

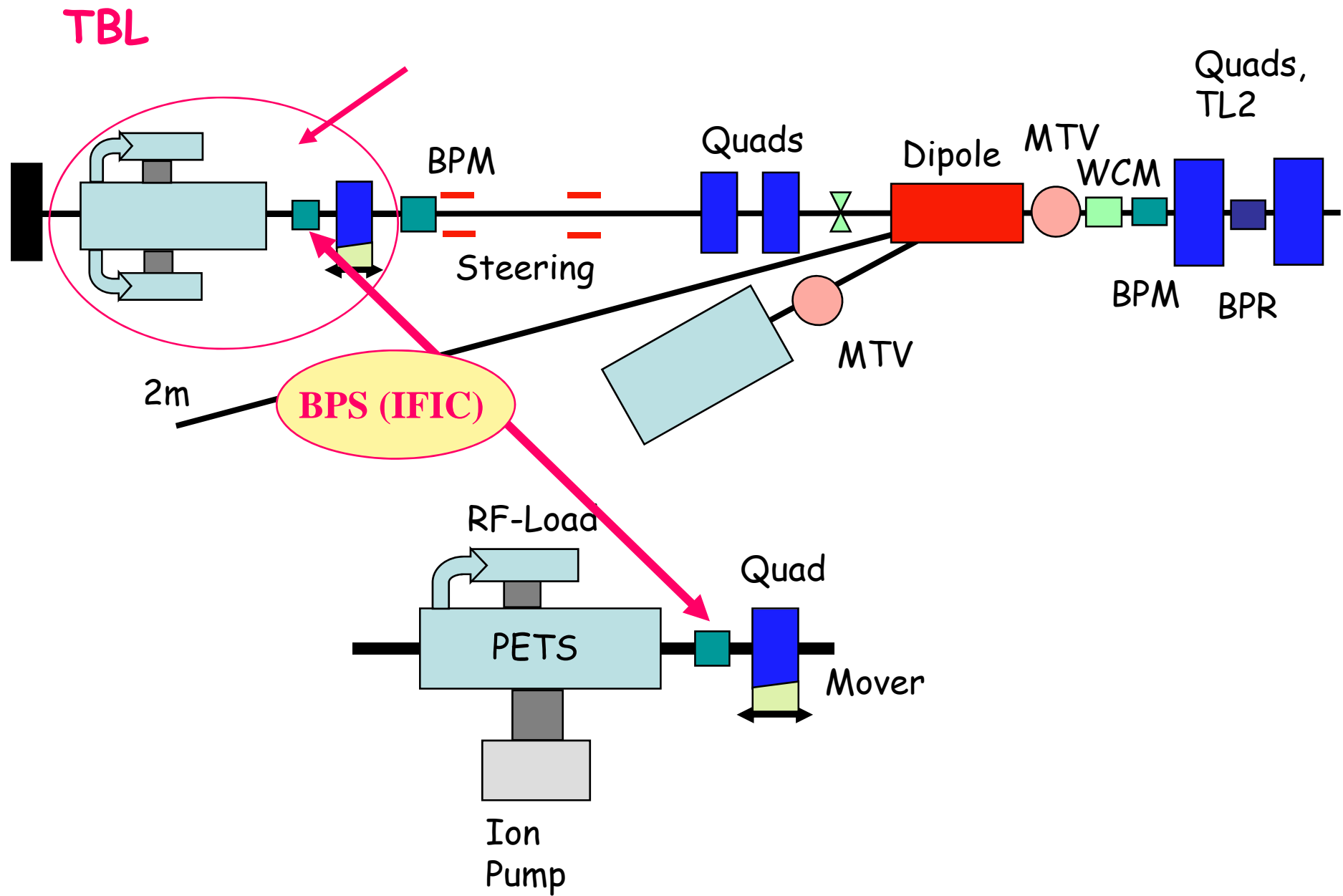
# BPM Amplifier for CTF3 TBL: Status and Future Work

