

# Optimizing 2212 with Overpressure (OP) Processing

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# Overview

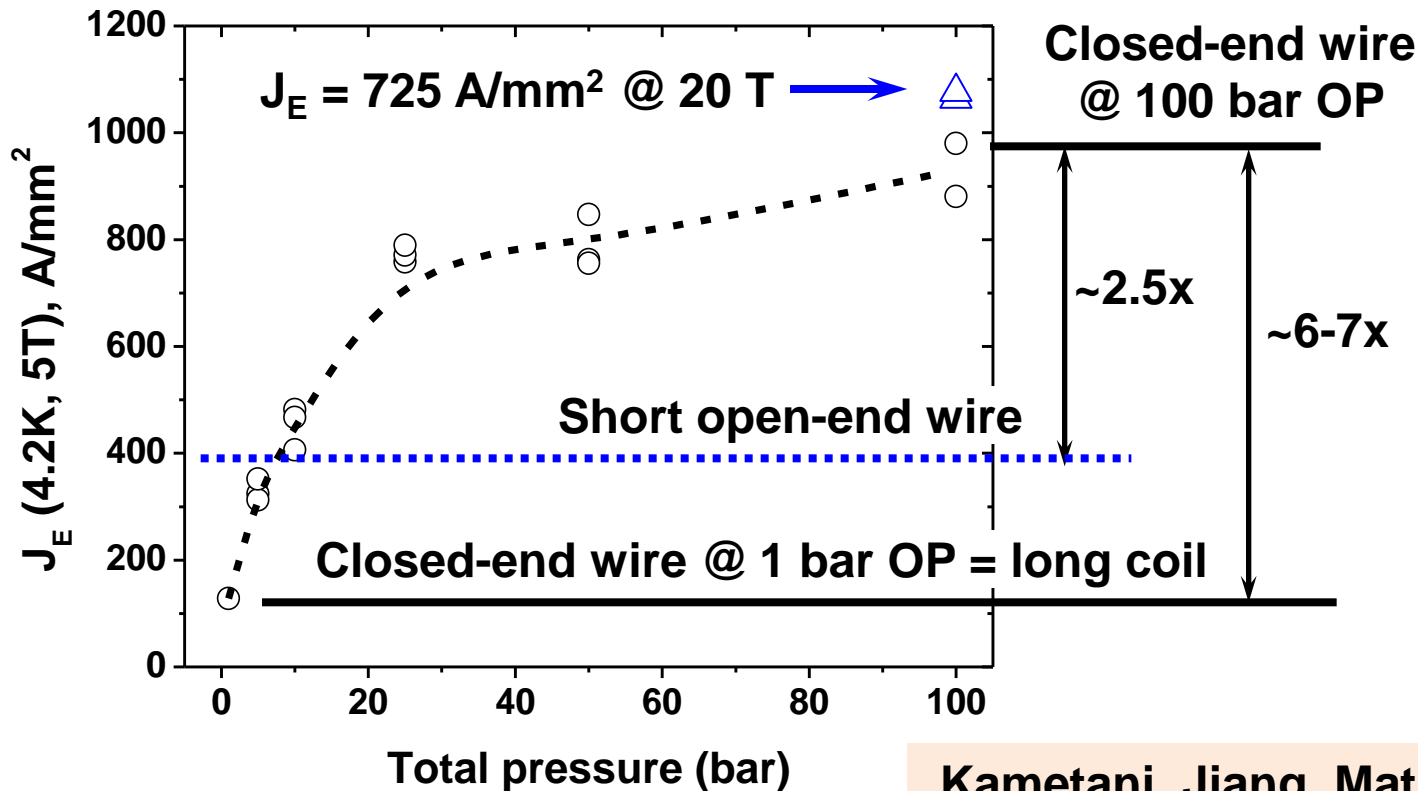
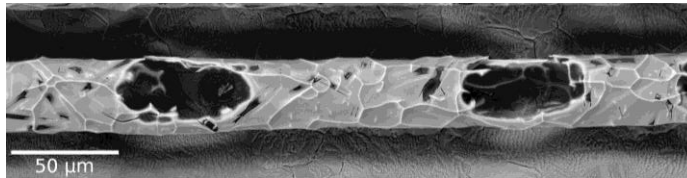
- **Why 2212 needs overpressure (OP) processing**
- **$J_E$  is now useful for accelerator magnets**
- **Questions that drive research at ASC**
- **Update on OP furnaces at ASC**

