# CHANGE OF DI LENGTH AND FIELD 

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Paper published at MT, Boston 2013

## BASELINE

- D1 is the separation dipole
- Superconductive, Nb-Ti, large aperture
- Started with 160 mm aperture, then decided that 10 mm more than quads was not needed after ebergy deposition studies
- 35 Tm required
- 70\% margin on the loadline was chosen, giving 5.2 T operational field with 15 mm one layer coil
- Two layers excluded since this magnet has a lot of fringe field already


Field verus coil width in accelerator magnets and models

## VARIATIONS

- The chosen margin is large w.r.t. quadrupoles, which are in Nb 3 Sn and in similar region for radiation and heat loads
- Possible to decrease from $30 \%$ to $20-25 \%$
- At the same time the length corresponding to 5.2 T and 35 Tm was exceeding the vertical test station length at KEK
- Study was carried out to explore the case of $25 \%$ margin and $20 \%$ margin
- Options look viable, with increase of stress and fring field which appears to be tolerable [talk on 25 June 2013, T. Nakamoto and Q. Xu]


## THREE OPTIONS AT 150 MM

|  | LHC outer cable With 70\% load line ratio | LHC outer cable With $75 \%$ load line ratio | LHC outer cable With $80 \%$ load line ratio |
| :---: | :---: | :---: | :---: |
| Bore diameter | 150 mm | 150 mm | 150 mm |
| Nominal field (dipole) | 5.22 T | 5.59 T | 5.97 T |
| Magnetic length * | 6.7 m | 6.3 m | 5.9 m |
| Operating current | 11.0 kA | 12.0 kA | 13.0 kA |
| Injection current | $\sim 0.70 \mathrm{kA}$ | $\sim 0.77 \mathrm{kA}$ | $\sim 0.84 \mathrm{kA}$ |
| Field homogeneity | $<0.01 \% \quad\left(\mathrm{R}_{\text {ref }}=50 \mathrm{~mm}\right)$ | $<0.01 \% \quad\left(\mathrm{R}_{\text {ref }}=50 \mathrm{~mm}\right)$ | $<0.01 \% \quad\left(\mathrm{R}_{\mathrm{ref}}=50 \mathrm{~mm}\right)$ |
| Peak field in the coil | 6.0 T | 6.5 T | 6.9 T |
| Load line ratio | 69\% @ 1.9 K | 75\%@1.9 K | 80\% @ 1.9 K |
| Inductance (low / nominal field) | $5.7 / 5.2 \mathrm{mH} / \mathrm{m}$ | $5.7 / 5.2 \mathrm{mH} / \mathrm{m}$ | $5.7 / 5.1 \mathrm{mH} / \mathrm{m}$ |
| Stored energy | $294 \mathrm{~kJ} / \mathrm{m}$ | $340 \mathrm{~kJ} / \mathrm{m}$ | 391 kJ/m |
| Peak field/central field | 1.15 | 1.15 | 1.16 |
| Lorenz force $\mathbf{X} / \mathbf{Y}$ ( $\mathbf{1}^{\text {st }}$ quadrant) | 1.3/0.5 MN/m | 1.5/0.6 MN/m | 1.7/0.7 MN/m |
| Outer dia. of iron yoke | 550 mm | 550 mm | 550 mm |
| Inner dia. of iron yoke | 222 mm | 222 mm | 222 mm |
| Strand diameter | 0.825 mm | 0.825 mm | 0.825 mm |
| $\mathrm{Cu} /$ Non-Cu ratio | 1.95 | 1.95 | 1.95 |
| Cable dimension | 15.1* 1.48mm ${ }^{\text {2 }}$ | 15.1* 1.48mm ${ }^{\text {2 }}$ | 15.1* 1.48mm ${ }^{\text {/ }}$ |
| / insulation | 0.16 mm (radial) | 0.16 mm (radial) | 0.16 mm (radial) |
|  | 0.145 (azimuthal) | 0.145 (azimuthal) | 0.145 (azimuthal) |
| No. of strands | 36 | 36 | 36 |
| Keystone angle | $0.9{ }^{\circ}$ | $0.9{ }^{\circ}$ | $0.9{ }^{\circ}$ |
| Superconductor current density | $1710 \mathrm{~A} / \mathrm{mm}^{2}$ | $1865 \mathrm{~A} / \mathrm{mm}^{2}$ | $1954 \mathrm{~A} / \mathrm{mm}^{2}$ |
| Total length of the cable | 618 m (Coil length $\sim 7.1 \mathrm{~m}$ ) | 566 m (Coil length $\sim 6.7 \mathrm{~m}$ ) | 548 m (Coil length $\sim \mathbf{6 . 3 ~ m}$ ) |

## IMPACT ON FIELD QUALITY



## CONCLUSIONS

- We propose to reduce the margin from $30 \%$ to $25 \%$, i.e. increasing the operational field from 5.2 to 5.6 T and reducing length from 6.7 to 6.3 m
- Minimal change needed to fit the test station
- Current increase from 11 to 12 kA



## SUMMARY

|  |  | $\begin{gathered} \text { Triplet } \\ \text { Q1,Q3/Q2a,b } \\ \hline \end{gathered}$ | Orbit corrector MCBX | $\begin{gathered} \hline \text { Sep. } \\ \text { dipole } \\ \text { D1 } \\ \hline \end{gathered}$ | Recom. dipole D2 | $\begin{gathered} \hline \text { Large 2-in- } \\ 1 \text { quad } \\ \text { Q4 } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Aperture | (mm) | 150 | 150 | 150 | 105 | 90 |
| Field | (T) |  | 2.1 | 5.6 | 3.5 |  |
| Gradient | (T/m) | 140 |  |  |  | 120 |
| Mag. Length | (m) | 8.0/6.8 | 1.2/2.2 | 6.3 | 10.0 | 4.5 |
| Int field | ( Tm ) |  | 2.5/4.5 | 35 | 35 |  |
| Int gradient | (T) | 1120/938 |  |  |  | 544 |
| Peak field | (T) | 12.1 | 3.9 | 6.5 | 4.1 | 5.9 |
| Current | (kA) | 17.5 | 2.2 | 11.8 | 6.8 | 16.0 |
| j overall | ( $\mathrm{A} / \mathrm{mm}^{2}$ ) | 528 | 455 | 1816 | 1040 | 2458 |
| Loadline margin | (\%) | 18\% | 45\% | 25\% | 56\% | 20\% |
| Stored energy | (MJ/m) | 1.440 | 0.090 | 0.338 | 0.140 | 0.204 |
| Saturation | (\%) | 9.0\% | 0.0\% | 12.0\% | 13.0\% |  |
| Material |  | $\mathrm{Nb}_{3} \mathrm{Sn}$ | $\mathrm{Nb}-\mathrm{Ti}$ | $\mathrm{Nb}-\mathrm{Ti}$ | $\mathrm{Nb}-\mathrm{Ti}$ | $\mathrm{Nb}-\mathrm{Ti}$ |
| N. layers |  | 2 | 1+1 | 1 | 1 | 1 |
| Cable width | (mm) | 18.1 | 4.37 | 15.1 | 15.1 | 15.1 |

