

# **Radiation damage simulations for CLIC and ILC spoilers and ATF tests**

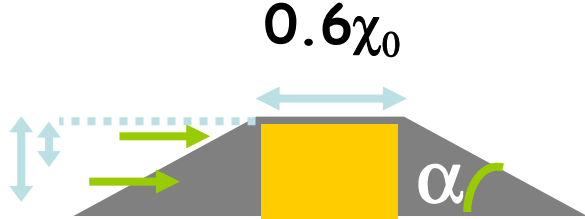
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**The collimator mission is to clean the beam halo from e- or e+ off orbit which could damage the equipment and mainly to stop the photons generated during the bending of the beam towards the Interaction Point. These photons, if not removed, would generate a noise background that would not allow the detectors to work properly.**

**The spoiler serves as protection for the main collimator body as it will disperse the beam, reducing the beam energy density by multiple Coulomb scattering, in case of a direct bunch hit avoiding severe radiation damage.**

	CLIC	ILC
Energy	1500 GeV	250/500 GeV
<b>Bunches it has to resist</b>	312	2/1
Particles per bunch	3.72E9	2E10
$\sigma_x$ in the spoiler position	796 $\mu\text{m}$	111 $\mu\text{m}$
$\sigma_y$ in the spoiler position	21.9 $\mu\text{m}$	9 $\mu\text{m}$

## Starting point

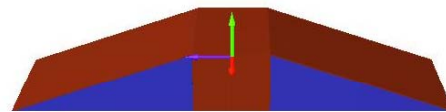
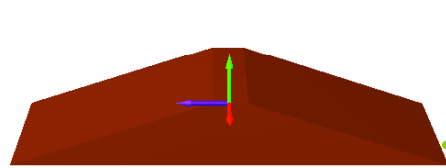
- Long, shallow tapers to reduce short range transverse wakes
  - High conductivity surface coatings
  - Robust material for actual beam spoiling
- 
- Long path length for errant beams striking spoilers
    - Large  $\chi_0$  materials (beryllium..., graphite, ...)
  - Design approach
    - Consider range of constructions, study relative resilience to damage (melting, fracture, stress)
    - Particularly important for beam-facing surfaces (wakefields)
    - Also within bulk (structural integrity, heat flow)
  - Design external geometry for optimal wakefield performance, reduce longitudinal extent of spoiler if possible

# Summary of simulations

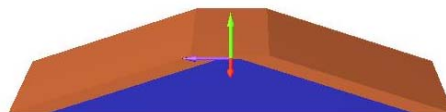
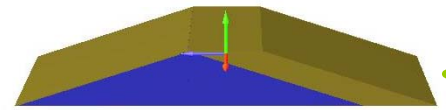
## Temperature increase from 1 bunch impact

Exceeds fracture temp.

Exceeds melting temp.



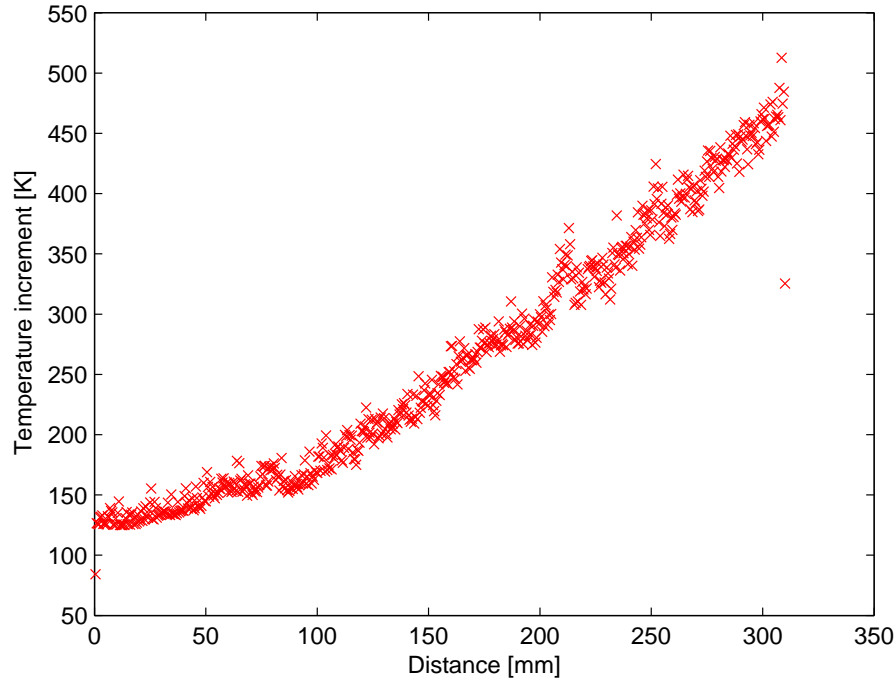
← Beam direction



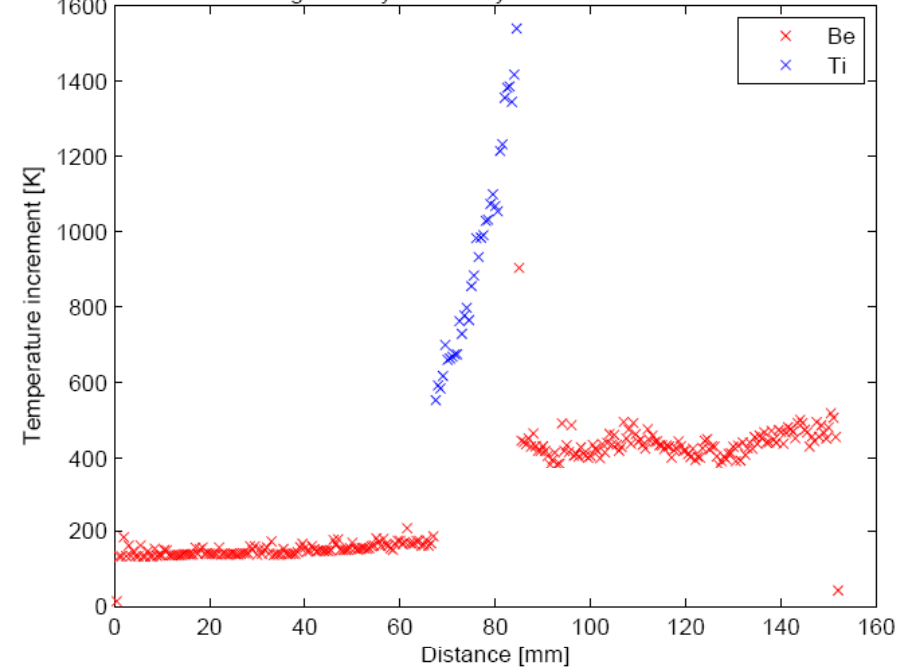
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	2mm depth		10mm depth	
	250 GeV e <sup>-</sup> 111×9 μm <sup>2</sup>	500 GeV e <sup>-</sup> 79.5×6.4 μm <sup>2</sup>	250 GeV e <sup>-</sup> 111×9 μm <sup>2</sup>	500 GeV e <sup>-</sup> 79.5×6.4 μm <sup>2</sup>
Solid Ti alloy	420 K	870 K	850 K	2000 K
Solid Al	200 K	210 K	265 K	595 K
Solid Cu	1300 K	2700 K	2800 K	7000 K
Graphite+Ti option 1	325 K	640 K	380 K	760 K
Beryllium+Ti ≈ option 1	-	-	-	675 K
Graphite+Ti option 2	290 K	575 K	295 K	580 K
Graphite+Al option 2	170 K	350 K	175 K	370 K
Graphite+Cu option 2	465 K	860 K	440 K	870 K
Graphite+Ti option 3	300 K	580 K	370 K	760 K

Temperature increment in a Be spoiler with tapers and a 0.5 rad. lengths body hit by a full CLIC train



Temperature increment in a spoiler with Be tapers and 0.5 rad. lengths body of Ti hit by a full CLIC train

