

# **Single-Cell Standing Wave Structures: Design**

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# Outline

- Introduction
- Strategy
- Structures

# Single Cell Accelerator Structures

## Goals

- Study rf breakdown in practical accelerating structures: dependence on circuit parameters, materials, cell shapes and surface processing techniques

## Difficulties

- Full scale structures are long, complex, and expensive

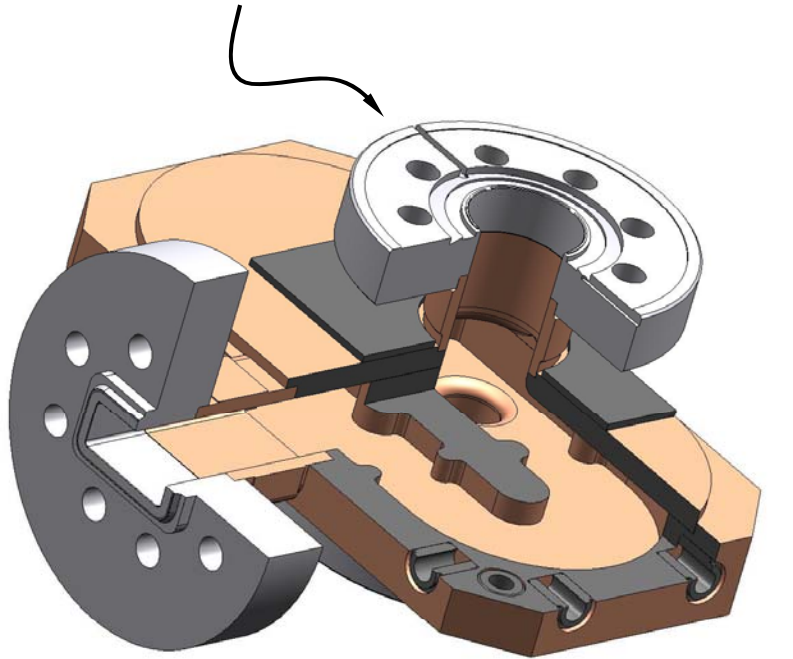
## Solution

- *Single cell Traveling wave (TW) and single cell standing wave (SW) structures with properties close to that of full scale structures*
- **Reusable couplers**

**We want to predict breakdown behavior  
for practical structures**

# Reusable coupler: $TM_{01}$ Mode Launcher

Pearson's RF flange



Cutaway view of the mode launcher



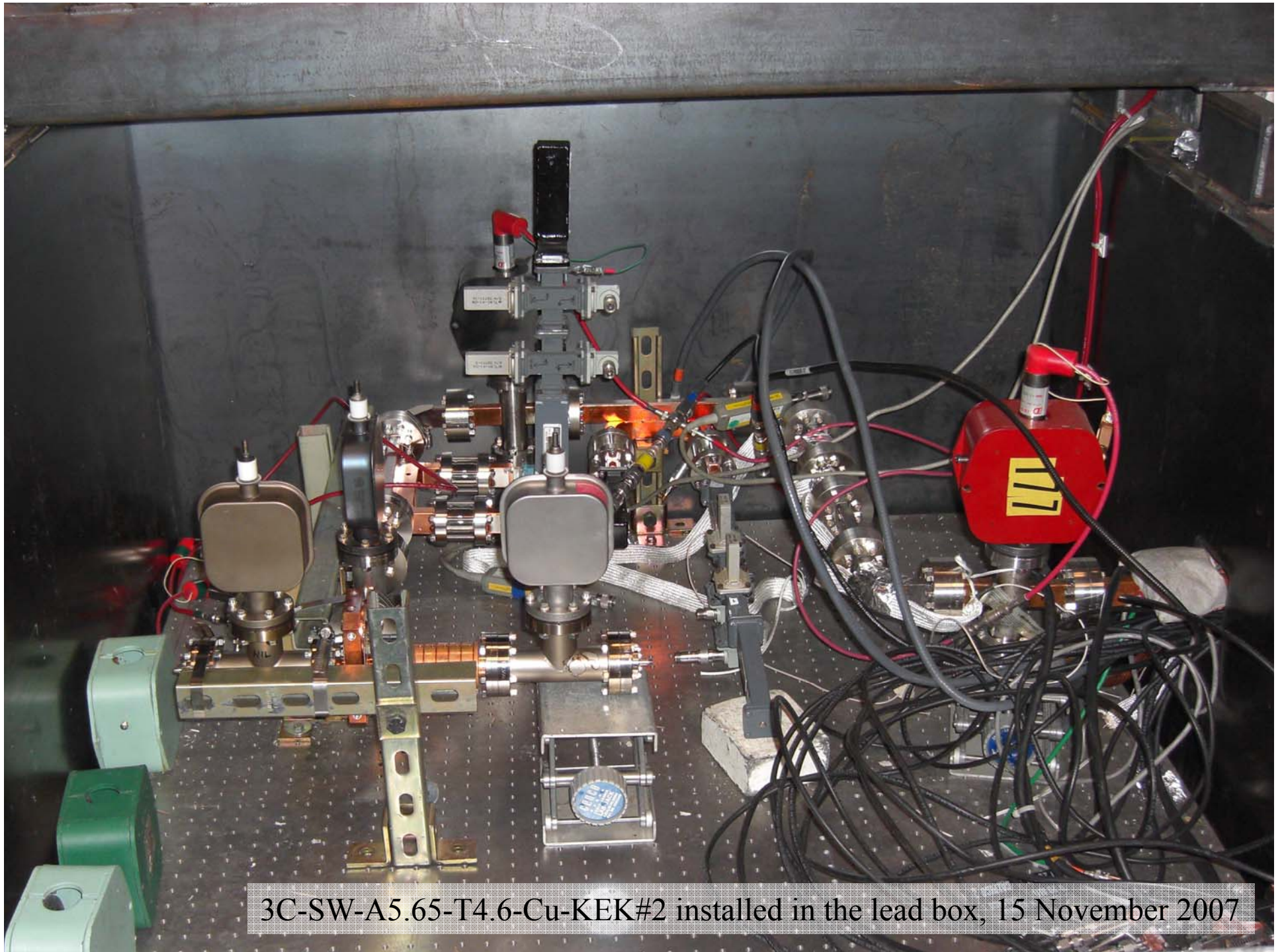
Two mode launchers

Surface electric fields in the mode launcher

$$E_{\max} = 49 \text{ MV/m for } 100 \text{ MW}$$

S. Tantawi, C. Nantista





3C-SW-A5.65-T4.6-Cu-KEK#2 installed in the lead box, 15 November 2007

# Strategy

## Geometry

- Stored energy
- Electric field for same magnetic field
- Choke
- Choke WR90 coupler
- Shunt impedance, iris size, etc.
- ...

## Materials

- CuZr
- Molybdenum

...

## Coatings

- TiN
- ...