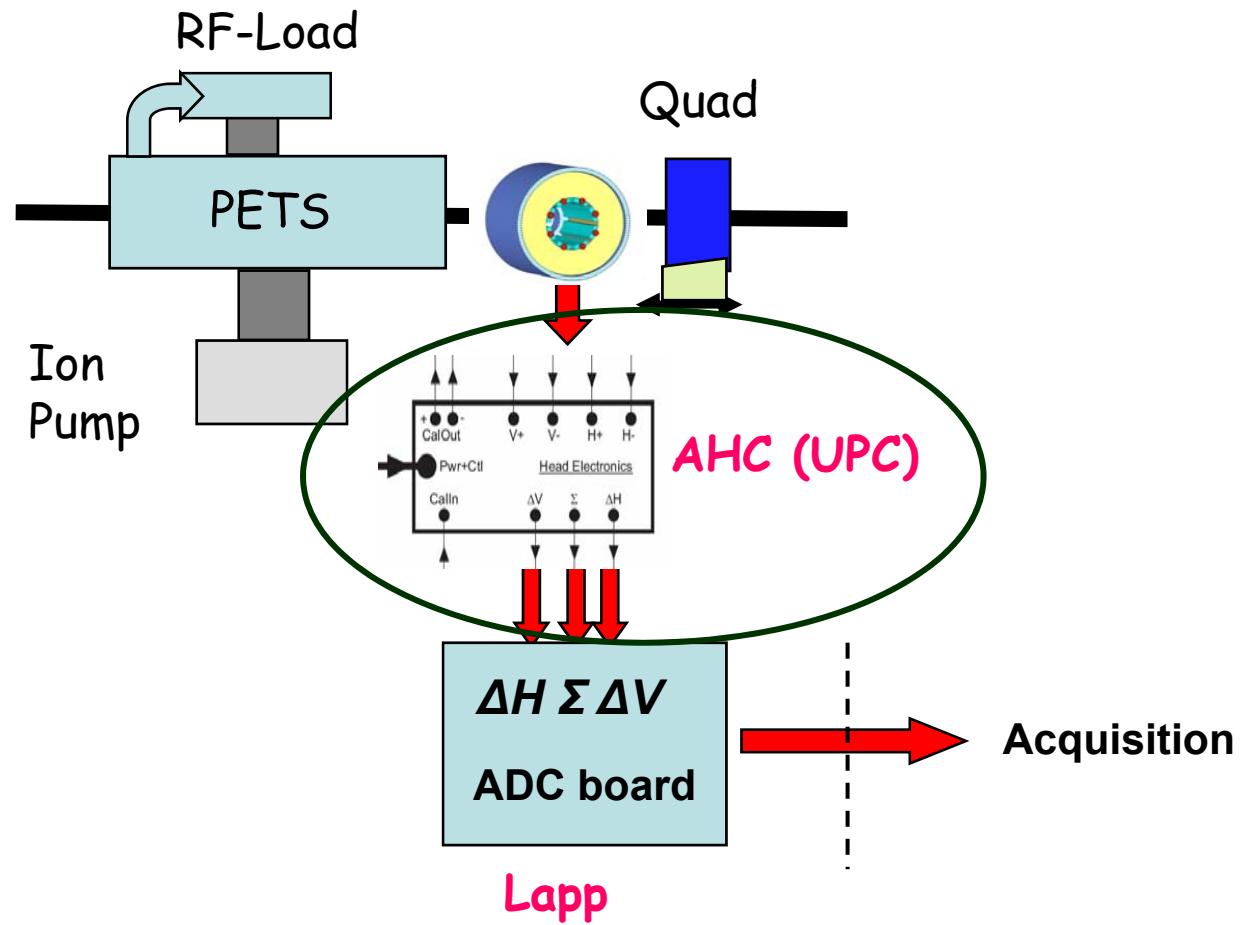
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# BPM+Amplifier specifications

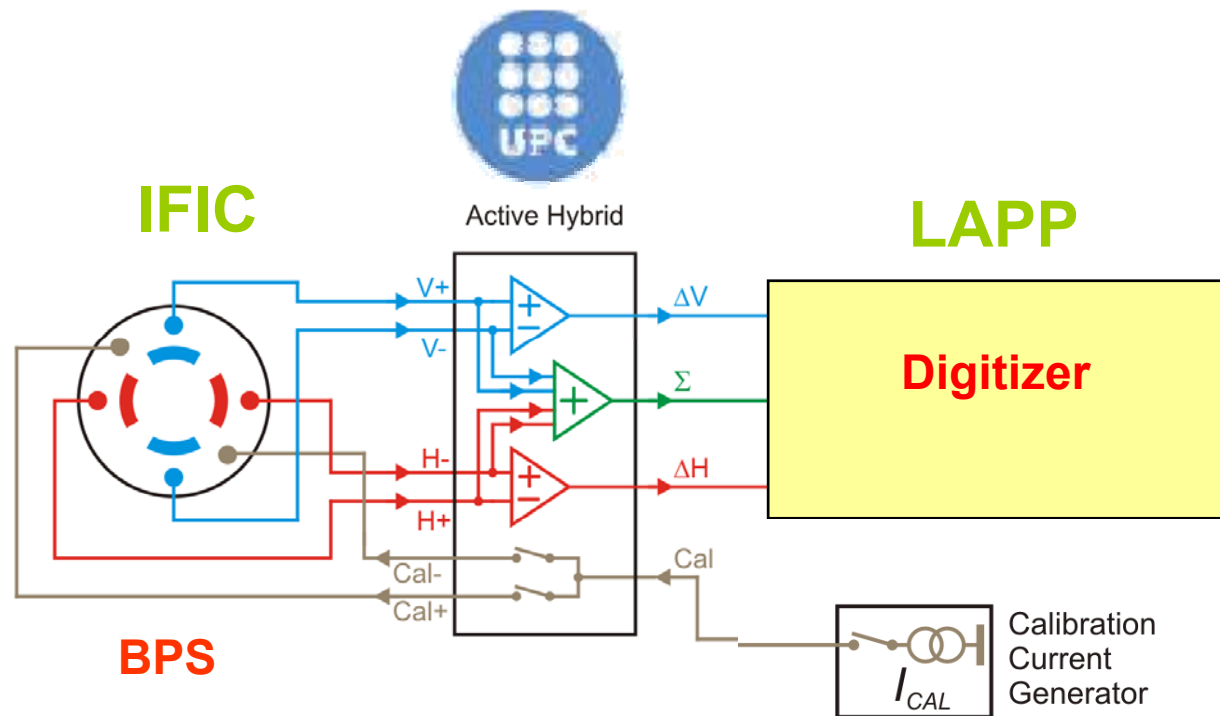
<b>BPMs for the TBL: parameters</b>	
<b><u>BPM analog bandwidth (BPM with associated electronics)</u></b>	<b><u>10 kHz -100 MHz (200 MHz is highly desirable)</u></b>
<b>Beam position range of interest</b>	<b>+/-5 mm horizontal and vertical</b>
<b>Beam aperture diameter</b>	<b>24 mm</b>
<b>Overall mechanical length</b>	<b>&lt; 100 mm</b>
<b>Number of BPM's in TBL</b>	<b>16</b>
<b>Resolution at maximum current</b>	<b>&lt;5 mm</b>
<b>Overall precision</b>	<b>&lt;50 mm</b>