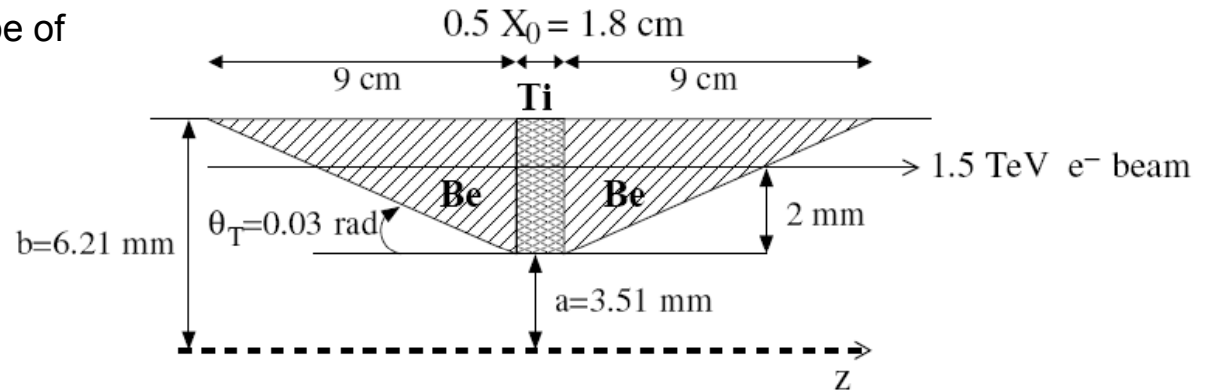


Be will not reach melting temperature (1267 K) but it will reach fracture temperature (370 K)

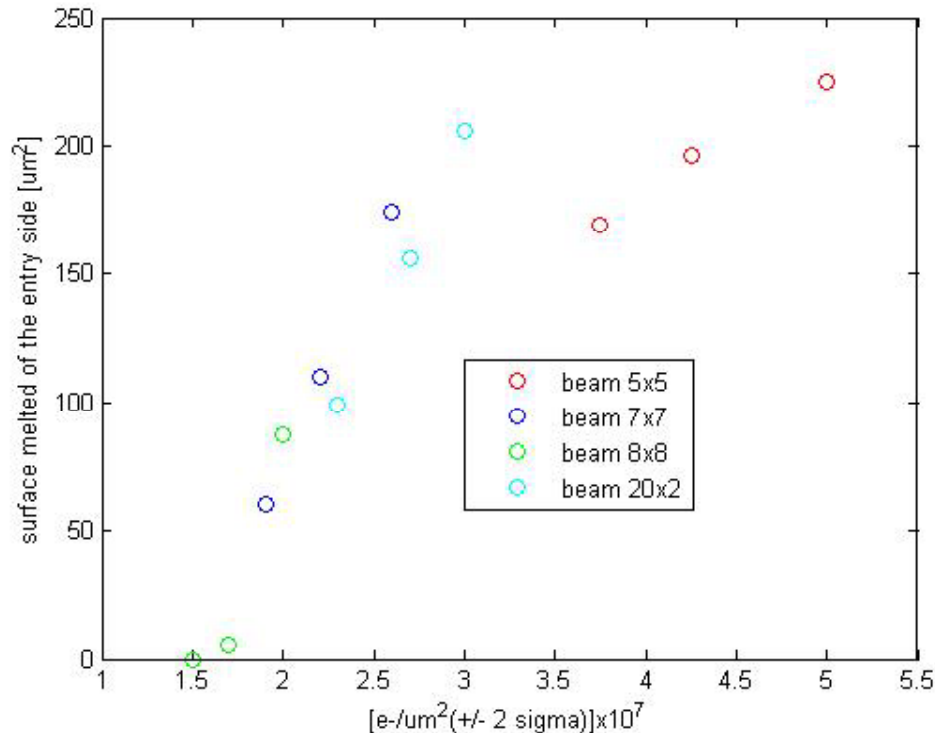
Ti alloy (Ti6Al4V) reaches a temperature just under melting temperature (1941 K) and would surpass fracture temperature (1710 K) if ambient temperature is above 110 K. Too close a call...

0.5  $X_0$  of Be is 17.65 cm

The total length of this spoiler would be of 35.65 cm



## Material damage test beam at ATF



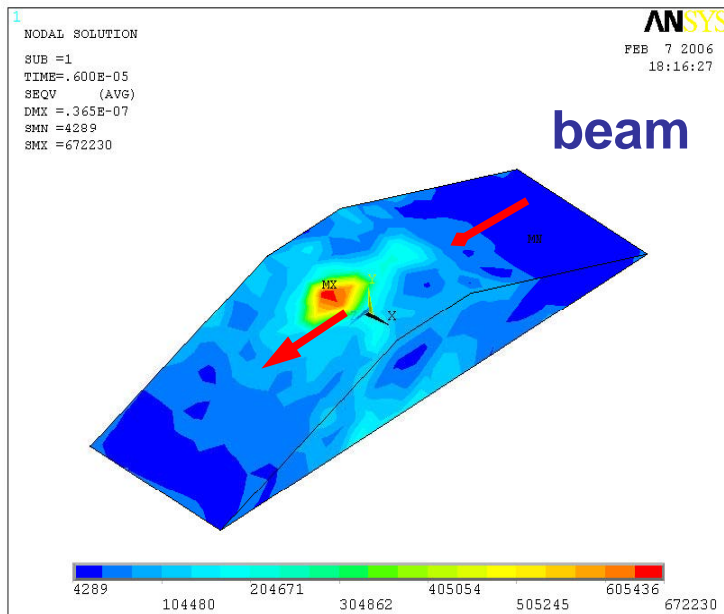
Simulations with FLUKA of melted surface on the Ti alloy target against the beam parameters.

The purpose of the first test run at ATF is to:

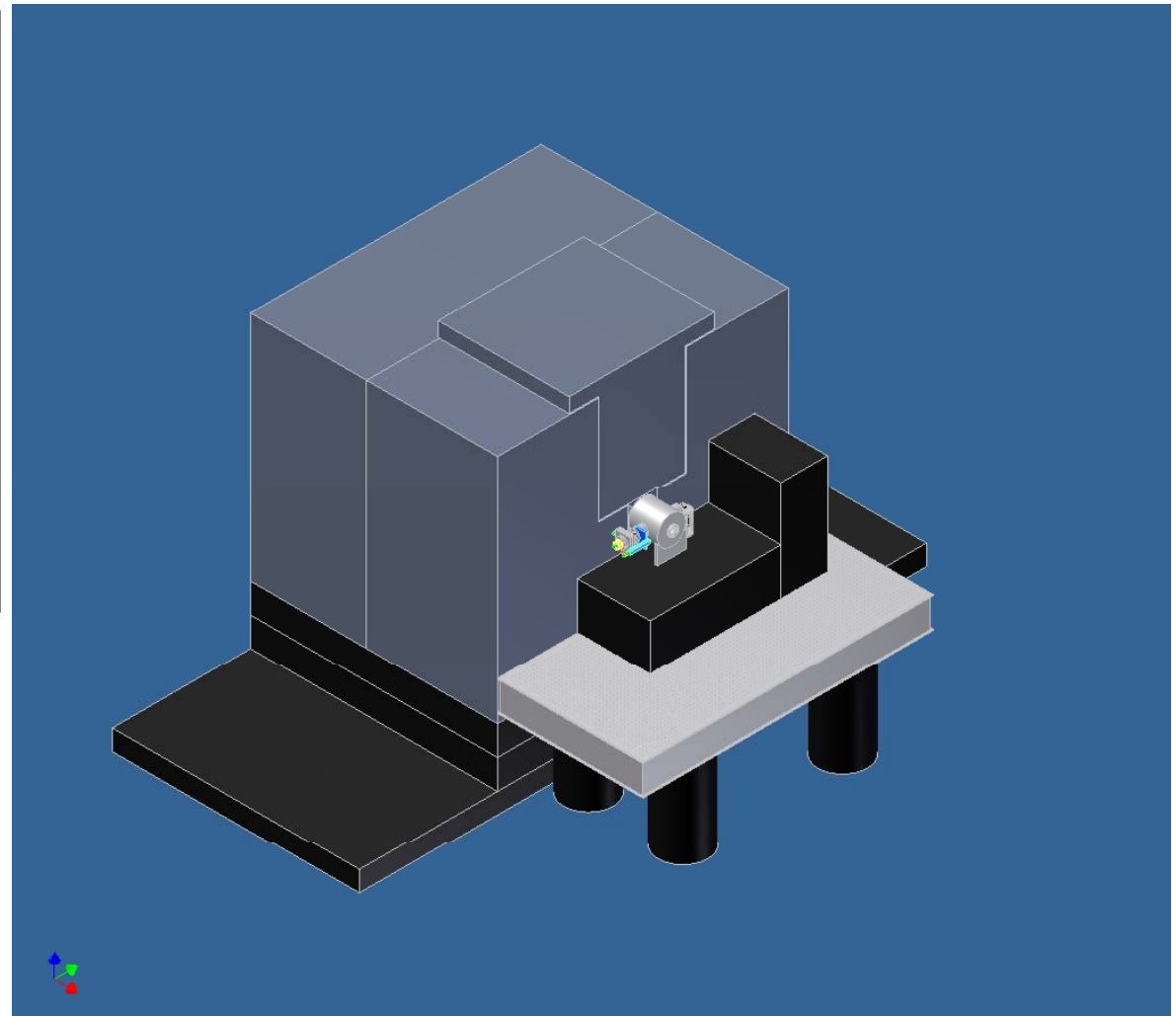
1. Make simple measurements of the size of the damage region after individual beam impacts on the collimator test piece. This will permit a direct validation of FLUKA/ANSYS simulations of properties of the materials under test.
2. Allow us to commission the proposed test system of vacuum vessel, multi-axis mover, beam position and size monitoring.
3. Validate the mode of operation required for ATF in these tests.
4. Ensure that the radiation protection requirements can be satisfied before proceeding with a second phase proposal.