## Some samples tested

- 1-C-SW-A5.65-T4.6-Cu
- 1-C-SW-A5.65-T4.6-Cu-TiN
- 3-C-SW-A5.65-T4.6-Cu
- 1-C-SW-A3.75-T2.6-Cu
- 1-C-SW-A3.75-T1.66-Cu

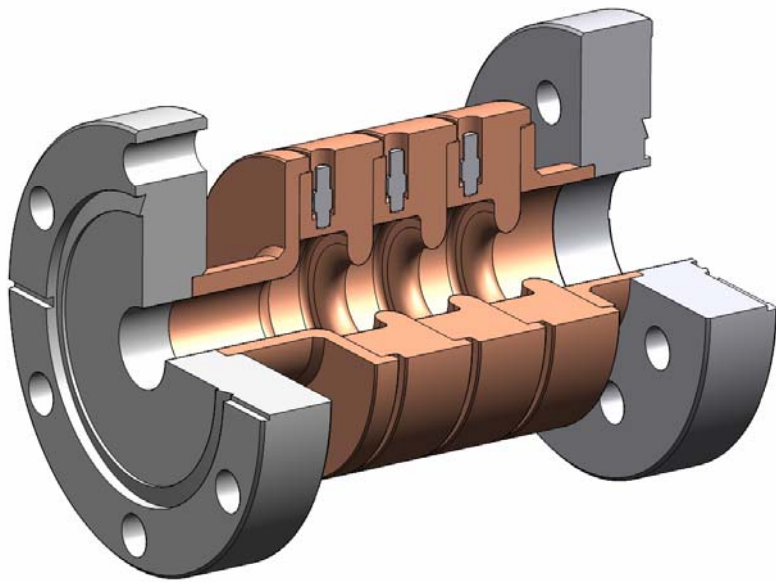
## To be tested

- 1-C-SW-A5.65-T4.6-Cu-Choke
- 1-C-SW-A5.65-T4.6-Cu-PBG
- 1-C-SW-A2.75-T2.0-Cu
- 3-C-SW-A5.65-T4.6-Cu-WR90
  
- One-C-SW-A3.75-T2.6-CuZr
- One-C-SW-A5.65-T4.6-CuZr
- ...

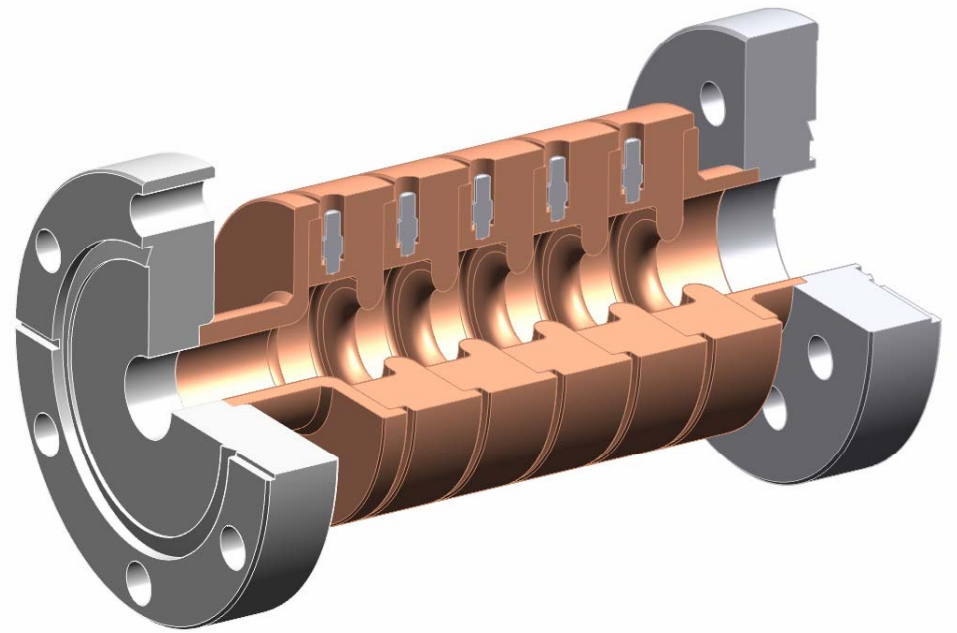
# Parameters of periodic structures

<b>Name</b>	<b>A2.75-T2.0-Cu</b>	<b>A3.75-T1.66-Cu</b>	<b>A3.75-T1.66-Cu</b>	<b>A5.65-T4.6-Choke-Cu</b>	<b>A5.65-T4.6-Cu</b>	<b>T53VG3</b>
<b>Stored Energy [J]</b>	0.153	0.189	0.189	0.333	0.298	<i>0.09</i>
<b>Q-value</b>	8.59E+03	8.82E+03	8.56E+03	7.53E+03	8.38E+03	<i>6.77E+03</i>
<b>Shunt Impedance [M<math>\Omega</math>/m]</b>	102.891	85.189	82.598	41.34	51.359	<i>91.772</i>
<b>Max. Mag. Field [A/m]</b>	2.90E+05	3.14E+05	3.25E+05	4.20E+05	4.18E+05	<i>2.75E+05</i>
<b>Max. Electric Field [MV/m]</b>	203.1	268.3	202.9	212	211.4	<i>217.5</i>
<b>Losses in a cell [MW]</b>	1.275	1.54	1.588	3.173	2.554	<i>0.953</i>
<b>a [mm]</b>	2.75	3.75	3.75	5.65	5.65	<i>3.885</i>
<b>a/lambda</b>	0.105	0.143	0.143	0.215	0.215	<i>0.148</i>
<b>Hmax*Z0/Eacc</b>	1.093	1.181	1.224	1.581	1.575	<i>1.035</i>
<b>t [mm]</b>	2	1.664	2.6	4.6	4.6	<i>1.66</i>
<b>Iris ellipticity</b>	1.385	0.998	1.692	1.478	1.478	<i>1</i>

# Low shunt impedance structures



**1C-SW-A5.65-T4.6-Cu**



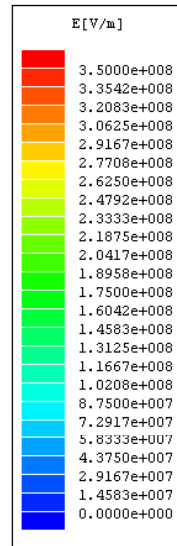
**3C-SW-A5.65-T4.6-Cu**

*Solid Model: David Martin*

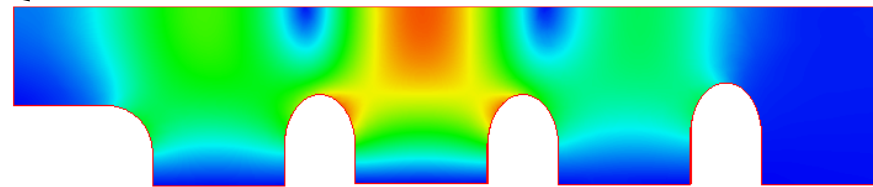


# Single-Cell-SW-A5.65-T4.6-Cu

10 MW input

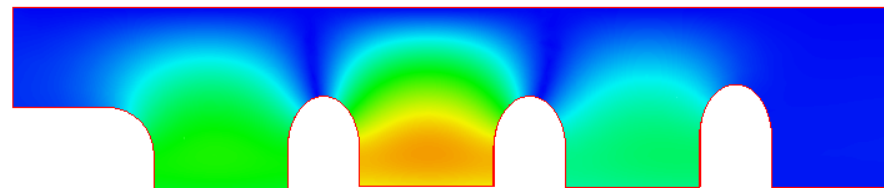
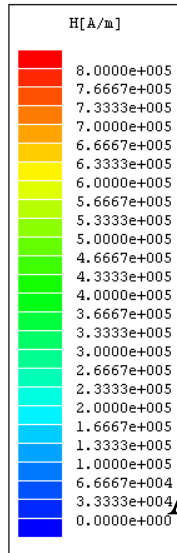


