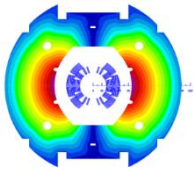


Experience with 11 T quench protection

G. Chlachidze and A. Zlobin for the 11T collaboration

QXF quench protection workshop at CERN
April 29, 2014



Introduction



Nb₃Sn based single-aperture 11T dipoles are developed at FNAL and CERN starting in 2011.

3 models were fabricated and tested at FNAL since then:

MBHSP01 with 2-m long coils #2 and #3 was tested in June 2012

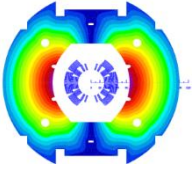
- 0.7 mm diameter RRP 108/127 strand
- 12 mm thick SS welded skin

MBHSP02 with 1-m long coils #5 and #7 was tested in February 2013

- 0.7 mm diameter RRP 150/169 strand
- 12 mm thick bolted skin
- 0.025 mm thick and 11.5 mm wide stainless steel core in the conductor

MBHSM01 mirror with coil #8 was tested in December 2013

- Mix of 0.7 mm diameter RRP 108/127 and RRP 114/127 strands
- 12 mm thick bolted skin
- 0.025 mm thick and 11 mm wide stainless steel core in the conductor

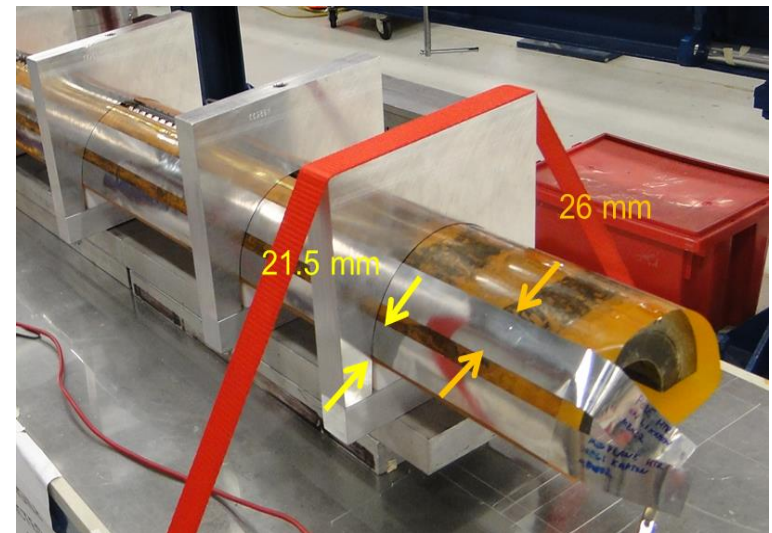
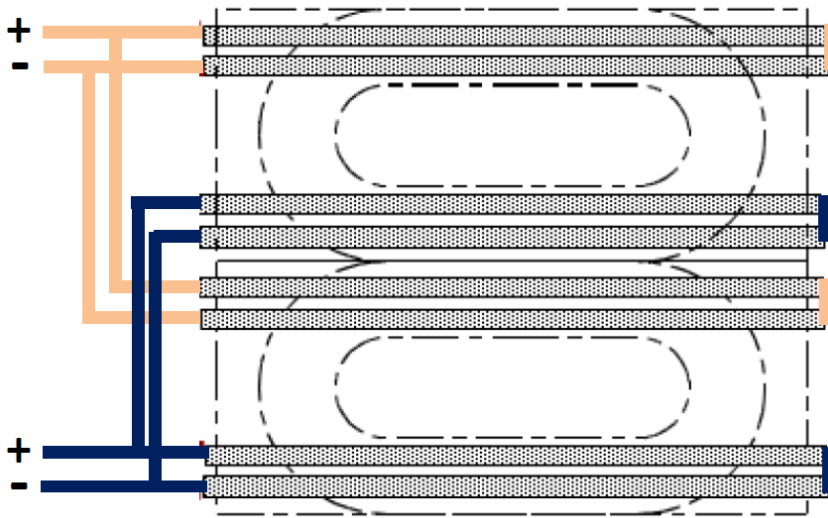


Protection Strip Heaters

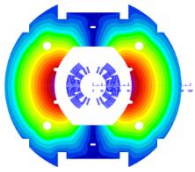


11T coils are equipped with 2 protection heaters on the outer coil surface

- Each heater consists of two 0.025 mm thick stainless steel (SS) strips
- SS strips are 21.5 mm wide in the mid-plane (LF) and 26 mm wide in pole area (HF)
- Heaters cover 31 turns per quadrant or about 56% of total coil surface



Due to difference in width of heater strips the peak power density dissipated in the LF is about 50% more than in the HF are



Heater to Coil Insulation



Heaters in 11T coils are placed between the ground insulation layers of *Kapton*

MBHSP01: two different heater-to-coil insulations were investigated

- One pair of strips was placed between the 1st and 2nd *Kapton* layers (PH-1L) and another pair – between the 2nd and 3rd *Kapton* layers (PH-2L)

0.125 mm layer of glass on the outer coil surface was impregnated with all 11T coils