<b><u>Typical radiation levels</u></b>	<b><u>&lt;1000 Gray/year (or 100 Krads)</u></b>
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# General scheme of the analog amplifier

- The signals ( $V+$ ,  $V-$ ,  $H+$  and  $H-$ ) captured by the BPM IPU are amplified and processed to the difference and sum signals which are then digitized.
- The amplifier is a part of head (front-end) electronics.



## Specifications of the interface between the analog amplifier and the BPM (developed by IFIC)

- 4 BPM outputs, one from each electrode: H+, H-, V+, V-
- 2 BPM calibration inputs
- Input and output impedances: 50 ohms
- Because of high signal levels from the BPM (due to the high current beam, around 30 A) the amplifier must include an input attenuator



## Specifications of the interface between the analog amplifier and the digitizer (developed by LAPP)

- The amplifier analog outputs must be differential and bipolars.
- Voltage levels:  $\pm 0,7V$  max
- Input and output impedances: 50 ohms
- As an output the amplifier provides 3 double (balanced) signals:
  - 1 sum signal ( $\Sigma$ )
  - 2 difference signals ( $\Delta H$  and  $\Delta V$ , corresponding to the horizontal and vertical pair of electrodes).



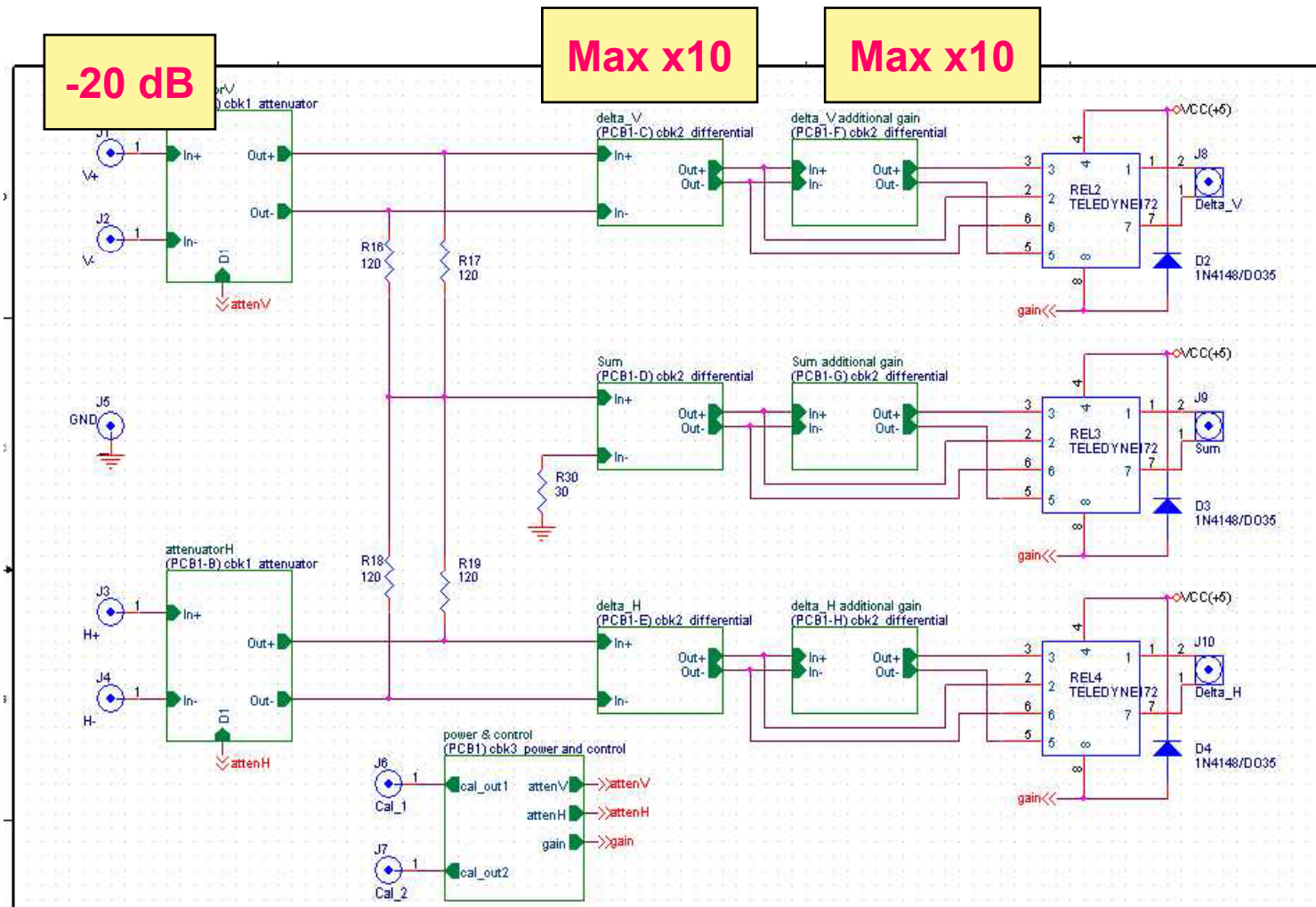
# Amplifier design: the most critical components