Assuming a successful first phase test, the test would be to measure the shock waves within the sample by studying the surface motion with a laser-based system, such as VISAR (or LDV), for single bunch and multiple bunches at approximate ILC bunch spacing.

**Second phase of radiation damage test beam at ATF2-KEK:**  
 Will be used to study the stress waves generated by a bunch hitting the material and this data will be compared to FLUKA + ANSYS simulations.



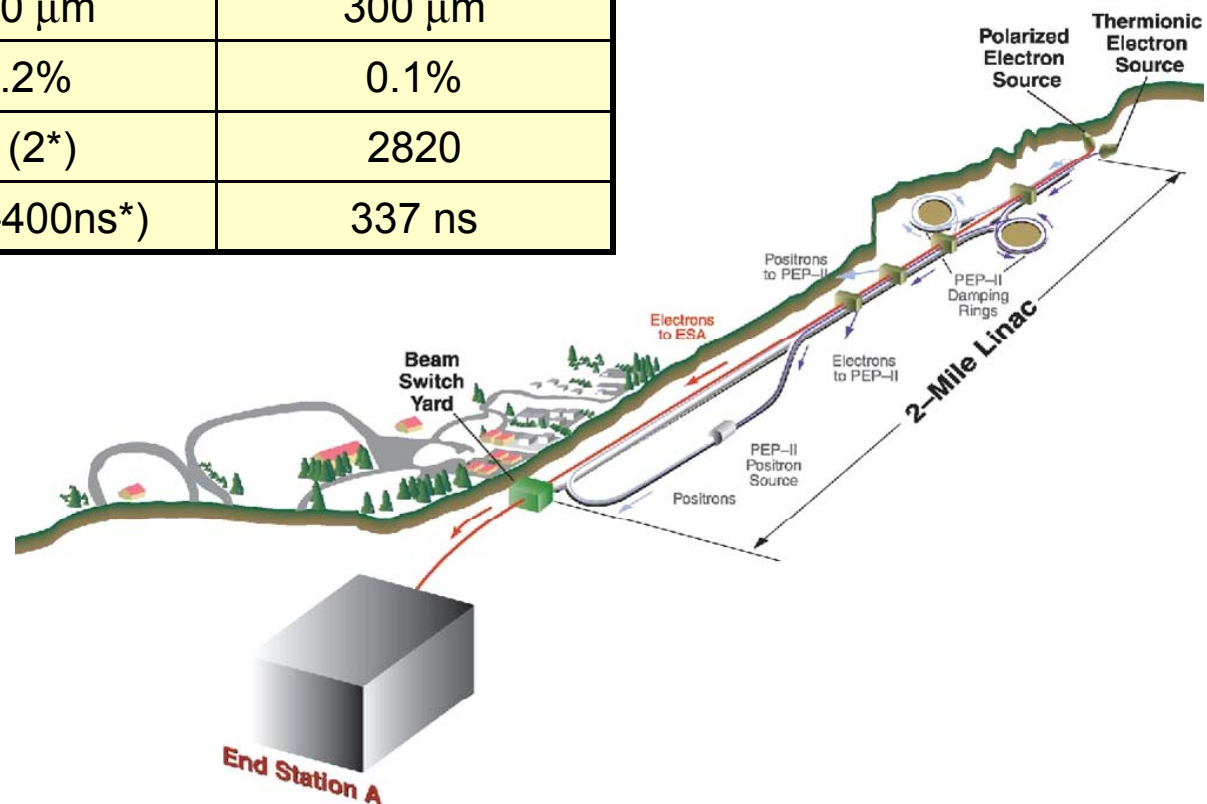
(George Ellwood)



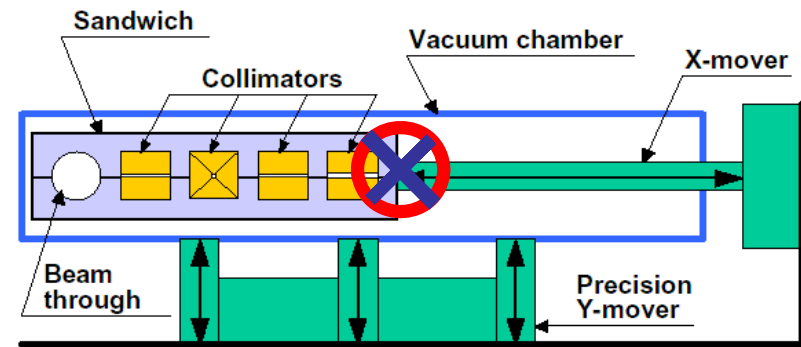
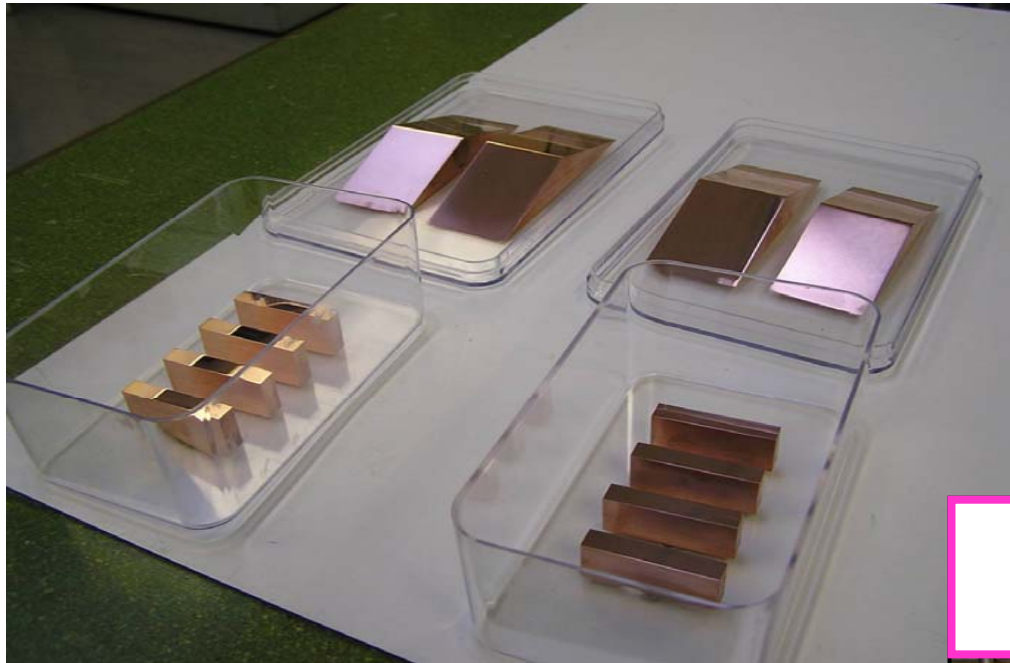
## Beam Parameters at SLAC ESA and ILC