To vacuum view port ←



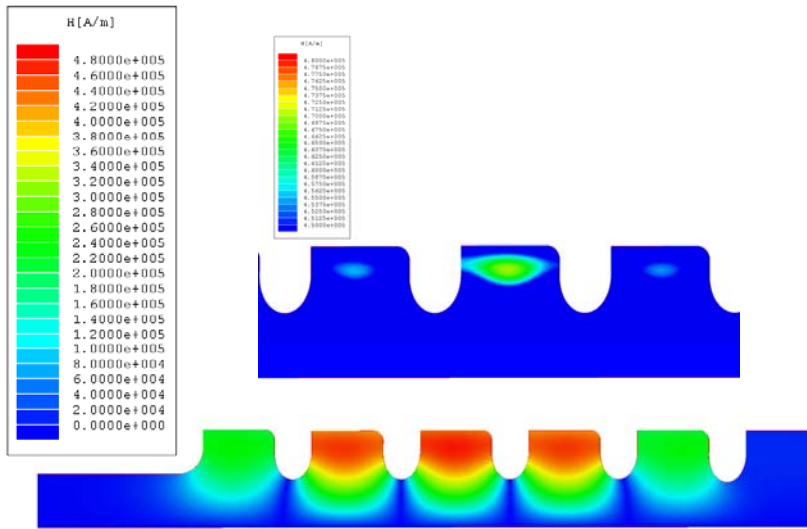
RF power from mode launcher ←

Amplitude of electric fields, maximum surface field  
**310 MV/m**

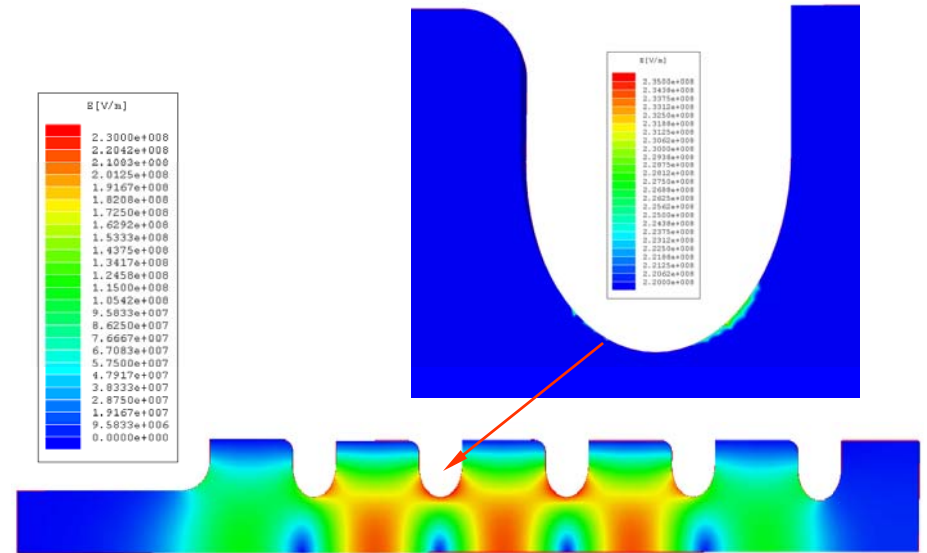


Amplitude of magnetic fields, maximum magnetic field  
**634.5 kA/m**

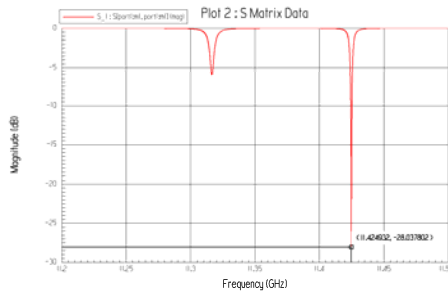
# Three-Cell-SW-A5.65-T4.6-Cu, 10 MW input



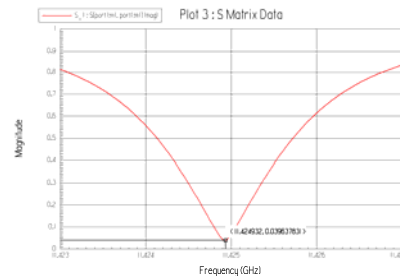
Maximum magnetic field **458 kA/m**  
(SLANS 457 kA/m)



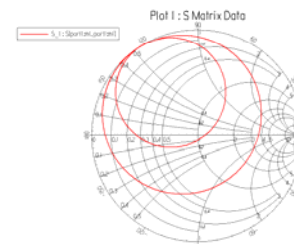
Maximum electric field **230 MV/m**  
(SLANS 230 MV/m)



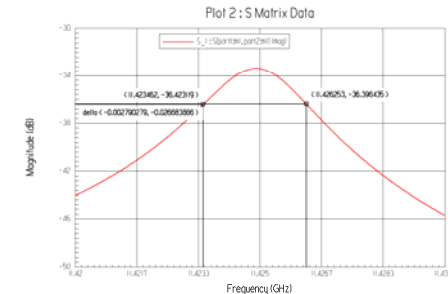
Resonance at **11.4249 GHz**  
(SLANS 11.424 GHz)



$\beta = 1.083$   
(SLANS 1.075)

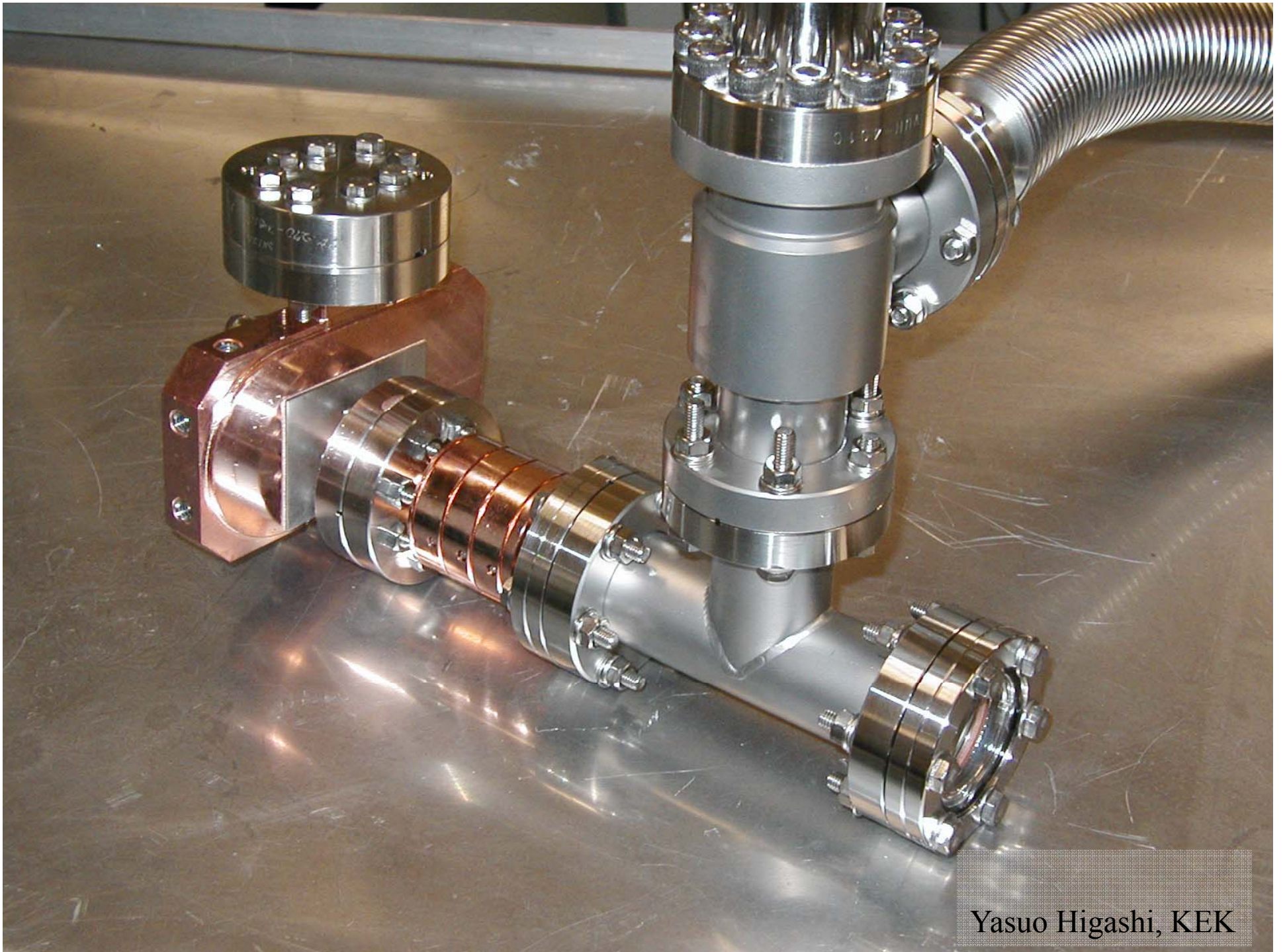


Over-coupled loaded Q  
Unloaded Q  
(SLANS 8.64e3)