MBHSP02, MBHSM01: both used only PH-1L heater insulation

PH-1L

1x 127 μ m
Kapton
between coil
and heater

25 μ m
SS Heater

2x 127 μ m Kapton
between coil and heater

2x 127 μ m Kapton
between coil and heater

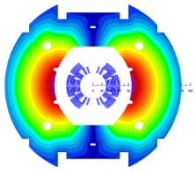
25 μ m
SS Heater

1x 127 μ m
Kapton
between coil
and heater

PH-2L

PH-2L

PH-1L



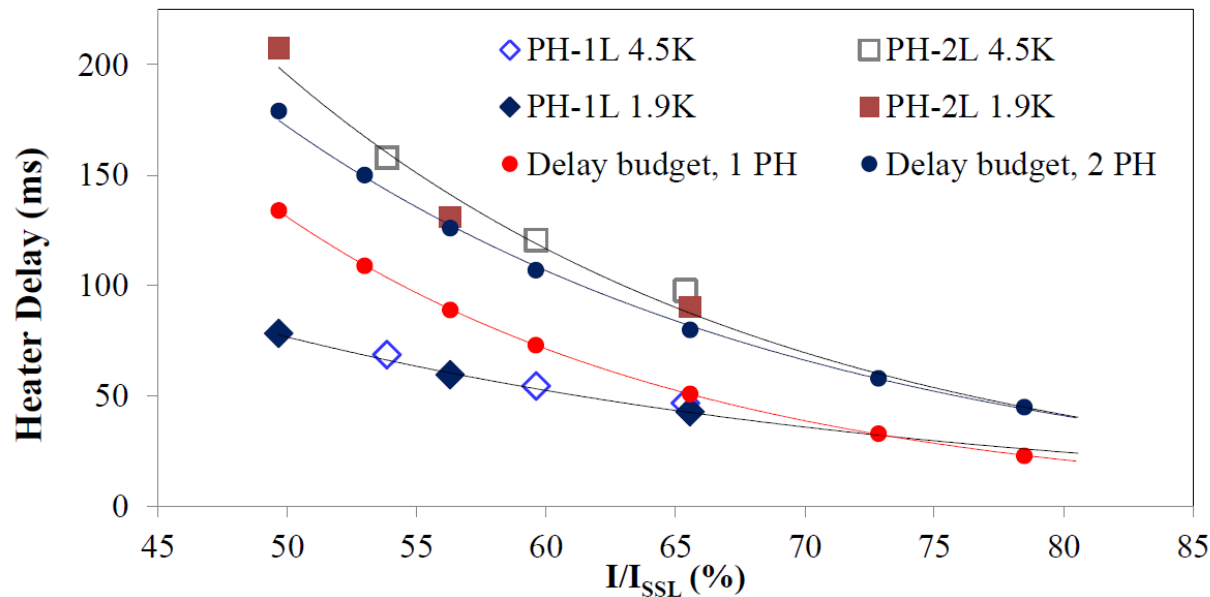
MBHSP01 Heater Tests



No available time margin was demonstrated when testing PH-2L heaters with 2 layers of the *Kapton* insulation.

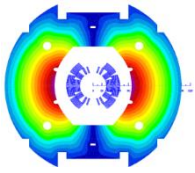
Heater delay budget was estimated as $(\text{MIITs budget} - \text{decay MIITs})/I^2$ for one or two PH per coil and coil T_{max} of 400 K

- $(\text{Delay budget} - \text{PH delay}) = \text{time for quench detection, validation, etc.}$



$P = 25 \text{ W/cm}^2$
 $\tau = 24 \text{ ms}$

Only one layer of *Kapton* insulation (0.114 mm) is used in all following 11T coils



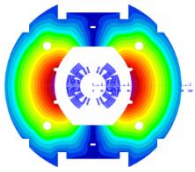
Quench Protection Study



Comprehensive quench protection study was performed in different 11T models:

- Heater efficiency at different magnet currents
- Effect of heater insulation thickness
- Heater efficiency in low-field (LF) and high-field (HF) areas
- Radial quench propagation from the outer to the inner coil layer
- Quench integral study for different dump resistors
- Longitudinal quench propagation velocity
- Quench temperature measurements
- Fast extraction

To keep the cable temperature during a quench below 400 K, the quench integral has to be less than 19-21 MIITs ($10^6 \text{ A}^2 \cdot \text{s}$). QI limit was set at 18 MIITs for quench protection study in 11T magnets.



