

# IRRADIATION EFFECTS IN LOW $T_c$ SUPERCONDUCTORS

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## Abstract

The effects of neutron irradiation on the superconducting parameters  $T_c$ ,  $B_{c2}$  and  $J_c$  of  $Nb_3Sn$  are reviewed in view of the determination of the radiation limit in the LHC upgrade magnets. The variation of  $J_c$  in binary as well as in Ti and Ta alloyed  $Nb_3Sn$  wires is presented. The coexisting defect mechanisms in irradiated  $Nb_3Sn$  type compounds are briefly presented and a model is discussed explaining the site exchange mechanism which leads to a decrease of atomic ordering after irradiation.

Based on calculations of F. Cerutti and coworkers (CERN), the neutron fluence at the inner winding of the quadrupole Q2a is estimated to values below  $10^{18}$  neutrons/cm<sup>2</sup> for a life time of 10 years, which is within the safety margin with respect to the critical current density and  $B_{c2}$ .

## INTRODUCTION

The construction of future colliders with higher energies implies the use of superconducting dipoles and quadrupoles with increasing magnetic fields. As an example, the envisaged magnetic field in the LHC upgrade project will be as high as 15 T. At the present state of knowledge, such dipoles have to be wound on the basis of round wires, which limits the possible choice of industrially available superconducting materials to  $Nb_3Sn$ ,  $Nb_3Al$  (both crystallizing in the A15 type structure) and Bi-2212. However, Bi-2212 wires still exhibit weak mechanical properties, while  $Nb_3Al$  can be produced in kilometer lengths, but is not yet available in large quantities. The present paper will thus only consider the effect of high energy irradiation on the low  $T_c$  superconductor  $Nb_3Sn$ .

The question arises whether the intense radiation produced by the collisions in the high LHC upgrade energy collider has an influence on the magnetic fields produced by the superconducting dipoles and quadrupoles. Of particular interest for the present paper are the Phase I and Phase II upgrades, with a luminosity of  $2.5 \times 10^{34}$  cm<sup>-2</sup>s<sup>-1</sup> and  $10^{35}$  cm<sup>-2</sup>s<sup>-1</sup>, i.e. 2.5 and 10 times larger than nominal LHC, respectively. This question is treated based on recent calculations of the maximum neutron fluence (also called radiation dose in a number of other publications) acting on a well localized magnet location (the quadrupole). These calculations have been recently performed by F. Cerutti et al. [1] at CERN.

The present paper is a review about the known neutron irradiation data on  $Nb_3Sn$  wires, based on neutron irradiation experiments performed before 1986. After this date, irradiation works have been performed on HTS superconductors and more recently, on  $MgB_2$  [2]. The mechanism of irradiation effects in A15 type compounds will be discussed, and a model explaining the observed changes of the superconducting properties is presented. The variation of  $T_c$ ,  $B_{c2}$  and the electrical resistivity  $\rho_o$  of  $Nb_3Sn$  wires with radiation will be discussed, as well as the effects on the critical current density,  $J_c$ , with and without additives.

These data show that the effect of neutron radiation fluence on the critical current density of  $Nb_3Sn$  wires during 10 years, the estimated lifetime of the LHC upgrades, will not affect the critical current density of the  $Nb_3Sn$  wires. This is also valid for the quadrupole magnets Q2a, where the highest radiation fluence is expected [1] (see also Fig. 1).

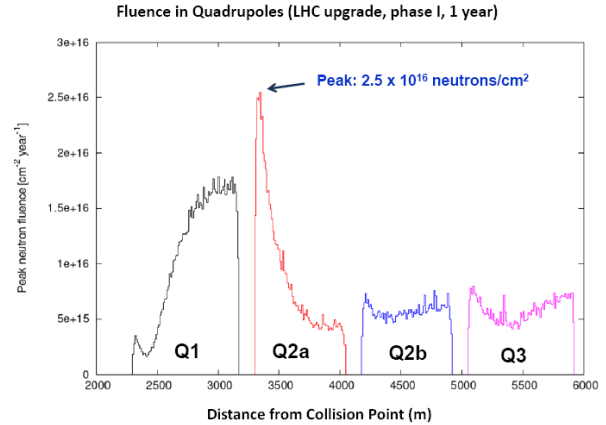


Figure 1: Calculated peak neutron fluence in phase I of LHC upgrade as a function of distance from the collision point, indicating a maximum for the inner winding of the quadrupole Q2a, as calculated by Cerutti et al. [1]).

## THE NEUTRON RADIATION FLUENCE AT THE INNER WINDING OF LHC QUADRUPOLES

The collisions in a high energy collider produce a very

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intense radiation, its intensity increasing with energy. Neutron radiation has a strong influence on all the components of the collider, i.e. the superconductor, the stabilizer and the insulator. It is well-known that the superconducting properties of most superconductors depend on the radiation fluence, and the question arises whether significant radiation-induced effects (e.g. decreased values of  $T_c$  and of the critical field, increased resistivity, etc.) will lead to a reduced magnet performance within the time of operation, which may reach several years.

When calculating these effects, it is important to know the spectrum of the various radiations interacting with the magnets. At the collision site, a very strong radiation environment will be created. Estimates for the produced radiation at the collision site yield particle energies up to 10 GeV, the radiation being composed by charged pions, protons, neutrons, photons, electrons,.... [3]. It follows that adequate shielding is vital in order to reduce these radiations to an acceptable level. Taking into account the planned shielding conditions as well as the distance between the collision site and the magnets, the maximum radiation load acting on the magnets has been recently calculated by Cerutti et al. [1]. It was found that after interaction with the shielding material, the radiation spectrum reaching the closest magnets (the quadrupoles) will be composed by:

Photons	87 %
Neutrons	6 %
Electrons	3.5 %
Positrons	2.5 %
Pions (+/-)	0.4 %
Protons	0.15 %.

It has been shown that neutron radiation has a strong effect on the superconducting properties of  $Nb_3Sn$ , while the effect of photons, electrons and photons is negligible. Since the total amount of pions and protons does not exceed 10% of the calculated intensity for neutrons, the present estimation will be done under the assumption that neutrons are the main source of damage to the superconductors. All other radiation sources will be neglected when considering the effect on the superconductor. Their effect on the insulator materials has to be analyzed separately and will not be treated in the present paper.

The calculations of Cerutti et al. [1] show that the neutron energy has a pronounced peak around 1 MeV. The neutron energies used in the previous works studying the effects of radiation damage on the superconducting properties of superconductors vary between 1 and 14 MeV (Sweedler et al. [4]) and 14 MeV (Weber et al. [5], Guinan et al. [6] and Weiss et al. [7]). A comparison between the various known data shows that within this energy range, one does not expect a strong difference between the effects of neutron radiation on the

superconducting properties. As shown in Fig. 1, the highest fluence will be reached at the inner winding of the quadrupole Q2a, at a distance of 33 m from the collision point. The expected maximum radiation fluence was calculated to  $2 \times 10^{16}$  n/cm<sup>2</sup> per year, assuming an operation of 200 days a year. For a total operation time of 10 years, the maximum fluences at the inner winding of the quadrupole Q2a after the upgrades of Phase I and Phase II will thus be  $2.5 \times 10^{17}$  n/cm<sup>2</sup> and  $10^{18}$  n/cm<sup>2</sup>, respectively. In Section VI, the effect of these fluences on  $T_c$  and  $J_c$  will be analyzed for both, binary and alloyed  $Nb_3Sn$  wires. An explanation for the higher sensitivity to radiation damage for alloyed  $Nb_3Sn$  wires with respect to binary wires will be discussed.

## THE EFFECTS OF NEUTRON IRRADIATION ON SUPERCONDUCTORS

### *Effect on $T_c$ of various superconducting compounds*

As mentioned above, the main damage at the magnet site in LHC upgrade phase I is expected to be caused by neutron irradiation. The overwhelming amount of neutron irradiation data of Low  $T_c$  (or LTS) superconductors has been performed prior to 1987, after which most work was performed on High  $T_c$  (or HTS) compounds. In Fig. 2, the variation of  $T_c$  vs.  $\phi t$  is shown for the most known Low  $T_c$  superconductors: Laves phases ( $HfV_2$ ) [9], Chevrel phases ( $PbMo_6S_8$ ) [10],  $MgB_2$  [2].  $T_c$  for  $NbTi$  [8] is not shown here, but is even less radiation sensitive than  $V_2Hf$ .

