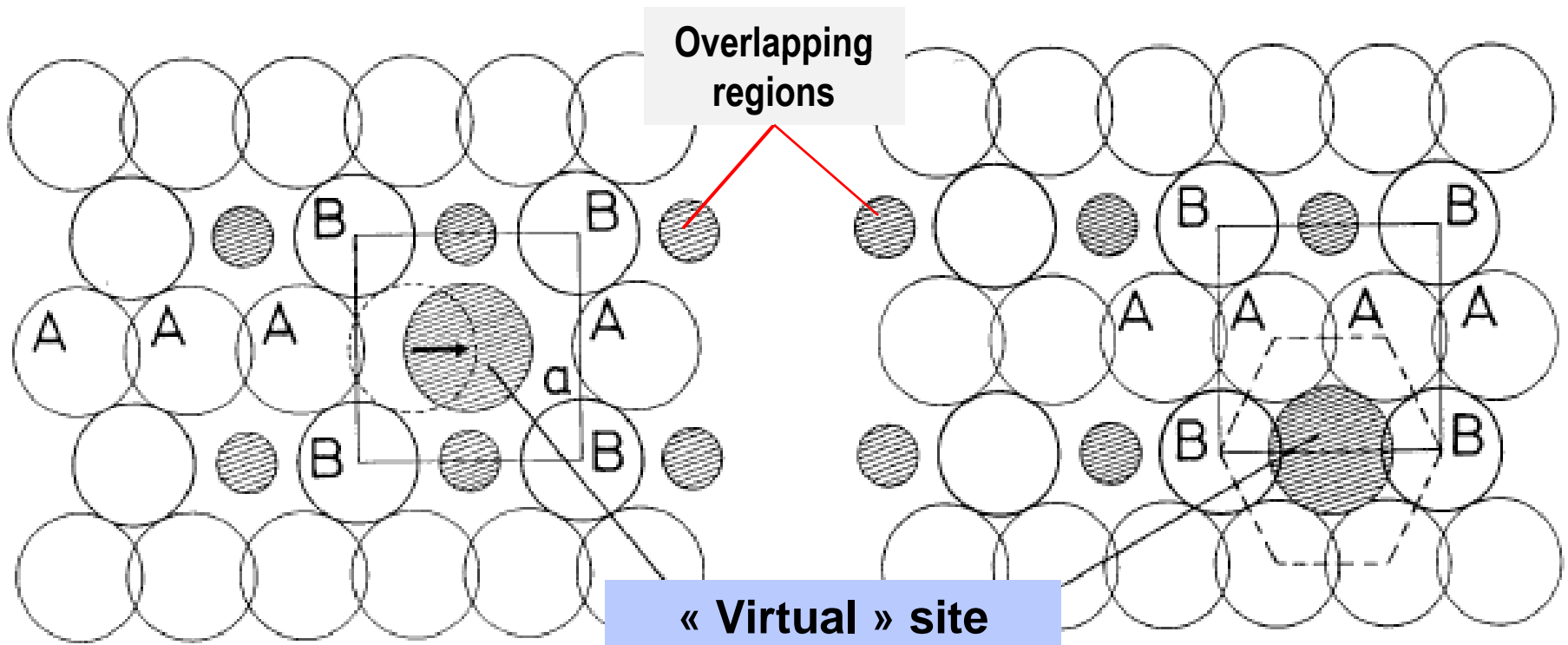
In case of a Nb vacancy:
Energetically more favorable for neighbour Nb to occupy the intermediate position
New « virtual » site

D. Welch, G. Dienes, O. Lazareth, R. Hatcher, Phys. Lett., 29A(1984)1225

A15 (A_3B): $A \leftrightarrow B$ site exchanges by vacancy diffusion

Chain parallel to plane

Chain perpendicular to the plane

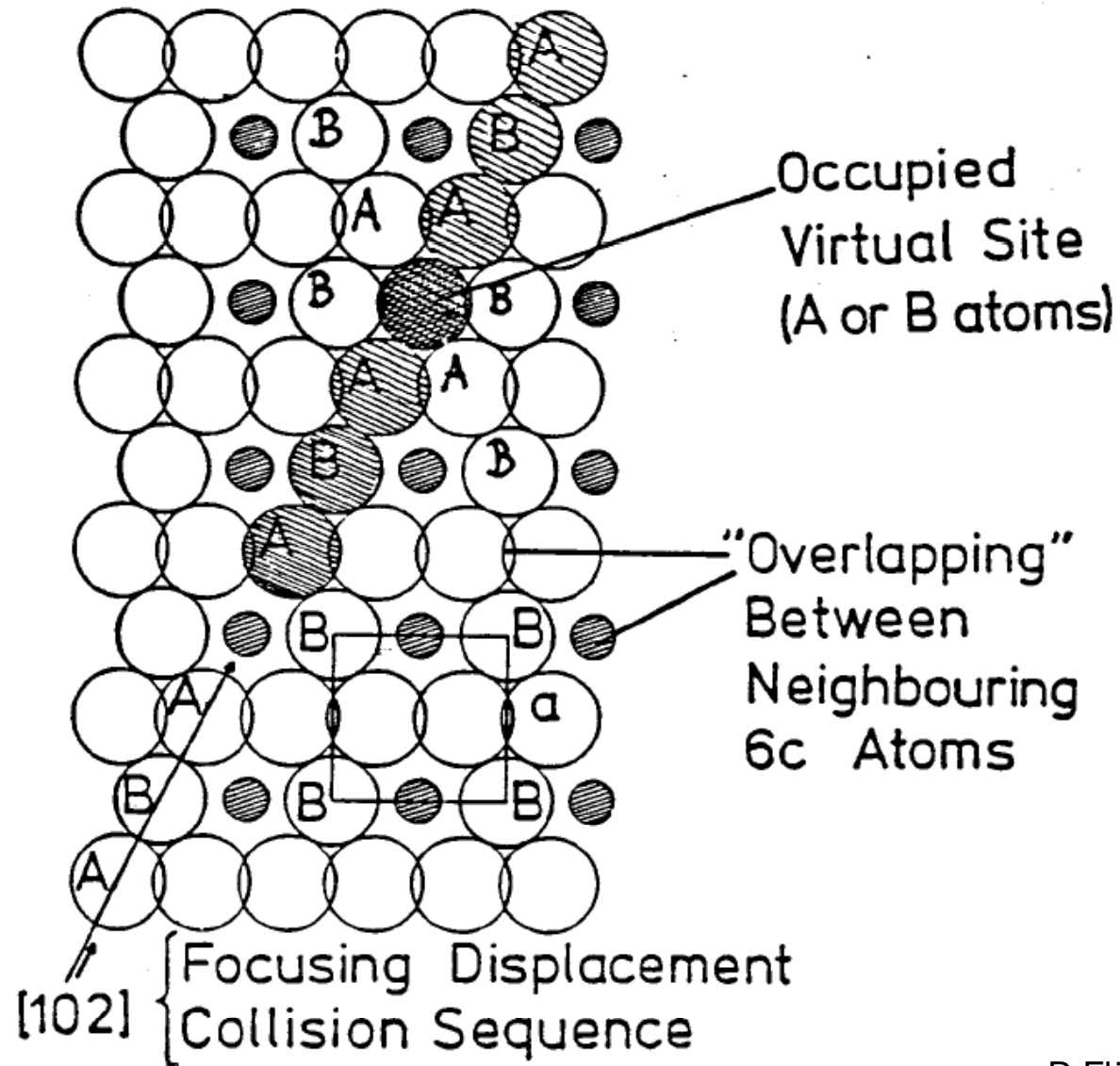


Jump of an A atom into a « virtual » vacancy

Jump of an A atom into a $2a$ vacancy

R. Flükiger, 1989

Site exchanges through Focusing Collision Sequences



R.Flükiger, 1989

Mechanisms for explaining “homogeneous” irradiation effects on T_c

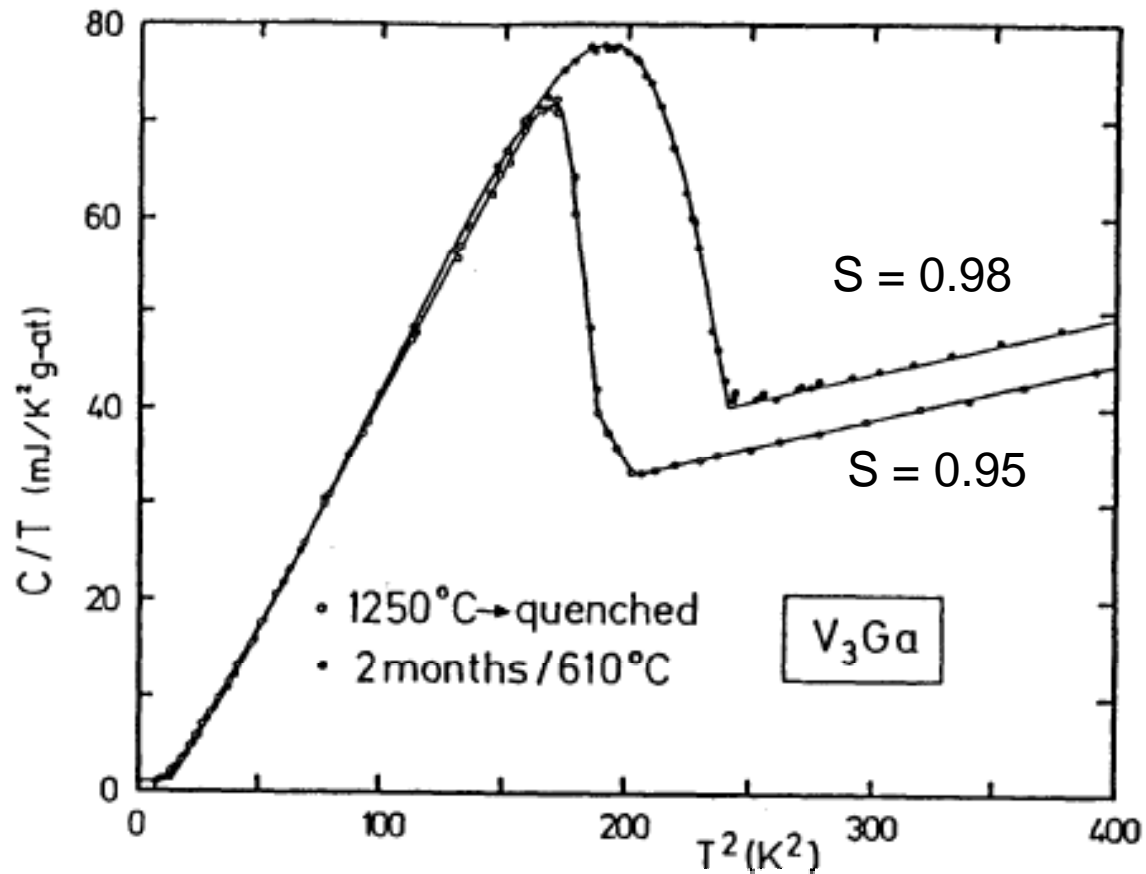
Dominant mechanism:

Decrease of atomic ordering due to focused collision sequences

(Sweedler et al., 1975, 1978, Söll et al., 1976, Snead et al., 1980, 1986, Hahn et al., 1991, Guinan et al., 1984, Weiss et al., 1987, Flükiger et al., 1989)

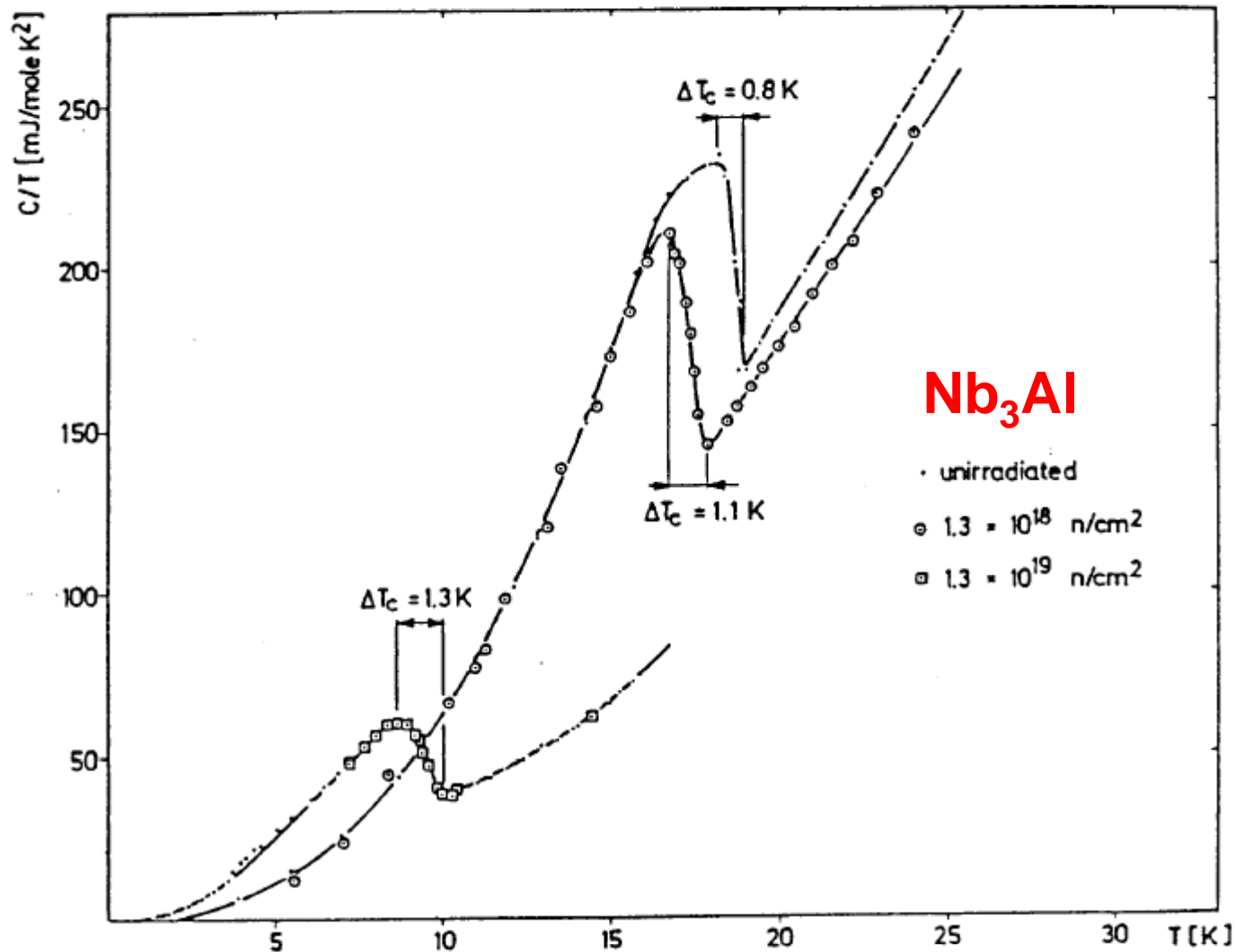
Another mechanism: **Proximity effects** due to deleted zones with lower T_c cannot explain the homogeneity of the observed effects

Homogeneity of T_c on quenched V_3Ga



P. Fischer, R. Flükiger, 1980

Homogeneity of T_c distribution (Specific Heat Measurements)



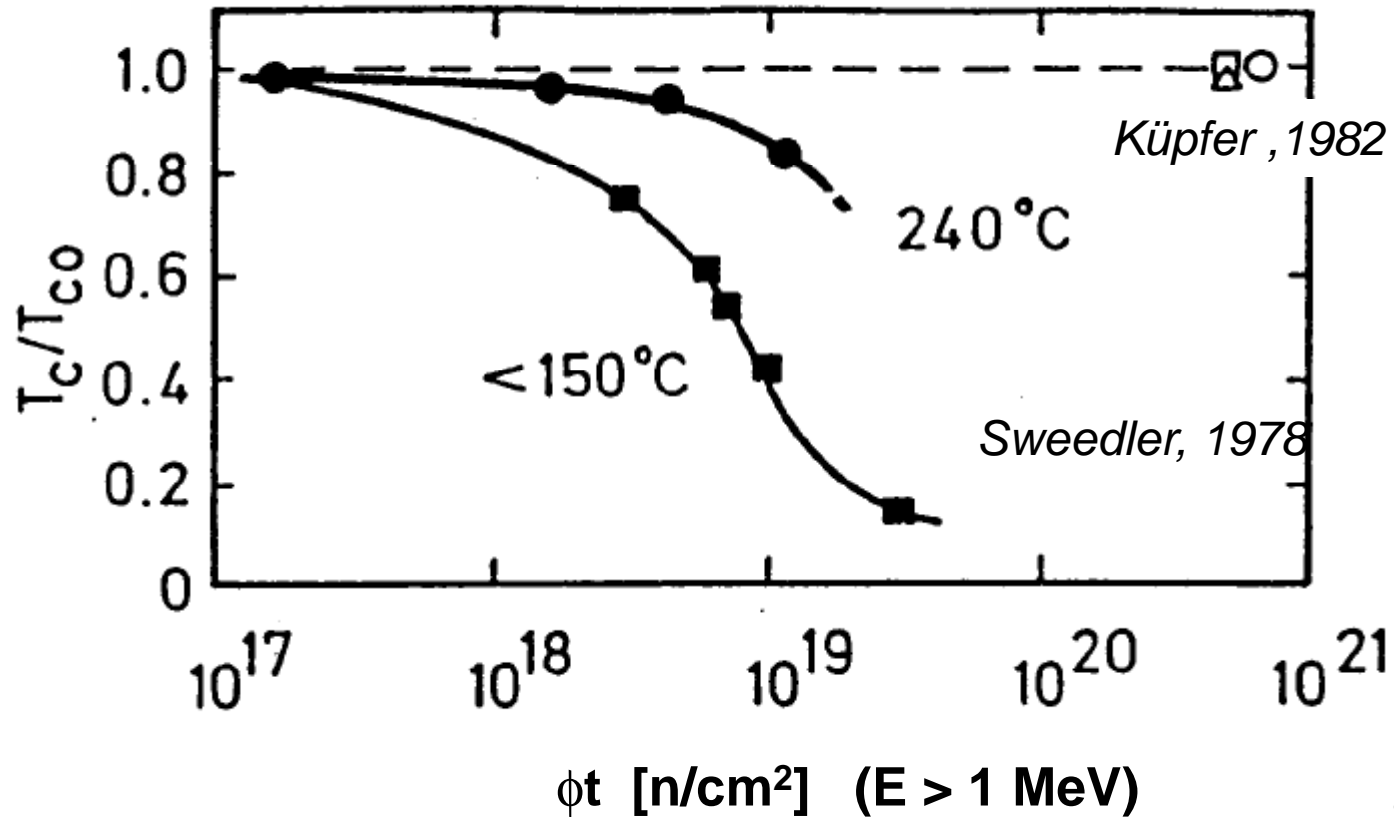
B. Cort, G.R. Stewart, C.L. Snead, A.R. Sweedler, Phys. Rev. B24(1981)379