PH efficiency studies

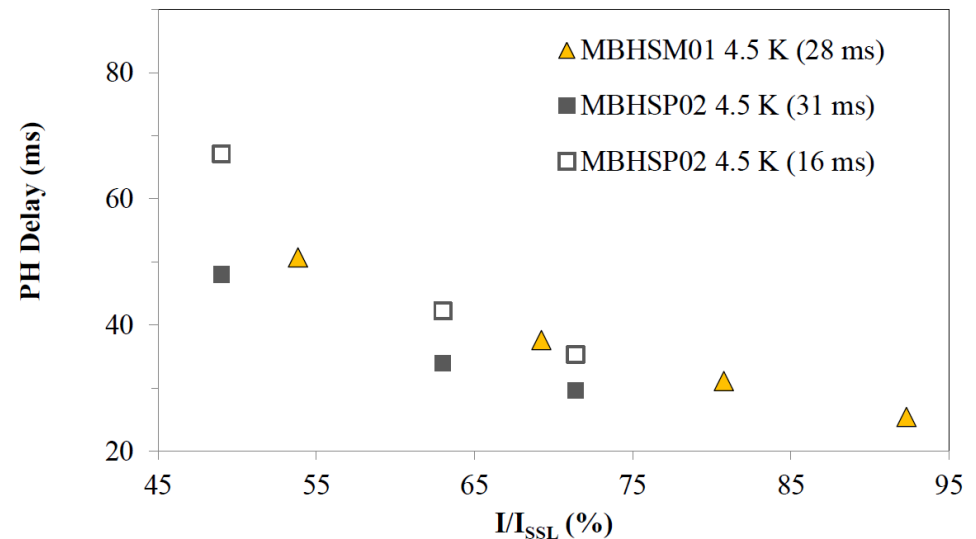
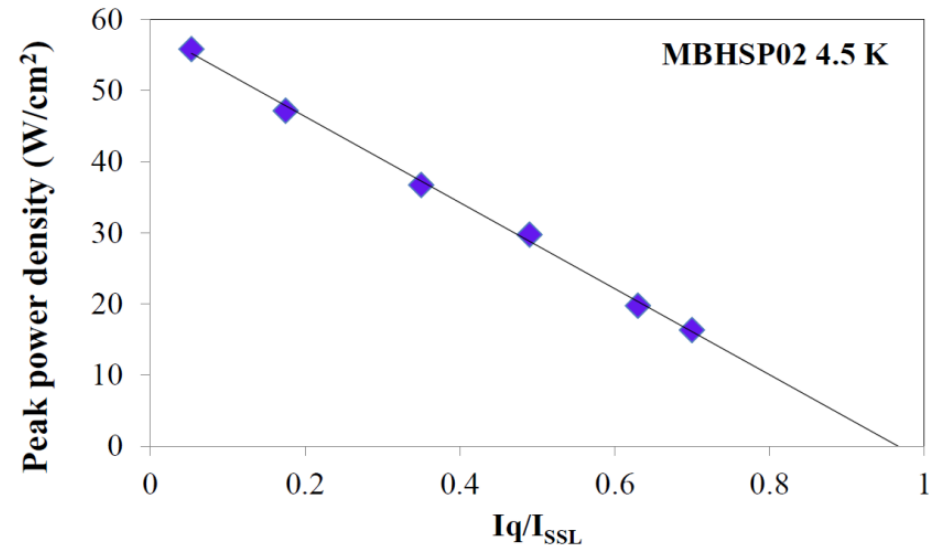


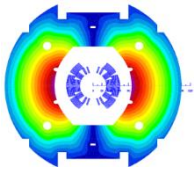
The minimum peak power density required to quench the magnet was estimated at different currents