$$\frac{11.4249}{0.00279027} = 4.095 \times 10^3$$

$$4.095(1 + 1.083) \cdot 10^3 = 8.53 \times 10^3$$



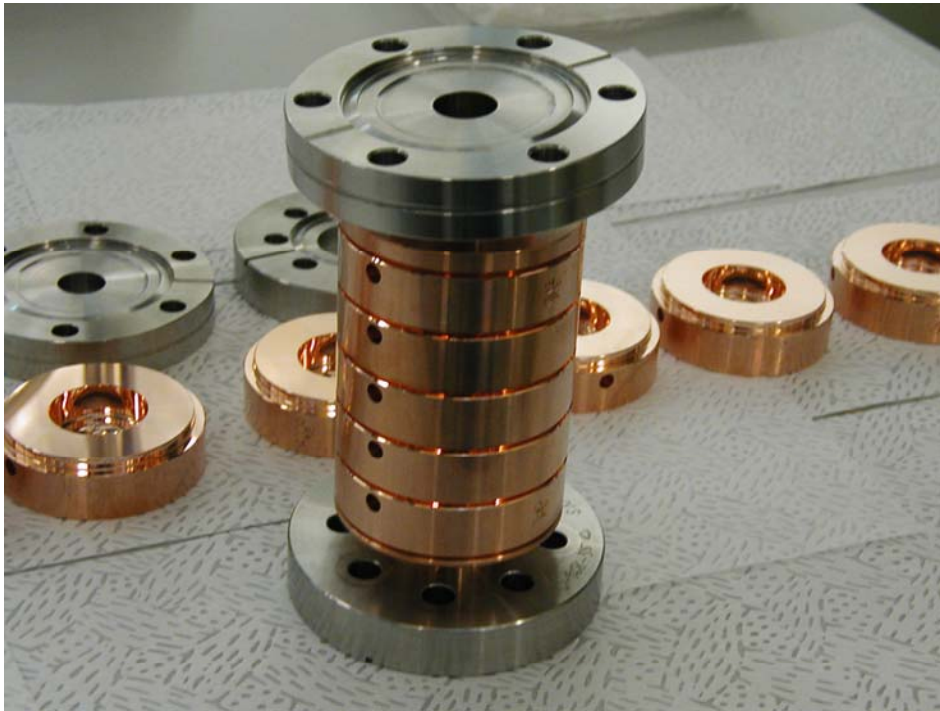
Yasuo Higashi, KEK





**Yasuo Higashi, KEK**

# Manufacturing of 3-cell SW structure (3C-SW-A5.65-T4.6-Cu-KEK#1) at KEK,

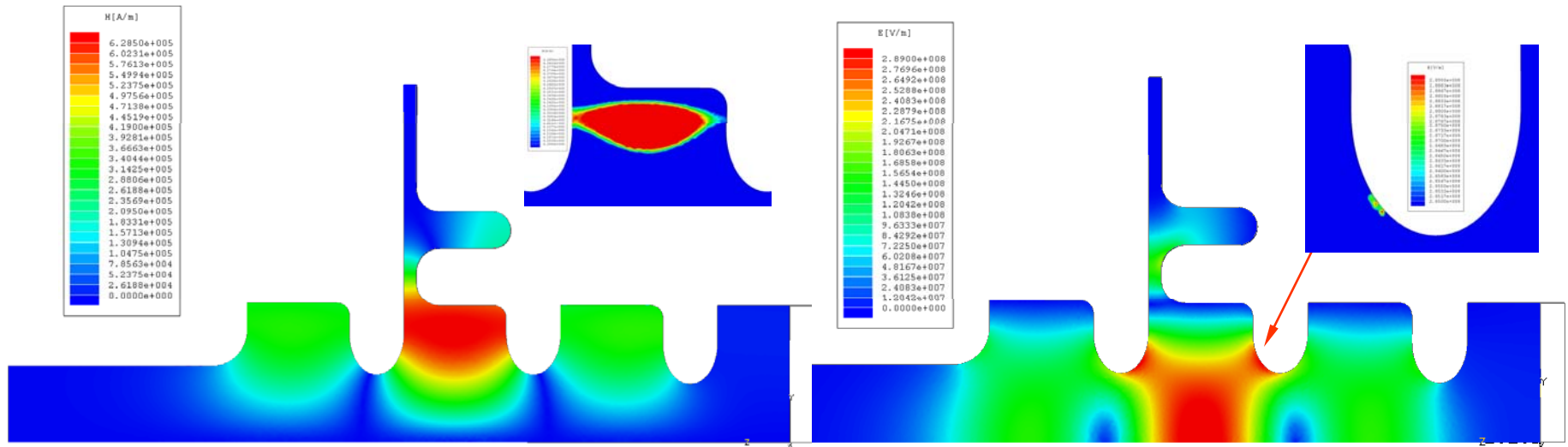


Yasuo Higashi, KEK



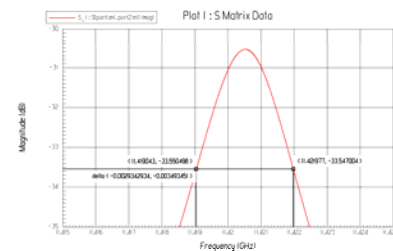
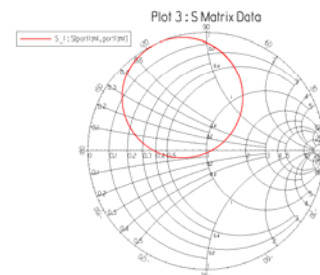
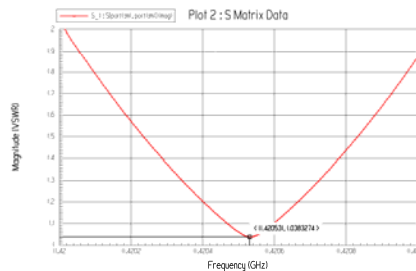
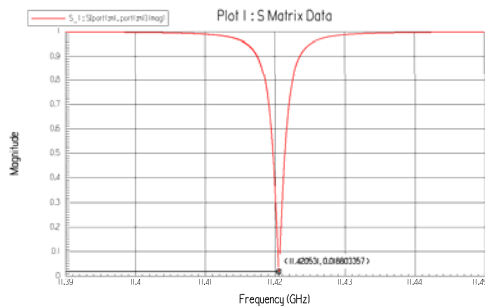
# 1C-SW-A5.65-T4.6-Cu-Choke

## 10 MW input



Maximum magnetic field 628.5 kA/m  
(SLANS 627.5 kA/m)

Maximum electric field 289 MV/m  
(SLANS 297.7 MV/m)



Resonance at 11.42053 GHz  $\beta = 1.03832$   
(SLANS 11.424 GHz) (SLANS 1.045)