Irradiation Temperature: Radiation Damage and Recombination

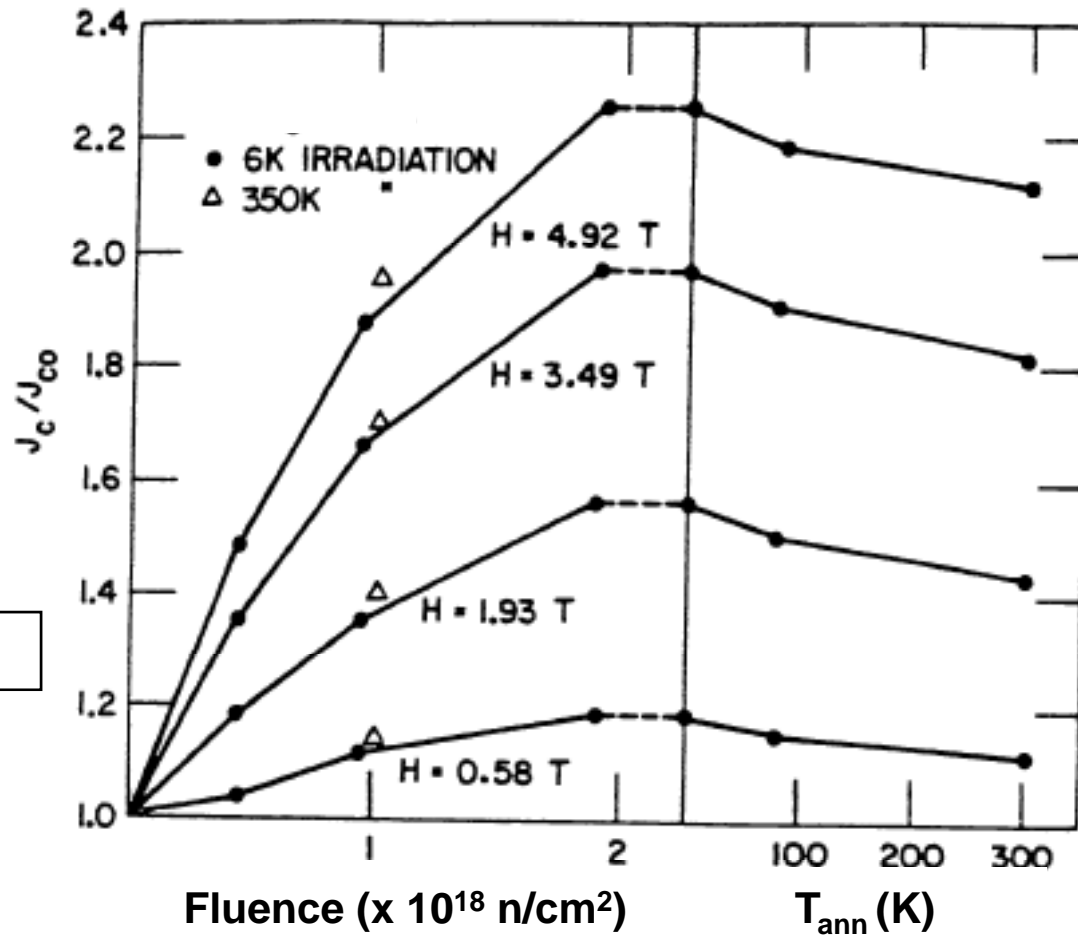
- * Highest damage: at lowest T_{irr}
- * Increase of T_{irr} : recombination
- * Even $T_{300\text{K}}$ causes partial recombination

Effect of Irradiation Temperature



T_c vs. fast neutron irradiation dose for V_3Si

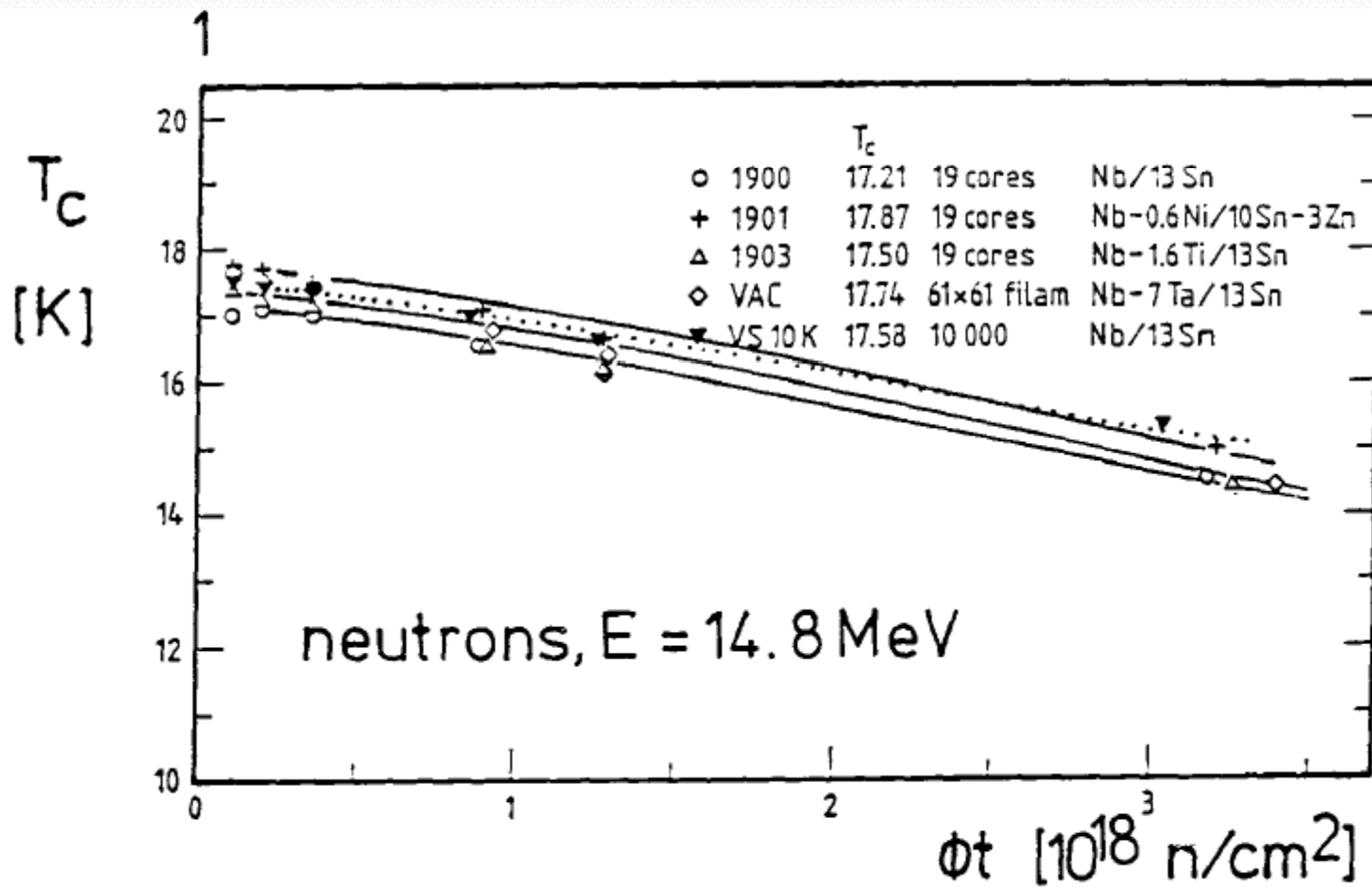
$E > 0.1 \text{ MeV}$



Neutron irradiation of a multifilamentary Nb_3Sn wire, followed by an anneal of 5 min. at T_{ann} .

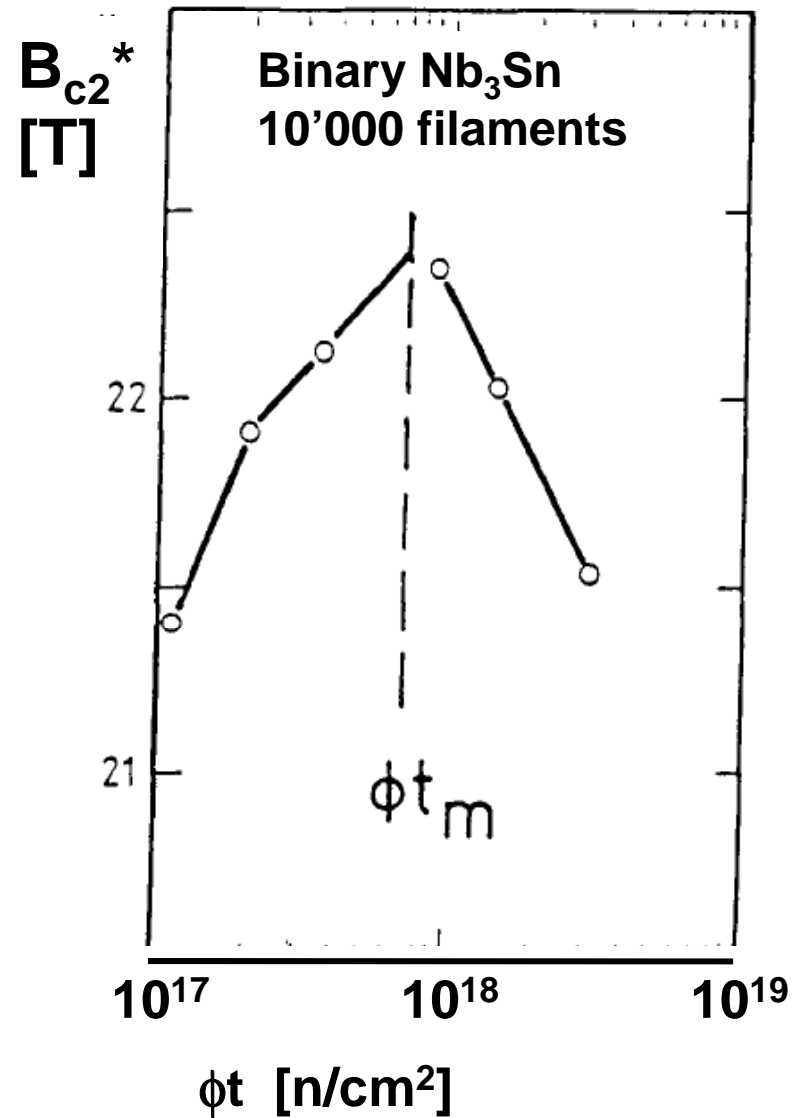
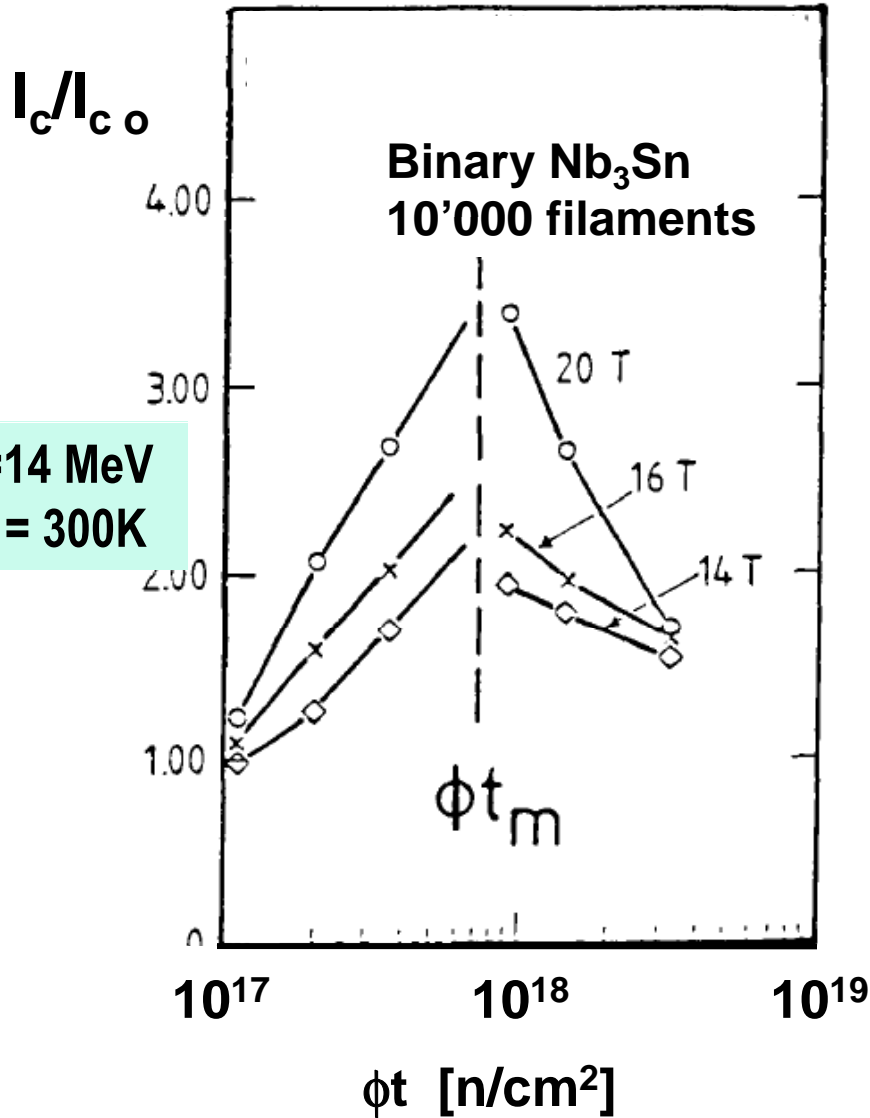