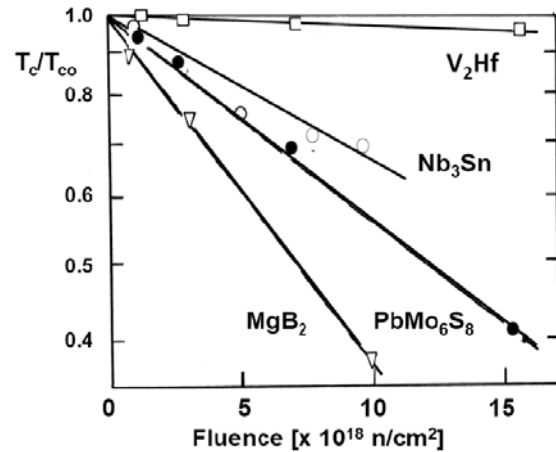


Figure 2: Variation of  $T_c$  vs. neutron fluence,  $\phi t$ , for various known low  $T_c$  superconductors. Laves phases ( $HfV_2$ ) [9], Chevrel phases ( $PbMo_6S_8$ ) [10],  $Nb_3Sn$  [4],  $MgB_2$  [2].

Although  $NbTi$  and  $HfV_2$  are little affected by neutron radiation, these materials must be excluded due to their too low  $H_{c2}$  values. Chevrel phases exhibit very high  $H_{c2}$ , but never reached the industrial level. In addition, they exhibit a relatively low  $T_c$  value (14 K in wires) and

astronger radiation sensitivity with respect to Nb<sub>3</sub>Sn. MgB<sub>2</sub> has also a stronger sensitivity to neutron irradiation than Nb<sub>3</sub>Sn, but the value of  $B_{irr}$  is not high enough for magnets producing 15 T.

The data for the HTS compounds Bi-2212, Bi-2223 and Y-123 are not shown here, but it must be noted that even if they show a relatively strong decrease of  $T_c$  with neutron fluence, this would be of little importance for operation at 4.2 K. Indeed,  $T_c$ ,  $J_c$  and  $B_{c2}$  would still be sufficiently high for this temperature. As mentioned above, mechanical stability for Bi-2212 and the tape geometry for Bi-2223 and Y-123 are at present important obstacles excluding their use in collider magnets.

### Radiation effects on $T_c$ of several A15 type compounds

It appears from Fig. 2 that Nb<sub>3</sub>Sn is well suited for being used in LHC upgrade, no significant decrease of  $T_c$  being observed up to radiation fluences up to  $10^{18}$  n/cm<sup>2</sup>. The decrease of  $T_c$  in various A15 type compounds as a function of the irradiation fluence,  $\phi$ , for neutrons with  $E \leq 1$  MeV at irradiation temperatures  $T_{irr} \leq 150^\circ\text{C}$  is represented in Fig. 3. The data on V<sub>3</sub>Si, Nb<sub>3</sub>Ge, Nb<sub>3</sub>Al, Nb<sub>3</sub>Pt, Nb<sub>3</sub>Ga and Mo<sub>3</sub>Os are extracted from Sweedler et al. [4,14], while V<sub>3</sub>Ga was analyzed by Francavilla et al. [15] and Mo<sub>40</sub>Tc<sub>60</sub> by Giorgi et al. [16]. It is remarkable that the variation of  $T_c$  with  $\phi$  is very similar for V<sub>3</sub>Si, Nb<sub>3</sub>Ge, Nb<sub>3</sub>Al, Nb<sub>3</sub>Pt, Nb<sub>3</sub>Ga and V<sub>3</sub>Ga, in contrast to Mo<sub>3</sub>Os and Mo<sub>40</sub>Tc<sub>60</sub>, where the decrease of  $T_c$  is considerably smaller.

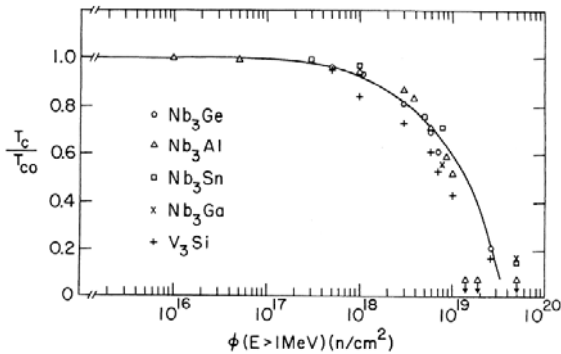


Figure 3:  $T_c$  as a function of neutron fluence ( $E \leq 1$  MeV,  $T_{irr} \leq 150^\circ\text{C}$ ) for various A15 type compounds (all data from Sweedler et al. [4]).

From X ray diffractometry, Sweedler et al. [4,14] concluded that the decrease of  $T_c$  at doses up to  $10^{19}$  n/cm<sup>2</sup> (where  $T_c/T_{c0} \sim 0.5$ ) is mainly caused by a decrease of the long-range atomic order parameter, S.

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observations, revealing the presence of depleted zones in irradiated samples. As previously shown in an unpublished Internal Report (Flükiger [18]), calorimetric measurements constitute a definitive proof for the validity of the “disordering” model proposed by Sweedler et al. [4,14]. This will be discussed in detail in the following.

### Irradiation temperature

At 1.8 K, the operation temperature of LHC and LHC upgrades, vacancies show any mobility, and site exchanges can only occur by the energy of transmitted by the multiple collisions. An increase of the irradiation temperature,  $T_{irr}$ , will lead to self-annealing effects. There is no complete series of measurements on irradiations at  $T < 10$  K and  $T > 300\text{K}$ , and a comparison can only be made using the data of different authors, who worked at with neutrons of different energies, between 0.1 and 14 MeV. The conversion from 0.1 to 14 MeV is problematic, and several approaches to find appropriate conversion factors have given unsatisfactory results. For this reason, the nominal fluences will be used for the present comparison, well knowing that a certain error is introduced.

Söll et al. [19] performed neutron irradiations ( $E > 0.1$  MeV) of Nb<sub>3</sub>Sn diffusion wires at 4.6 K and moved the samples from the irradiation position to the test cryostat without warmup. The irradiation was performed up to a fluence of  $3.9 \times 10^{18}$  n/cm<sup>2</sup>, after which a  $T_c$  reduction of 0.8 K was observed. After irradiation at  $>150^\circ\text{C}$  (in reality, the temperature before irradiation was 300 K) to  $10^{18}/\text{cm}^2$  ( $E > 1$  MeV), Sweedler et al. [4] reported a similar decrease in  $T_c$ , which indicates that changes in superconducting properties of Nb<sub>3</sub>Sn after irradiation at  $> 150^\circ\text{C}$  may be similar to effects of 4.6 K irradiation. This was later roughly confirmed by  $J_c$  measurements by Hahn et al. [20]. Söll et al. [21] extended their cryogenic irradiations to a fast neutron fluence of  $10^{19}$  n/cm<sup>2</sup> ( $E > 0.1$  MeV) at  $T_{irr} \sim 10$  K. A slight extrapolation of their results reveals that a fluence of  $\sim 1.2 \times 10^{19}$  n/cm<sup>2</sup> would be required to reduce  $T_c$  to 13.5 K, the value obtained by Sweedler et al. [4] at  $>150^\circ\text{C}$  after a higher fluence of  $5 \times 10^{18}$  n/cm<sup>2</sup> ( $E > 1$  MeV). Again, this confirms that there is a small, but not negligible difference between the decrease of  $T_c$  after irradiation at  $\sim 10$  K and at  $> 150^\circ\text{C}$ . It follows that there is only a weak recovery from 4.2 K to room temperature.

Meier-Hirmer and Küpfer [22] irradiated V<sub>3</sub>Si single crystals with fast neutrons at  $240^\circ\text{C}$ . As shown in Fig. 4, the decrease of  $T_c$  with increasing fluence  $\phi$  is substantially reduced for  $T_{irr} = 240^\circ\text{C}$  [22] when compared with data taken at  $T_{irr} \leq 150^\circ\text{C}$  by Sweedler et al. [23]. The observed lower decrease of  $T_c$  after heavy irradiation fluences with higher  $T_{irr}$  values has its origin in thermal recombination effects during irradiation. The data in Fig. 4 show that the activation of vacancies at between

$T_{\text{irr}} \leq 150$  and  $240$  °C has the effect of an annealing which increases the long-range order parameter of the crystal.