- **Rad-hard** wideband IC amplifier: THS4508  
(manufactured by TI and tested by up to 100 Krads)
- RHFL4913 (**rad-hard** positive regulator)  
(tested up to 100 Krads by the manufacturer, ST)
- RHFL7913A (**rad-hard** negative regulator)  
(tested up to 100 Krads by the manufacturer, ST)

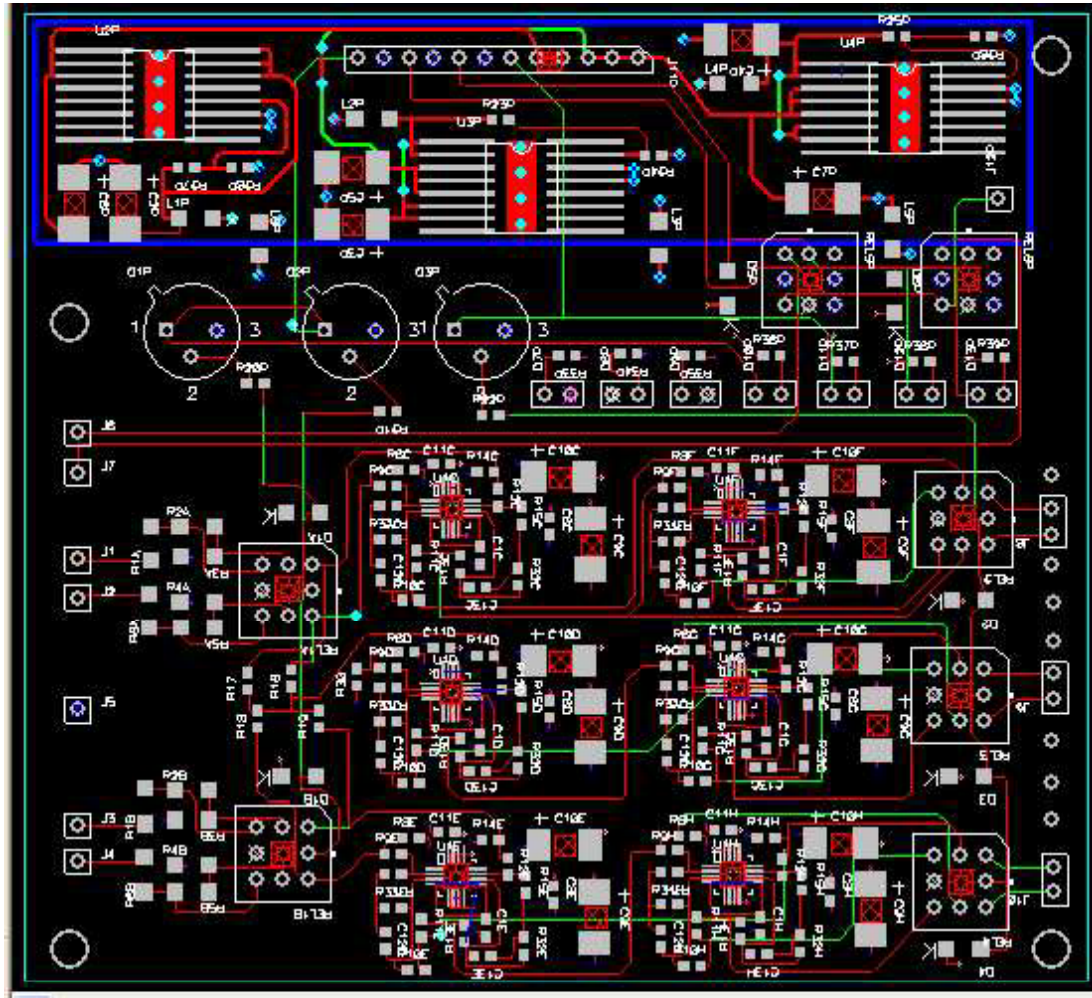




# Schematics done according to the previous specifications (first prototype)

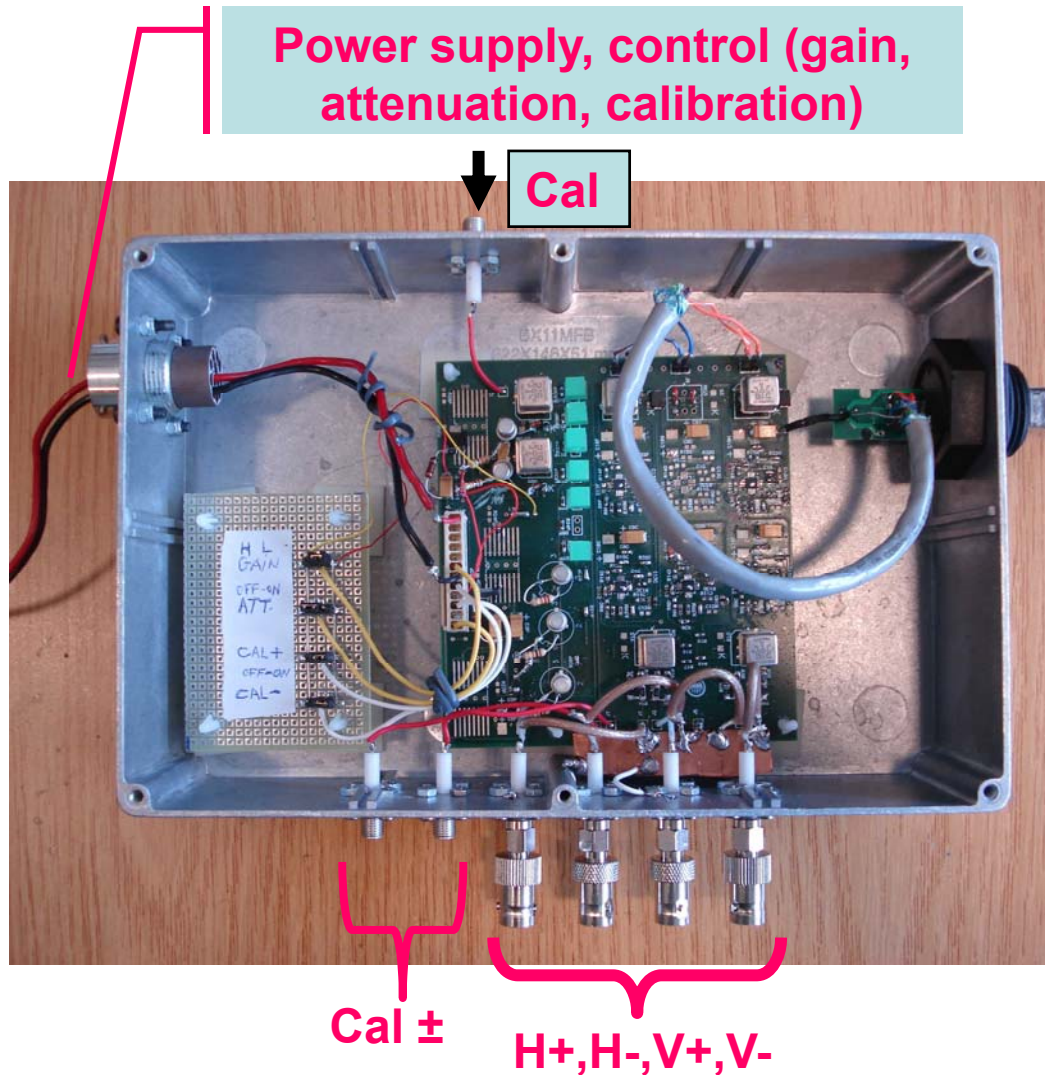


# CAD design of the PCB (first prototype)





# First version of the amplifier completed



$\Delta H, \Delta H, \Sigma$