Parameter	SLAC ESA	ILC-500
Repetition Rate	10 Hz	5 Hz
Energy	28.5 GeV	250 GeV
Bunch Charge	$2.0 \times 10^{10}$	$2.0 \times 10^{10}$
Bunch Length	300 $\mu\text{m}$	300 $\mu\text{m}$
Energy Spread	0.2%	0.1%
Bunches per train	1 (2*)	2820
Microbunch spacing	- (20-400ns*)	337 ns

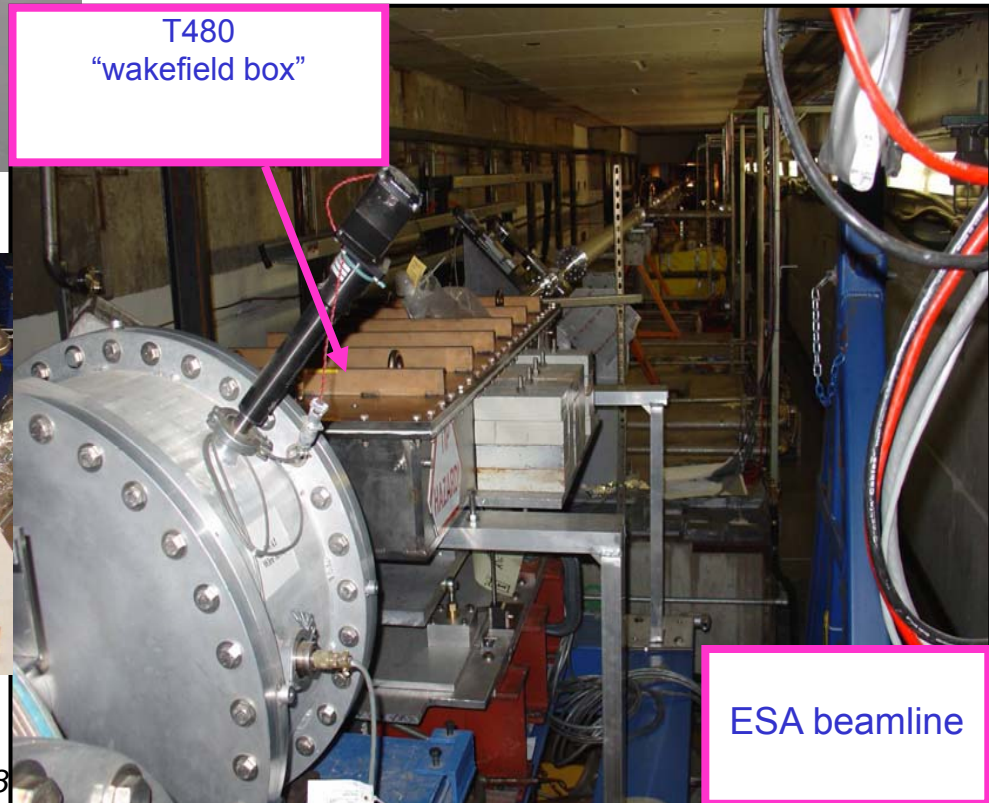
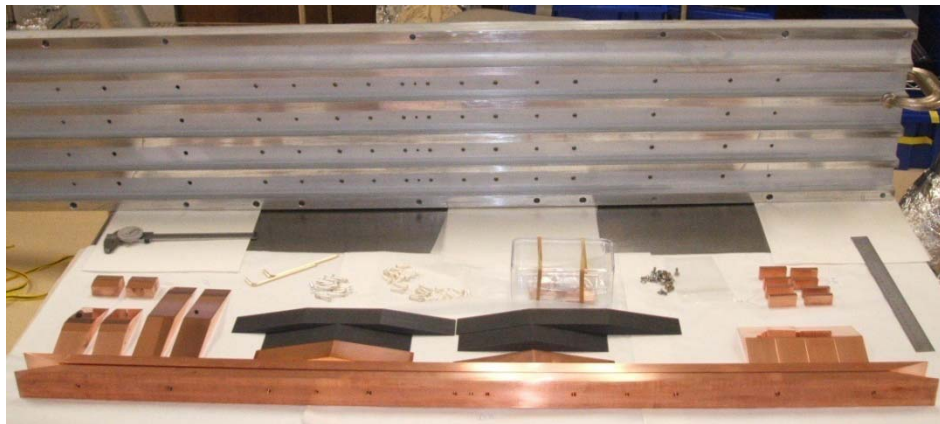
\*possible, using undamped beam



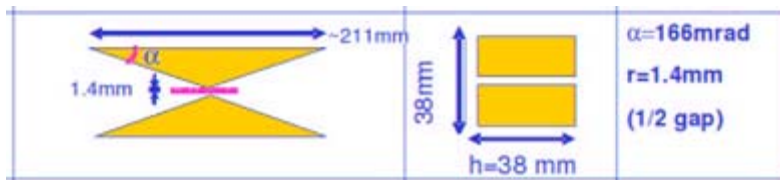


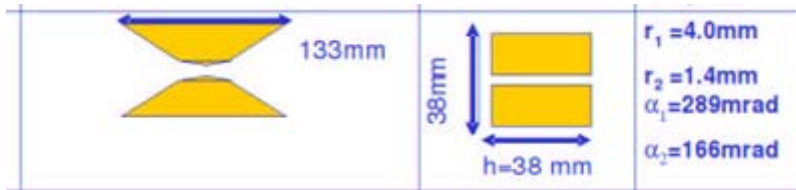
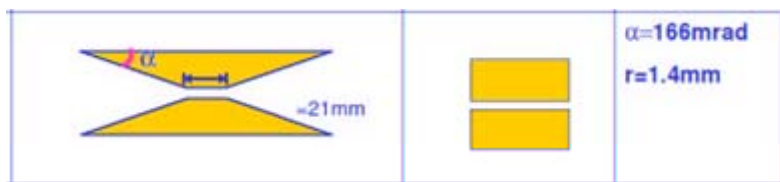
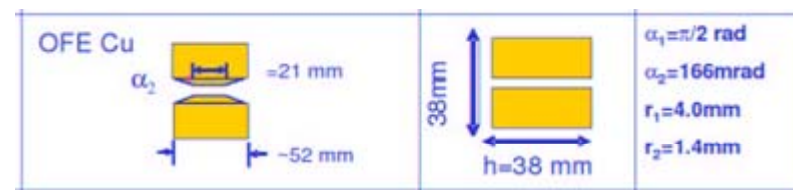


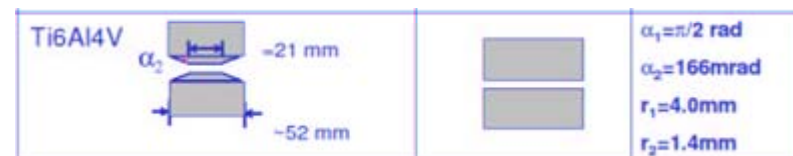
T480  
"wakefield box"



ESA beamline


 $1 \pm 0.1 \text{ V/pC/mm}$ 

 $1.4 \pm 0.3 \text{ V/pC/mm}$ 

 $1 \pm 0.2 \text{ V/pC/mm}$ 

 $1.7 \pm 0.1 \text{ V/pC/mm}$ 

 $1.9 \pm 0.2 \text{ V/pC/mm}$ 

 $1.7 \pm 0.1 \text{ V/pC/mm}$ 

 $2.6 \pm 0.1 \text{ V/pC/mm}$

Flexural Section (wakefield taper) Peripheral cooling sufficient? Angle varies from 0 at max aperture opening to **90mrad  $\sim 5^\circ$**  (full included angle (or  $\pm 20\text{mrad}$  about axis)