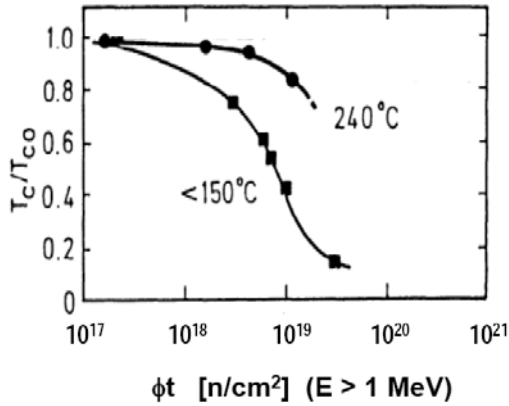


Figure 4:  $T_c$  of  $V_3Si$  as a function of fast neutron irradiation fluence  $\phi_t$  for various irradiation temperatures.  $T_{\text{irr}} \leq 150^\circ\text{C}$  (Sweedler et al. [23],  $T_{\text{irr}} = 240^\circ\text{C}$  (Küpfer et al. [22])).

## COEXISTING DEFECT MECHANISMS IN IRRADIATED A15 TYPE COMPOUNDS

From the wealth of published data, it follows that the decrease of  $T_c$  in irradiated A15 type compounds has been attributed to three competing defect mechanisms. These mechanisms are analyzed in the following.

### *Homogeneous Defects (decrease of long-range atomic ordering)*

The "defects" are here lattice sites occupied by the wrong atoms (in analogy to the quenched state), also called "antisite defects". A decrease of the long-range order parameter  $S$  (defined by van Reuth et al. [24] in irradiated A15 compounds was first observed by Sweedler and Cox [23] in  $Nb_3Al$ . It was later confirmed by Moehlecke et al. [25] for  $Nb_3Pt$  and by Cox and Tarvin [26] for  $V_3Si$ , while Schneider et al. [27] reported a decrease of  $S$  in  $Nb_3Al$  after irradiation with 700 keV  $N^{2+}$  ions. It is important to note that the attribution of the observed effects on the superconducting properties of A15 type compounds after irradiation to a change of atomic ordering implies the assumption of *homogeneous* disordering over the sample volume. The decrease of  $T_c$  is explained by changes of the electronic density of states at the Fermi level.

### *Inhomogeneous defects (disordered microregions or "depleted zones")*

The defects are represented by the depleted zones of 4 nm diameter, generally observed by means of TEM microscopy in solids after high energy irradiation [17]. The depleted zones can be either highly disordered or amorphous, and were also called "disordered

microregions" by Pande [17, 24]. The presence of inhomogeneities was also observed by Nikulin et al. [29], by means of small angle neutron scattering. The inhomogeneous defect mechanism [17] assumes that the matrix enclosing the depleted zones is essentially unaffected by the radiation, in contrast to the antisite defect mechanism (disordering) [14,18], which is based on a homogeneous decrease of the atomic order parameter over the whole sample volume.

As pointed out by Pande [17], the weakening of A15 superstructure lines after irradiation, (which is interpreted as a decrease of  $S$  [14,18], could also arise from an increasing volume fraction of disordered microregions (also called depleted zones), concentrated in regions of  $\sim 5$  nm diameter. The inhomogeneous defect mechanism explains an overall degradation of the superconducting properties by the proximity effect [17] between the ordered, high  $T_c$  matrix and the disordered low  $T_c$  microregions of a size comparable to the coherence length,  $\xi_0 \sim 4$  nm.

### *Static Displacement of the Atoms from their Equilibrium Positions*

This kind of defect was first observed by Meyer [30] and Testardi et al. [31] after heavy irradiation of  $V_3Si$  single crystals by means of the channeling technique. The existence of all three defect types  $\alpha$ ,  $\beta$  and  $\gamma$  is based on sound experimental data. It is also ascertained that all three types of defects occur simultaneously during irradiation. In the past, each of these defects has been independently made responsible for the decrease in  $T_c$ . Depending on the total radiation fluence, each one of these defect types will be dominant over the concurrents. As will be shown in the following, antisite defects (or decreasing atomic ordering) are mainly responsible for the observed decrease of  $T_c$  for radiation doses up to  $\sim 10^{19}$  n/cm<sup>2</sup>, while inhomogeneous defects and static displacement are dominant for higher doses, where the value of  $T_c$  is too low for being of interest for the present considerations. The effects of high energy radiation on A15 type compounds are complex and are schematically represented in Fig. 5.

### *Volume change after irradiation*

The number of vacancies in unirradiated A15 type compounds at 300K is generally below  $2 \times 10^{-3}$ , the experimental error limit. This is in agreement with other dense structures, for which vacancy concentrations of the same order of magnitude have been reported. The only case where a measurable amount of vacancies could be produced in A15 crystals was reported by Cox and Tarvin [26], who found that the density of a  $V_3Si$  single crystal after a fast neutron irradiation dose of  $22.2 \times 10^{18}$  n/cm<sup>2</sup> decreased by -0.3%. This observation allows the estimation whether a lattice expansion of  $Nb_3Sn$  filaments

after irradiation has to be taken into account for LHC upgrade II.

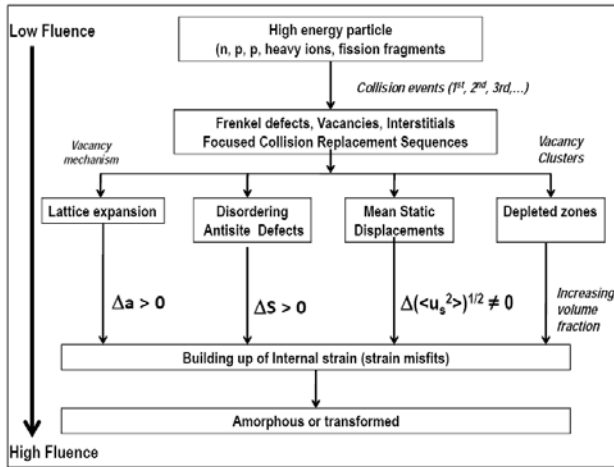


Figure 5: Schematic representation of the radiation induced effects in A15 type compounds, with increasing fluence (R. Flükiger [18]).

Assuming a total fluence of  $10^{18}$  n/cm<sup>2</sup>, on the quadrupole Q2a after 10 years of operation, the decrease of density inside the Nb<sub>3</sub>Sn filaments is estimated to - 0.03%. This would correspond to a volume expansion of + 0.03%, and thus of a linear expansion of ~ 0.01%, thus creating an additional stress acting on the filaments. A comparison with the effect of uniaxial stress or compressive transverse stress on  $J_c$  of Nb<sub>3</sub>Sn wires shows that an increase of stress by 0.01 % as a consequence of irradiation would cause a small, but non negligible effect on  $J_c$ . Additional precise irradiation measurements should be performed on multifilamentary Nb<sub>3</sub>Sn wires samples, not only as single wires but in the same configuration as in the cable, comprising all reinforcing and insulating elements. This rough estimation shows that the additional stress effect due to radiation damage on  $J_c$  after 10 years of operation of LHC upgrade phase II may be below 5%.

### CORRELATION BETWEEN ANTISITE DEFECTS AND $T_c$ AFTER NEUTRON IRRADIATION

Several arguments can be invoked for proving the validity of antisite disorder as the dominant mechanism influencing the variation of  $T_c$  vs.  $\phi t$  for radiation doses up to ~  $10^{19}$  n/cm<sup>2</sup>:

- Homogeneous distribution of the antisite defects over the whole sample after irradiation, detected by specific heat measurements;
- Comparison between the variation of  $T_c$  vs. the order parameter S for A15 type compounds after irradiation and after fast quenching from high temperatures (in both cases, S is measured by diffraction methods);

- Irradiation with high energy electrons and neutrons.

### Homogeneous distribution

The question about a *homogeneous* distribution of the damage can be answered on the basis of the known low temperature specific heat measurements before and after irradiation for the A15 type compounds Nb<sub>3</sub>Sn [32], Nb<sub>3</sub>Al [33] and V<sub>3</sub>Si[34].

The measurements of Cort et al. [33] for Nb<sub>3</sub>Al are represented in Fig. 6, showing the specific heat jump at  $T_c$  after irradiation at 150°C at a fluence of  $13 \times 10^{18}$  n/cm<sup>2</sup>. The transition width was found to increase from 0.8 to 1.3 K, for a significant decrease of  $T_c$  from 18 to 10K. The compound V<sub>3</sub>Si was studied by calorimetry by Viswanathan et al. [34] after neutron irradiation at 200°C at a fluence of  $22.2 \times 10^{18}$  n/cm<sup>2</sup>. A decrease of  $T_c$  from 17 to 7.5 K was found, the width  $\Delta T_c$  increasing slightly from 0.5 to 1.2 K. The specific heat measurements of Karkin et al. [32] on Nb<sub>3</sub>Sn before and after neutron irradiation are shown in Fig. 7. These authors studied the effect of neutron irradiation at 80°C in Nb<sub>3</sub>Sn. At a dose of  $10^{19}$ n/cm<sup>2</sup> they found a  $T_c$  value of 12.5 K, while the transition width  $\Delta T_c$  measured by specific heat increased from 0.8 to 2.5 K.

