



### Roebel cable industrial optimization -General Cable Superconductors

Dr Nick Long, Robinson Research Institute, Victoria University of Wellington, New Zealand

### WAMHTS-1, February 2014

Acknowledgements: Rod Badcock, Kent Hamilton, Chris Bumby, Marc Mulholland, Zhenan Jiang

## Contents

- Introduction to Roebel
- Design of strands
- Punching strands
- Testing  $I_{\rm c}$
- Cable assembly
- Cable  $I_{\rm c}$
- Mechanical properties
- Insulation and reinforcement





## Cable attributes for magnet applications

- High current; uniform  $I_c$
- Available in long lengths
- \$/kA-m
- Stability (risks of quench, equal current sharing among strands)
- Mechanical behaviour
  - $I_{\rm c}$  stress, transverse and longitudinal
  - Bending radii
  - Coil manufacture; potting
- Manageable AC losses





## **HTS Roebel cable**

- Started R&D at IRL in 2004
- Commercialised through General Cable Superconductors •

#### Goals

- Develop long length Roebel cable manufacture
- Prove applications in high current and/or AC machines
  - 150 MW generator (Siemens)
  - 1 MVA Transformer (Robinson Research Institute (ex IRL))









## What is HTS Roebel Cable?

- A high capacity winding cable from coated conductor
- Continuously transposed



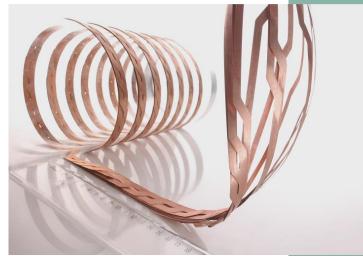


Photo courtesy of Siemens

Cables are labelled (no. of strands) / (strand width)





## Design of strands/cable

- Existing designs are a compromise
  - Use the wire which was available
    - 12 mm SuperPower
    - 10 mm Fujikura and STI (from 2013)
  - Keep tool piece manufacture simple
  - Minimise problems in automated winding
  - Minimise mechanical problems





## Design of strands

Figure – Roebel strand

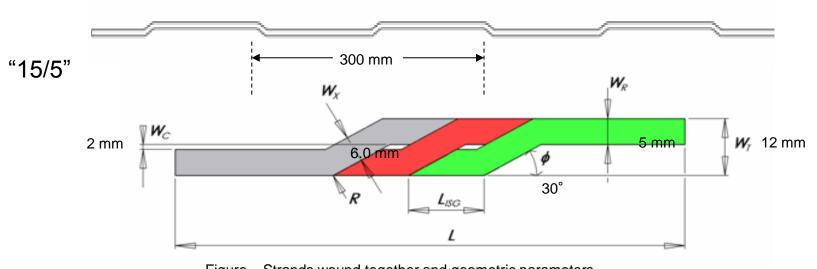


Figure – Strands wound together and geometric parameters

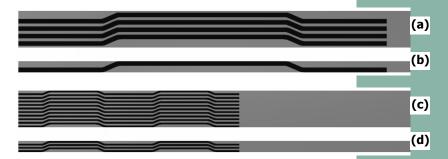
	Parameter	Name	2 mm Cable	4.5 mm Cable	5 mm Cable
	L <sub>TRANS</sub> (=2L)	Transposition length	90 mm	300 mm	300 mm
	W <sub>R</sub>	Strand width	2 mm	4.5 mm	5 mm
	W <sub>X</sub>	Crossover width	1.7 mm	5.0 mm	6.0 mm
-	SUPERCONDU	JCTORS			

### Strand manufacture

#### Punching



Automated multi-strand production



Formation of Roebel punched strands in 40 mm and 12 mm wide feedstock material.

- (a) 4 x 5 mm strands in 40 mm wide material,
- (b) 1 x 5 mm wide strand in 12 mm wide material,
- (c) 10 x 2 mm strands in 40 mm wide material,
- (d) 3 x 2 mm wide strands in 12 mm wide material.