- To quench magnet at all operation currents $P \geq 55 \text{ W/cm}^2$

PH delays measured for the peak power density of $\sim 50 \text{ W/cm}^2$

- PH delays consistent in different magnets



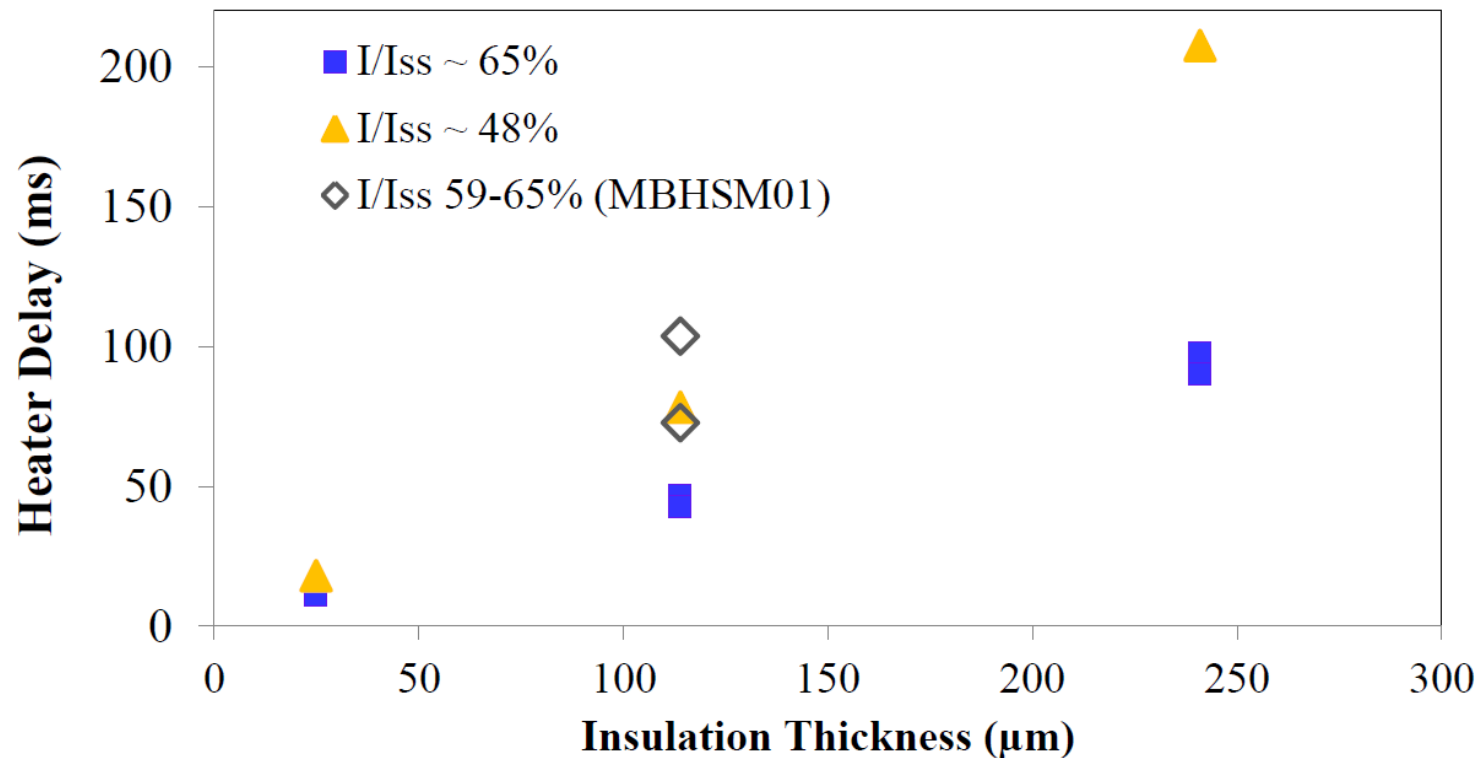


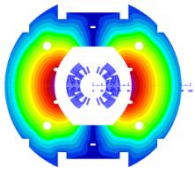
Effect of PH insulation



Peak power density of 15-20 W/cm² in MBHSM01 and 25 W/cm² for remaining data

- PH delay is increasing proportionally to the insulation thickness



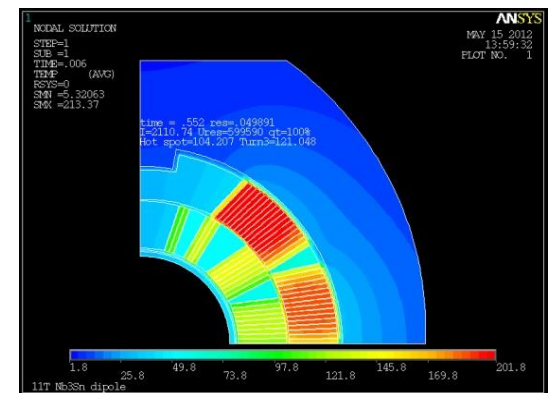
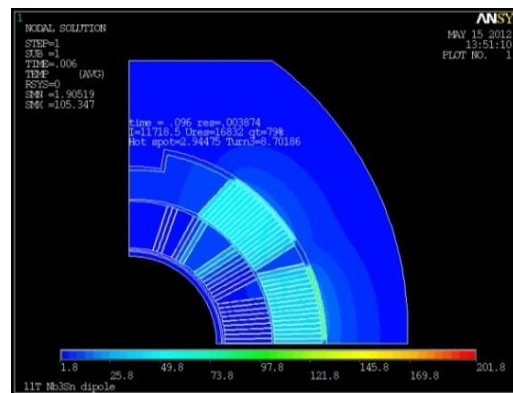
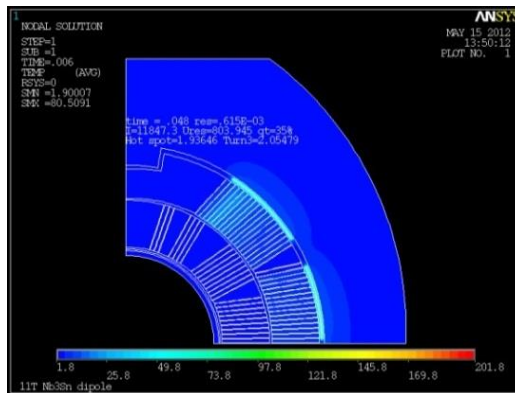


Radial & Azimuthal Quench Propagation



Heat transfer from the heater to the OL and then from the OL to the IL coil helps to spread and absorb the magnet stored energy

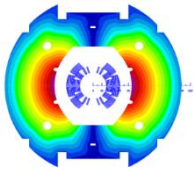
- Temperature profile in the magnet after 48 , 96 and 552 ms from the OL PH induced quench at a nominal current of 11.8 kA (ANSYS)