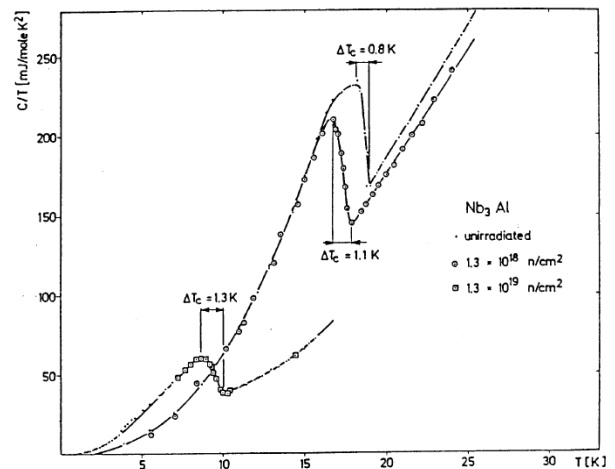


Figure 6: Specific heat of Nb<sub>3</sub>Al before irradiation and after neutron doses of  $1.3 \times 10^{18}$  and  $1.3 \times 10^{19}$  n/cm<sup>2</sup>, respectively. The linear representation  $C/T$  vs.  $T$  has been chosen in order to visualize the moderate increase in  $\Delta T_c$  with dose (after Cort et al. [33]).

Table 1. Specific heat data of the compounds  $\text{Nb}_3\text{Sn}$ ,  $\text{V}_3\text{Si}$  and  $\text{Nb}_3\text{Al}$  after neutron irradiation. Indicated are the  $T_c$  values before and after irradiation as well as the transition width  $\Delta T_c$ .

Compound	Mass (g)	$T_{co}$ (K)	$T_{irr}$ (°C)	Fluence	$T_c$ (K)	$T_c/T_{co}$	$\Delta T_c$
$\text{Nb}_3\text{Sn}$	11.0	17.9	80	$10 \times 10^{19}$	12.5	0.69	2.5 [28]
$\text{Nb}_3\text{Al}$	0.2	18.7	150	$13 \times 10^{19}$	9.6	0.51	0.5 [29]
$\text{V}_3\text{Si}$	1.5	17.1	200	$22 \times 10^{19}$	7.5	0.44	0.7 [30]

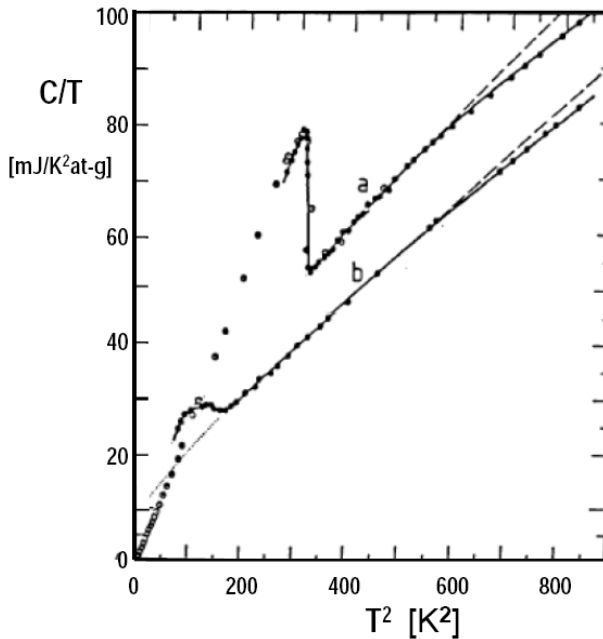


Figure 7: Specific heat of  $\text{Nb}_3\text{Sn}$ , a) in the unirradiated state and b) after a dose of  $10^{19} \text{ n/cm}^2$  according to Karkin et al. [32]. For unirradiated  $\text{Nb}_3\text{Sn}$  at lower temperatures, data of Junod et al. [35] have been superposed.

When comparing the transition width of superconducting compounds after irradiation, one has to take into account the nuclear heat recovery, which depends on the size of the sample. Viswanathan et al. [34] pointed out that  $\text{V}_3\text{Si}$  single crystals with masses of  $\geq 1 \text{ g}$  exhibited additional heating during irradiation, leading in one case even to a visible darkening of the surface, i.e. to estimated temperatures  $T_{irr}$  of  $300^\circ\text{C}$  and above. This is due to increasing difficulties in transferring the nuclear heat to the sample environment (Argon gas) with increasing volume to surface. The masses of  $\text{V}_3\text{Si}$  and  $\text{Nb}_3\text{Al}$  were 1.5 and  $\sim 1 \text{ g}$ , respectively, in contrast to  $\text{Nb}_3\text{Sn}$ , which had 11 g [32]. The latter had a  $T_c$  value of 12.5 K, which is markedly higher than 9.9 K, the value estimated from the behavior of  $T_c$  vs.  $\phi t$  for small samples in Fig. 3.

The corresponding values for  $\text{Nb}_3\text{Al}$  and  $\text{V}_3\text{Si}$  are 9.6 and 7.6 K, which is in good agreement with the values reported in Table 1. It can thus be estimated that the increase of  $T_c$  due to nuclear heat recovery at  $\phi t = 10^{19} \text{ n/cm}^2$  for this “heavy”  $\text{Nb}_3\text{Sn}$  samples is  $\sim 1.5 \text{ K}$ . It follows that for the 3 systems  $\text{Nb}_3\text{Sn}$ ,  $\text{Nb}_3\text{Al}$  and  $\text{V}_3\text{Si}$ , heavy neutron irradiations up to fluences of  $2 \times 10^{19} \text{ n/cm}^2$

only causes a very small enhancement of the transition width,  $\Delta T_c$ . It is interesting that for a neutron fluence reducing  $T_c$  to about 50% of the initial value, the transition width  $\Delta T_c$  is only enhanced by  $\leq 1 \text{ K}$ .

In the specific heat curves, there is no trace of the original superconducting transition temperature,  $T_{co}$ , in any of the 3 systems  $\text{Nb}_3\text{Sn}$ ,  $\text{Nb}_3\text{Al}$  and  $\text{V}_3\text{Si}$  after irradiation. This implies that the amount of depleted zones (with considerably lower  $T_c$ ) is very small and cannot account for the observed decrease of the superstructure lines. After having shown that the damage is homogeneous, this is a strong argument in favour of the antisite defect mechanism as the dominant one up to  $10^{19} \text{ n/cm}^2$ .

#### Comparison between irradiated and quenched A15 type compounds

Quench induced disordering constitutes a particularly simple case, where the only possible defects are the antisite defects (up to a few %) and quenched-in vacancies ( $\leq 0.02\%$  at  $300 \text{ K}$ ). No direct comparison between neutron irradiation and quenching has been performed on  $\text{Nb}_3\text{Sn}$  and the data reported here concern the system  $\text{Nb}_3\text{Pt}$ , another A15 type compound.

Fig. 8 shows the variation of  $T_c$  for  $\text{Nb}_3\text{Pt}$  vs. the long-range order parameter,  $S$ , after fast quenching from temperatures up to  $1900^\circ\text{C}$  by Flükiger et al. [36] and after from neutron irradiation ( $E > 1 \text{ MeV}$ ) by Moehlecke et al. [37].

It follows from Fig. 8 that the variation of  $T_c$  vs.  $S$  is the same, regardless whether the compound was fast quenched or irradiated. This constitutes an additional argument in favour of variations of the degree of atomic order for the observed decrease of  $T_c$  after irradiation up to fluences of  $10^{19} \text{ n/cm}^2$ .

#### Irradiation with High Energy Electrons and Neutrons

According to Seeger [38], the complex situation in an irradiated crystal can be described as follows. The high energy particle transfers a kinetic energy,  $E_T$ , to an atom of the target, the primary knock-on atom. At sufficiently high values of  $E_T$ , this atom will be removed from its equilibrium lattice site: a Frenkel defect is formed. Due to inelastic collisions with electrons, the energy of the primary knock-on atom towards the end of its path falls to values of the order of  $E$ , the displacement energy ( $\sim 25 \text{ eV}$ ), and almost every collided atom is displaced [39].