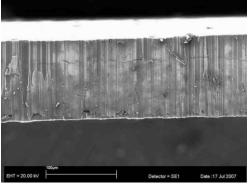


#### Wire demonstrated: AMSC, SuperPower, Fujikura, STI

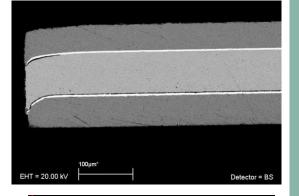


### Quality of punching: AMSC wire

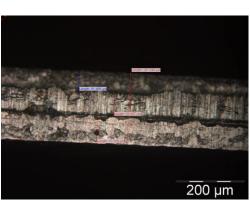
Electroplated copper/NiW



Electroplated copper/NiW



#### AMSC 3 ply SS/NiW/SS



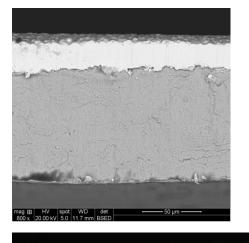
AMSC 4 ply Cu/2x NiW/Cu

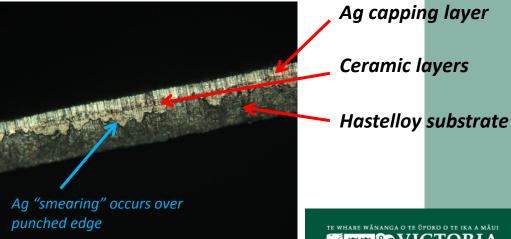




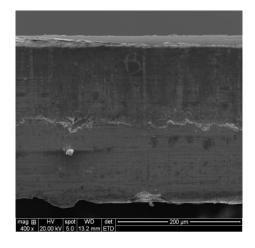
### Fujikura: Silver-stabilised punched strand

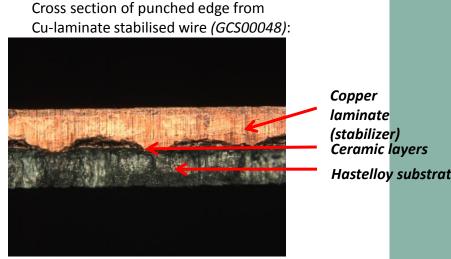






## Fujikura Cu-laminated wire – punched strand

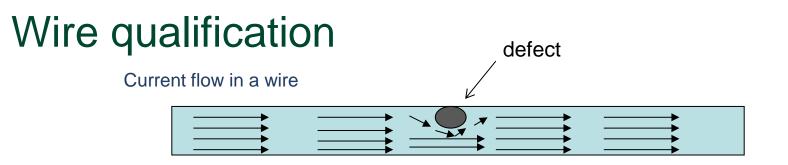




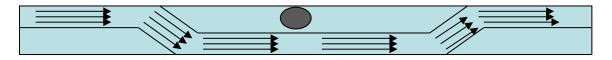
Total thickness: ~200µm

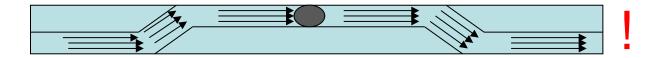
Hastelloy substrate





#### Current flow in a Roebel strand









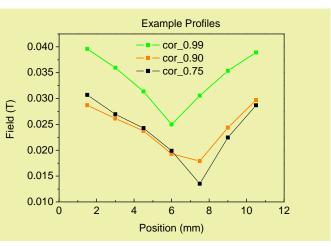
## Wire qualification

- Scan wire magnetically (penetrated or remanent field)
- Quantify uniformity using statistical correlation with an ideal magnetic profile

$$Corre[X,Y] = \frac{\sum (x-\bar{x})(y-\bar{y})}{\sqrt{\sum (x-\bar{x})^2 \sum (y-\bar{y})^2}}$$

Where  $|Correl| \le 1$ 

X is a dataset representing calculated field  $Y\{y_1...y_i\}$  is magnetic data across tape