Vessel (wire seal UHV compatible)

Precision encoded actuators with bi directional repeatability to  $<10\mu\text{m}$  ( $<5\mu\text{m}$  possible?). Note with  $10\mu\text{m}$  over 300mm span,  $0.03\text{mrad}$  angle control is possible on pitch of collimator surfaces

Vented Side Grill for Wakefield continuity and pumping

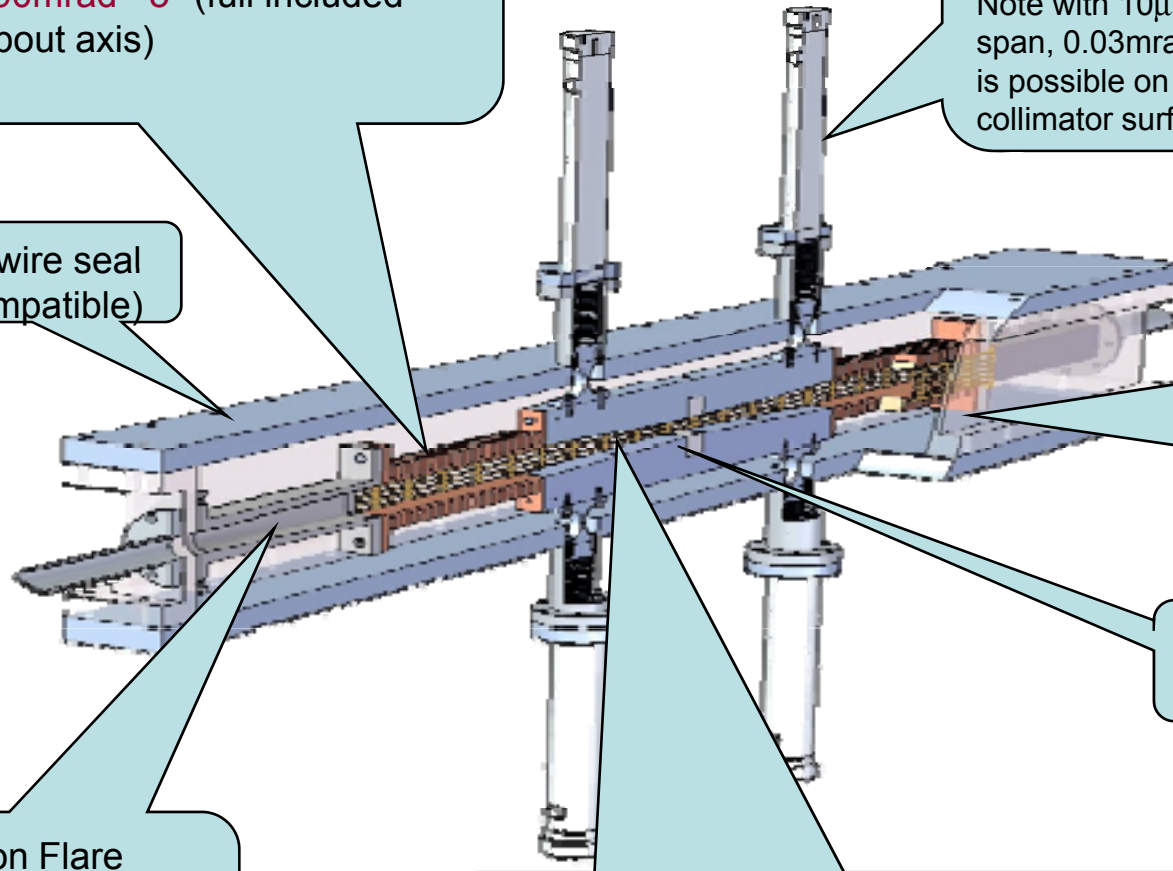
Spoiler Block  
21mm width Ti

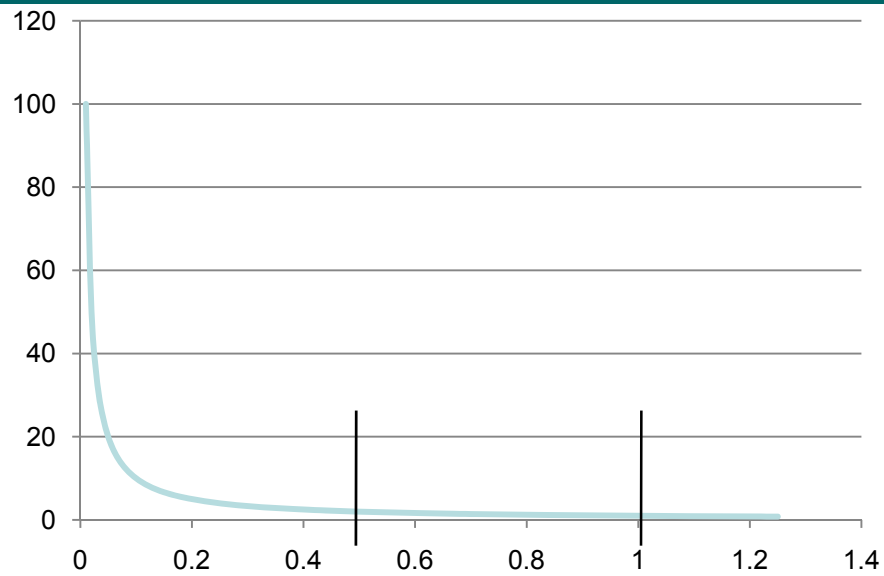
Entrance Transition Flare  
From 20mm diameter to 30(h)x40(w)mm rectangular section.

Inclined Wakefield Collimator Block  
Bulk Material – Be, semi-transparent to 500GeV electrons. Converging in 2 steps of opening angle  $65\text{mrad}$  ( $3.7^\circ$ ) &  $40\text{mrad}$  ( $2.3^\circ$ ) nearer the spoiler block (note: opening angle =  $\pm 32.5\text{mrad}$  &  $\pm 20\text{mrad}$  about central axis respectively) then diverges at same angular rate downstream of the spoiler block