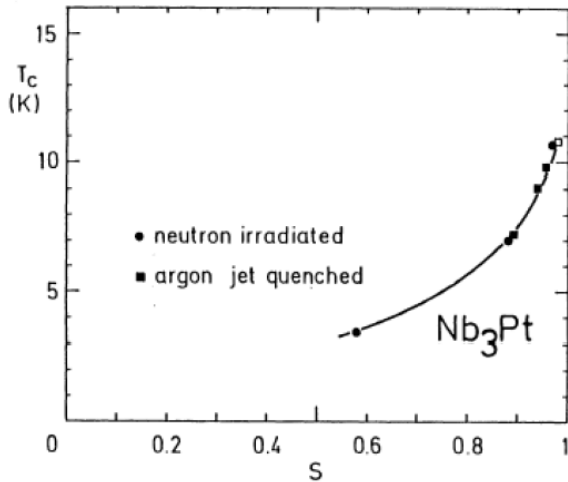


Figure 8;  $T_c$  vs. long-range order parameter  $S$  (determined by X ray diffraction) for  $Nb_3Pt$  after fast quenching from different temperatures [36] and after neutron irradiation [37].

As a result of this displacement cascade, regions with high concentrations of vacancies are formed, called "depleted zones" by Seeger [38], which are surrounded by a zone enriched with interstitial atoms. In A15 type compounds, the existence of depleted zones has first been reported by Pande [17,24], who called them "disordered microregions". In reality, the structure of this region can be either amorphous, of the A15 type (but strongly disordered), or of another structure type, as for example bcc (A2 type) in  $Nb_3Al$  [40] or in  $Nb_{-3}Si$  [41]. The term "disordered zone" seems thus to be more appropriated and will be adopted in the present work.

A further strong argument in favour of ordering effects was given by Ghosh et al. [42] and Rullier-Albenque et al. [43]. These authors used the fact that electrons with energies of the order of 1 MeV do not produce the displacement cascade (or disordered zones) described above, in contrast to irradiation with fast neutrons or high energy ions. Due to their low mass, electrons of 1 MeV create only isolated Frenkel defects (Schulson [44]). Rullier-Albenque et al. [43] have irradiated  $Nb_3Ge$  films (with  $T_{co} = 19.5$  K) with 1 MeV neutrons and with 2.5 MeV electrons, respectively, while Ghosh et al. [42] performed an analogous experiments on  $Nb_3Sn$  films, which were irradiated with 2 MeV He ions and with 2 MeV electrons. Both investigators came to the same conclusion, i.e. a strong decrease of  $T_c$  is observed, regardless of the nature of the projectile. In particular, it was found that the ratio  $\Delta T_c / \Delta \rho_{irr}$  (where  $\rho_{irr}$  is the increase of residual resistivity after irradiation) for  $Nb_3Ge$  does not differ between fast neutron and high energy electron irradiation. For  $\Delta \rho_{irr}$  values between 0.1 and 10  $\mu\Omega\text{-cm}$ , the ratio  $\Delta T_c / \Delta \rho_{irr}$  remained almost unchanged,

close to 0.1 K [43]. Although these experiments do not give a direct evidence that the order parameter is the same in both cases, they lead to an important conclusion: the presence of "disordered zones" is not necessary to cause a decrease of  $T_c$ . This result is analogous to that of fast quenching experiments, and furnishes an additional proof for atomic ordering effects as the dominant effect causing the decrease of  $T_c$  after neutron irradiation.

## THE SITE EXCHANGE MECHANISM IN IRRADIATED A15 TYPE COMPOUNDS

*Vacancy diffusion: the "virtual" lattice site (or split vacancy)*

In the tightly packed A15 structure, each atom is closely surrounded by its neighbors. The atoms would need to be considerably compressed before any two could squeeze past one another and interchange positions as required for ordering changes. Among different possible diffusion mechanisms, vacancy diffusion is the most probable one. It is based on the fact that at thermal equilibrium each solid at a temperature above zero contains a certain number of vacant lattice sites. An atom will now jump into a neighbouring vacancy, thus creating a new vacant site. Atoms and vacancies undergo a series of position exchanges, in order that a very small number of vacant lattice sites is sufficient to induce a substantial diffusion. Most studies dealing with diffusion have been undertaken on bcc or fcc structures. In the A15 structure, however, the situation is more complex, the  $6c$  and  $2a$  sites being not equivalent from the point of view of electronic bonding. Indeed, interactions between atoms on the  $6c$  and on the  $2a$  sites are characterized by metallic bonding, while the intrachain bonding between two A nearest neighbors is of the covalent type, as was shown by Staudenmann [45], who established electron density maps of  $V_3Si$ . This covalent bond is correlated with the very short AA distances on the chains of A15 type compounds, which are noticeably shorter than the sum of the atomic radii of the A element. This configuration leads to highly nonspherical shapes for the A atoms. The region of covalent bonding between two A atoms on  $6c$  sites will be called "overlapping region" in the following. This region corresponds to a high electron density in V-Si [45].

The question arises whether this overlapping (or covalent bonding) between two A neighbors on the chain sites still resides if one of them is next to a  $6c$  vacancy. Welch et al. [46,47] have shown by means of pair potential calculation that such an individual vacancy of an A atom on a  $6c$  site is unstable. They found that the state of lower energy corresponds to a configuration where one of the two A atoms adjacent to the single  $6c$  vacancy is shifted towards a new site which is equidistant from the next two A neighbors (see Fig. 9). This particular type of "split vacancy" [46,47], located in the overlapping region

corresponds to a nonequilibrium state and will thus in the following be called "virtual" lattice site [48].

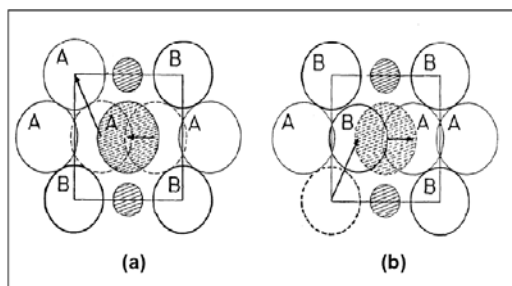


Figure 9:  $A \leftrightarrow B$  exchanges by vacancy diffusion in A15 type compounds  $A_3B$ . a) Jump of an A atom into a B vacancy, followed by the occupation of the "virtual" site by the neighbour A atom, b) Jump of a B atom into an equilibrium A site (two-step processes). Small circles: overlapping region between two A atoms or region of covalent bonding (Flükiger [18,48]).

It thus appears that the vacancy diffusion mechanism in the A15 type structure comprises two steps, in contrast to the one-step mechanism acting in simple bcc or fcc structures. Since the calculations of Welch et al. [46,47] show that the mobility of  $6c$  vacancies is quite high, the author has used the "virtual site" concept as a basis for a mechanism of homogeneous disordering in irradiated A15 tape compounds [18,48].

### Disordering by Focused Replacement Collision Sequences

In spite of the fact that the observations in Section V strongly support a homogeneous decrease of the long-range order parameter over the whole sample volume in irradiated A15 type compounds, a question arises: How is it possible that a homogeneous decrease of  $S$  implying site exchanges over several lattice spacings can occur during irradiations at temperatures  $T \leq 100^\circ\text{C}$ , where little thermal diffusion takes place?

Under these conditions, disordering in irradiated A15 type compounds can be caused either by a) local cascade replacements or b) focused replacement collision sequences, a superposition of both being even more probable.

### Local Cascade Replacements

Interaction between high energy incident particles and the lattice atoms produces a cascade, i.e. the atoms are displaced to produce Frenkel defects in a three-dimensional zone, the disordered (or depleted) zone [38,39]. Simultaneously, an even larger number of atoms change their mutual positions (i.e. they are replaced), thus producing locally a decrease of the degree of ordering. In principle, it could be argued that the atomic replacements

produced in the cascade would be sufficient to produce disorder in the whole A15 lattice.

However, this argument cannot be generalized, since electron irradiation of A15 type compounds causes the same effect on the superconducting transition temperature,  $T_c$ , and the electrical resistivity [43] but produces only isolated Frenkel defects rather than depleted zones (or cascades). Thus, an additional mechanism must be effective in causing a homogeneous decrease of the order parameter. Such a mechanism, requiring atomic transport over several interatomic distances (the condition for a collective phenomenon) is constituted by the focused replacement collision sequences.