Irradiation of binary and ternary Nb₃Sn wires with 14 MeV neutrons

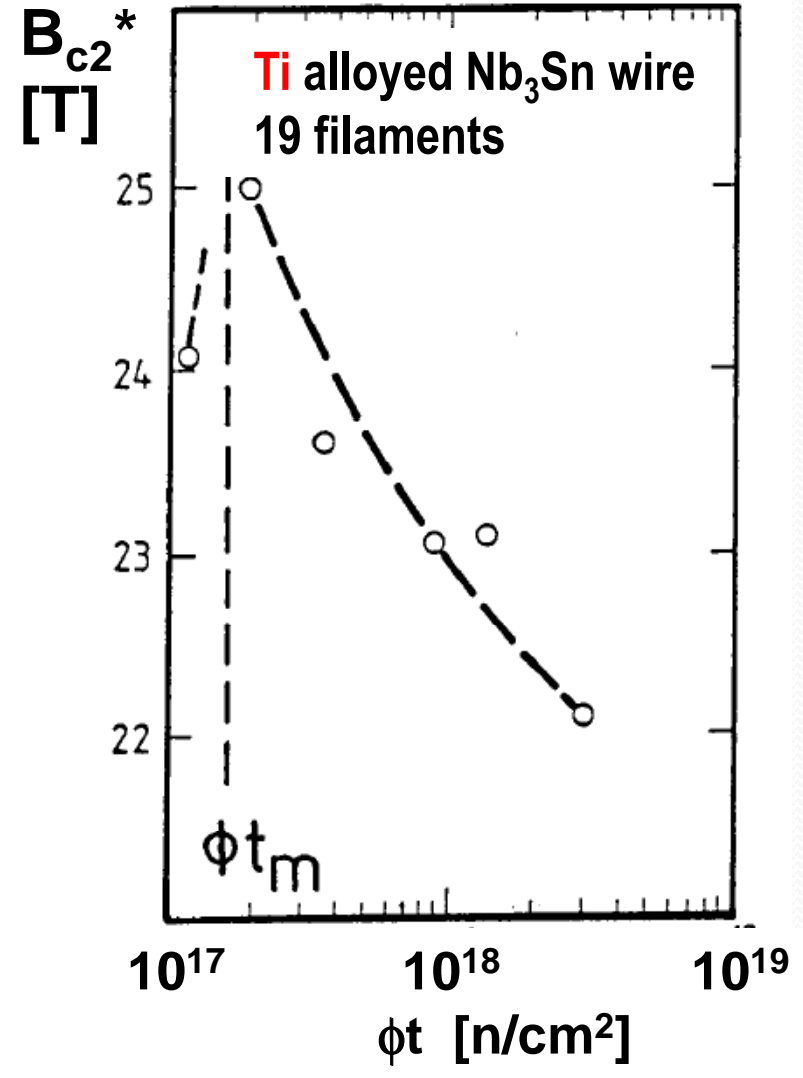
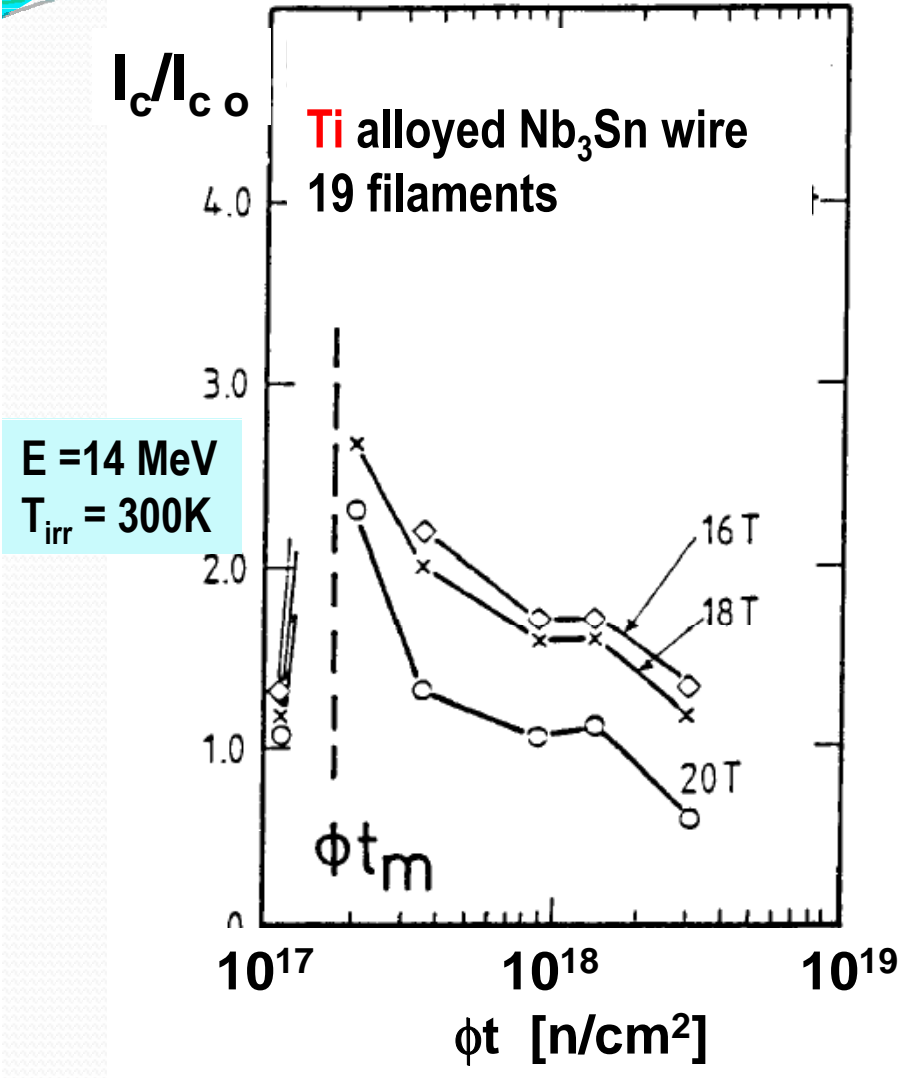


F. Weiss, R. Flükiger, W. Maurer, IEEE Trans. Magn., MAG-23(1987)976

Binary Nb₃Sn wire (10'000 filaments)