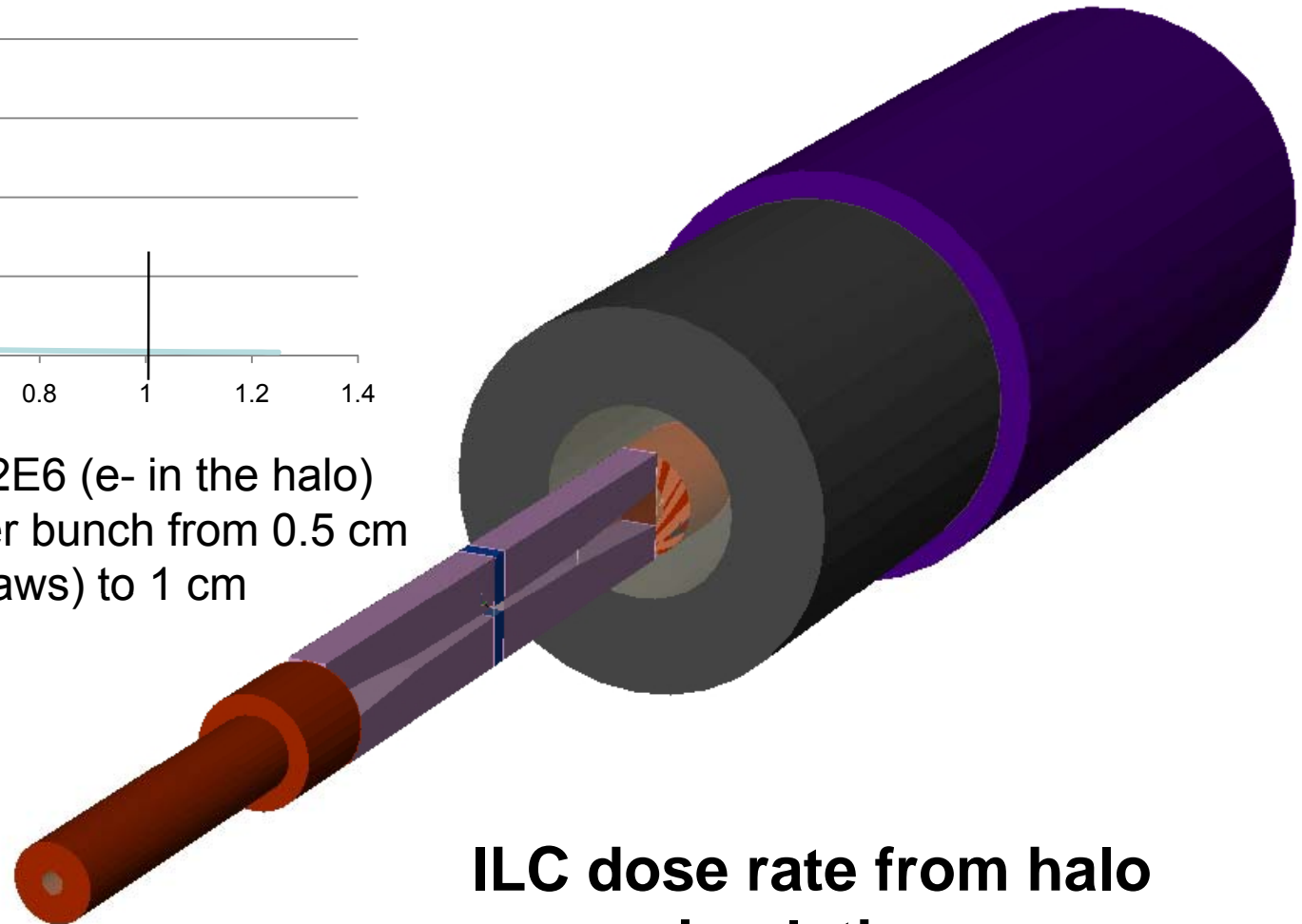
EPAC08, WEPP168

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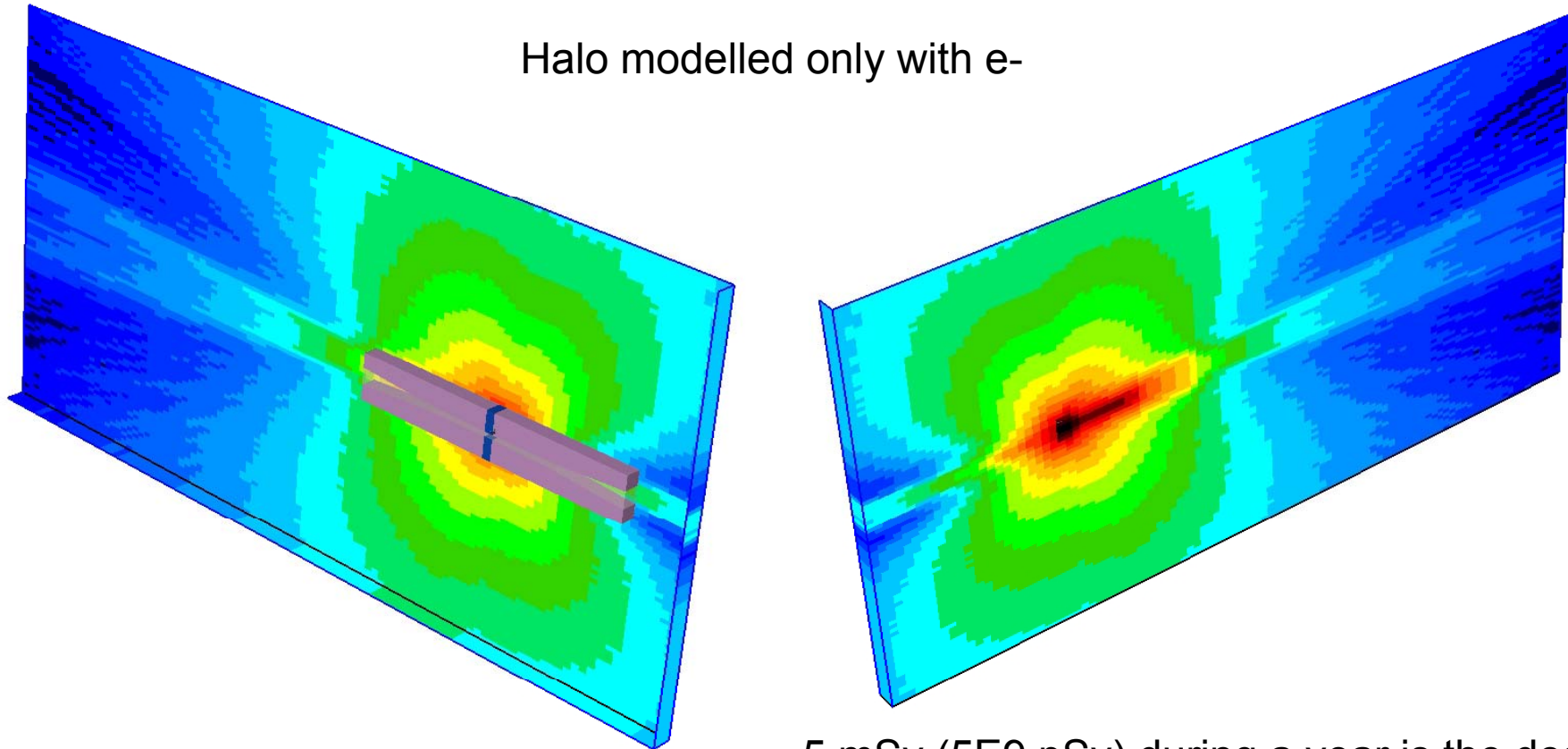


$C(\ln(1)-\ln(0.002))=2E6$  (e- in the halo)  
 $C(\ln(1)-\ln(0.5))=e-$  per bunch from 0.5 cm  
 (start of the jaws) to 1 cm