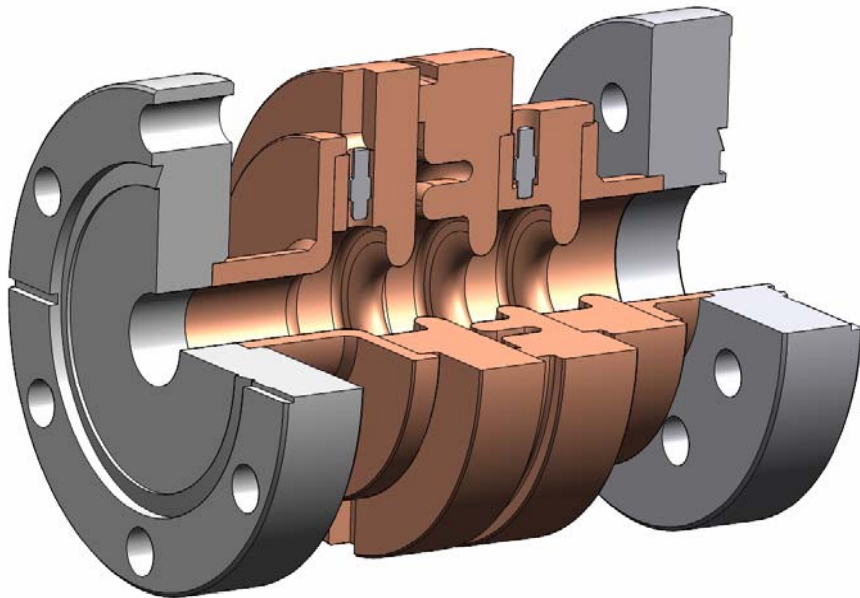
Over-coupled loaded Q  
Unloaded Q=7,933  
(SLANS 7,933.5)

$$\frac{11.42053}{0.00293429} = 3.892 \times 10^3$$

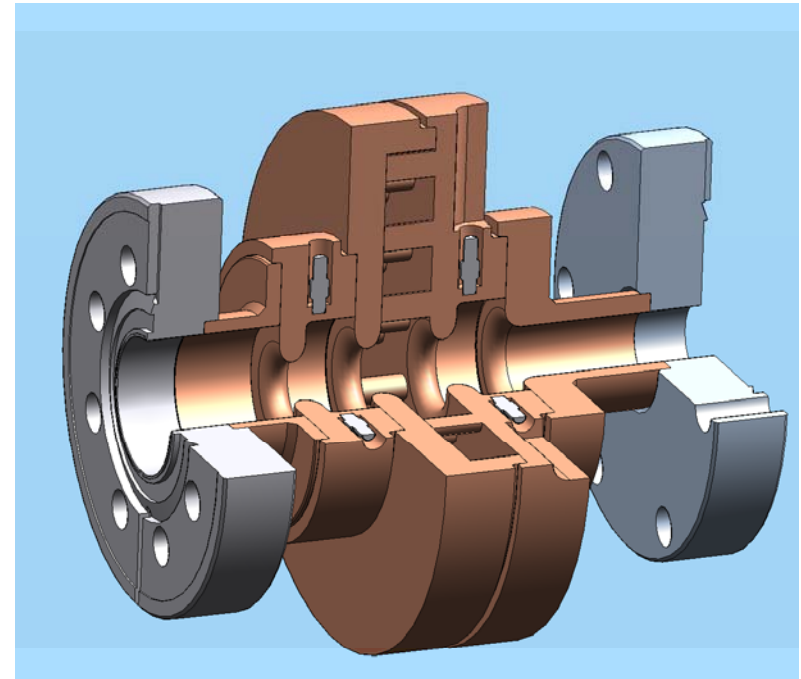
$$\frac{11.42053}{0.00293429} \cdot (1 + 1.03832) = 7.933 \times 10^3$$