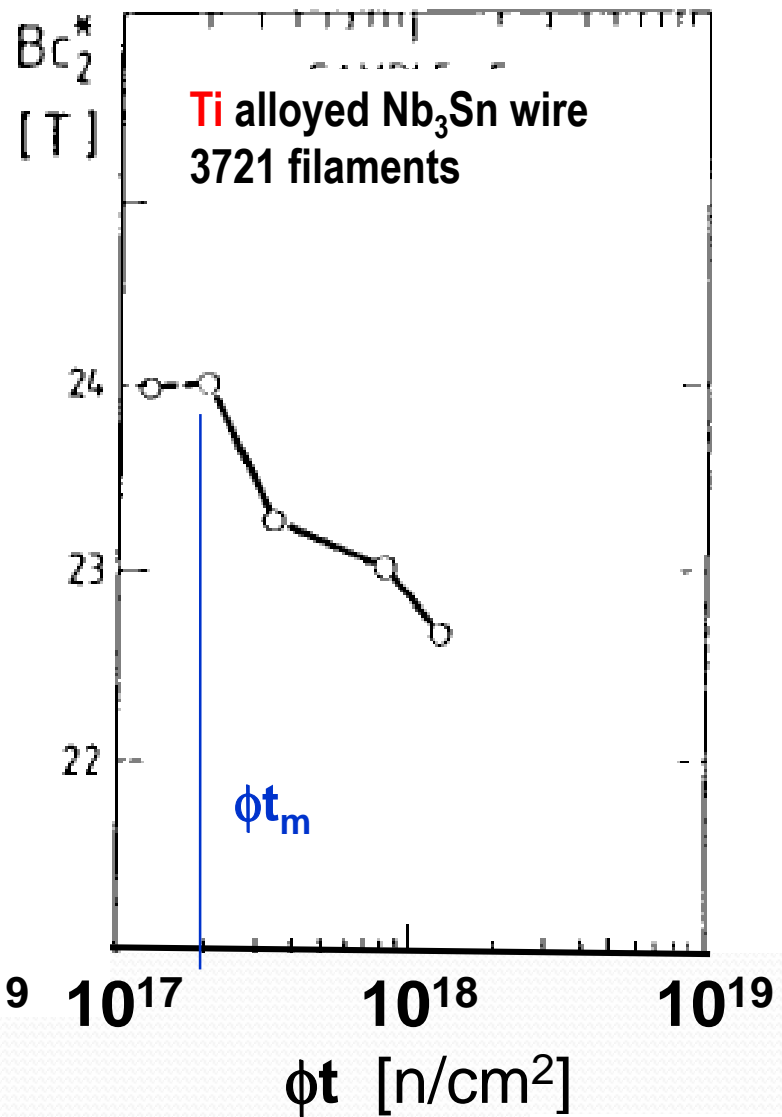
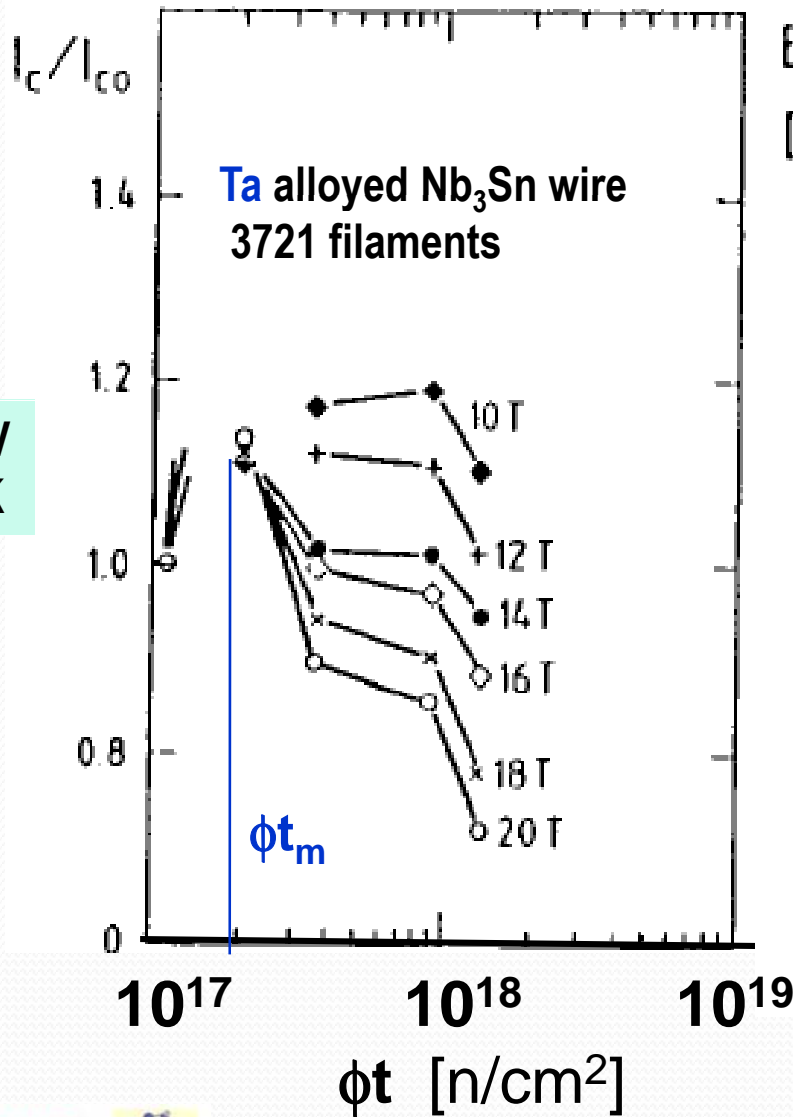


Ti alloyed Nb₃Sn wires



Ta alloyed multifilamentary Nb₃Sn wires

E = 14 MeV
T_{irr} = 300K



Alloyed Nb₃Sn wires: J_c more sensitive to irradiation

1) Maximum of I_c/I_{c0} and B_{c2} at **lower fluences** for alloyed Nb₃Sn wires

Wire	ϕt_m
Binary Nb ₃ Sn wire	8 x 10 ¹⁷ n/cm ²
Ti alloyed Nb ₃ Sn wire	1.8 x 10 ¹⁷ n/cm ²
Ta alloyed Nb ₃ Sn wire	1.8 x 10 ¹⁷ n/cm ²

2) At ϕt_m the increase $\Delta(I_c/I_{c0})$ and $\Delta(B_{c2})$ is **lower** for alloyed Nb₃Sn wires

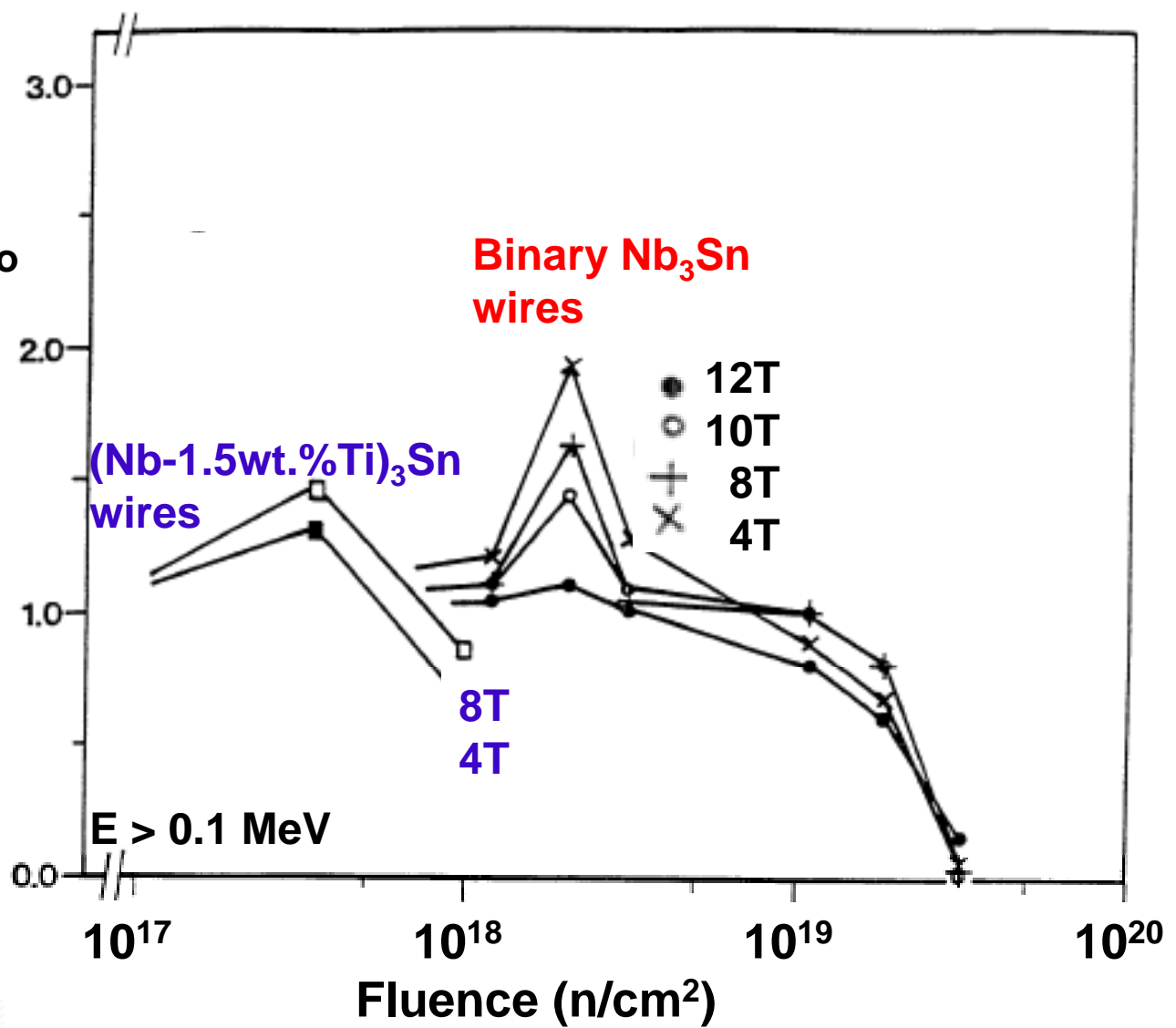
3) At $\phi t = 3 \times 10^{18}$ n/cm²:

I_c/I_{c0} for binary Nb₃Sn wire **higher** than before irradiation

but:

I_c/I_{c0} for to alloyed Nb₃Sn wires **lower** than before irradiation

J_c/J_{c0}



E > 0.1 MeV

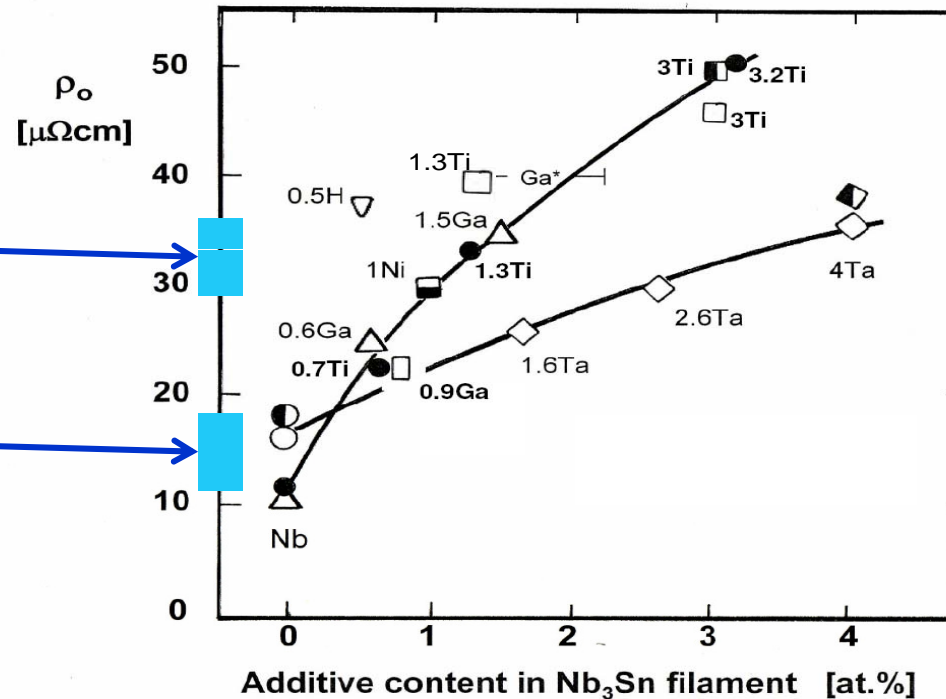
H.W. Weber, 1986, Adv. Cryo. Eng., Vol. 32, 853

Why Stronger Radiation Effects in Alloyed Nb₃Sn wires ?