- It was necessary to modify the **input attenuators** to reduce the high level signals transmitted from the BPM:

At the center position and in a high beam current case (30 A) each electrode output is around 4 V (at 50 ohms input impedance)



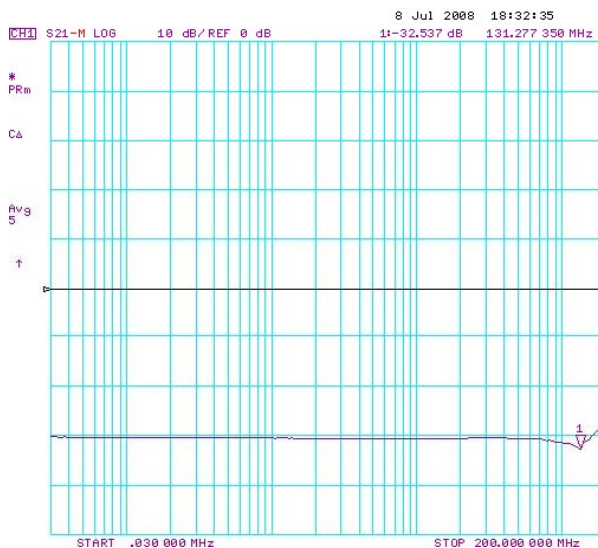
# Amplifier frequency response (test done at the UPC lab., June 2008)



-  $\Delta V$  (differential) frequency response without 'droop' compensation (from 30 KHz to 200 MHz). The curve is quite flat: OK

- The correct  $\Delta$ -channel response from 10 KHz to 30 KHz was verified by using an oscilloscope