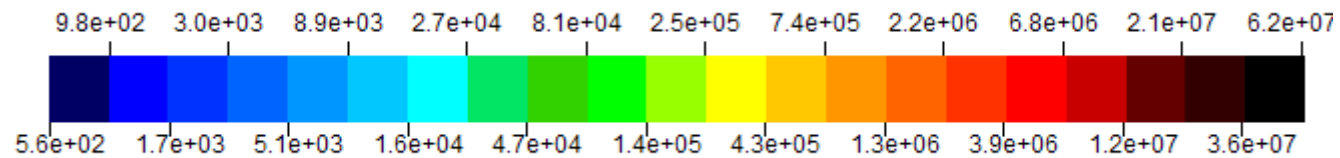


## ILC dose rate from halo simulations

Halo modelled only with e-

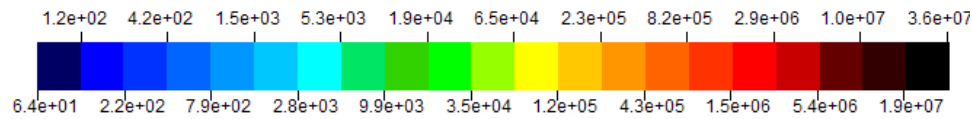
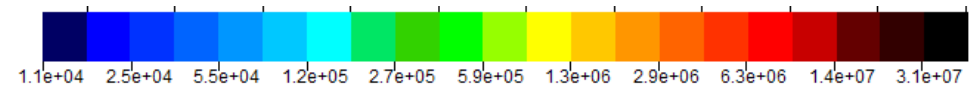
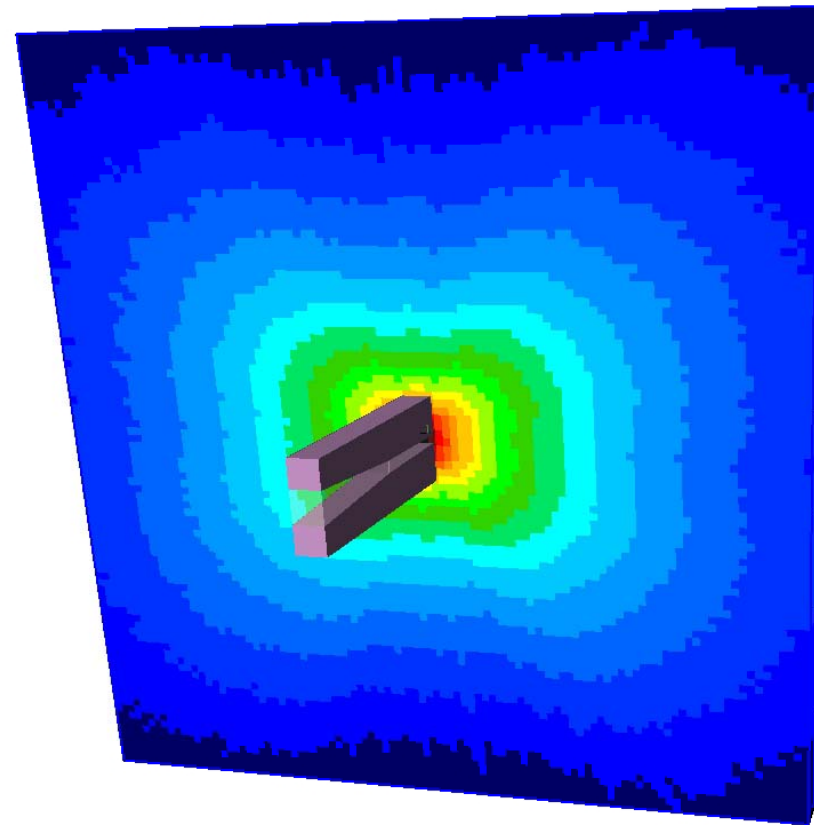
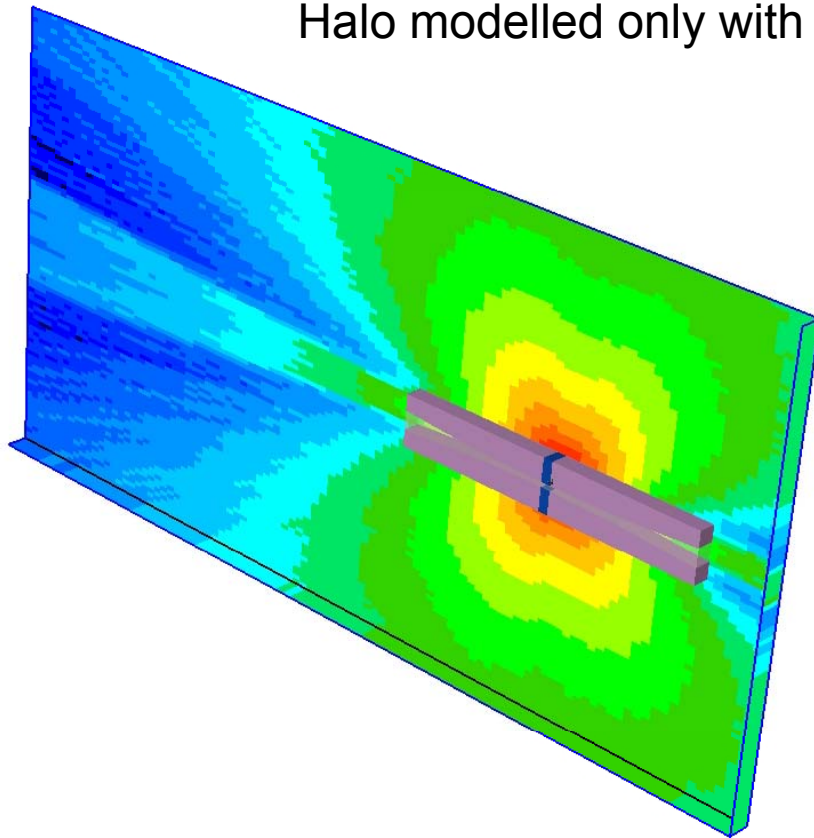


5 mSv (5E9 pSv) during a year is the dose limit for radiation workers.



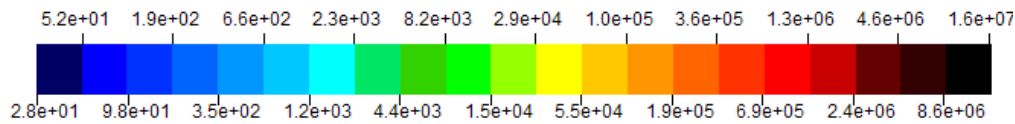
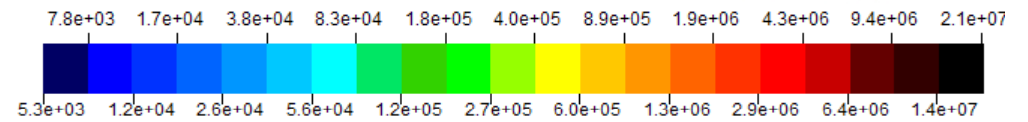
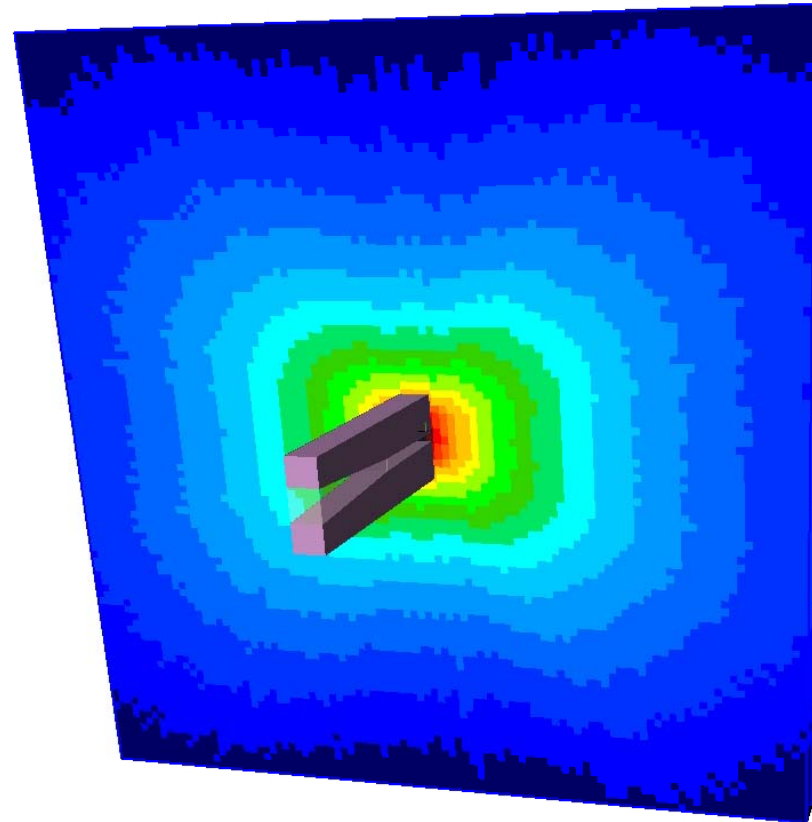
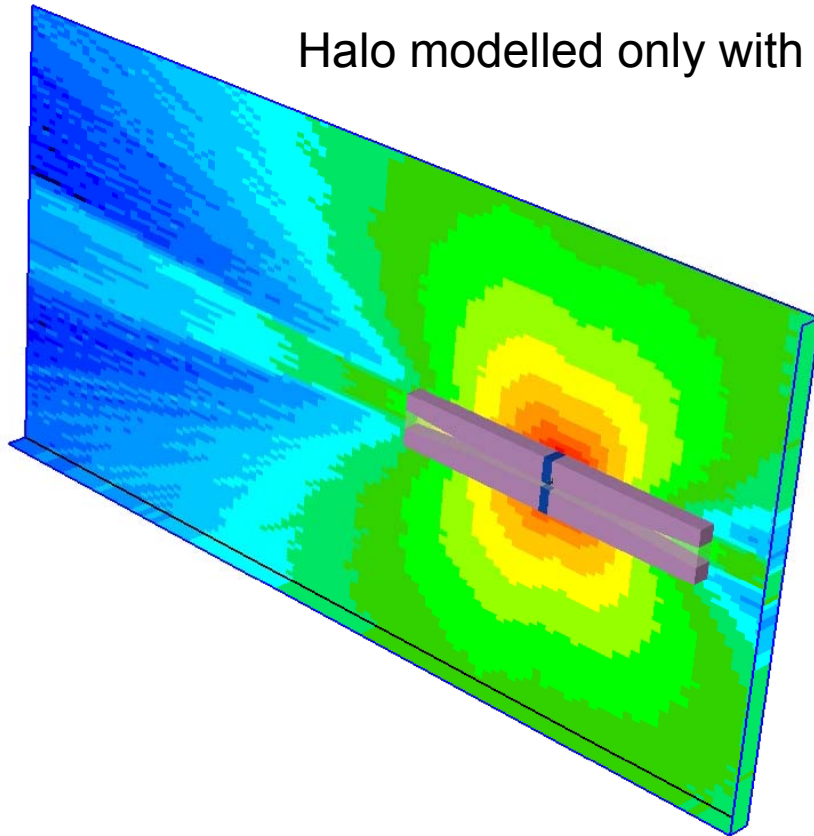
[pSv/s] after 2 months of constant operation