1) Normal state electrical resistivity ρ_o before irradiation:

$\rho_o = 30 - 35 \mu\Omega\text{cm}$
Optimized Alloyed
Nb₃Sn wires

$\rho_o = 10 - 15 \mu\Omega\text{cm}$
Binary Nb₃Sn wires



R.Flükiger, C.Senatore, F.Buta,
D.Uglietti, B.Seeber, 2007
Superc. Sci. Technol. 21 054015

After Irradiation: $\Delta\rho_o$ much lower for alloyed Nb₃Sn wires

Consequences of lower $\Delta\rho_o$ for alloyed Nb₃Sn wires

- * The increase $\Delta(B_{c2})$ is smaller
- * The maximum value and B_{c2} is reached at lower ϕt_m values
- * The increase of I_c/I_{c0} at ϕt_m is smaller
- * Above fluences $\sim 0.5 \times 10^{18}$ n/cm², faster decrease of J_c

Conclusion

(Based on neutron irradiated Bronze Route wires of 1986, with $J_c \sim 700$ A/cm² at 12 T; has to be proven for Internal Sn or PIT wires)

For **higher fluences**, J_c of alloyed Nb₃Sn wires is **lower** than that of binary wires.

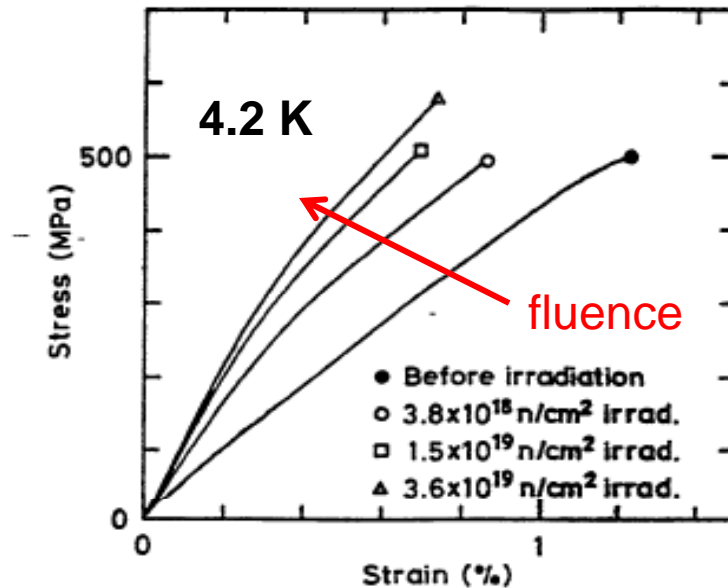
Threshold value: 3×10^{17} n/cm²

This effect is stronger for higher magnetic fields; important for high field accelerators, e.g. NED



Behavior of J_c under stress after irradiation

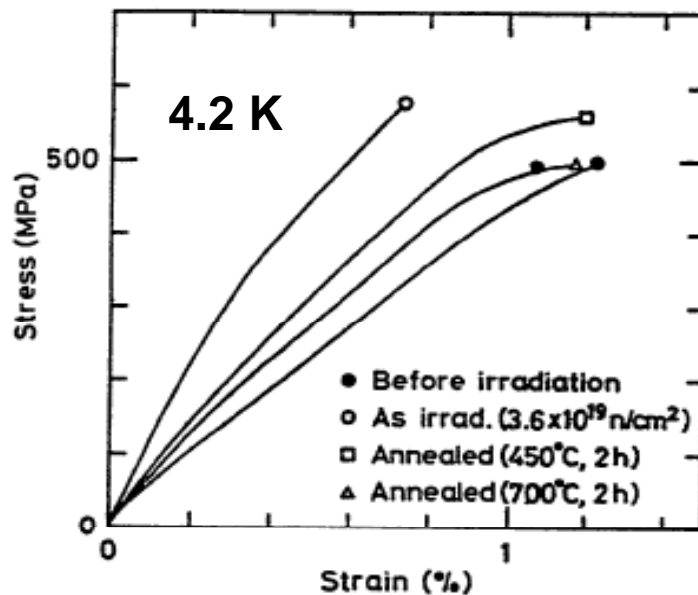
Stress – strain curves before and after irradiation



Bronze Route multifilamentary wire

$T_{\text{irr}} = 350$ K

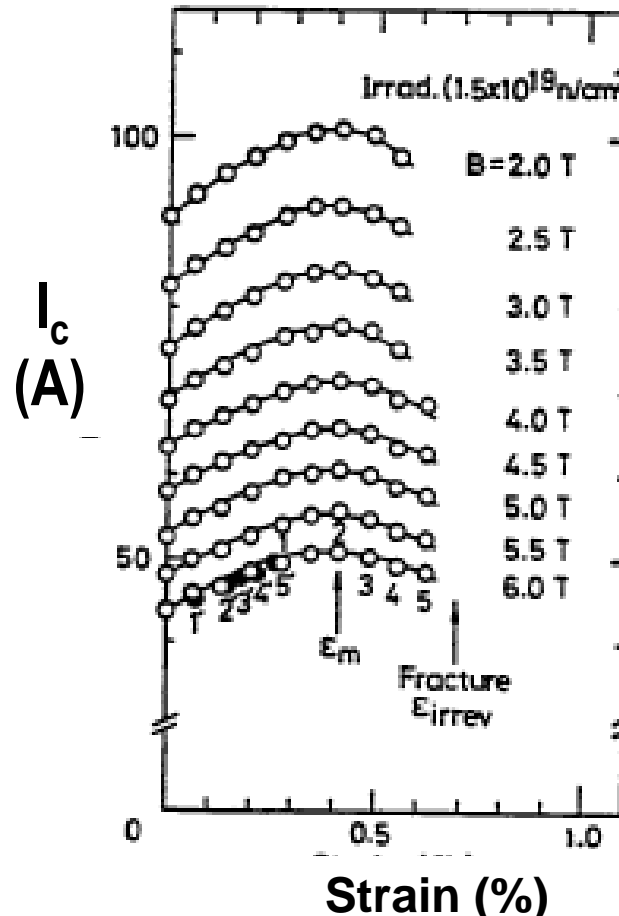
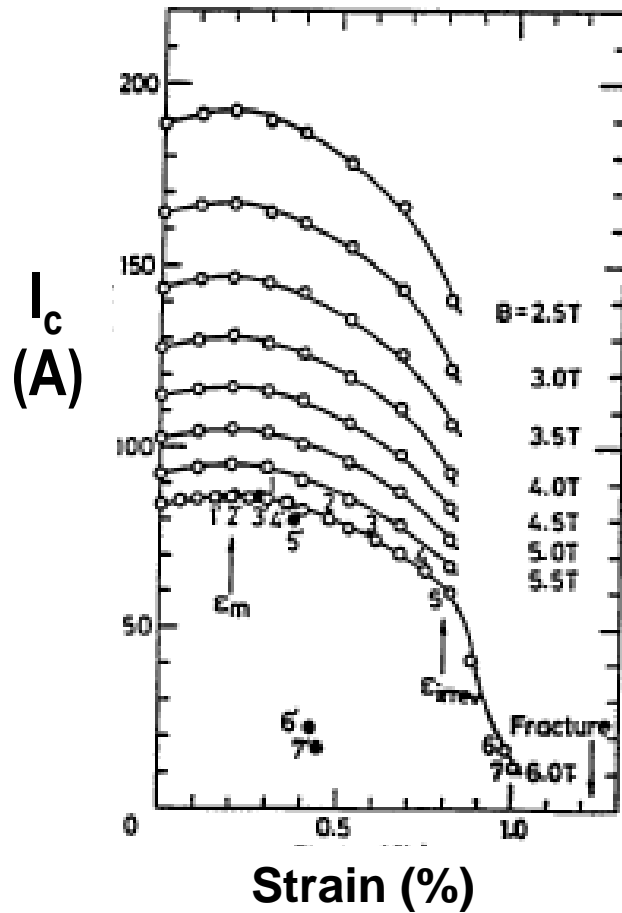
Hardening with higher fluence