# Removing bubbles with overpressure (OP) processing more than doubles $J_E$

Gas-filled bubbles due to powder being only 60-70% dense

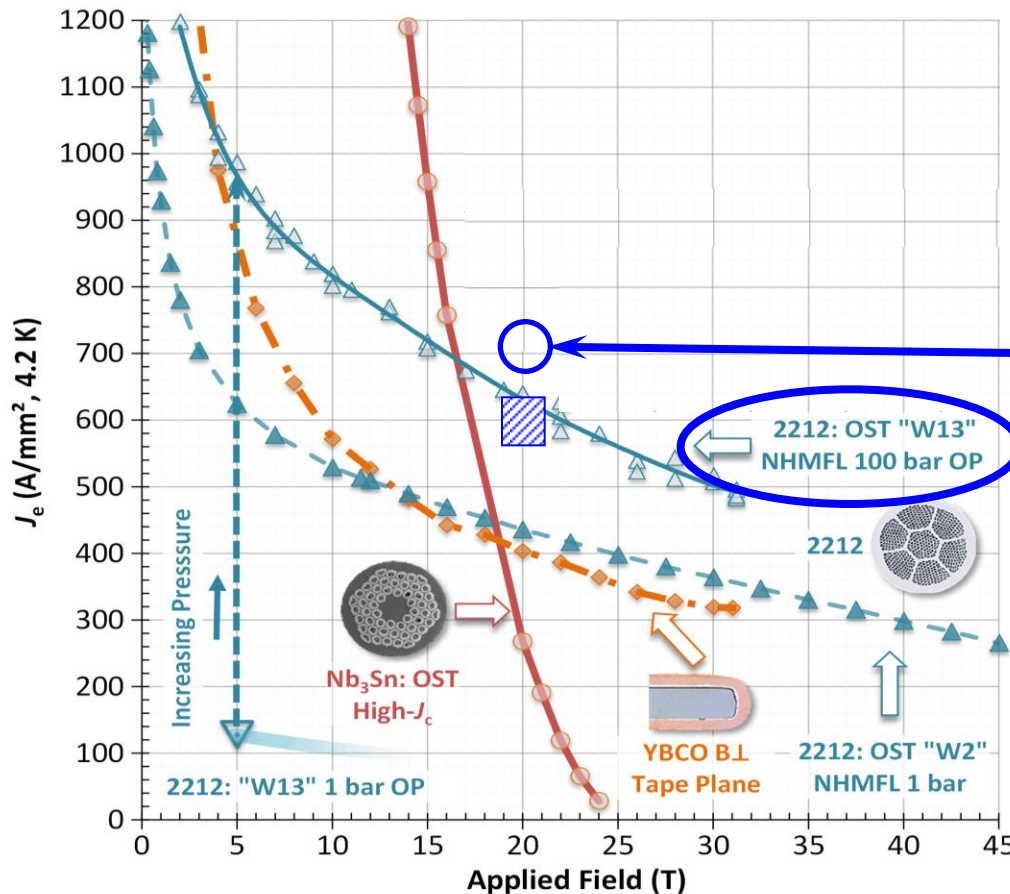


Squeeze wire to remove bubbles



# High $J_c$ and $J_E$ in OP wire (4.2 K, 20 T)

$$J_E = 640 \text{ A/mm}^2 \quad J_c = 2500 \text{ A/mm}^2$$

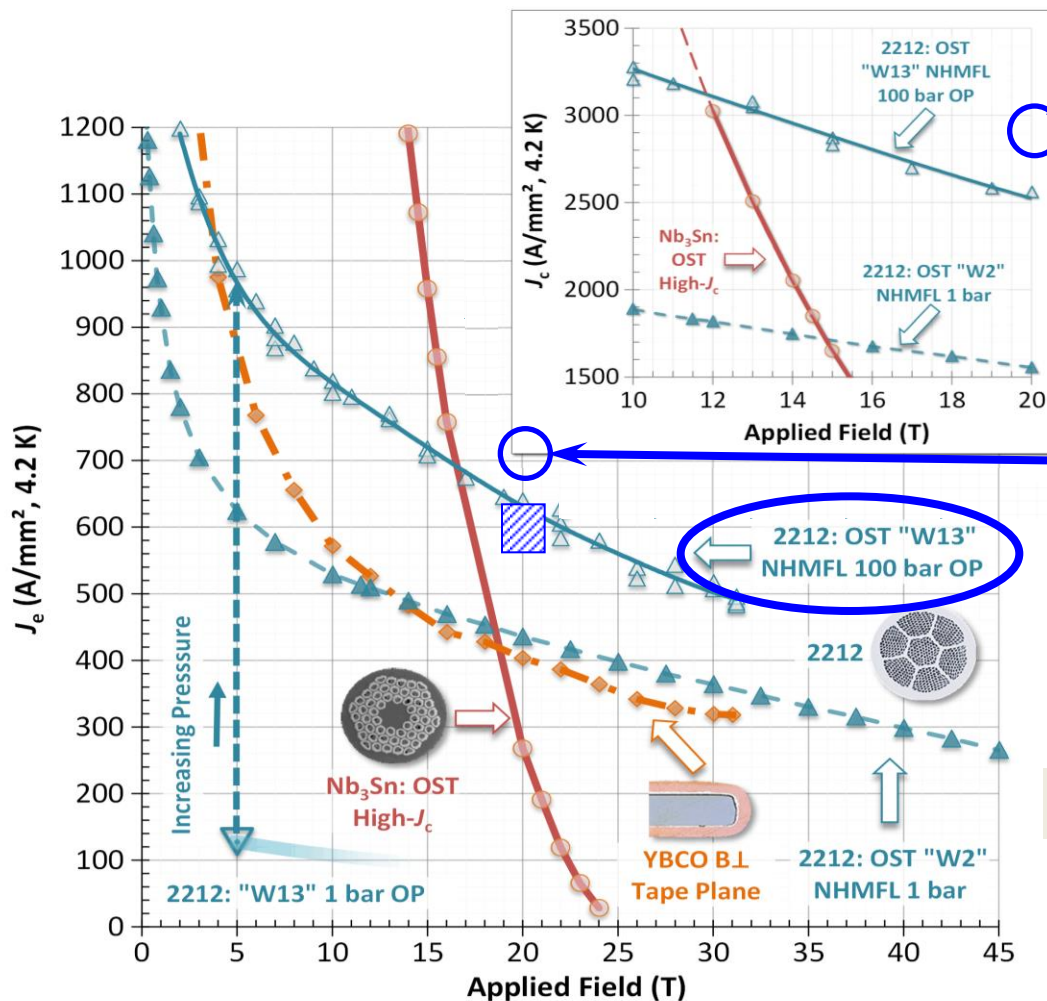


$$J_E = 725 \text{ A/mm}^2$$

Lee and Dalban-Canassy

# High $J_c$ and $J_E$ in OP wire (4.2 K, 20 T)

$$J_E = 640 \text{ A/mm}^2 \quad J_c = 2500 \text{ A/mm}^2$$



$J_c = 2900 \text{ A/mm}^2$

$J_E = 725 \text{ A/mm}^2$

Lee and Dalban-Canassy

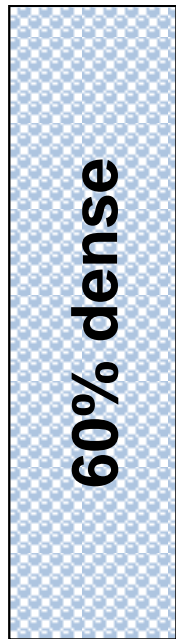
# What can happen to 2212 filaments during melt processing?