- 2D calculations - resistance in IL blocks #2 and #3

Radial quench propagation was measured in all 11T models

- Currently in the list of a standard 11T magnet measurements

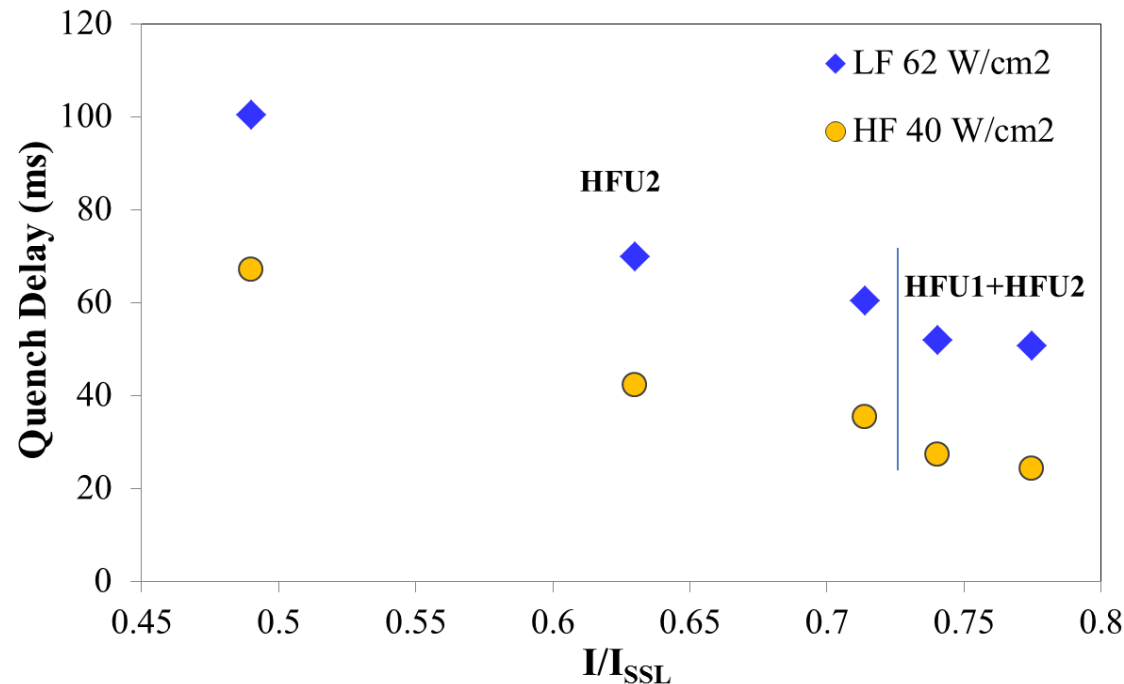


PH delay in LF and HF areas

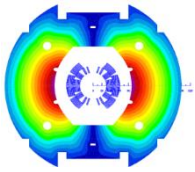


Due to different heater width the peak power density is also different in low-field (LF) and high-field (HF) blocks

$$P_{LF} = 1.24 \cdot P_{av}, \quad P_{HF} = P_{av} / 1.24 \quad \text{where} \quad P_{av} = I^2 (R_{LF} + R_{HF}) / (A_{LF} + A_{HF})$$



The difference in quench time between LF and HF blocks is ~30 ms



PH efficiency (cont'd)

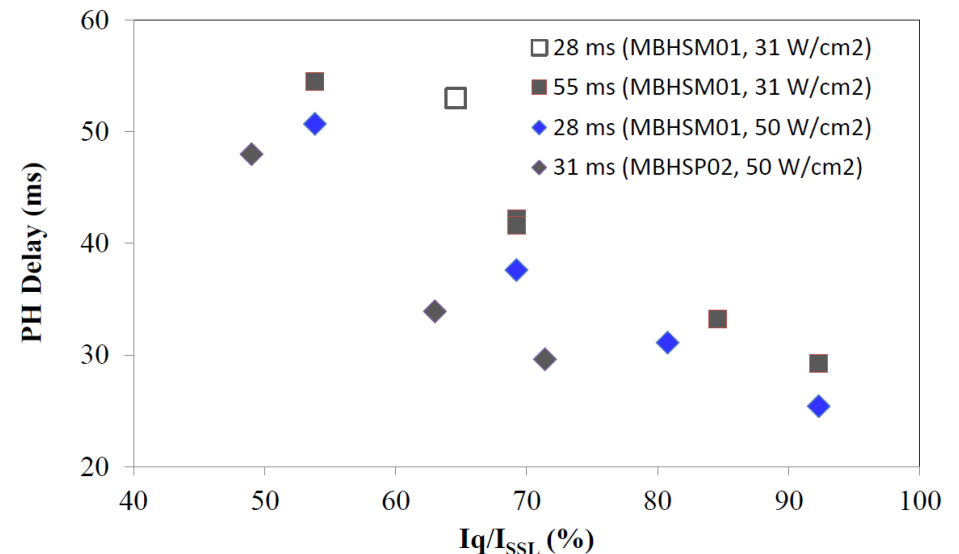
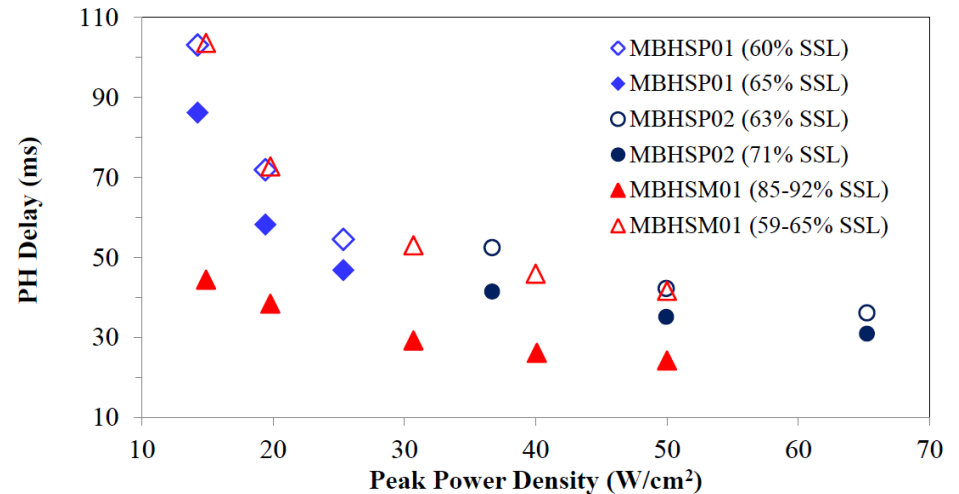