Recovery after annealing at 450 and 700 °C

T. Okada, M. Fukumoto, K. Katagiri, K. Saito, H. Kodaka, H. Yoshida, IEEE Trans. Magn., MAG-23(1987)972

Effect of uniaxial tensile strain after irradiation

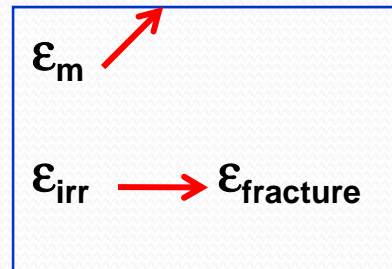
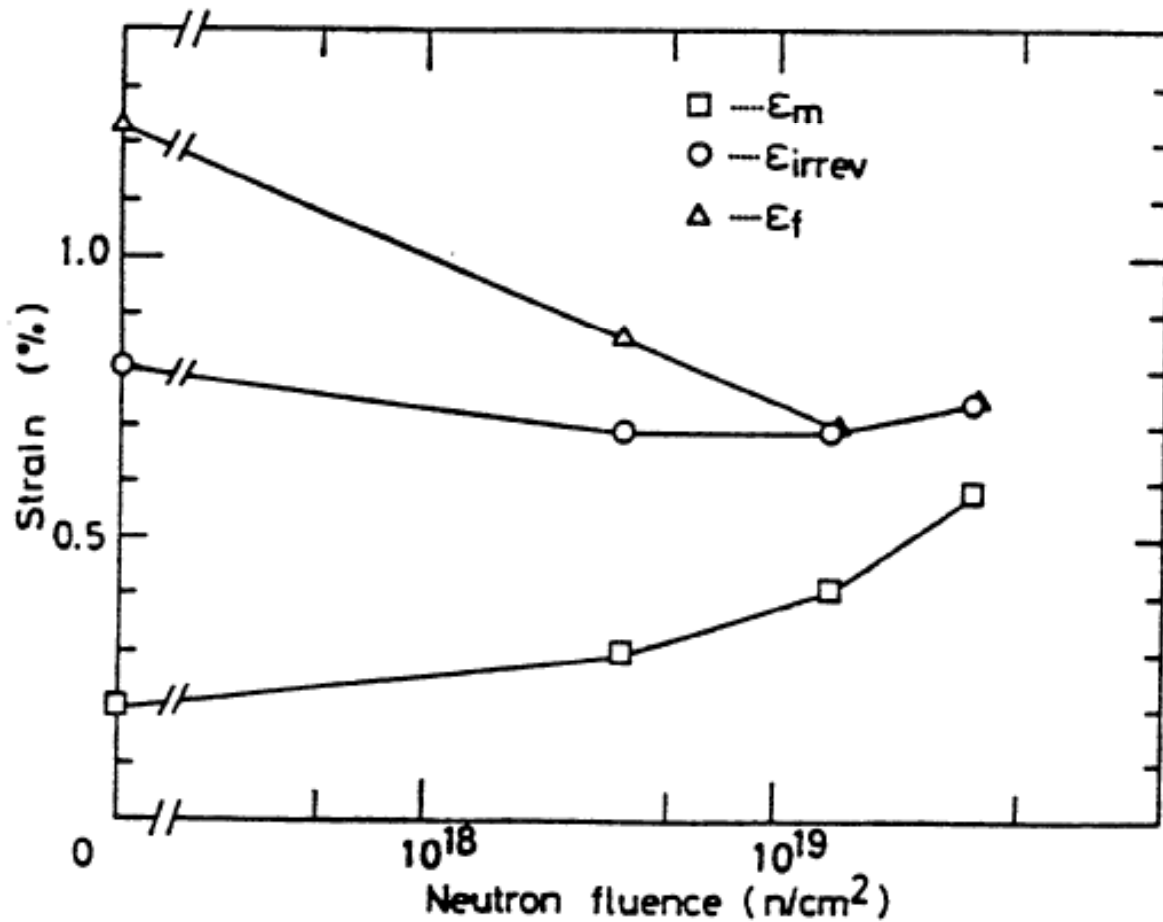


Bronze Route
 Multifilamentary
 Nb_3Sn wire

T. Okada, M. Fukumoto, K. Katagiri, K. Saito, H. Kodaka, H. Yoshida, IEEE Trans. Magn., MAG-23(1987)972

Mechanical Effects of Neutron Irradiation

Binary Nb₃Sn wires



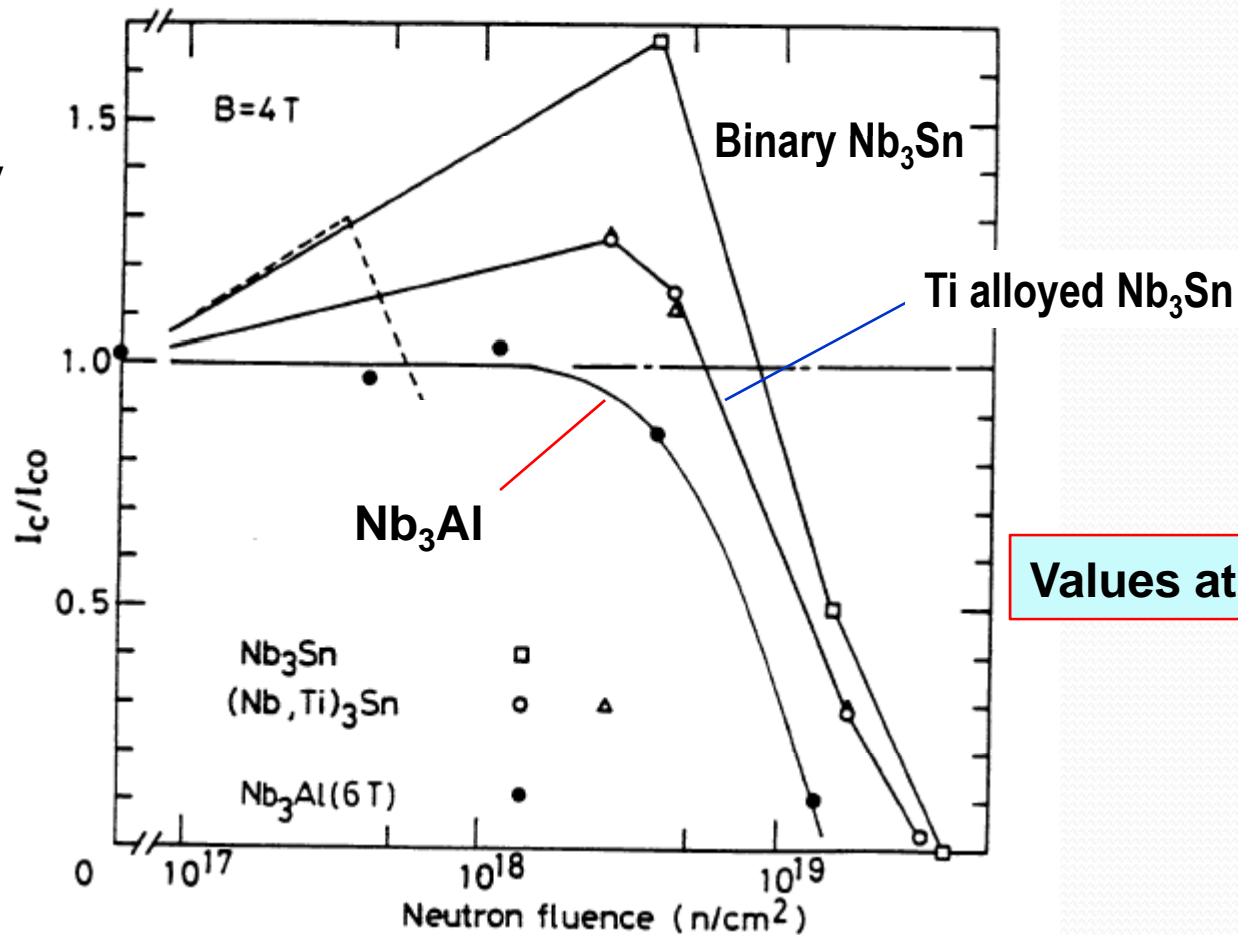
T. Okada, M. Fukumoto, K. Katagiri, K. Saito, H. Kodaka, H. Yoshida, IEEE Trans. Magn., MAG-23(1987)972

Effect of uniaxial tensile strain after irradiation

Ti alloyed Nb_3Sn wires

$E > 0.1$ MeV

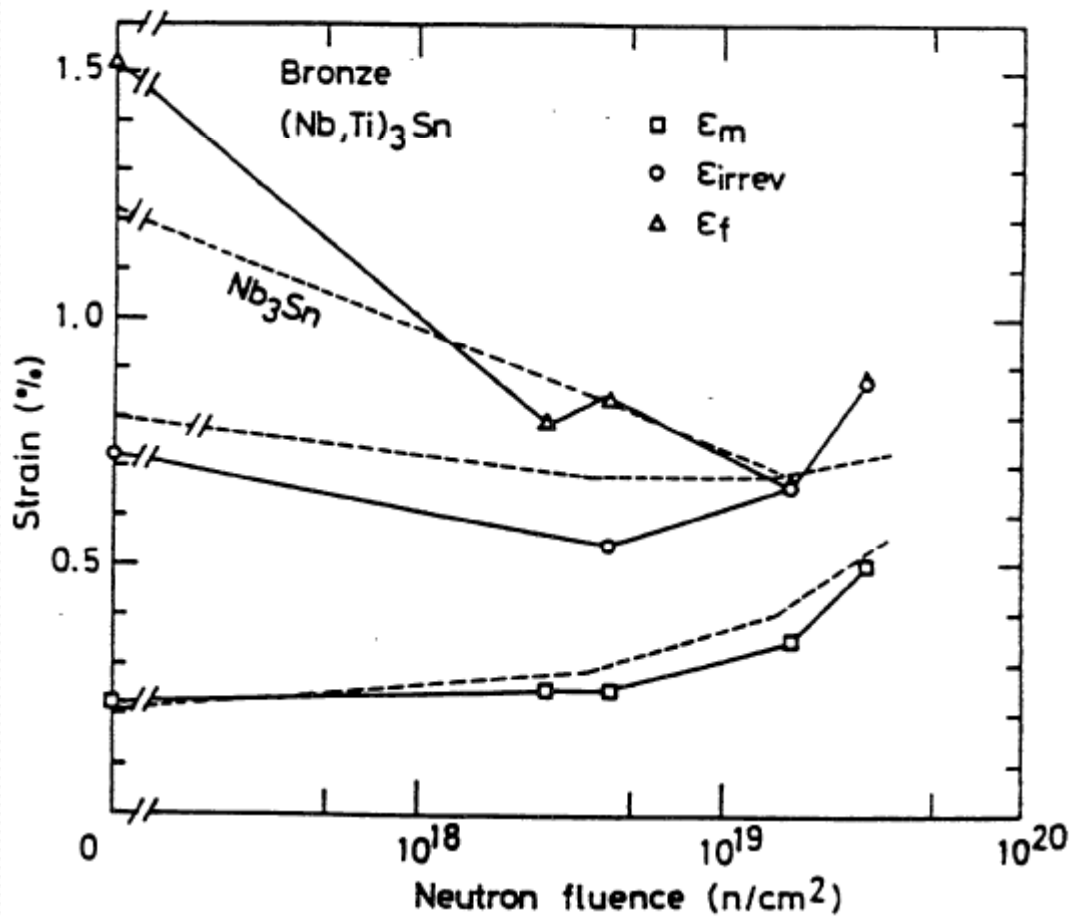
$T_{irr} = 300$ K



K. Katagiri, T. Okada, K. Noto, T. Kuroda, H. Kodaka, Fusion Eng. Design, 20(1993)423

Mechanical Effects of Neutron Irradiation

Ti alloyed Nb_3Sn wires



Increase of ϵ_m : not fully explained by hardening of bronze matrix

$\epsilon_m \nearrow$

$\epsilon_{irr} \rightarrow \epsilon_{fracture}$

Similar to binary wires

K. Katagiri, T. Okada, K. Noto, T. Kuroda, H. Kodaka, Fusion Eng. Design, 20(1993)423

Expected Radiation Load on the LHC Quadrupoles

Calculated for the Quadrupole Inner Winding by:

Francesco Cerutti , CERN

Alessio Mereghetti, CERN

Marco Mauri, CERN

Elena Widmer, CERN

Peak Fluence during Phase 1 Upgrade (2.5 x luminosity of $10^{34} \text{ cm}^{-2} \text{ s}^{-1}$)

TRIPLET Quadrupoles (Q1, Q2a, Q2b, Q3) are closer to Collision Point than Dipoles: **23 m**

Radiation spectrum close to Collision Point:

Pions, Neutrons, Photons, electrons, with energies $\gg 1 \text{ GeV}$
(Calculations of Mika Huhtinen, CERN)

Radiation spectrum at the Quadrupole site:

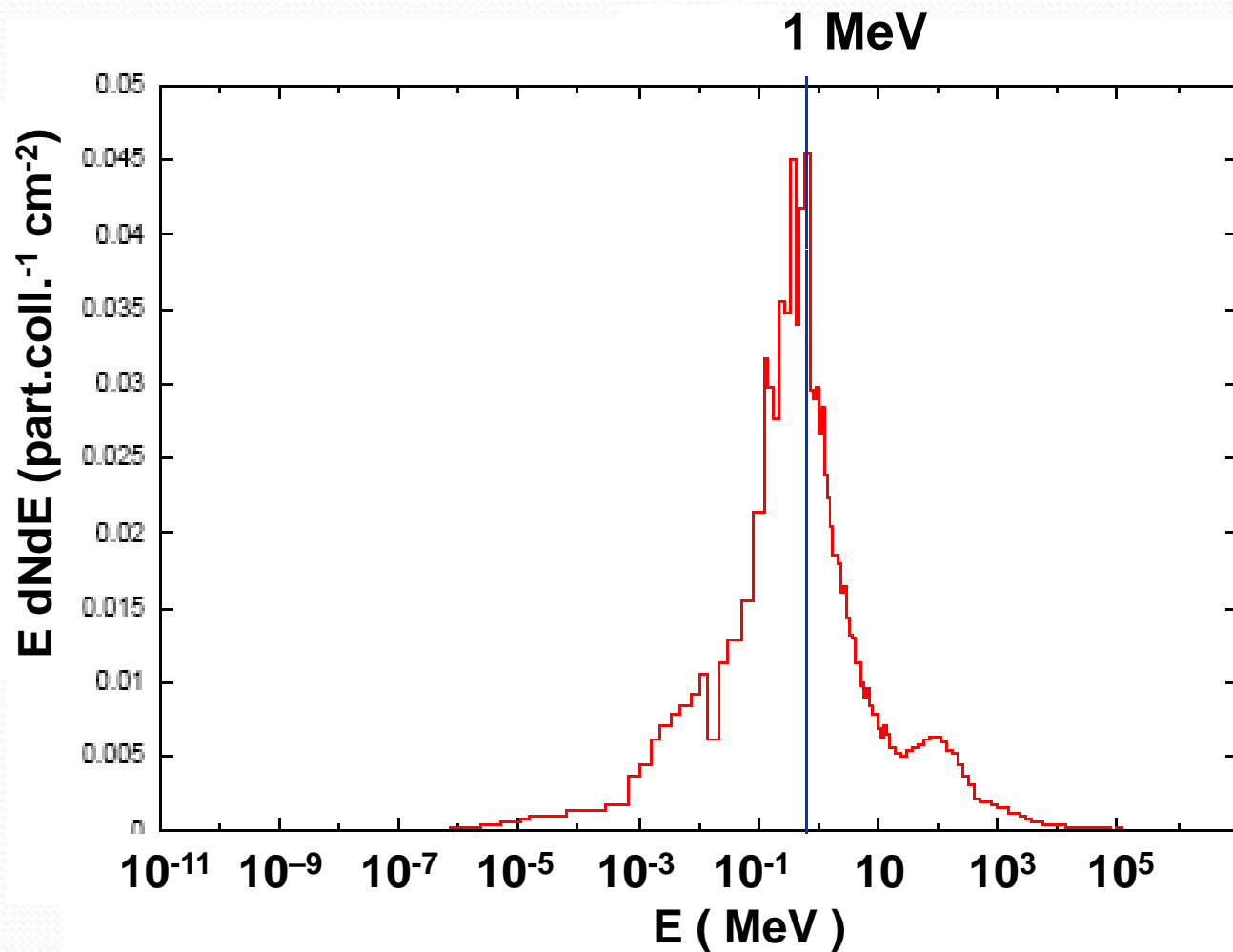
Very different, after interactions with various shielding materials:

Photons	87 %
Neutrons	6 %
Electrons	3.5 %
Positrons	2.5 %
Pions (+/-)	0.4 %
Protons	0.15 %

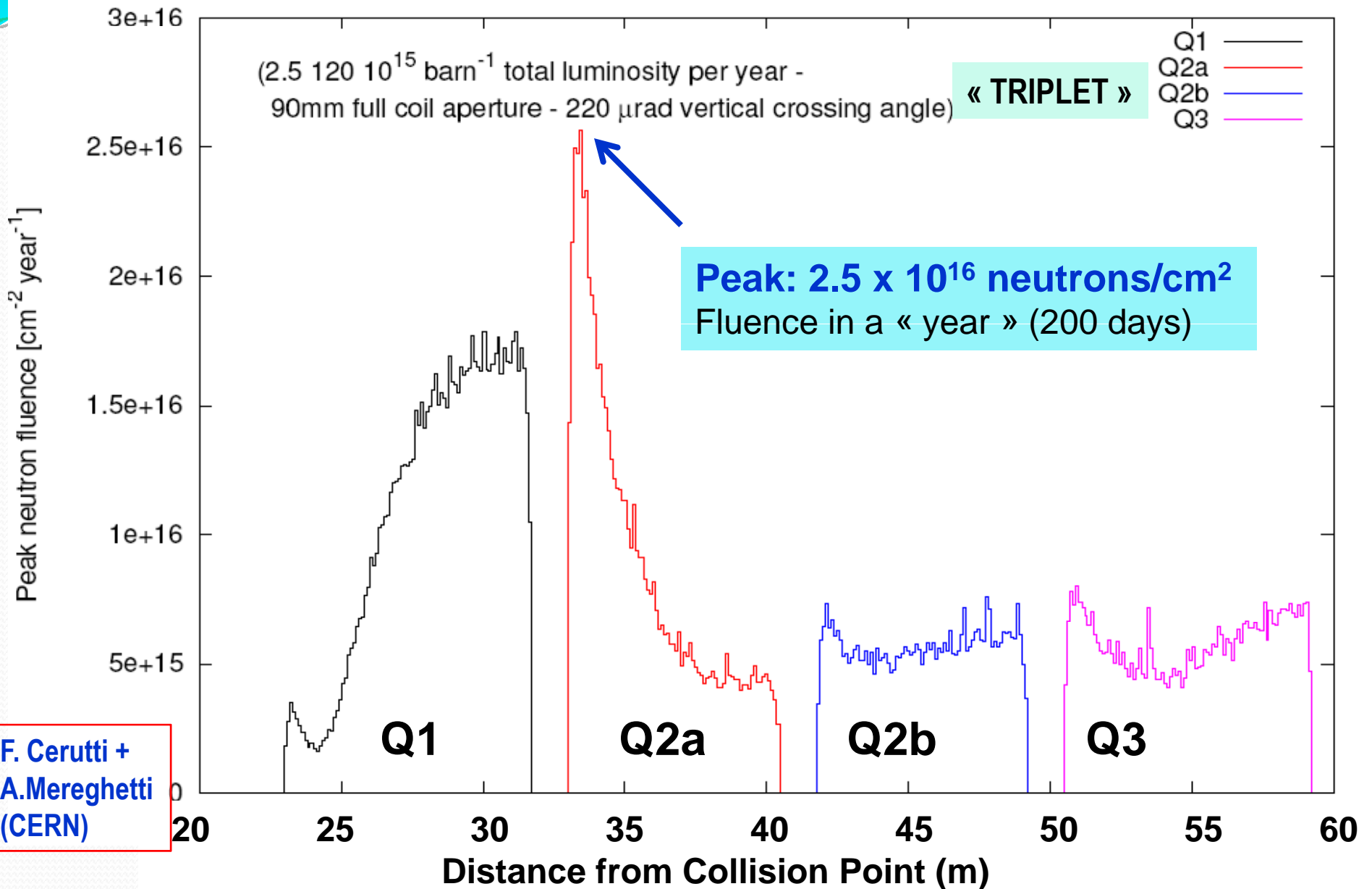
Neutrons are the main source of damage to the superconductors.
Photons have a much lower effect . Almost no pions.

Neutron spectrum in the inner winding of Quadrupole Q1

The neutron energy fully covers the possible interval, down to thermal energies



Neutron fluence in the inner winding of Quadrupoles (Phase 1 Upgrade)



Conclusions

High energy irradiation, in particular neutrons with $E > 0.1$ MeV:

- * NbTi wires are almost not affected
- * Nb₃Sn wires sensitive above 3×10^{17} n/cm² .

Alloyed Nb₃Sn wires more sensitive to radiation than binary wires

Reason: normal state resistivity ρ_0 .

Neutron Irradiation causes hardening of matrix and wire

Mechanical behavior of irradiated binary and alloyed Nb₃Sn wires is similar: ϵ_m increases.

Damage caused by low temperature irradiation can only partially be recovered at $T = 300\text{K}$

Little difference expected between irradiated Bronze Route, Internal Sn and PIT wires



Peak Fluence at Quadrupole Q2a: 2×10^{16} n/cm² after 1 year (Phase I upgrade)

For NbTi: no effect

Later, for Nb₃Sn wires:

Even after several years of operation, peak fluence remains below $> 1 \times 10^{18}$ n/cm².

Different fluences for Q1 - Q3: the operation conditions of these quadrupoles may have to be individually modified with time, for maintaining a constant field.

Ta is activated by neutron irradiation: For reducing induced radioactivity: minimize Ta in the wires.