- Maximum packing density of 2212 powder in filaments is 60-70%
- Focus on the 30-40 vol% of the filament that is gas-filled void space

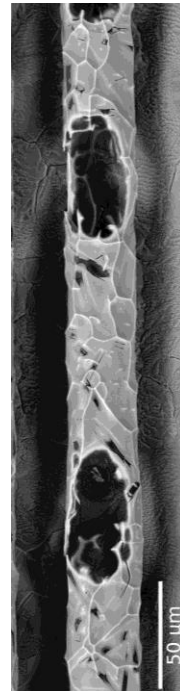
60% dense 2212 powder in green wire



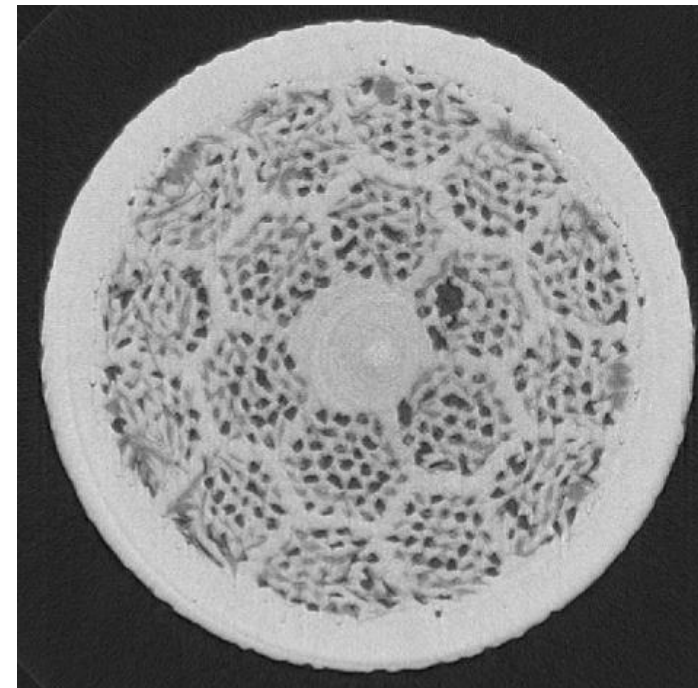
# Best case with 1 bar processing: 30-40% gas bubbles in filament



1 bar – clean powder, no  $\text{CO}_2$ ,  $\text{H}_2\text{O}$



Kametani



Scheuerlein

# **Real-time, *in situ* x-ray microtomography shows how bubbles form and grow during heat treatment**

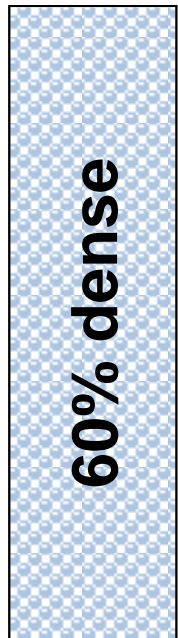
- **Video shows filaments in 2212 wire  
during heating and cooling in 1 bar air**

Scheuerlein

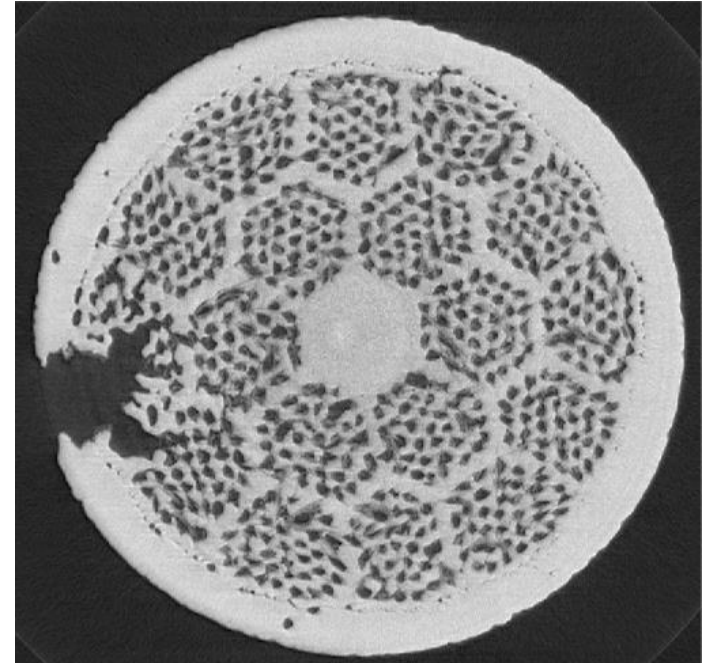
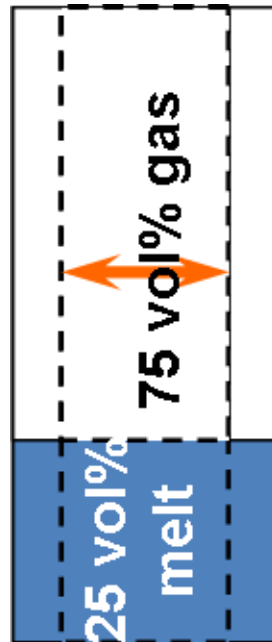