Halo modelled only with e-



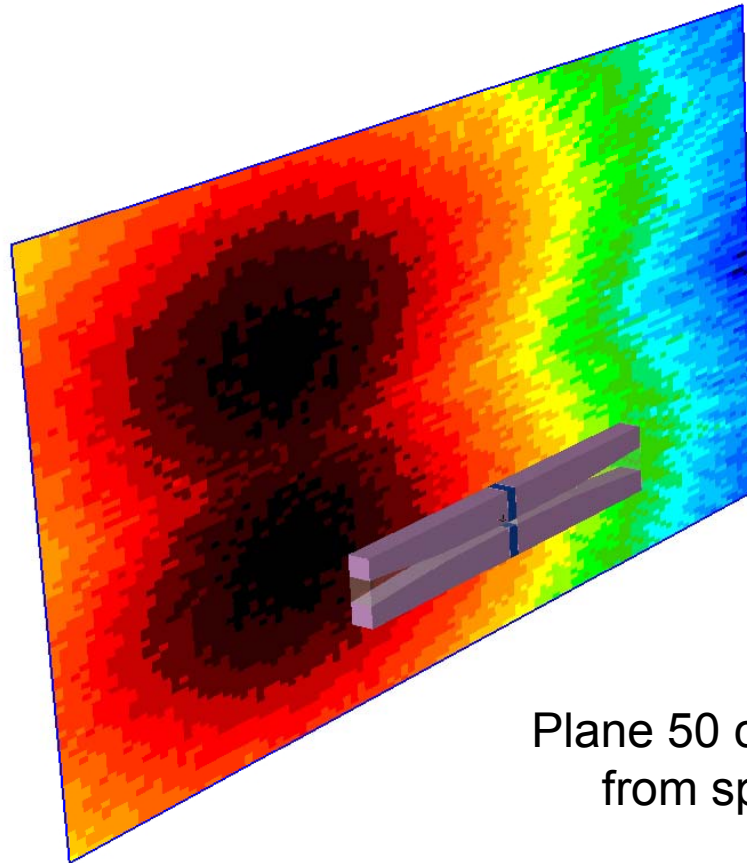
[pSv/s] after 2 months of constant operation  
and after 1 hour without beam

Halo modelled only with e-

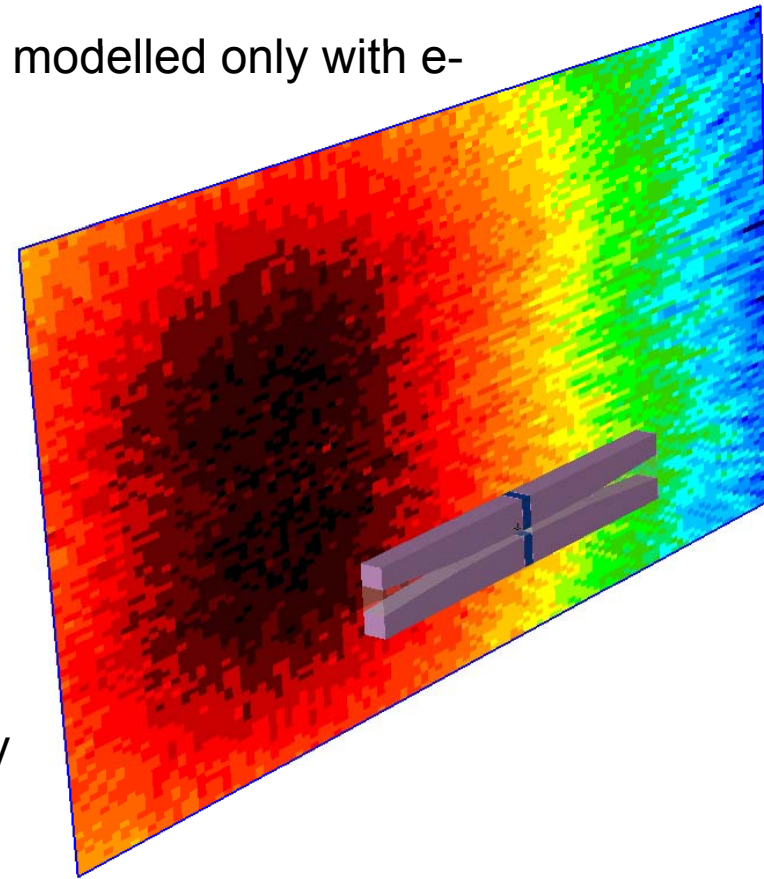


[pSv/s] after 2 months of constant operation  
and after 1 day without beam

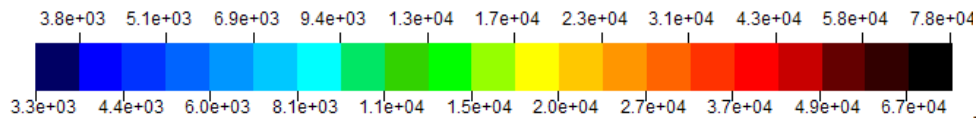
Halo modelled only with e-



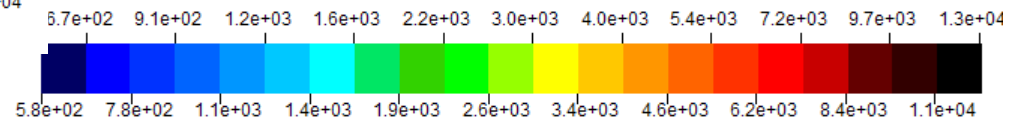
Plane 50 cm away from spoiler



[pSv/s] after 2 months of constant operation and after 1 day without beam



[pSv/s] after 2 months of constant operation and right after beam stops





## Conclusions:

**A spoiler with a central Ti alloy body and Be tapers emerges as the most reasonable material configuration for ILC, Ti alloy and graphite core it is also an option, whilst for CLIC further design studies should be done: A full Be spoiler would fracture in worst case scenario, using Ti alloy would fracture as well and it could melt in worst case. Possible solution could be to share the 0.5 radiation lengths between Ti alloy and Be.**

**Analysis of T480 wakefield test beams showed that a combination of taper angles can be used, shallower closer to the beam.**

## Outlook:

**Phase 2 of the damage tests at ATF2 were stress-waves will be measured. Benchmarking both FLUKA and ANSYS simulations.**

**Analysis of activation and dose rate to prototype model due to beam halo and photons using FLUKA (first results given here, geometry is done, still working on halo modelling).**