# Wakefield damping “ready” structures



**1C-SW-A5.65-T4.6-Cu-Choke**



*Electrical design: Roark Marsh, MIT*

**1C-SW-A5.65-T4.6-Cu-PBG**

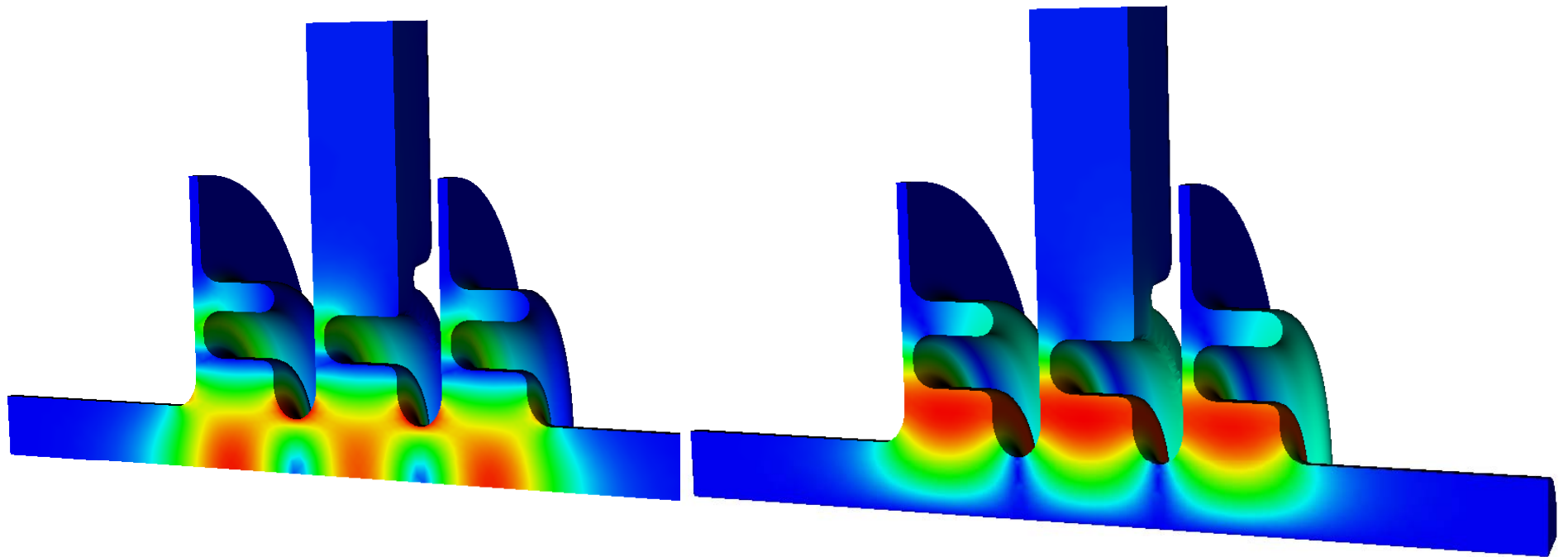
*Solid Model: David Martin*

# 1C-SW-A5.65-T4.6-Cu-Choke-SLAC-#1 after bead-pull measurement



# 3-Cell structure with choke coupler and WR90 inputs

## **3C-SW-A5.65-T4.6-Cu-WR90**



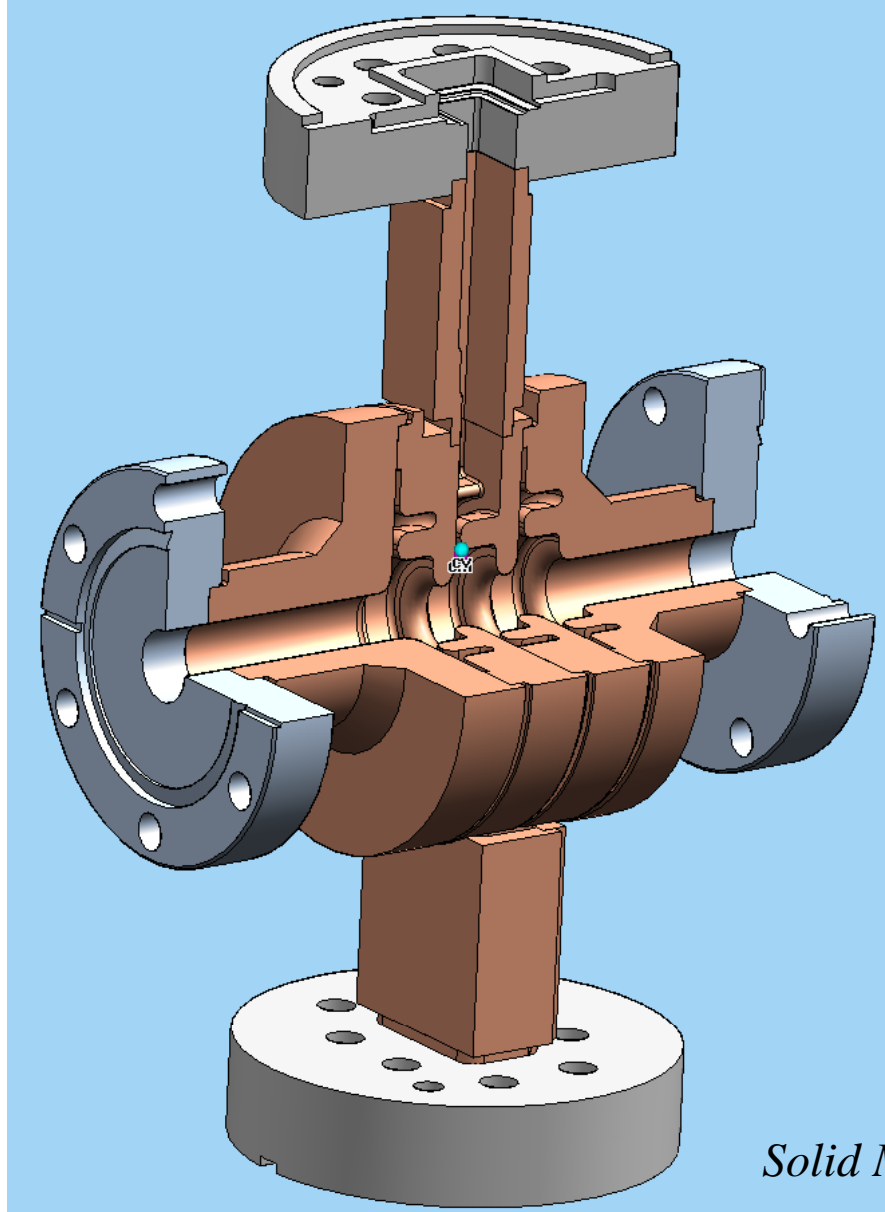
Surface electric fields

Surface magnetic fields

*Electrical design: Z. Li, 8 November 2007*

3-Cell structure with choke coupler and WR90 inputs

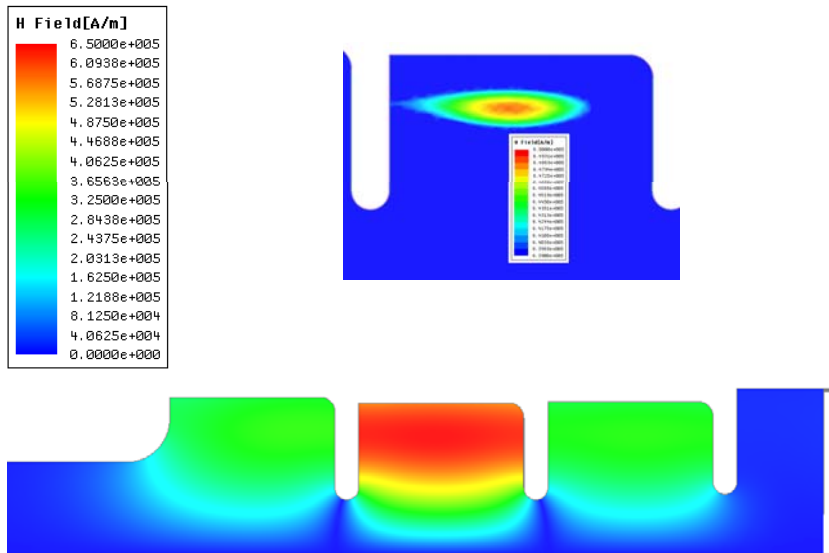
**3C-SW-A5.65-T4.6-Cu-WR90**



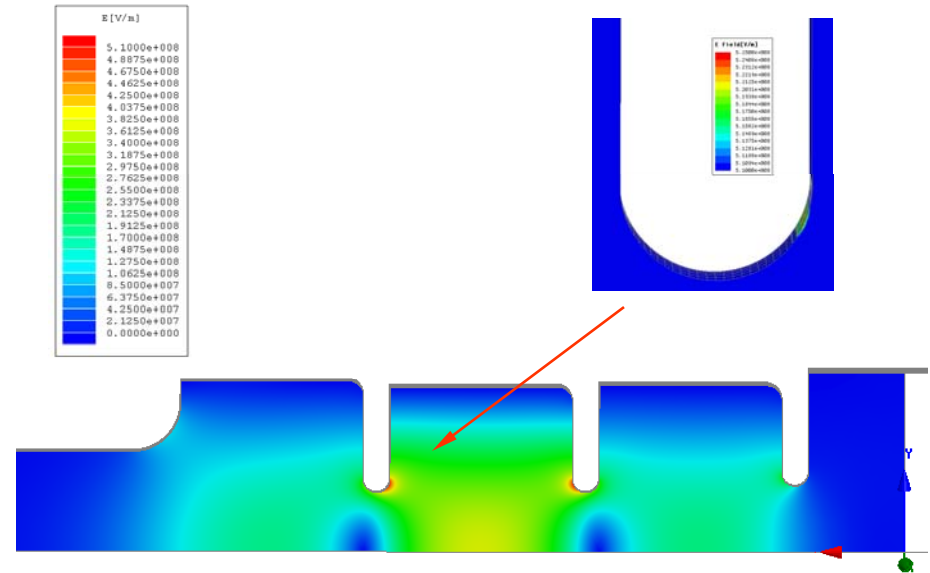
*Solid Model: David Martin*

# 1C-SW-A3.75-T1.66-Cu

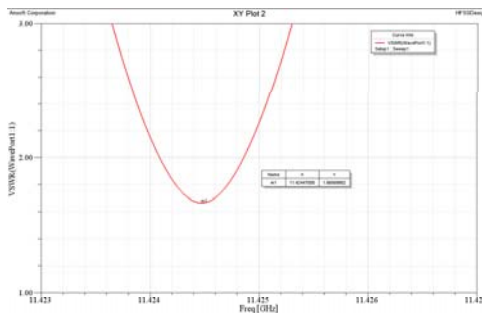
10 MW input



Maximum magnetic field 639 kA/m  
(SLANS 642.37 kA/m)



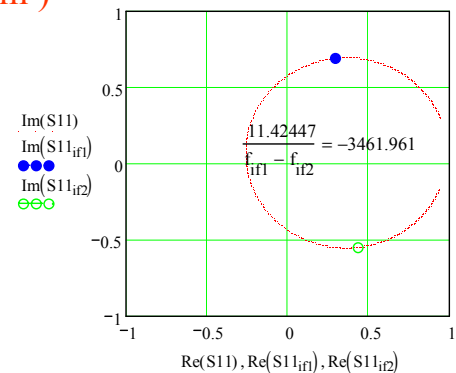
Maximum electric field 525 MV/m  
(SLANS 533.3087 MV/m)



Resonance at 11.42447 GHz  $\beta = 1.666$   
(SLANS 11.423.91 GHz) (SLANS 1.788)

$$\frac{11.42447}{f_{if1} - f_{if2}} \cdot (1 + 1.666) = -9229.587$$

Unloaded Q=9.229 (Smith Chart)  
(SLANS 9,182.93)