# Worst case with 1 bar processing: dedensification and leakage

Internal gas pressure  
expands filament hole



1 bar – dirty  
powder: CO<sub>2</sub>, H<sub>2</sub>O



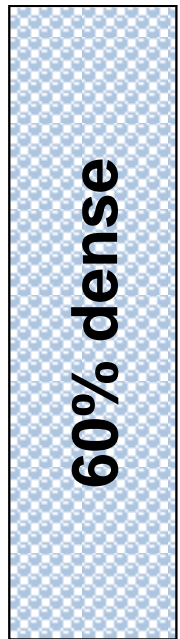
- Malagoli
- Shen

Scheuerlein

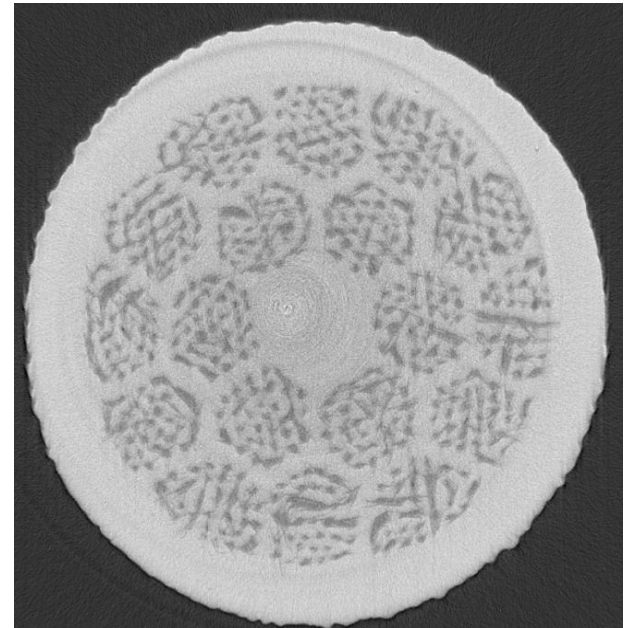
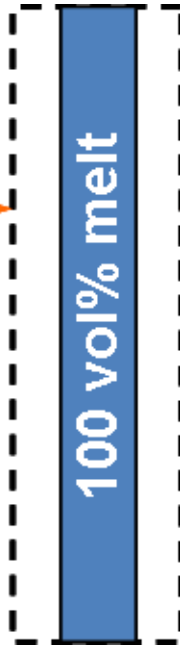
# Best processing: apply overpressure to squeeze Ag so filament hole matches 2212 volume $\Rightarrow$ 100% dense