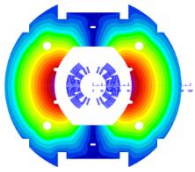
PH delay measured at different peak power density. Time constant (RC) of the PH circuit was:

- ~25 ms in MBHSP01,
- ~16 ms in MBHSP02,
- ~55 ms in MBHSM01

PH Delay measured for different time constant (RC)

PH delay can be reduced by adjusting the PH peak power or decay constant



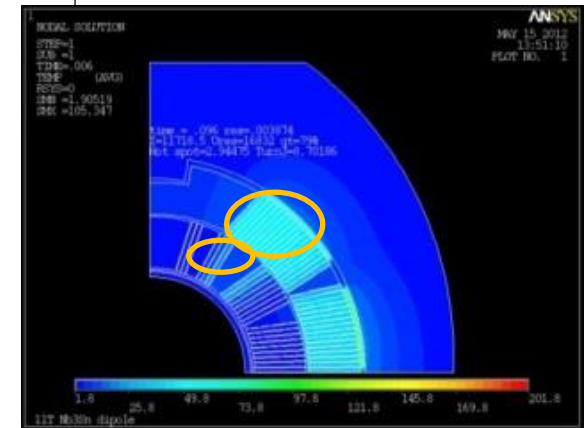
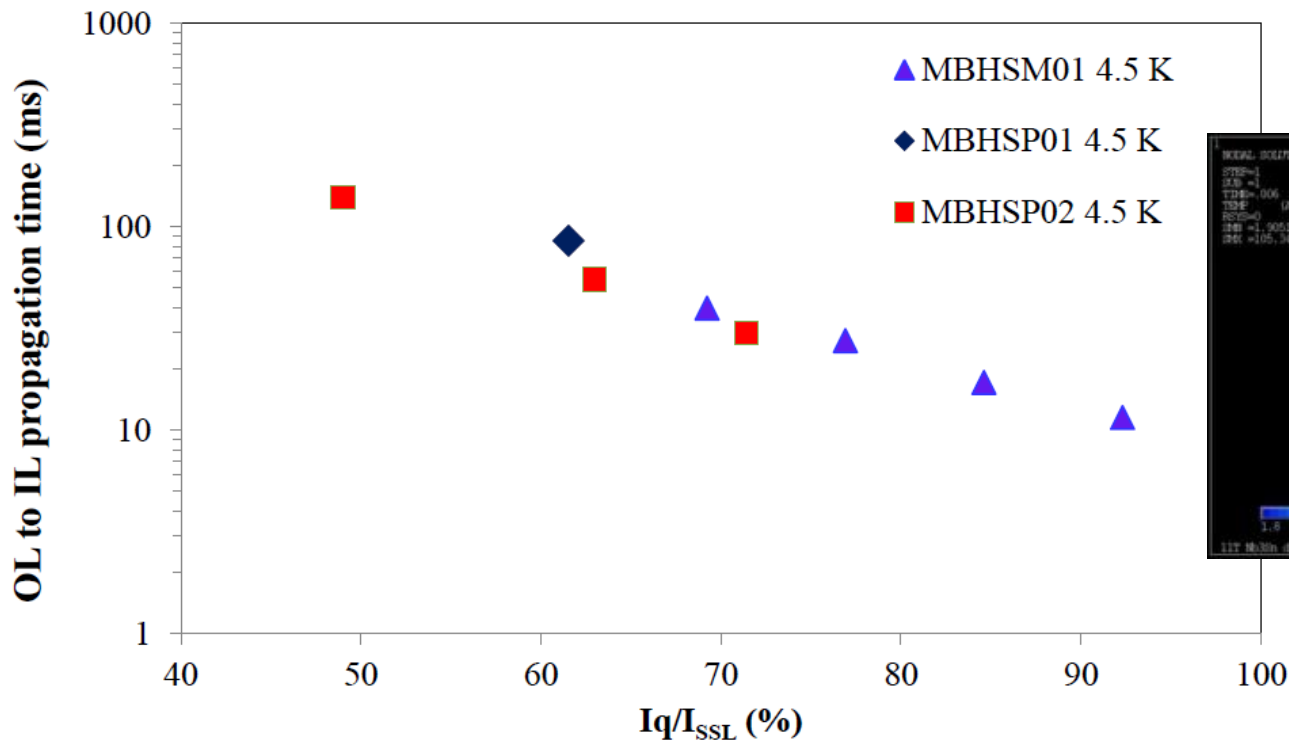