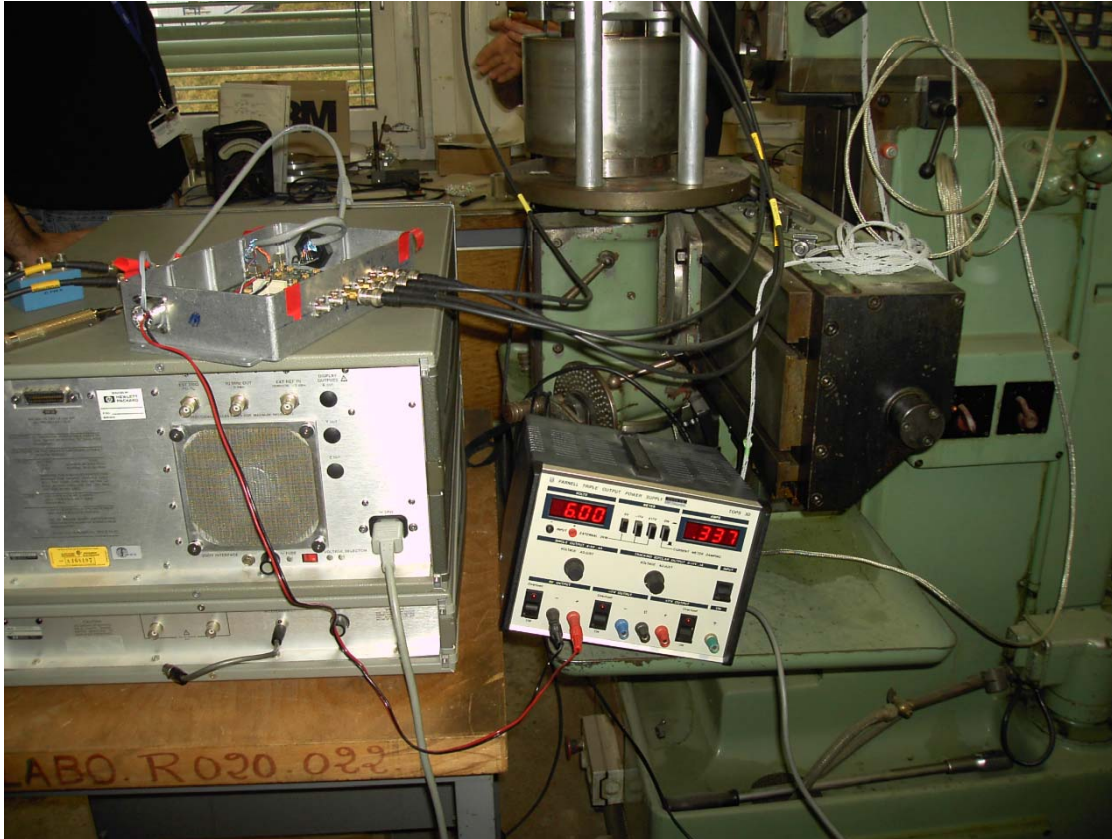
$\Delta H$  results are similar



-  $\Sigma$ -channel frequency response (from 30 KHz to 200 MHz). The curve is quit flat: OK

- The correct  $\Sigma$  channel response from 10 KHz to 30 KHz was verified by using an oscilloscope

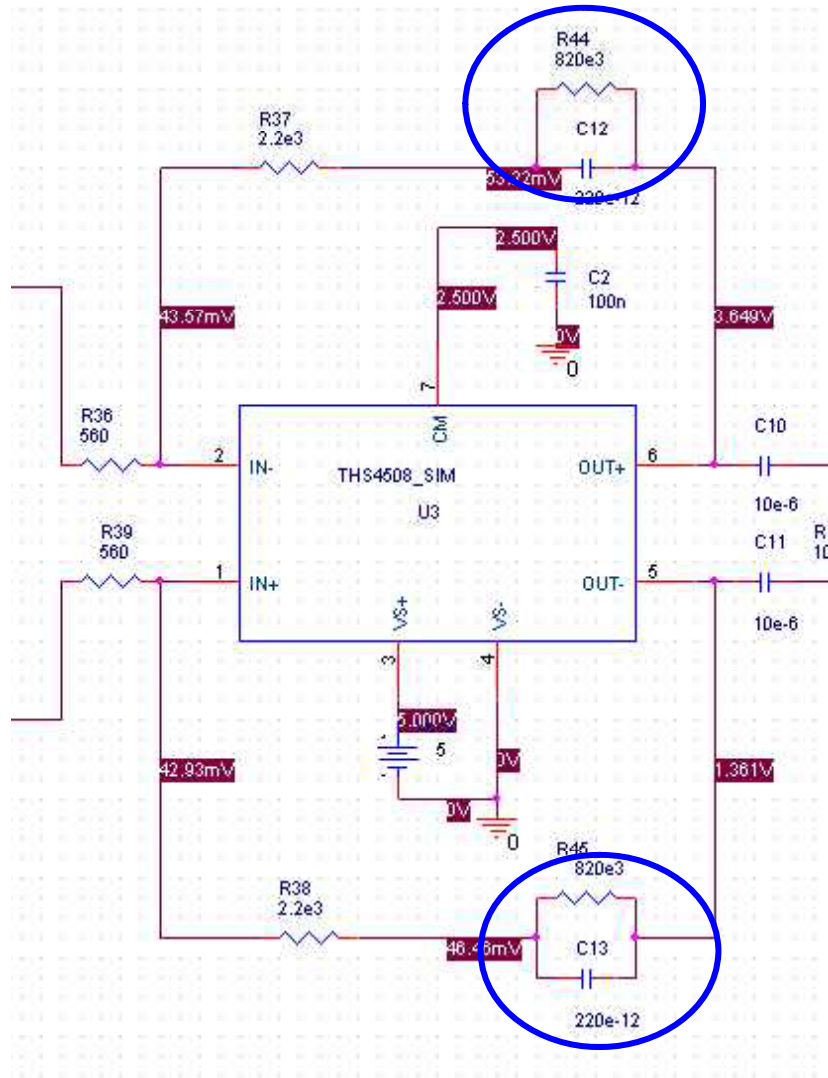




Wire test at the laboratory of Lars Soby (December, 2007)