External overpressure decreases filament hole

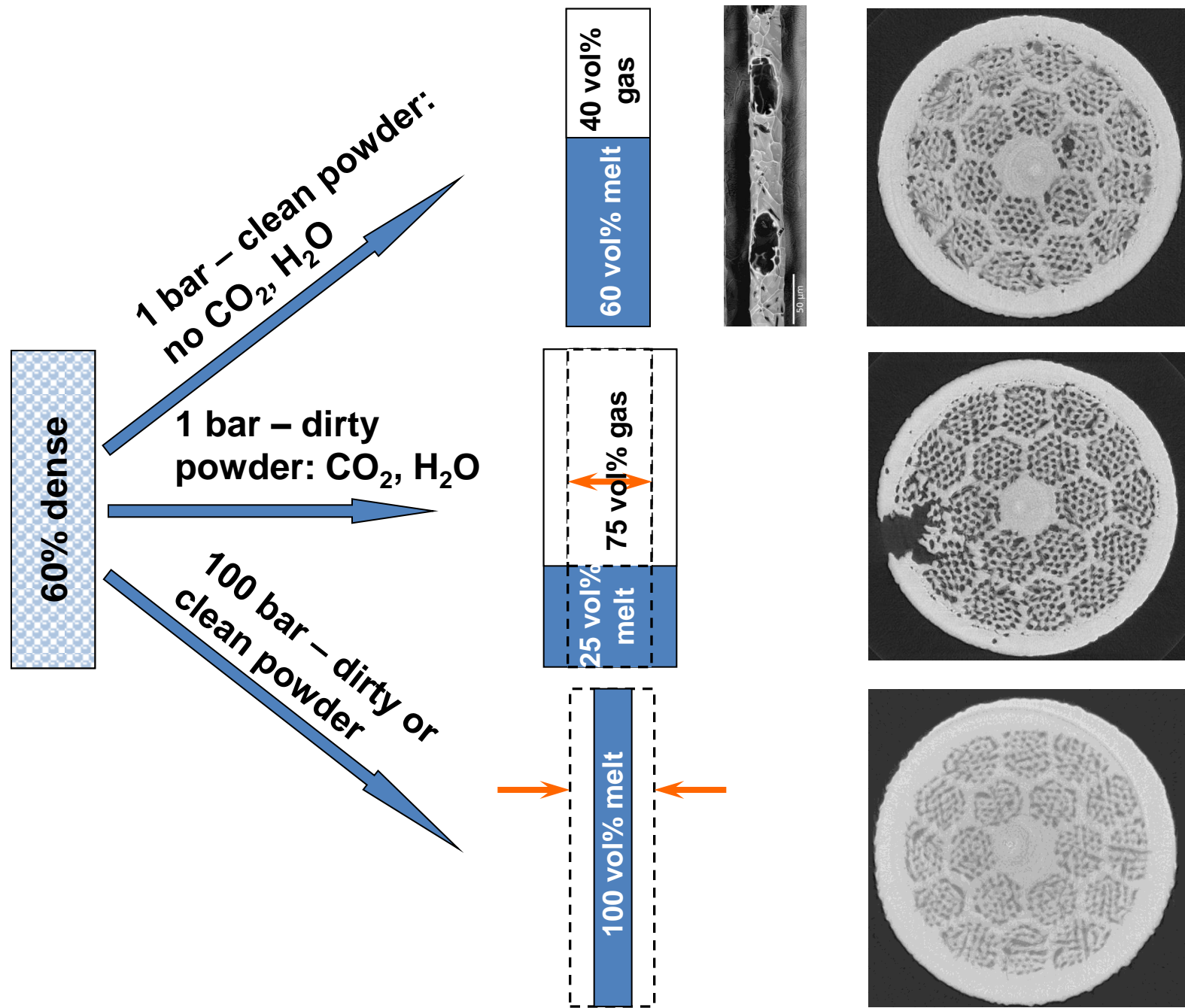
OP decreases wire diameter



100 bar – dirty or clean powder



Scheuerlein

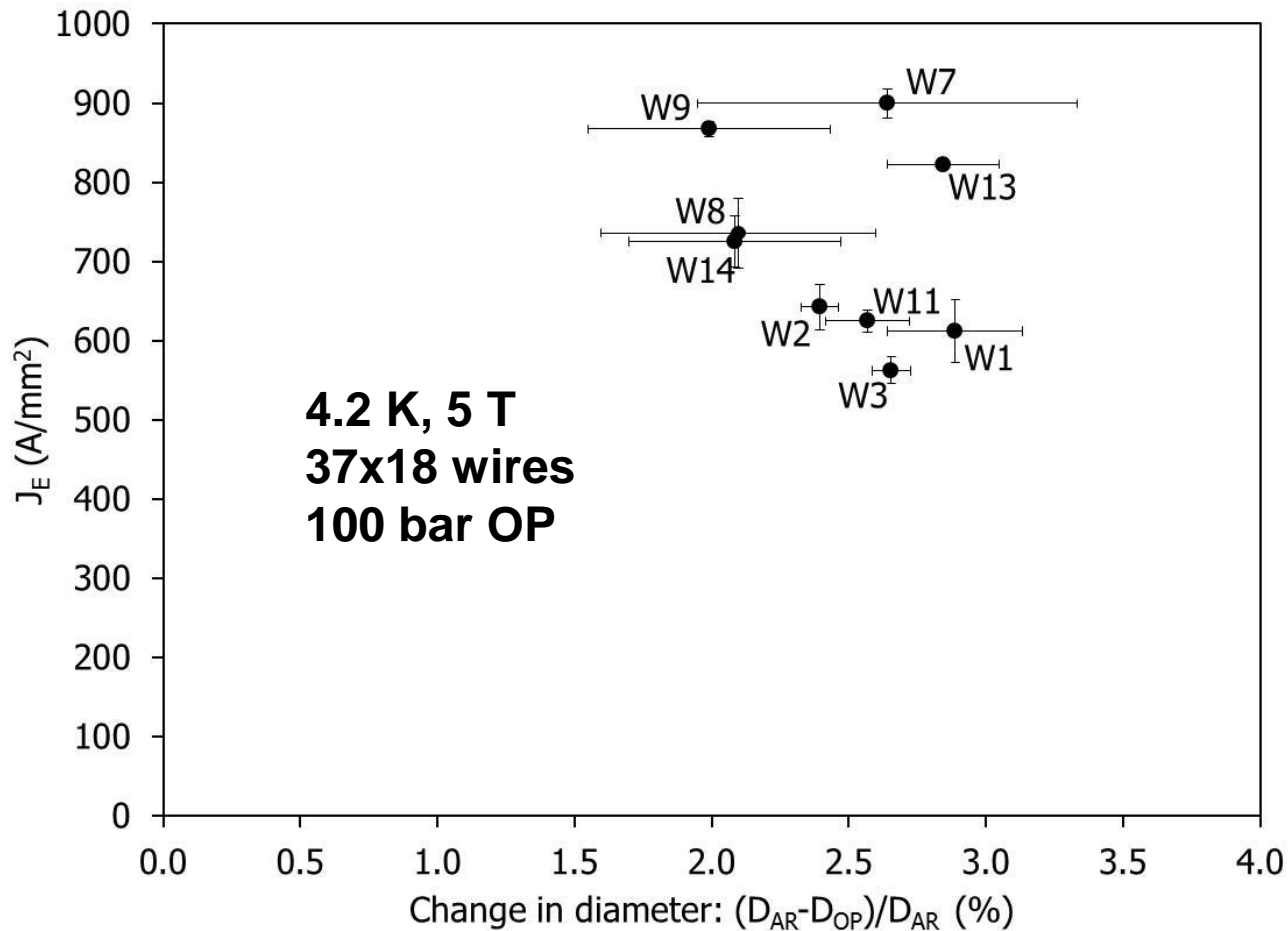


# Questions driving our 2212 studies

In some cases we repeat earlier studies now using OP processed (dense) samples.