0.023 T

Correlation along

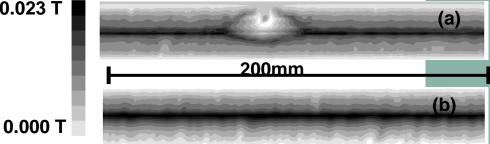
a length of YBCO

specified for input

wire, a minimum

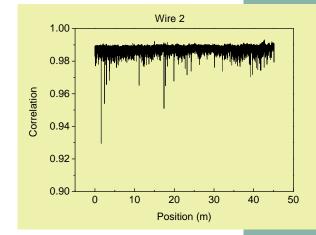
Correl can be

wire



We use continuous scanning of the Remanent magnetic field to assess tape quality (a) tape with a known defect, and (b) tape with only small scale variability.

#### Some wire is extremely good !



### $I_{\rm c}$ measurement of strands

Spiral racetrack former for testing strands up to length 30 m.



- Punched strands are moisture sensitive
- Heat in dry nitrogen only





Sample #	Length	Tape transport Ic	Min{Correl}	Strand transport Ic
	(m)	(A/cm)		(A/cm)
1	27	248	0.98	232
2	27	213	0.89	200
3	27	213	0.85	239
4*	27	265	0.94	191
5	27	263	0.9	236
6	27	329	0.88	310
7	27	215	0.9	243
8	27	322	0.9	309
9	27	363	0.94	334
10*	27	400	0.78	307

Table 1. Example performance of selected wire and 5mm strands



### Summary of strand performance

- $(J_{\rm e} \, {\rm strand}) \, / \, (J_{\rm e} \, {\rm wire}) \sim 90-95\%$
- High minimum value of *Correl* is necessary but not sufficient condition

 $\rightarrow \Delta I_{\rm c}$  also needs to be considered

→ Length of defect important

→ Scaling to low T, defects look like a cross sectional loss of conductor

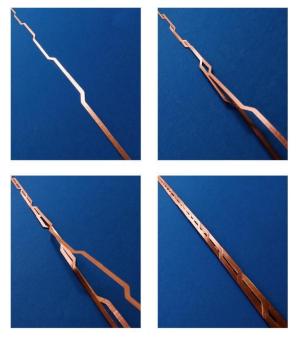
- Can we mitigate low Correl values?
  - Probably not!

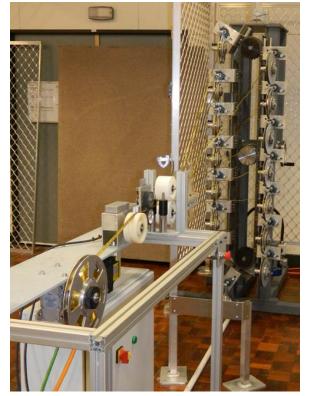




### Cable assembly

#### Illustration of the assembly process





Automated planetary wind system for 15/5 cable



## Assembly issues

- Long length registration of crossovers
  - Need high precision for each transposition length in the punching process
  - Need tension control on strands in winding
  - Difficult to simulate (relevantly) with low cost dummy cables
    - Mechanical properties
    - Camber





### $I_{\rm c}$ measurement of cables @ 77 K

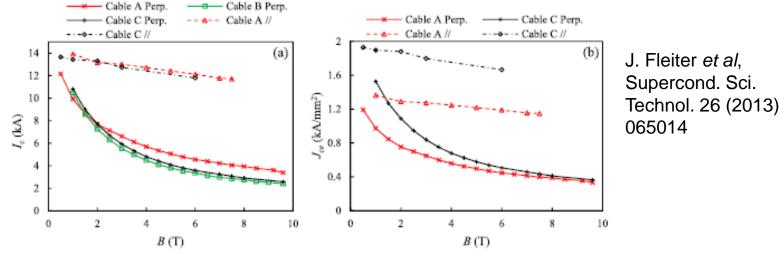
Cable details	Cable $I_c(A)$		
	Design $I_{\rm c}$	Measured	Computed
5/2	252	203	220.1
9/2	426	318.8	339.1
9/2	426	341.9	359.1
15/5	1454	1100	1033
15/5 SRC0024	1616	1010	1109
15/5 SRC0027	2093	1410	1372