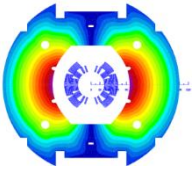
Radial Quench Propagation



OL to IL quench propagation time was measured in quenches with dump delay of 1000 ms. Average peak power density was $\sim 50 \text{ W/cm}^2$

- $\Delta t(I_{\text{nom}}) \sim 25 \text{ ms}$, reproducible, OL pole block and IL 2nd block quenching first



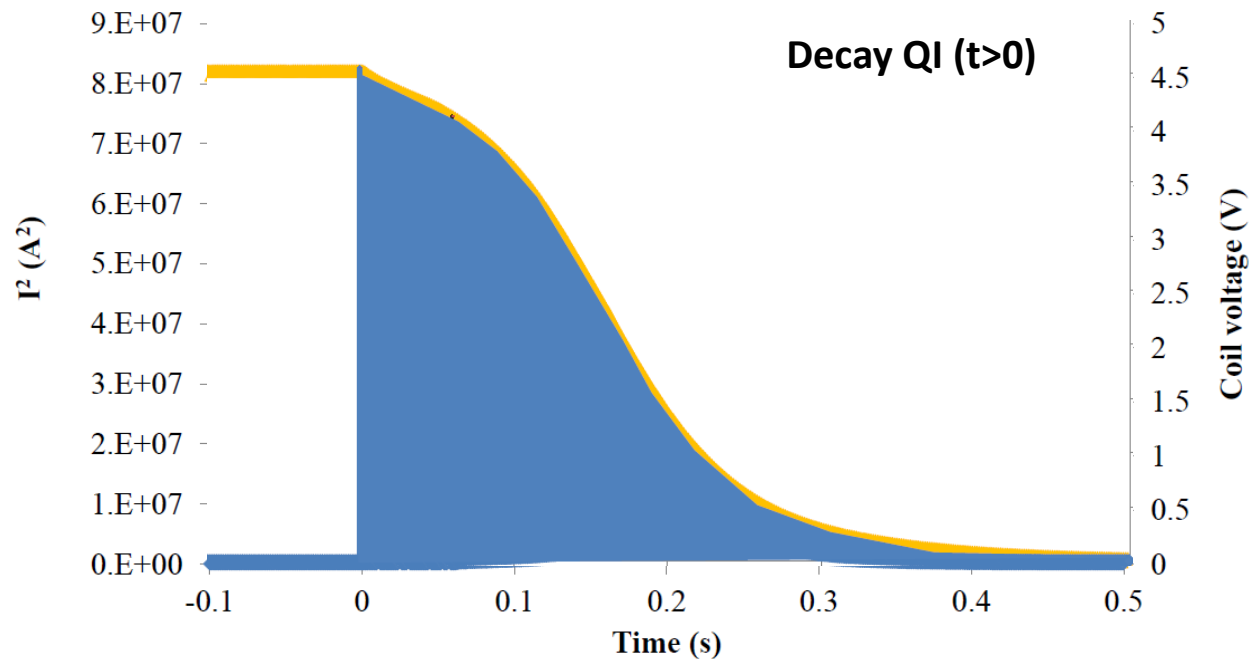


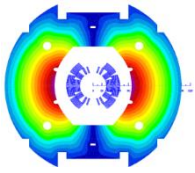
Quench Integral Study



The Quench Detection system was manually tripped; the outer layer heaters included in the magnet protection system

- Decay QI was calculated for the whole current decay, including the heater delay
- Decay QI can be used to estimate expected QI in a spontaneous quench by adding MIIIs corresponding to the quench detection time





QI Study in 11T magnets

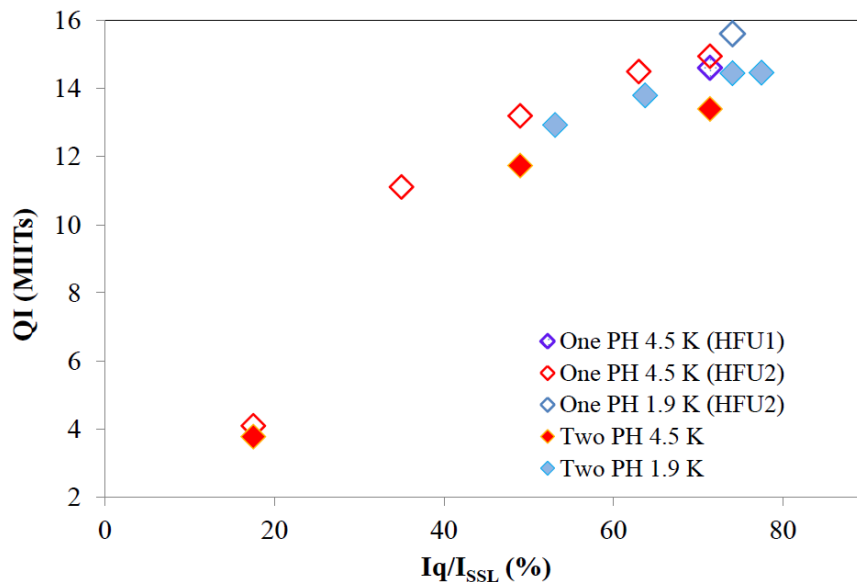


QI was measured in MBHSP01-02 with the external dump delayed for 1000 ms (“no dump”)