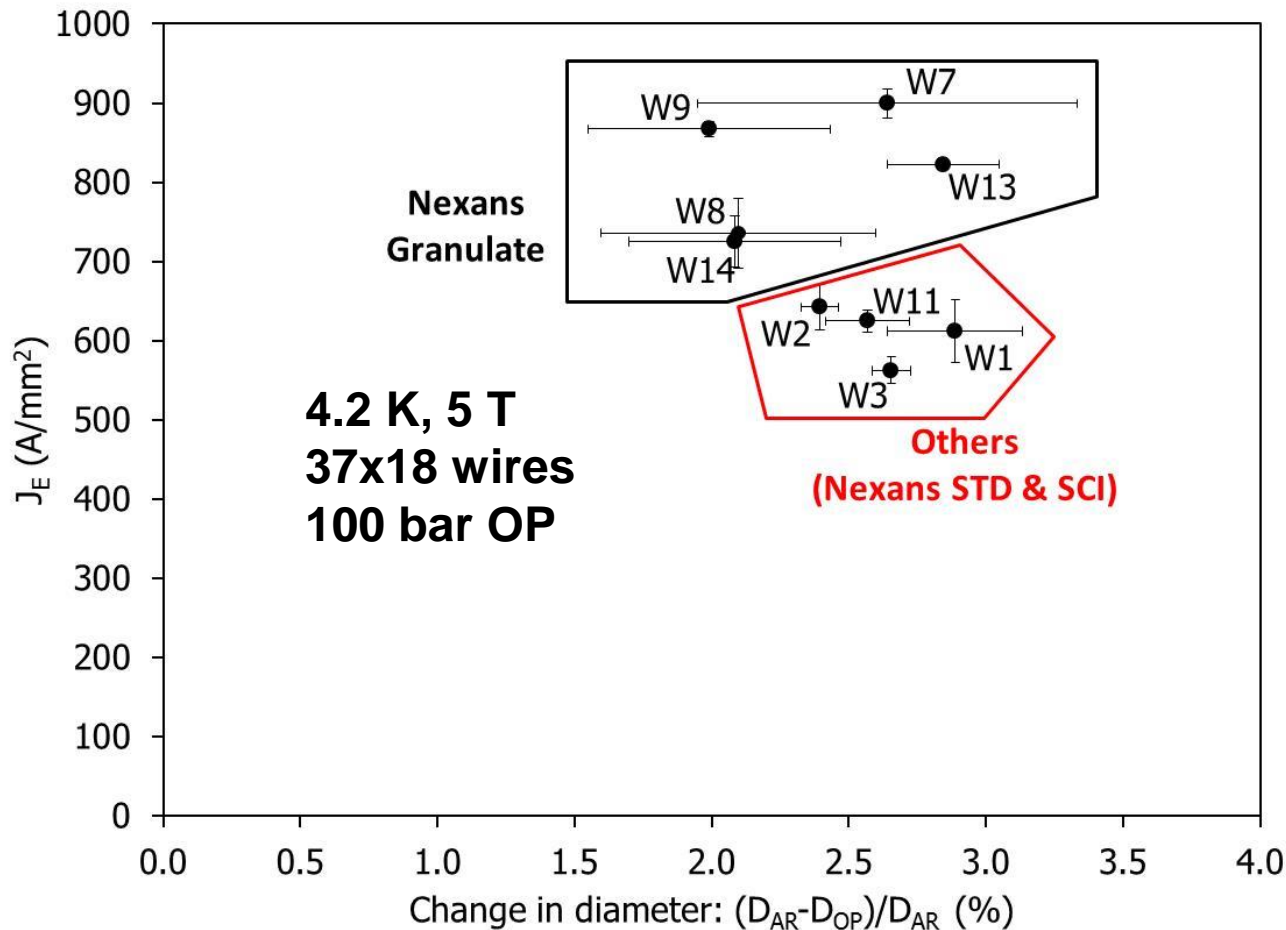
- Is there any clear evidence that one powder is better than another?
- How uniform along the length does OP leave the samples?
- Do billets with less C and H require lower OP pressure?
- What is the optimum filament diameter ( $d_f$ ) for optimum  $J_c$ ?
- Can we do a better ODS on both Ag/Mg and Ag/Al than we are doing at present?
- How do we measure powder quality?

# 1 - Q: Is there clear evidence that one powder is better than another?



**1 - Q: Is there clear evidence that one powder is better than another?**

**A: Nexans granulate gives highest  $J_E$  after OP processing.**



**Potential new powder sources**

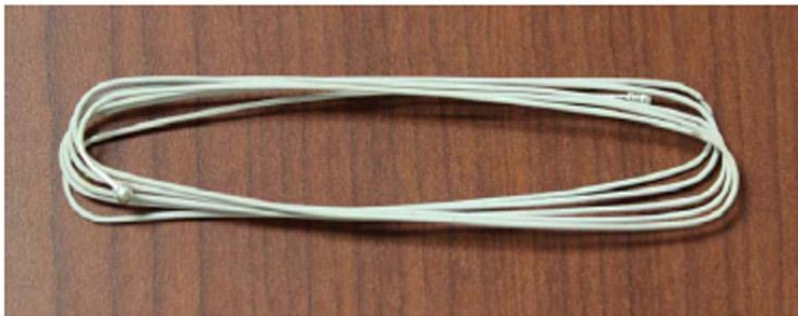
- Metamateria
- nGimat
- SMS

2 - Q: How uniform along the length does OP leave the samples?

A:  $I_c$  across 1 m sample shows  $\pm 1.1\%$  standard deviation

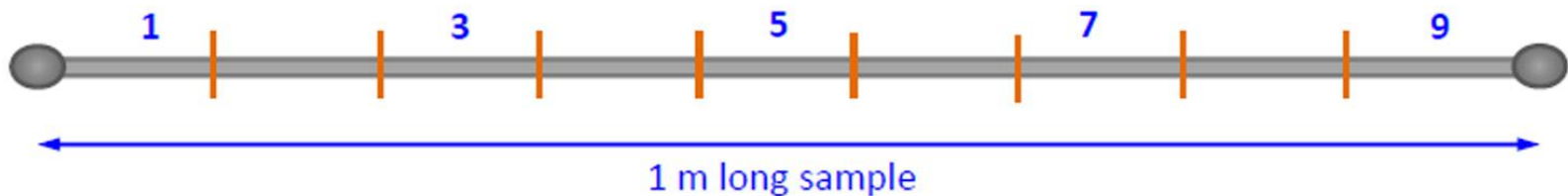
1 m long wire vs. 8 cm long witness with closed ends and processed at 100 atm