### Focused Replacement Collision Sequences.

The so-called focusing replacement collision sequences, introduced by Seeger [38,39] represent the transport of matter and energy in irradiated crystals along dense crystallographic directions. Regardless of the crystal structure, an interstitial atom produced by irradiation processes is transported several interatomic distances away from its associated Frenkel vacancy, along these "focalizing" crystallographic directions. Focused replacement collision sequences can occur at the external boundaries or depleted zones with sizes of 4 to 5 nm for neutron irradiation [17,24] and up to 15 nm for irradiation with  $^{32}\text{S}$  ions [50]. At these boundaries, highly disordered regions are adjacent to the matrix, and a sufficient but still small number of virtual sites is thus occupied, a necessary condition for the occurrence of focused replacement collision sequences (it may be recalled that this number is still very small,  $< 0.1\%$ ). As irradiation further proceeds, the number of occupied virtual sites will increase, thus leading to an increase of site exchange processes. At the same time, thermal reordering will occur, as follows from the recombination theory of Liou and Wilkes [51].

It can be immediately seen that in the unirradiated state the replacement collision sequences in A15 type compounds occurring in the  $\langle 100 \rangle$  and  $\langle 111 \rangle$  directions, i.e. along the chains and the diagonal of the cube, are not effective in producing  $A \leftrightarrow B$  site exchanges. The only focusing direction where collision sequences could in principle produce  $A \leftrightarrow B$  site exchanges is the  $\langle 102 \rangle$  direction. However, the atomic sequence in the  $\langle 102 \rangle$  direction is oABAoABAo, the space between two ABA sequences coinciding with the region of overlap of two A atoms on the chain being perpendicular to the  $\{100\}$  plane. It can be easily shown that this configuration excludes extended site exchanges. Indeed, the potential encountered by A or B atoms on their way along the  $\langle 102 \rangle$  direction, calculated using a Born-Mayer interatomic potential [52] shows that  $V_{A \rightarrow B}$  and  $V_{B \rightarrow A}$  are of the same order of magnitude,  $\sim 10$  eV, while  $V_{A \rightarrow A}$  reaches 52 eV.

The situation in irradiated crystals is, however, quite different from that encountered prior to irradiation. With



the occupation of the virtual sites (a very small number of occupied non-equilibrium sites represented in Fig. 9 is sufficient), the potential  $V_{A \rightarrow A}$  is considerably lowered. The new sequence of atoms in the focusing  $\langle 102 \rangle$  direction around the occupied virtual site is now  $oABAAABAoABAo$  or  $oABABABAoABAo$ , depending on the occupation of the virtual site by an A or a B atom, respectively (see Fig. 10).

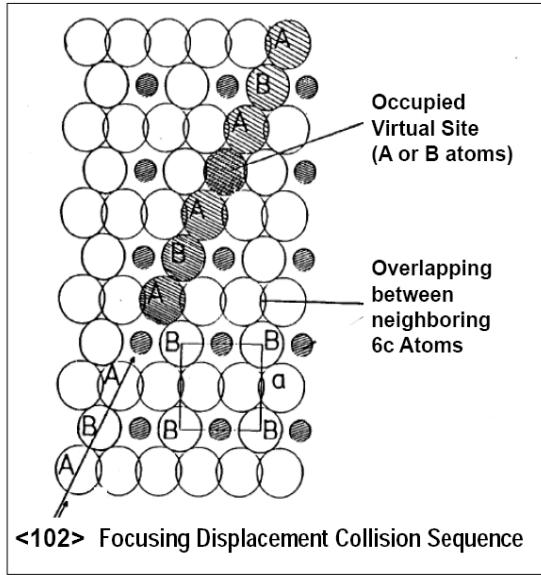


Figure 10: Focusing replacement collision sequences in A15 type compounds. Representation of the  $\{100\}$  plane of the A15 lattice (the radii are scaled for  $Nb_3Al$ ). The small circles correspond to the overlapping region between two A atoms belonging to the chains perpendicular to the  $\{100\}$  plane. The occupation of the virtual site by an A or a B atom leads to the sequences  $oABAAABAo$  or  $oABABABAo$ , respectively instead of  $oABAoABAo$  as in the unirradiated case, thus enabling  $A \leftrightarrow B$  site exchanges in the  $\langle 102 \rangle$  direction,  $a$  is the lattice parameter (Flükiger [18,48]).

As mentioned above, a very small amount of vacancies (or occupied virtual sites) is sufficient for the occurrence of the present mechanism. It should be recalled that for example, density measurements have revealed  $\sim 0.3\%$  of lattice vacancies in neutron irradiated  $V_3Si$  after a fluence of  $22.2 \times 10^{18} \text{ n/cm}^2$ , corresponding to a decrease of  $T_c$  to a value less than one half of the initial  $T_c$  value. Due to the very large number of replacement collisions over the whole crystal volume during the whole irradiation time, the virtual sites will be many times occupied and abandoned again, alternatively by A or B atoms, respectively. The latter constitute a "bridge" between neighbouring ABA sequences, thus allowing  $A \leftrightarrow B$  exchanges over several interatomic distances. This is a necessary condition for a homogeneous decrease of the

degree of ordering over the whole crystal after irradiation at low temperatures.

A very important conclusion can be drawn from a consideration of the close neighborhood of an occupied "virtual" lattice site. Its nearest neighbors, 6 A and 2 B atoms, are in close contact with the interstitial, which is either an A or a B atom. In the  $\{100\}$  plane, this leads to a hexagonal arrangement, as shown in Ref. 18. If the interstitial atom is of the A type, the occupation of the virtual site leads to 4 additional AA contacts, with AA distances of  $5/16a = 0.559a$ , thus 6% more than the AA distances in the chains,  $a/2$ . In addition, there are 2 AB contacts with interatomic distances of  $a/2$  compared to  $9/16a$  in the unirradiated A15 lattice, i.e. 6% shorter.

This situation can be compared to that in quench disordered A15 type compounds, where the AB distances are the same, i.e.  $a/2$ . The case of a B element occupying the virtual site with 4 AB and 2 BB close contacts is more interesting. The AB distances are now  $5/16a$ , i.e. they are still the same as in the unirradiated A15 structure, but the BB distances are now 36% shorter ( $a/2$  with respect to  $3a/2$ ). This would mean that in each case, BB distances shorter than the sum of two B radii would be encountered. Such an "overlapping" between B elements is only possible in the nonequilibrium situation caused by low temperature irradiations or in a dynamic situation during site exchanges at high temperature. It is particularly interesting to consider the case of nontransition B elements, where such close BB contacts are expected to cause strong electrostatic repulsive forces. The occurrence of such BBB sequences furnishes the key for understanding the causes of the lattice expansion and the static displacements observed in irradiated A15 type compounds (see Fig. 7).

From these remarks, it can be recognized that the diffusion in the A15 type structure is not a single vacancy diffusion as suggested by Sweedler et al. [23] nor it corresponds to a so-called interstitialcy diffusion mechanism, where the atom diffuses from a normal site to an interstitial site. In the case of the A15 structure, the situation is complicated by the fact that a jump into the virtual site (which is an interstitial site) requires simultaneously a rearrangement of the other atoms.

## NEUTRON IRRADIATION AND ITS EFFECTS ON $J_c$ AND $B_{c2}$ OF MULTI-FILAMENTARY $Nb_3Sn$ WIRES

There are only two investigations on alloyed  $Nb_3Sn$  wires, by Weber et al. [5] ( $E > 0.1 \text{ MeV}$ ) and by Weiss et al. [7] ( $E = 14 \text{ MeV}$ ). The latter compared the behavior of binary and alloyed  $Nb_3Sn$  wires at  $T_{irr} = 300K$  and performed  $J_c$  vs.  $B$  measurements at higher fields (between 14 and 20 T).

### Variation of $T_c$

As shown in Fig. 11, the variation of  $T_c$  vs.  $\phi t$  at low fluences is very similar for binary and alloyed wires: at  $10^{18}$  n/cm<sup>2</sup> the  $T_c$  reduction is close to 4% for fluences up to ~ 20% at  $2 \times 10^{18}$  n/cm<sup>2</sup> [7]. At the highest fluences in Ref. 7, i.e.  $4 \times 10^{18}$  n/cm<sup>2</sup>,  $\Delta T$  varies between - 2.3 and - 2.6 K for the binary wires. The variation  $\Delta T$  for alloyed wires is slightly higher: - 2.9 K for Ti additions and - 3.3 K for Ta additions. The slightly larger decrease for Ta additions may be caused by the considerably larger amount of Ta (3.5 at.%) in the filaments with respect to Ti (~ 1 at.%). As recently shown, the fact that Ta and Ti occupy different lattice sites prior to irradiation (Ta on Nb sites, Ti on Sn sites) may give an explanation for the observed difference [53]. As will be shown in the following, a considerably larger difference is observed when comparing the variation of  $J_c$  with fluence.