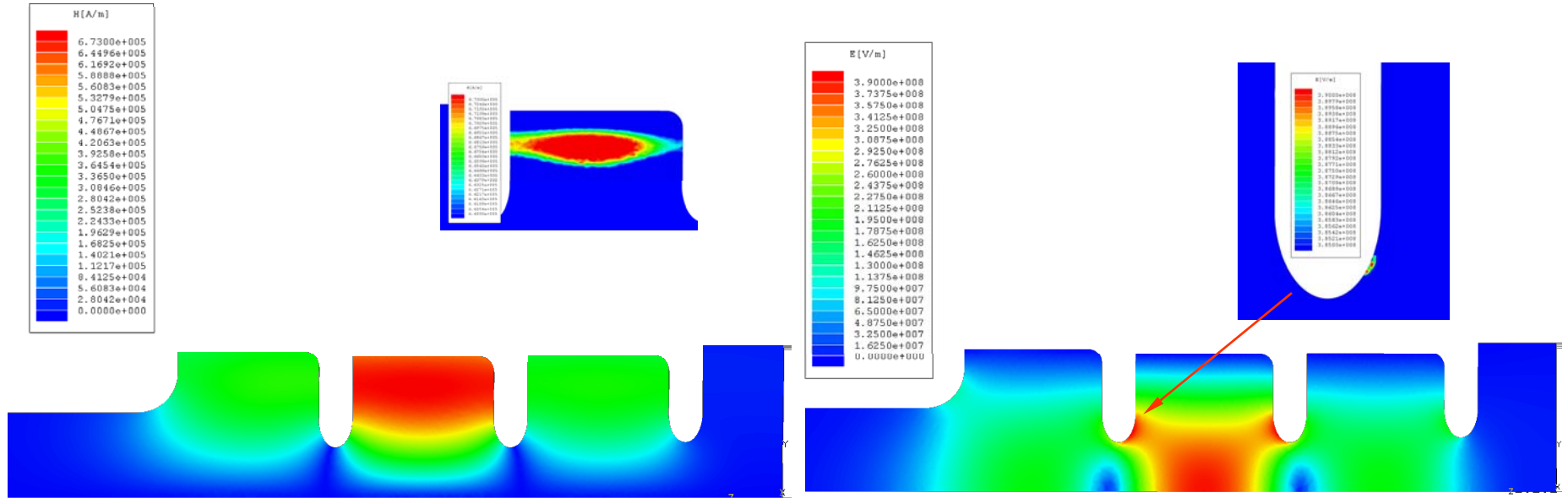


Over-coupled loaded Q



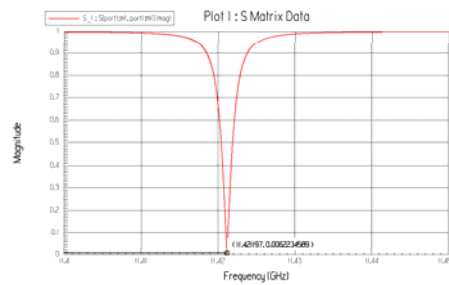
# 1C-SW-A3.75-T2.6-Cu

10 MW input

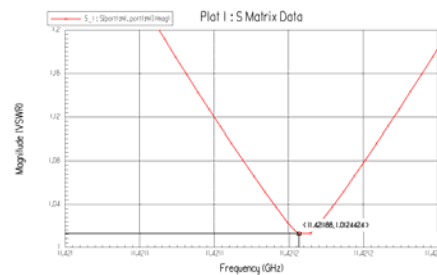


Maximum magnetic field 672 kA/m  
(SLANS 668.0 kA/m)

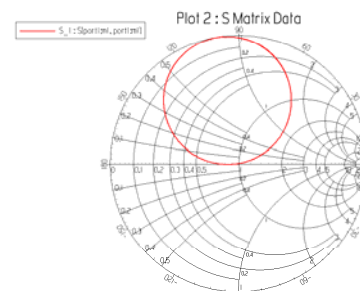
Maximum electric field 390 MV/m  
(SLANS 398.9 MV/m)



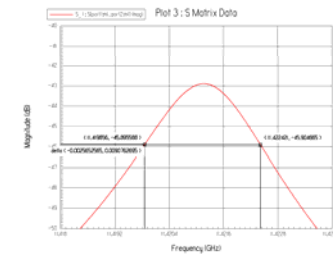
Resonance at 11.4212 GHz  
(SLANS 11.4241 GHz)



$\beta = 0.988$   
(SLANS 1.032356)



Under-coupled loaded Q  
Unloaded Q=8,849.8  
(SLANS 8,912.5)



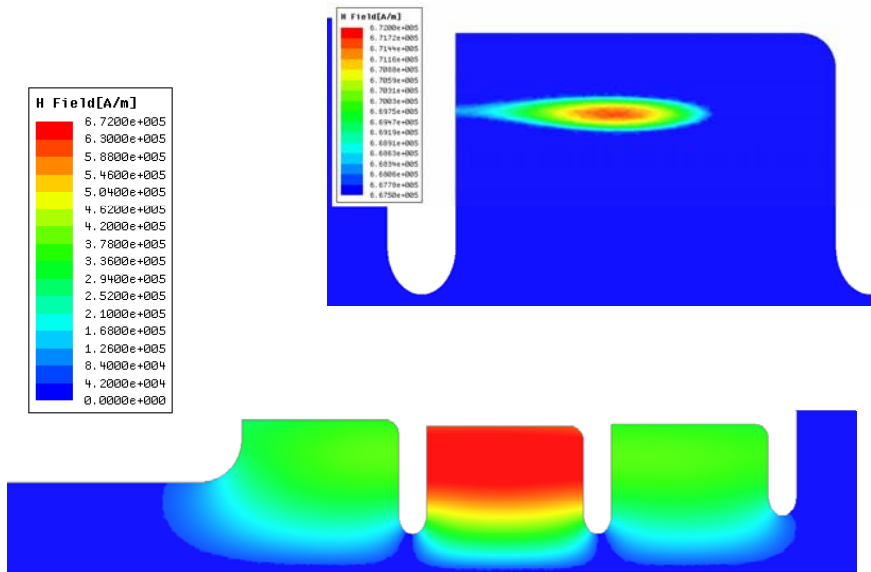
$$\frac{11.4212}{0.00256526} = 4.452 \times 10^3$$