RRI – 1 MVA Transformer

- Measured  $I_{\rm c}$  has been close to expected  $I_{\rm c}$
- For short length cables accurate  $I_c$  measurement is difficult
- At 77 K there are strong self-field effects



#### $I_{\rm c}$ measurement of cables @ 4.2 K



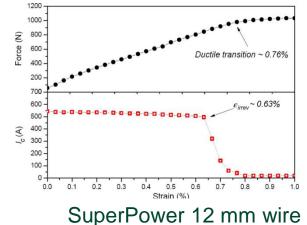
**Figure 5.** (a) Critical current measured on RACC cables (markers) as a function of applied field. The  $I_c$  was measured using the 0.2  $\mu$ V cm<sup>-1</sup> criterion. (b)  $J_{ce}$  of cable A and C in parallel and perpendicular field.

#### From manufacturing perspective cables work as advertised

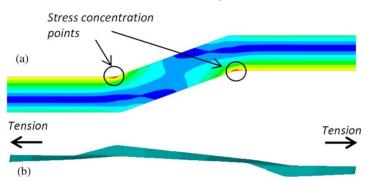
- Measured  $I_c$  close to expected  $I_c$  (taking into account self-field)
- These cables used both 'CF' (Cable A) and 'AP' (B + C) Superpower wire
- Actual strand  $I_c$  @ 4 K values were not measured



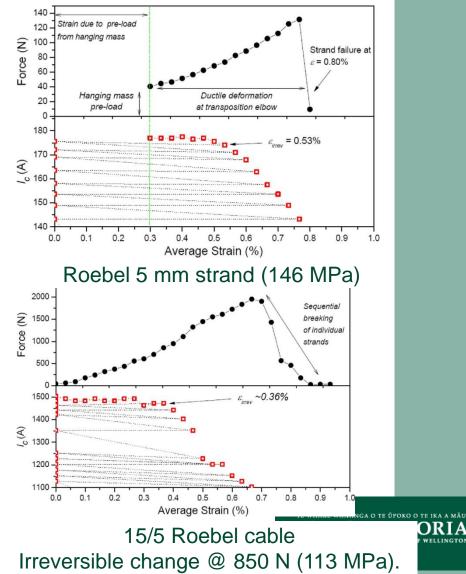
# Mechanical properties – longitudinal stress-strain



Irreversible change @ 840 N (700 MPa).



Von Mises stress @ 0.4% strain



## Mechanical properties

- Roebel shape weakens structure
  - 1/6 reversible strain limit of straight wire
- Mitigate through
  - Potting
  - Reinforcement and wrapping
- Transverse stress effects
  - Again get stress concentration
  - Up to 45 MPa without  $I_c$  degradation (15/5 cable CERN)
  - Degradation at 10 MPa, (10/2 cable with insulated strands -EPFL)



## Wrapped insulation



- Nomex wrapped 12 mm wide cable
- Need to include a reinforcing Hastelloy or stainless steel tape
- Nomex adds 200 microns total thickness



Roebel cable ready for testing at Siemens Corporate Technology, Germany.



## Winding and Potting coils

- Strands need to move during coil winding
  - Tight insulation wrapping not advisable
- Coated conductor has known interfacial mechanical weakness which can cause problems in potting
  - This applies to Roebel as well
  - We have damaged cable by using Stycast
- Getting complete void filling needs consideration for large coils



## Conclusions

- Manufacturing procedures in place for long lengths
- *I*<sub>c</sub> performance
  - Cables preserve tape performance (~90%)
- Quality control
  - Measuring magnetic Correl is relatively easy
  - Measuring strand  $I_c$  is time consuming and adds risk
- Cables up to 25 m (15/5 cables) delivered to customers
  - We have wound up to 40 m length
- Cost ultimately dominated by wire cost
- AC loss well characterised (not discussed here)



## Thank you for your attention!