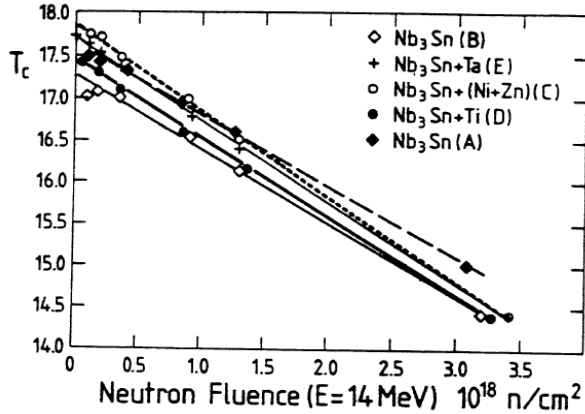


Figure 11:  $T_c$  vs. fluence  $\phi t$  for binary and alloyed  $Nb_3Sn$  multifilamentary wires after irradiation with 14.8 MeV neutrons at 300 K. Wire A: binary, 10'000 filaments, wires B, C, D and E: 19 filaments (Weiss et al. [7]).

### Binary multifilamentary $Nb_3Sn$ wires

In view of the use of multifilamentary alloyed  $Nb_3Sn$  wires in the LHC upgrade collider, it is interesting to know the effects of the expected neutron radiation on  $J_c$  at 15 T at fluences up to  $10^{19}$  n/cm<sup>2</sup>. As mentioned in Section V, fast neutron irradiation of  $Nb_3Sn$  causes a decrease of the long-range order parameter,  $S$ , which causes the decrease of  $T_c$ .

A second consequence of the decrease of  $S$  is the enhancement of the electrical resistivity  $\rho_o$ , which is correlated to the enhancement of the upper critical field,  $B_{c2}$ . At low fluences, this leads to a situation where  $T_c$  decreases, but  $B_{c2}$  increases. This means that at a given magnetic field, the initial values of  $J_c$  also increase: all known investigations report a maximum of  $J_c$ . At higher fluences, the decrease of  $T_c$  becomes the dominant effect, and  $B_{c2}$  decreases again.

An example for the binary multifilamentary wire [7] is shown in Fig. 12. The maximum of  $J_c/J_{c0}$  and  $B_{c2}$  is reached at  $0.8 \times 10^{18}$  n/cm<sup>2</sup>. The increase of the ratio  $J_c/J_{c0}$  at the maximum fluence is strongest for the highest fields and reaches ~ 2.1 at 15 T and ~ 3.5 at 20 T.

As mentioned before, a certain difference is observed between the fluence values given in different papers. This is illustrated by a comparison with a publication of Weber et al. [5], where the same maximum of  $J_c/J_{c0} \sim 2$  was reached after neutron irradiation at 300 K for a fluence of  $1.1 \times 10^{19}$  n/cm<sup>2</sup> ( $E > 0.1$  MeV). It follows that the conversion factor between 14 MeV and  $> 0.1$  MeV is close to 1.4. The maximum of  $B_{c2}^*$  was reached at the same ratio  $J_c/J_{c0}$ , the initial value of 21.4 T being enhanced to ~ 22.5 T [7].

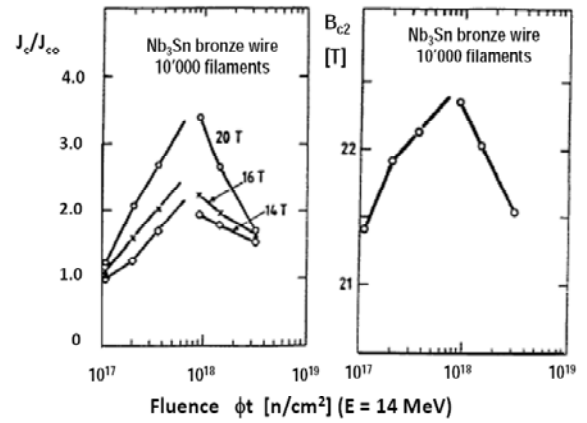


Figure 12:  $J_c/J_{c0}$  and  $B_{c2}^*$  of a 10000 filament binary Bronze Route  $Nb_3Sn$  wire after neutron irradiation at 300K ( $E=14$  MeV).  $B_{c2}^*$  is the critical field at 4.2 K determined by the Kramer extrapolation (Weiss et al. [7]).

### Alloyed multifilamentary $Nb_3Sn$ wires

The trend towards a stronger degradation for neutron irradiated wires observed for  $T_c$  vs.  $\phi t$  (see Fig. 13) is even accentuated when comparing the behavior of the normalized critical current density,  $J_c/J_{c0}$ , and the upper critical field,  $B_{c2}$ , with fluence. The results for the Ti alloyed wire with the composition (Nb-1.6wt.%Ti)<sub>3</sub>Sn are represented in Fig. 13. The most evident differences between the irradiated binary wires in Fig. 12 and the Ti and Ta alloyed wires are [7]:

a) The fluence  $\phi_{t,m}$  at which  $T_c$  and  $B_{c2}^*$  reach their maximum is  $0.18 \times 10^{18}$  n/cm<sup>2</sup> for the Ti alloyed wire (Fig. 11), i.e. it is four times smaller than for binary  $Nb_3Sn$  wires, where  $\phi_{t,m}$  is  $0.8 \times 10^{18}$  n/cm<sup>2</sup>. For the Ta alloyed wire,  $\phi_{t,m}$  is very close to that of the Ti added wire: it is slightly below  $0.2 \times 10^{18}$  n/cm<sup>2</sup>, as shown in Fig. 12. In their paper, Weiss et al. [7] also mention another additive, Ni+ Zn, which leads to a smaller enhancement of  $J_c$ , the amount of substituted elements in the filaments being smaller. For this rather unusual additive, the value of  $\phi_{t,m}$

lies at  $\sim 0.25 \times 10^{18}$  n/cm<sup>2</sup>, i.e. close to the values for Ti and Ta alloyed wires. It can be concluded that irradiation of alloyed Nb<sub>3</sub>Sn wires with 14 MeV neutrons at 300 K has a very similar effect on the maximum value of  $J_c/J_{c0}$ .

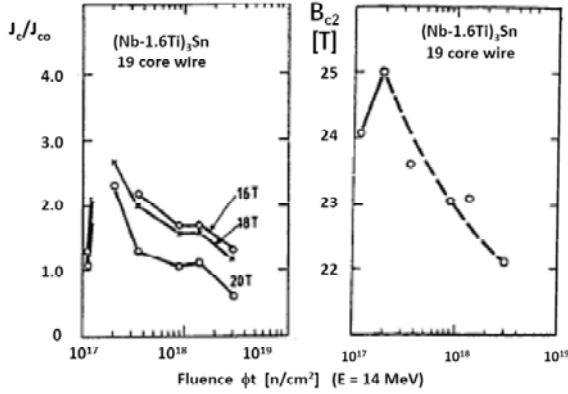


Figure 13:  $J_c/J_{c0}$  and  $B_{c2}^*$  of a 19 core (Nb-1.6wt.%Ti)<sub>3</sub>Sn produced by the Bronze Route after neutron irradiation at 300 K (Weiss et al. [7]).