# A 'droop' compensation has been done



- R-C network compensation:

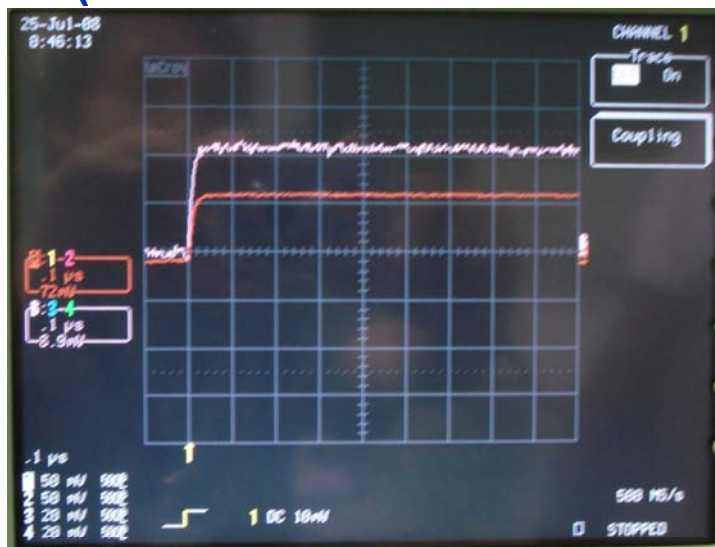
$$f_c = 74kHz$$



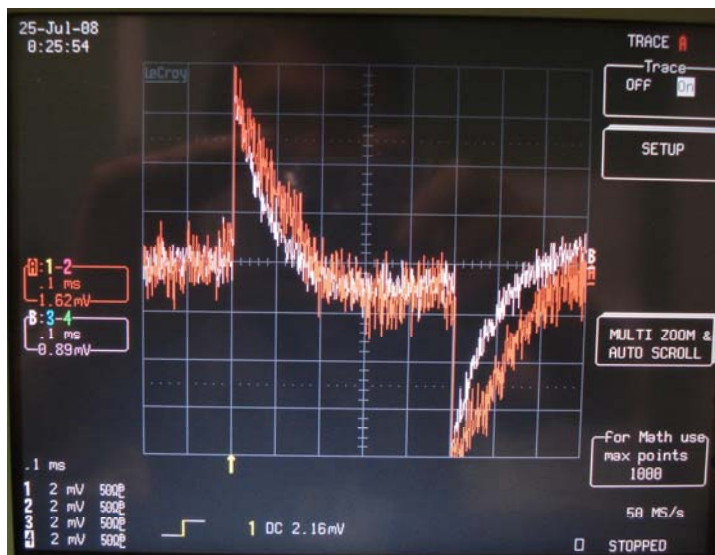
$$f_c = 10kHz$$



**IFIC BPM + Amplifier: time responses after 'droop' compensation**  
(wire and calibration tests done at the lab of Lars Soby, July 2008)



$\Delta$  and  $\Sigma$  responses to a calibration excitation signal (the oscilloscope scale is of 100 ns/div)



$\Delta$  and  $\Sigma$  responses to a 'wire test' excitation signal (the oscilloscope scale is of 10.000 ns/div)

