# Tools in CTF3 

Simona Bettoni
for the CTF3 operation team


## Outline

$\rightarrow$ The modeling:
$\rightarrow$ Quad scans
$\rightarrow$ Online model
$\rightarrow$ The automatization of the measurements in CTF3:
$\rightarrow$ Reading and writing on the machine
$\rightarrow$ The measurements:
$\rightarrow$ kick measurements
$\rightarrow$ Dispersion measurements
$\rightarrow$ Tune measurements
$\rightarrow$ The tools:
$\rightarrow$ Orbit correction in the ring
$\rightarrow$ Orbit correction in the LINAC (see E. Adli talk)

## Online MAD-X model of the machine

The currents in the machine are read and the K values are calculated

Energy profile and starting optical parameters (LINAC) are used


Several matchings can be easily integrated


The currents of the quads can be read and directly sent to the machine

## Online MAD-X model of the machine: energy profile

$\rightarrow$ The energy profile is determined from the loading in the klystrons
$\rightarrow$ Excel spreadsheet used


Input power in a klystron and beam current


## Extracted power



Beam acceleration


Beam energy variation in each structure

## Online MAD-X model of the machine: initial conditions

$\rightarrow$ Six monitors are installed in the machine to measure the twiss parameters and the emittances

$\rightarrow$ For each part of the machine a Matlab function defines the structure of the line or the ring (kind of equipment and name in the MAD model, status of the device)

$\rightarrow$ Function to read the orbit

$\rightarrow$ Function to automatically read and write the currents in the magnets
function readvalues $=$ readdevices(devdescr)
function writedevices(devdescr,values)

## Kick measurements

$\rightarrow$ A reference orbit and the beam current along the line (ring) are measured
$\rightarrow$ The current in a corrector is changed
$\rightarrow$ The new orbit and the current in each beam position monitor are saved
$\rightarrow$ The orbit variation is compared to the MAD model prediction



## Dispersion measurements: local

$\rightarrow$ The contribution to the dispersion of each part of the machine is isolated and compared to the model predictions assuming 0 incoming dispersion


$\rightarrow$ A reference orbit of one shot saved along the machine
$\rightarrow$ The orbit variation in a not free and well known dispersion (Frascati chicane) is used to compute the shot to shot energy deviation: from $\Delta x(\Delta y)$ to $\Delta \mathrm{p} / \mathrm{p}$
$\rightarrow$ Known the energy jittering, measuring the orbit deviation along the entire machine, the dispersion is computed: from $\Delta \mathrm{p} / \mathrm{p}$ to Dx (Dy)

## Dispersion measurements: energy step

$\rightarrow$ An energy variation along the pulse in the last klystron of the LINAC is introduced
$\rightarrow$ The beam position difference between the different parts of the pulse in the BPM is used to determine the dispersion


## Tune measurements


$\rightarrow$ The measurement:
$\rightarrow$ Tune determined from the Fourier transform of
the $\mathrm{H}(\mathrm{V})$ signal in a BPM (scope signal)
$\rightarrow$ Compromise between oscillation amplitude
and number of turns (typically about 200)
$\rightarrow$ Scan varying the current in a quads family


## Orbit correction: the algorithm

$$
\min \left\|x_{\text {BPM }}-x_{\text {REF }}-R M \cdot I\right\|_{I}
$$

RM: response matrix
$\mathrm{X}_{\text {BPM }}$ : transverse beam displacement at BPM
$\mathrm{x}_{\text {REF }}$ : reference orbit at BPM
I: currents in the correctors

$$
\begin{aligned}
& \Delta x \equiv x_{\text {REF }}-x_{B P M} \\
& \min \|\Delta x+R M \cdot I\|_{I} \\
& \Delta I=\widetilde{R}(\varepsilon) \cdot \Delta x \text { where } \quad \tilde{R}(\varepsilon) \equiv V \cdot \tilde{W}(\varepsilon) \cdot U^{T} \\
& \text { Singularity rejection parameter (eps) }
\end{aligned}
$$