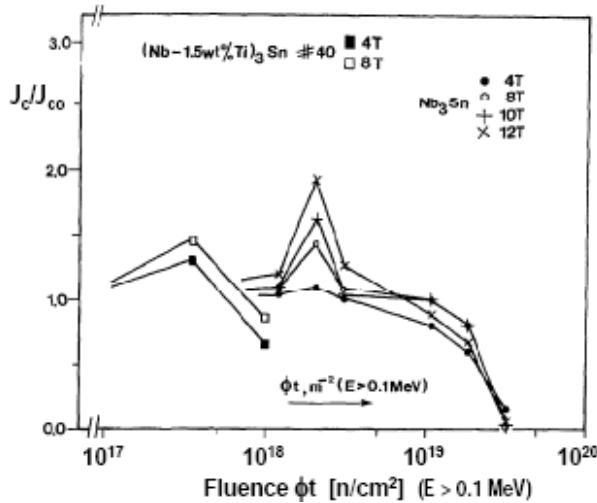


Figure 14:  $J_c/J_{c0}$  and  $B_{c2}^*$  of a 19 core (Nb-1.6wt.%Ti)<sub>3</sub>Sn produced by the Bronze Route after neutron irradiation at 300 K (Weber et al. [5]).

b) The enhancement of  $J_c/J_{c0}$  at  $\phi t_m$  for the same value of  $h^* = H/H_{c2}^*$  is smaller for alloyed than for binary wires. At  $h^* = 0.7$ ,  $J_c/J_{c0}$  for the Ti and Ta alloyed wires is  $\sim 3$  and 1.2, respectively, which is considerably smaller than for binary Nb<sub>3</sub>Sn ( $\sim 4.5$  for the binary 19 core wire and 2.2 for the binary 10'000 filament wire) (see Figs. 12).

c) In view of the application in LHC upgrade, it is interesting to know at what fluence  $J_c/J_{c0}$  starts to be lower than 1 under an applied field of 15 T. It is remarkable that for both binary wires, this is the case for

fluences close to  $1 \times 10^{19}$  n/cm<sup>2</sup>, which is considerably higher than for alloyed wires. For the additives Ti and Ni+Zn, the corresponding fluences are estimated to 5 and  $4 \times 10^{18}$  n/cm<sup>2</sup>. A much stronger effect was observed for the Ta alloyed wire, where  $J_c/J_{c0} = 1$  is already reached at  $0.3 \times 10^{18}$  n/cm<sup>2</sup>! This tendency is confirmed by neutron

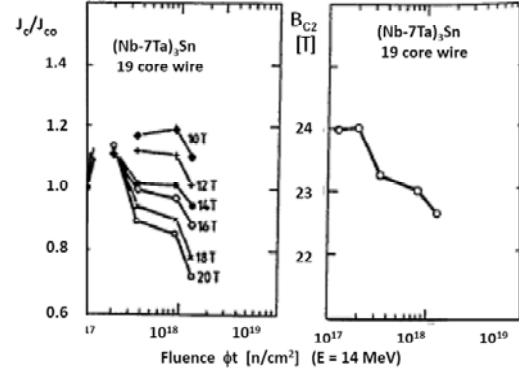


Figure 15:  $J_c/J_{c0}$  and  $B_{c2}^*$  of a 19 core (Nb-7wt.%Ta)<sub>3</sub>Sn produced by the Bronze Route after neutron irradiation at 300 K (Weiss et al. [7]).

irradiation measurements of Weber et al. [5], who reported measurements up to 12 T and found  $J_c/J_{c0} = 1$  at  $7 \times 10^{18}$  n/cm<sup>2</sup> for binary Nb<sub>3</sub>Sn wires, but  $0.8 \times 10^{18}$  n/cm<sup>2</sup> for (Nb-1.5wt.%Ti)<sub>3</sub>Sn wires.

It follows that alloyed wires are much more sensitive to radiation than binary wires. This can be explained by the disordering effect of the various additives. Indeed, it was found in unirradiated samples that the maximum of  $J_c$  is reached when the initial residual resistivity  $\rho_0$  of the ordered binary Nb<sub>3</sub>Sn system is enhanced to values of 30-35  $\mu\Omega\cdot\text{cm}$  by the substitution of the additives into the A15 lattice [53]. In binary wires, the necessary fluence to reach this optimum value of  $\rho_0$  (and thus  $B_{c2}$ ) is considerably higher than in alloyed wires. Before irradiation, the  $\rho_0$  value of alloyed wires is already close to the optimum value of 30-35  $\mu\Omega\cdot\text{cm}$ . Irradiation will thus only lead to a small enhancement of  $B_{c2}$ , followed by a decrease with higher fluences.

## CONDITIONS FOR Nb<sub>3</sub>SN WIRES IN THE LHC UPGRADE

### Radiation damage on the superconducting properties

As shown in Fig. 1 [1], the highest fluence in LHC upgrade will occur at the Quadrupoles Q2a, the second highest fluence being expected for the quadrupole Q1. For a total operation time of 10 years, calculating 200 operation days a year, the total fluence at the inner winding of the quadrupole Q2a after the upgrades of Phase I and Phase II will be  $0.25 \times 10^{18}$  n/cm<sup>2</sup> and  $10^{18}$

n/cm<sup>2</sup>, respectively. For the quadrupole Q2 (external winding), the corresponding fluences are  $0.17 \times 10^{18}$  n/cm<sup>2</sup> and  $0.68 \times 10^{18}$  n/cm<sup>2</sup>, the total fluence for the quadrupoles Q2b and Q3 being considerably smaller. No problem is expected for the dipoles. Since the highest radiation damage will be expected on the inner winding of the quadrupole Q2a, the present estimation will be limited to this location.

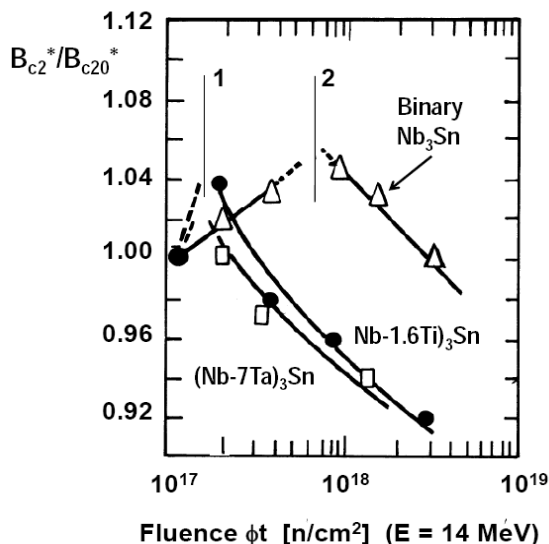


Figure 16: Variation of the upper critical field of binary and alloyed Nb<sub>3</sub>Sn wires (additives: Ti and Ta), after Weiss et al. [7].

### Radiation induced change of Cu resistivity and thermal stability

A point to be discussed when analyzing the properties of Nb<sub>3</sub>Sn wires in view of operation in a LHC upgrade collider at  $\geq 15$  T is the effect of neutron radiation on the thermal stability. Little is known about the change of the electrical resistivity of pure Cu submitted to neutron irradiation. Fabritsiev et al. [54] studied the effects of neutron irradiation on the electrical resistivity of precipitation hardened (PH) and dispersion strengthened (DS) copper alloys in the fast neutron reactor BOR-60 with doses of  $8-16 \times 10^{21}$  n/cm<sup>2</sup> and in the mixed spectrum neutron reactor SM-2 with doses of  $3.7-5.5 \times 10^{21}$  n/cm<sup>2</sup>. The experimental data on the change  $\Delta\rho$  in electrical resistivity of DS-type copper alloys irradiated in the BOR-60 reactor show that irradiation to 7-10 dpa at  $T=340-450$  °C causes a drop in electrical conductivity by not more than 20%. The obtained results show that in mixed-spectrum reactors the rate of  $\Delta\rho$  normalized to the dpa is about 20 times as high as in fast neutron reactors. The conclusion is made that the calculations performed for ITER must take into account the presence of appreciable fluxes of thermal neutrons in certain components of the reactor. The latter will play a decisive

role in the drop in thermal conductivity of copper alloys in these components. This problematics may be of smaller importance in LHC upgrade, the neutron spectrum being narrower. Nevertheless, this question must be studied in detail if the thermal stability of the magnets has to be guaranteed for the whole lifetime of approximately 10 years.

## CONCLUSIONS

An overlook of the effects of neutron irradiation on the superconducting parameters  $T_c$ ,  $B_{c2}$  and  $J_c$  of Nb<sub>3</sub>Sn wires as reported in the literature has been given in view of the determination of the radiation limit in the LHC upgrade magnets. The coexisting defect mechanisms in irradiated Nb<sub>3</sub>Sn type compounds are briefly presented and a model is discussed explaining the site exchange mechanism which leads to a decrease of atomic ordering after irradiation.

The variation of  $J_c$  in binary as well as in Ti and Ta alloyed Nb<sub>3</sub>Sn wires is presented, showing a higher sensitivity to neutron radiation for the latter. Based on calculations of F. Cerutti and coworkers (CERN), the neutron fluence at the inner winding of the quadrupole Q2a is estimated to values below  $10^{18}$  neutrons/cm<sup>2</sup> for a life time of 10 years, which is within the safety margin with respect to the critical current density and  $B_{c2}$ .

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