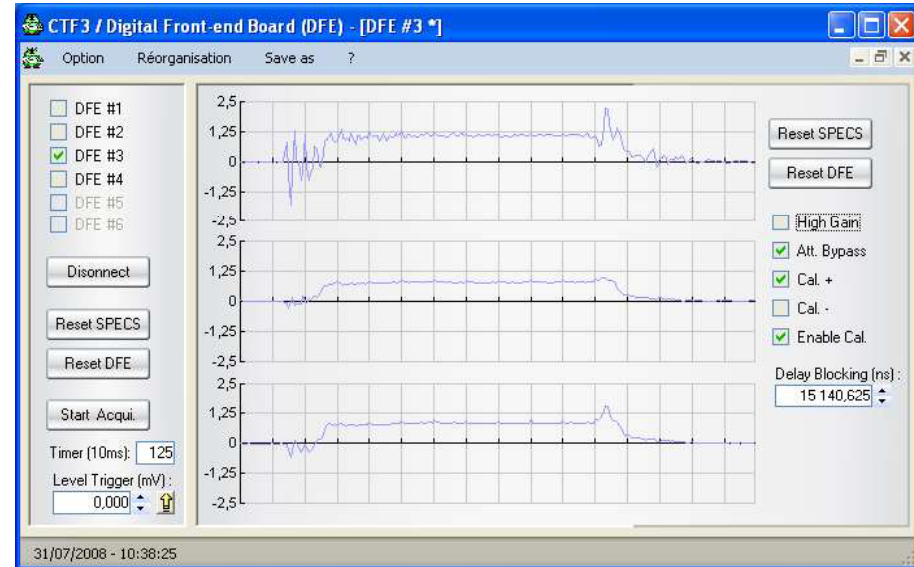




# The first prototype of the **BPS + amplifier** has been installed at the TBL (July 2008)

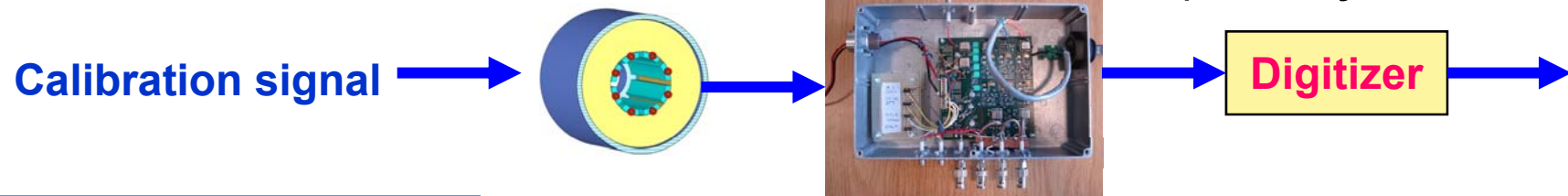


First amplifier prototype (July 2008)



First **BPS + amplifier + digitizer** test: time response to the calibration signal

(Courtesy V. Sebastien)



# Conclusions after the tests of the 1st amplifier prototype

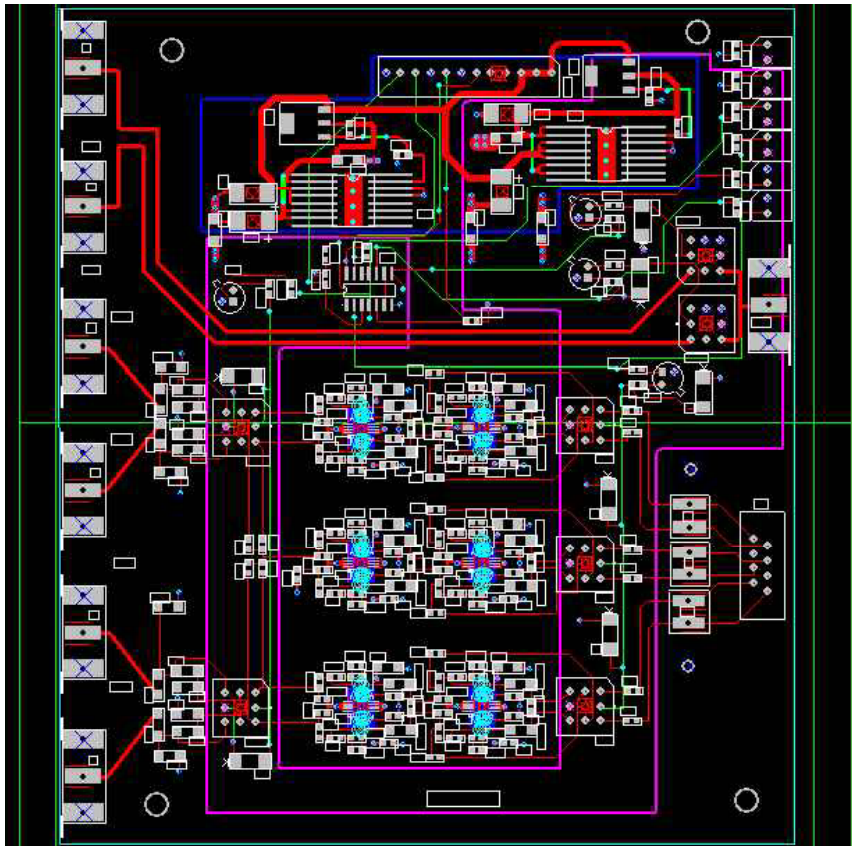
The results of the tests at the UPC lab and CERN show that the amplifier fulfills the main requirements:

- Each amplifier stage can achieve a gain up to 10.
- A bandwidth up to 170 MHz (above 100 MHz for sure) is achieved for each channel.
- The required voltage output levels are accomplished
- The amplifier electronic components are 100 Krad radiation tolerant.



## Recent work:

- The schematic and PCB routing of the second prototype of the amplifier are completed
- The following improvements are incorporated:



- ✓ The position of the connectors has been changed with the aim to eliminate the need of internal connecting cables
- ✓ The width of some tracks has been changed for a better 50  $\Omega$  matching
- ✓ Some delay differences between the channels has been compensated
- ✓ Some imperfections and drawbacks of the first prototype design have been improved



## Summary of the work done:

- **First amplifier prototype designed and manufactured** 2007
- **First laboratory tests at the UPC**
- **Wire test at CERN** December 2007
- **Improvements and tests (wire and calibration signal) at CERN with BPS** June-July 2008
- **Installation at TBL and calibration test at the TBL** July 2008



## Ongoing and future work:

- **First contact with the manufacturer of the PCB of the second amplifier prototype** **October 2008**
- **Manufacturing and testing of the second amplifier prototype** **November 2008**
- **Building and testing the total required series of the TBL amplifiers (16 units)** **Starting from December 2008**

**Acknowledgements: Thanks to our collaborators from CERN: L. Soby, F. Guillot, S. Döbert et al., IFIC and Lapp groups.**