1 m long wire with insulation after 100 bar OP HT



Presented at MT-23  
and EUCAS-2013

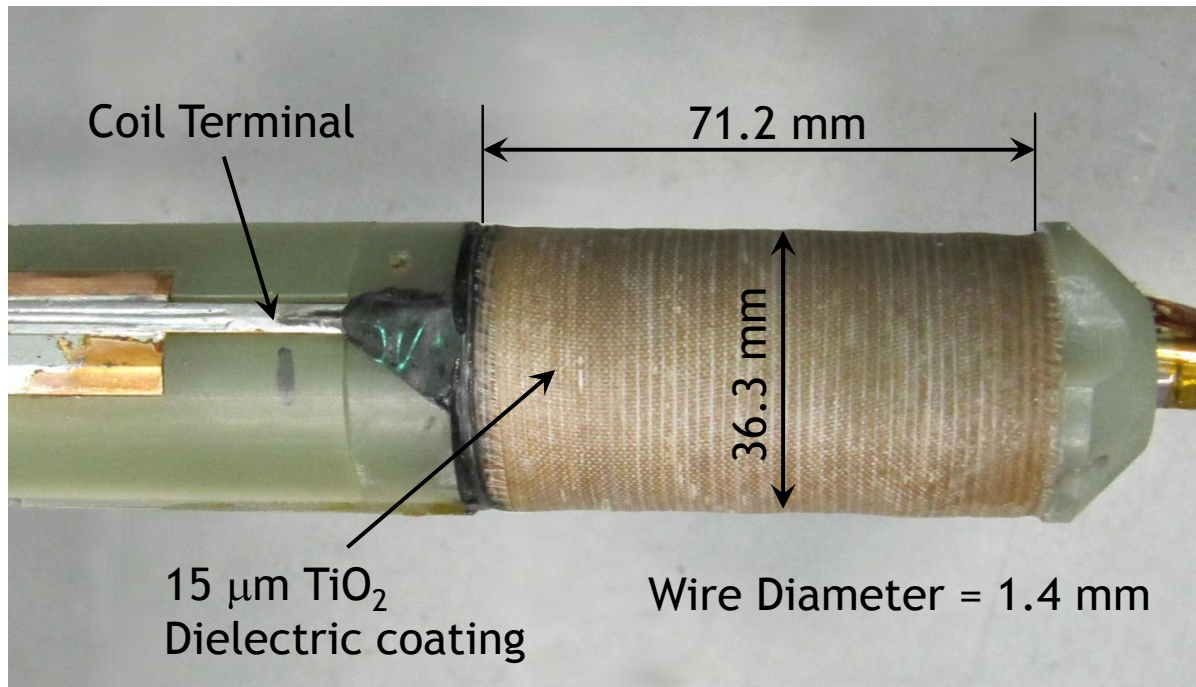
Section	1	3	5	7	9	witness
$J_E$ [4.2K, 5T] (A/mm <sup>2</sup> )	817.9	816.2	825.4	798.8	813.6	759.3



# OPed 2212 coil at 10 bar - generated 2.6 T in 31.2 T background = 33.8 T

10 bar OP processing

- Pressure was only high enough to prevent wire from expanding
- Did not compress Ag sheath and remove bubbles
- Insulation -  $\sim 15 \mu\text{m}$  thick  $\text{TiO}_2$

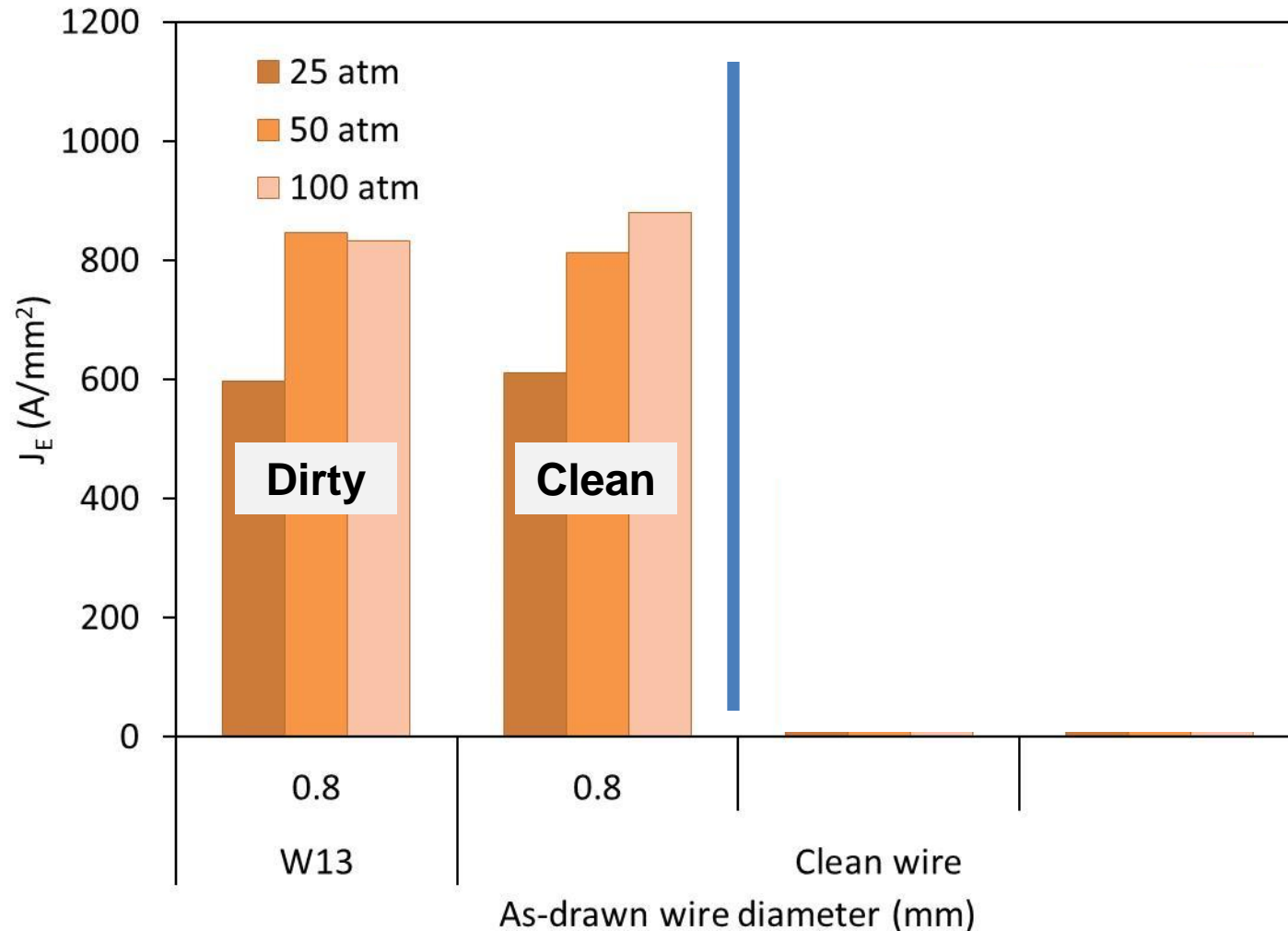


Wire dia. (mm):	1.40
nGimat Insulation (mm):	0.015
Turn-turn non-tightness (mm):	0.085
layer-layer tightness (mm):	-0.065
Inner Radius (a1) (mm):	7.25
Outer Radius (a2) (mm):	18.17
Height (2b) (mm):	71.21
Radial Layers (-):	8
Turnss/Layer (-):	47
Total turns (-):	376
Conductor Length (m):	30.03