$$\frac{11.4212}{0.00256526} \cdot (1 + 0.987710) = 8.8498 \times 10^3$$

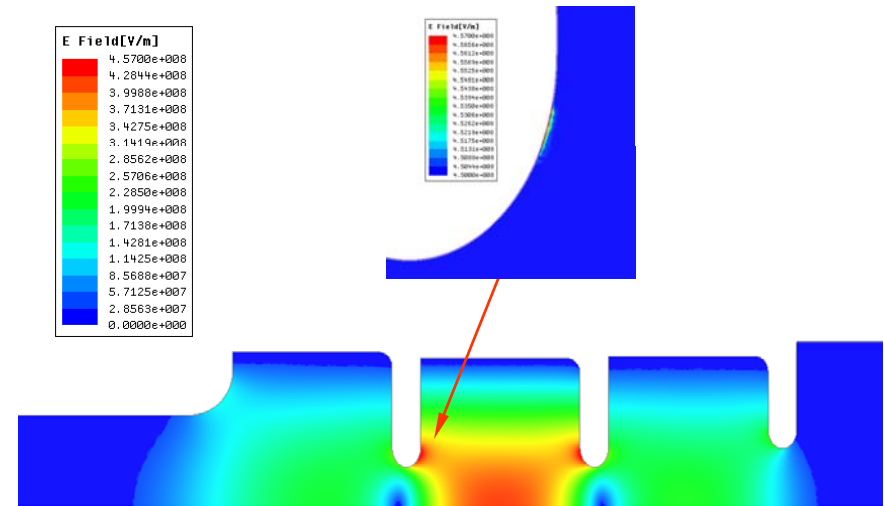


# 1C-SW-A2.75-T2.0-Cu

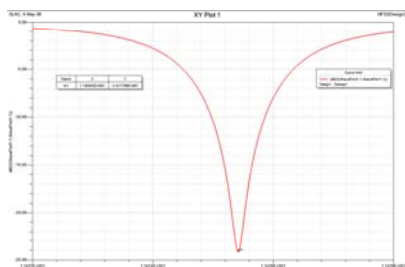
## 10 MW input



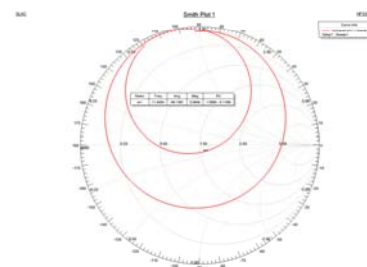
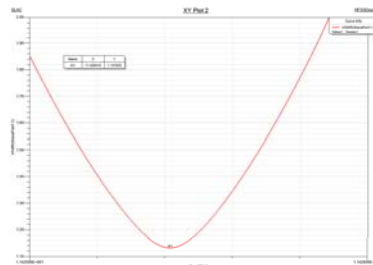
Maximum magnetic field 667.5 kA/m  
(SLANS 666.8 kA/m)



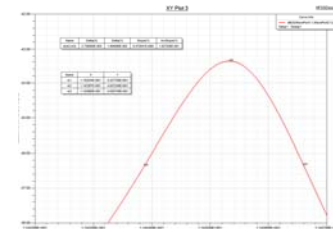
Maximum electric field 457 MV/m  
(SLANS 456.3 MV/m)



Resonance at 11.42542 GHz  $\beta = 1.131$   
(SLANS 11.42398 GHz) (SLANS 1.164)



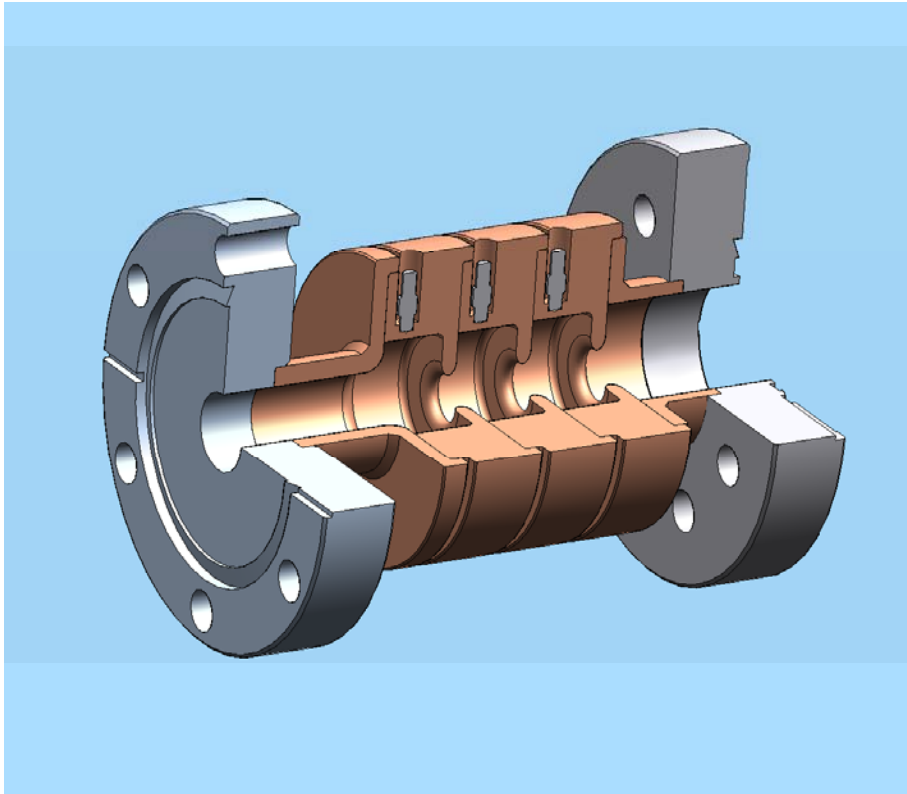
Over-coupled loaded Q  
Unloaded Q=8,919  
(SLANS 8,9594)



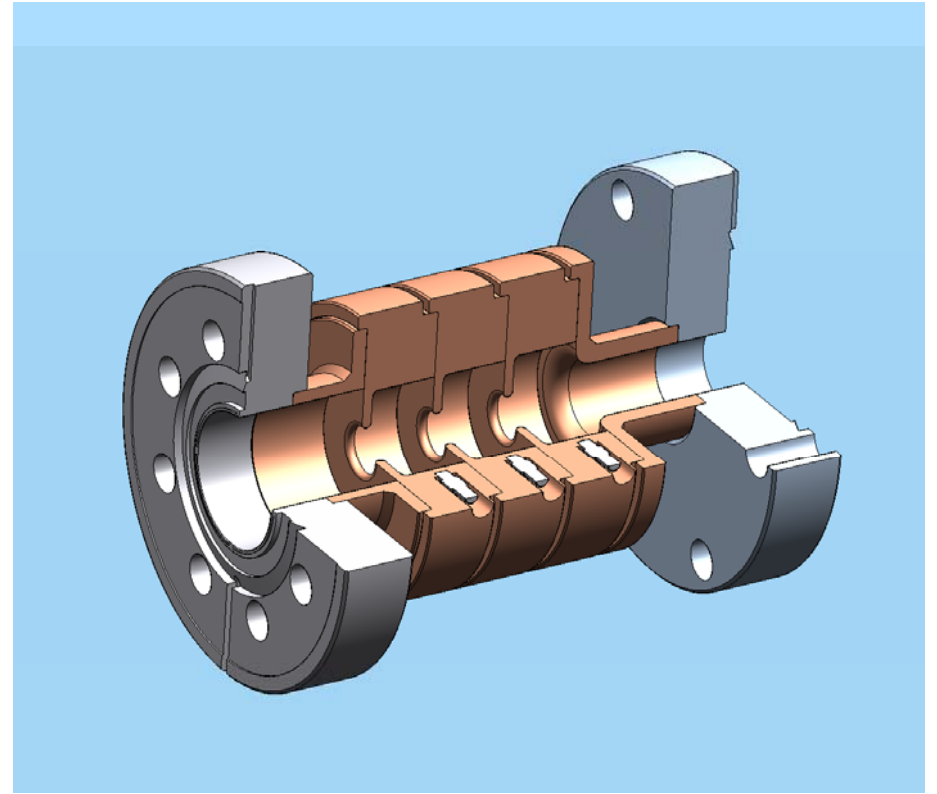
$$\frac{11.4254\text{GHz}}{2.73\text{MHz}} = 4.185 \times 10^3$$

$$\frac{11.4254\text{GHz}}{2.73\text{MHz}} (1 + 1.131) = 8.919 \times 10^3$$

# High shunt impedance structures



**1C-SW-A3.75-T2.6-Cu**



**1C-SW-A3.75-T1.66-Cu**

*Solid Model: David Martin*

# Summary

We designed a set of single cell standing wave structures. We attempted to cover range parameters need for high-gradient, heavy wake-field loaded accelerator. These structures being built at KEK, SLAC and Frascati and high-power tested at SLAC. As we learn results of the high power tests, we design new structures.