$\mathcal{E}=0 \Longrightarrow$ Normally most accurate orbit correction, BUT large current values can be obtained
$\mathcal{E}=1 \quad$ No orbit correction $(\tilde{R}(\varepsilon)$ null matrix)

## Orbit correction: the algorithm improvement

Best eps value iteratively determined:
$\rightarrow$ Tolerance on the maximum allowed beam displacement and maximum value of the currents in the correctors

```
eps_start=1
n_max_step = 10000;
fact = 1;
```

for $i=1:$ n_max_step $^{\text {s }}$

```
if i== l
    eps(i)=eps_start*fact;
else
    eps(i)=\operatorname{eps}(i-1)*fact;
end
```

[theta_s,thetap_s,corr_s,final_s,idec_s] = correction_1_mod(eps(i),RM', x_BP');
Curr_tot_s(i,:) = start_corr'+theta_s;
Curr_tot_max(i) $=\max \left(a \bar{b} s\left(s t a r t \_c o r r '+\right.\right.$ theta_s) $)$;
if abs (Curr_tot_max(i)) > max_I_corrs_tol
fact = 1.1;
else
$x^{\prime} \max \exp =\max \left(a b s\left(x \_B P+R M{ }^{\prime} * t h e t a \_s\right)\right) ;$
if x_max_exp < tol
break
else
end
fact $=0.9 ;$
end
end
Curr_tot = Curr_tot_s(end,:);

## Orbit correction: the response matrix

Orbit closure:
$\rightarrow$ The response matrix is built using both the first and the second turn orbits


| Correctors | $145-\mathrm{S}$ | 200 | 242 | 252 | 292 | 345 | 408 | 452 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  |  |  |  |
| BPM/BPI | 155 | 195 | 208 | 248 | 275 | 305 | 395 | 405 |

Kicks in the correctors:
$\rightarrow$ The value of the kick in each corrector is determined according to the maximum tolerated losses in the last read BPM/BPI

## Orbit correction: the results

## Inputs:

$\rightarrow$ Tolerated maximum $x$-displacement $=4 \mathrm{~mm}$
$\rightarrow$ Maximum current in the correctors $=10 \mathrm{~A}$
$\rightarrow$ Maximum allowed losses $=10 \%$



$\rightarrow$ Tolerance on the orbit correction limited by the incoming orbit jittering


$\rightarrow$ Possible cures:
$\rightarrow$ Increase the number of averaging (time consuming)
$\rightarrow$ Subtract the orbit jittering due to dispersion pattern (to be tested next week)

## Orbit correction: model-based correction

Use the model response matrix to correct the orbit at least for the first iteration:
$\rightarrow$ Quicker (response matrix measurement takes about 20 minutes)
$\rightarrow$ Immediately scaled for the energy


## Conclusions

$\rightarrow$ In CTF3 Matlab scripts have been developed to modify the machine settings and read the orbits in the machine. This allows to do automatically:
$\rightarrow$ Kick measurements
$\rightarrow$ Dispersion measurements
$\rightarrow$ Quad scans
$\rightarrow$ Several tools have been developed to determine the optics model and to operate the machine:
$\rightarrow$ Online model
$\rightarrow$ Tune measurements
$\rightarrow$ Orbit correction
$\rightarrow$ Future developments:
$\rightarrow$ Better study of the dependence of the measurements (kick and dispersion) on the energy jittering
$\rightarrow$ Tune measurement automatization
$\rightarrow$ Integration of the Matlab tools in the control system (more user-friendly)

## Extra slides

## Orbit correction: the results (vertical)

Inputs:
$\rightarrow$ Tolerated maximum y-displacement $=1.5 \mathrm{~mm}$
$\rightarrow$ Maximum current in the correctors $=10 \mathrm{~A}$
$\rightarrow$ Maximum allowed losses $=10 \%$