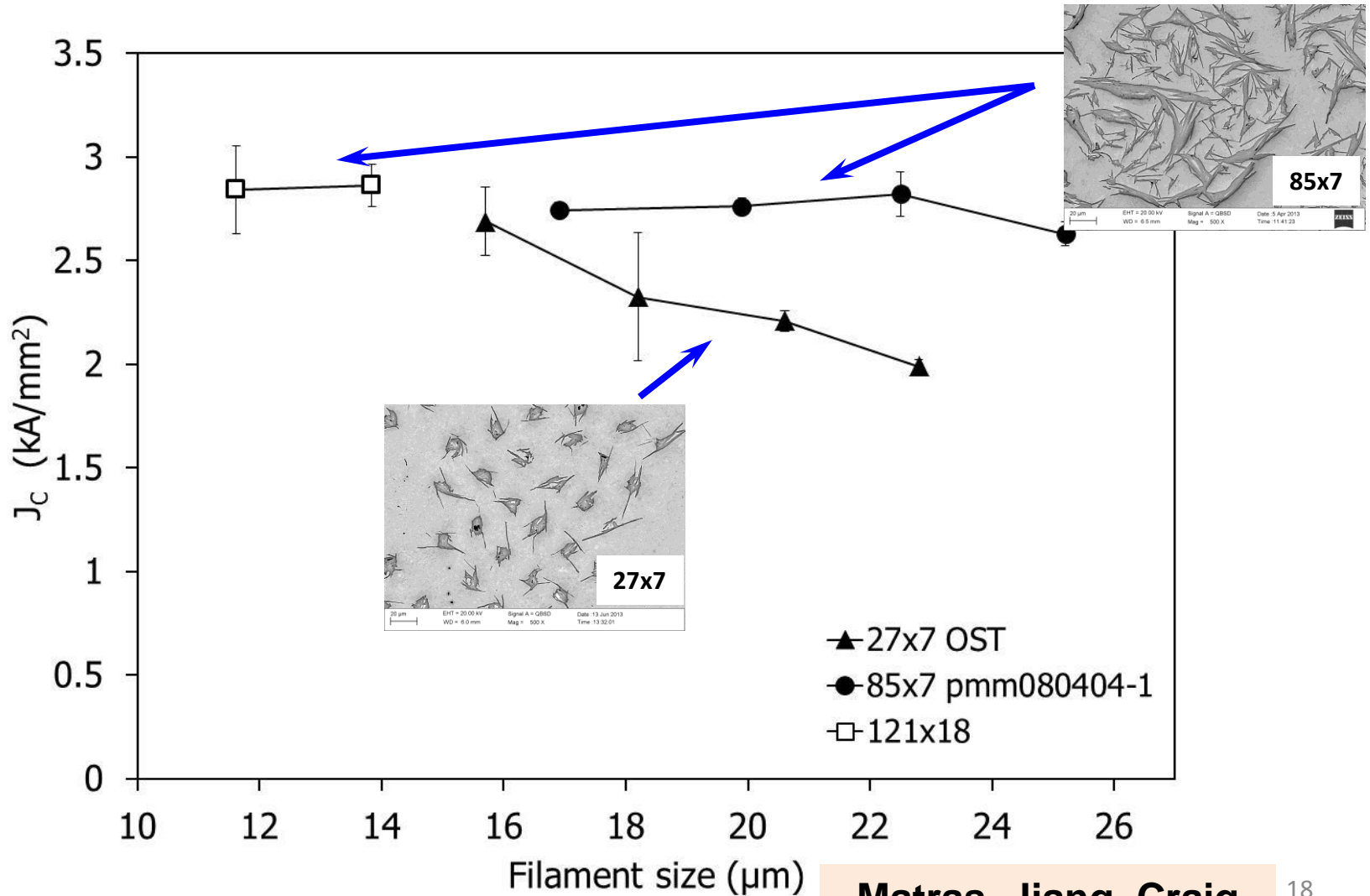
**3 - Q: Do billets with less C and H require lower OP pressure?**

**A: No marked difference in densification at 25 bar between high and low C + H wire**



4 – Q: What is the optimum filament diameter ( $d_f$ ) for optimum transport  $J_c$ ?

A:  $J_c$  decreases with decreasing diam in 27x7 wire with discrete filaments. Inconclusive for wires with extensive bridging.



**5 – Q: How do we measure powder quality?**

**A: No specific answer yet.**

- **Overall composition**
- **Phase assemblage**
- **Purity – no extra chemical species (Ba, Fe ...)**
- **C and H (and S) content – gas formers**
- **Particle shape and size distribution**
- **The gold standard for powder quality is  $J_c$  and  $J_E$  in wire.**
  - **Build subscale, multifilamentary wires.**

# Update on OP furnaces at FSU

Max pressure	Hot Zone		Type of heating	Comments
	Diameter	Length		
100-200 bar	25 mm	10 cm	Hot wall (external)	Will be used for PhD studies
25 bar	48 mm	10 cm	Hot wall (external)	In use
75-120 bar	45 mm	25 cm	Hot wall (external)	Starting to be used regularly
100 bar	170 mm	50 cm	Cold wall (internal)	Commissioning

# 100 bar OP furnace for large coils

**Hot Zone:**

**16 cm  $\phi$ , 50 cm**

**Furnace is being commissioned**



- **Controlling uniform hot zone**
- **Maintaining total pressure in system**
- **Measuring and controlling  $pO_2$  during heat treatment**
- **Mixing gases in chamber during heat treatment**

# Summary

- **Overpressure processing makes 2212 a viable candidate for accelerator magnets**
  - Round wire geometry
  - $J_E(B, \theta)$
  - Flexible, multifilamentary architecture
  - Can be easily cabled
    - Rutherford
    - 6-on-1