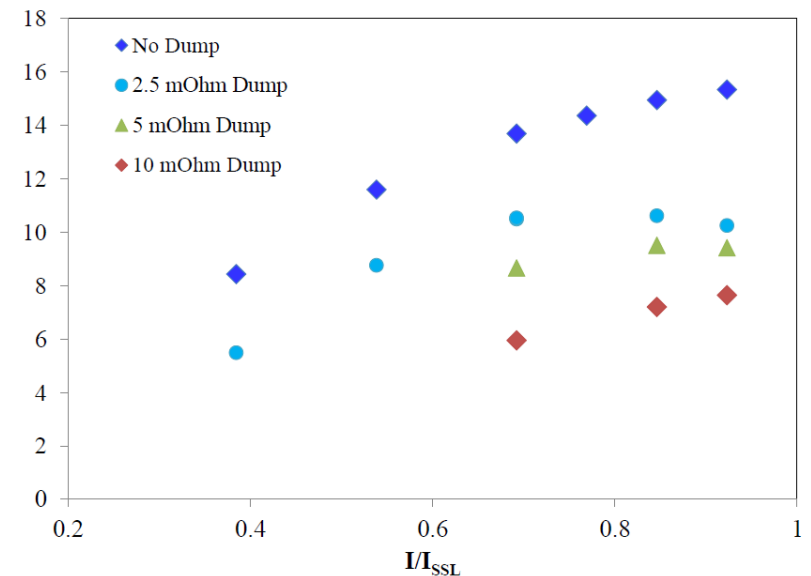
In MBHSM01 QI was estimated for “no dump”, as well as for 2.5 m Ω , 5 m Ω and 10 m Ω dump resistors

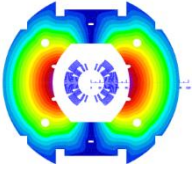
- QI(I_{nom}) \sim 16 MIITs, QI $_{max}$ =19/21 MIITs (HF/LF) - estimated time budget for Quench Detection seems reasonable: \sim 20 ms in HF and \sim 35 ms in LF

MBHSP01-02 Decay QI, “no dump”



MBHSM01 Decay QI



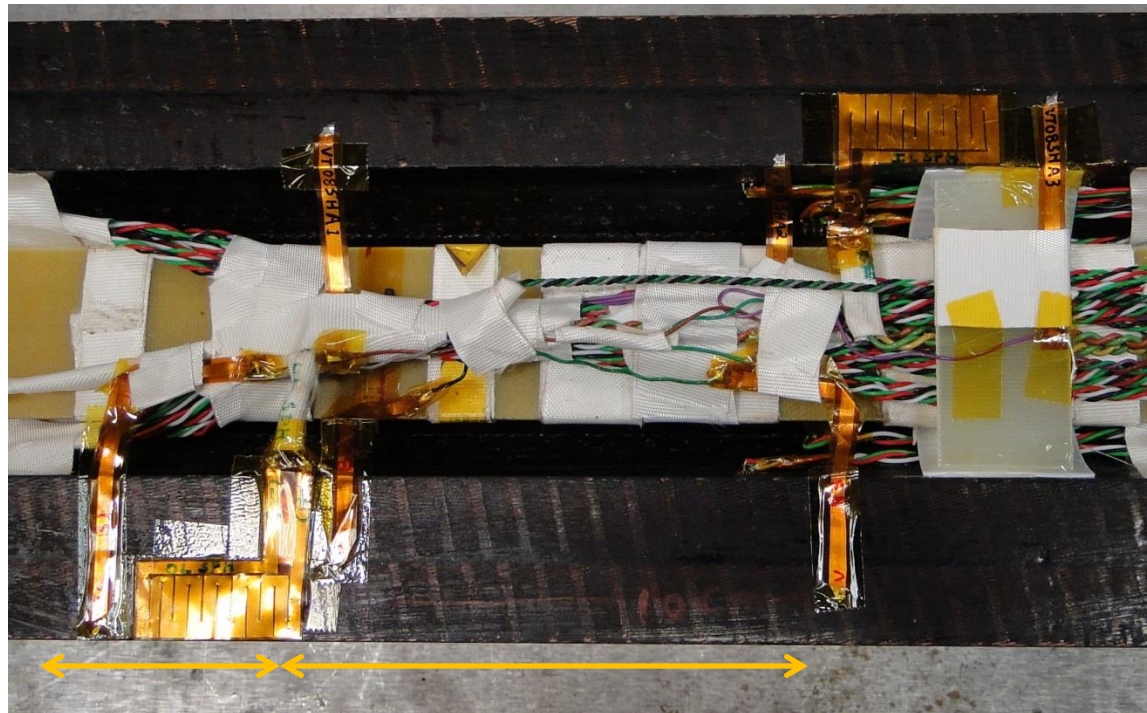


Spot Heaters in MBHSM01



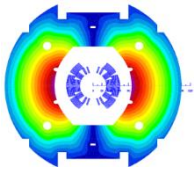
Spot heaters (SH) installed for estimation of the quench temperature and longitudinal propagation velocity

- VT installed in close proximity to the SH



5 cm

10 cm

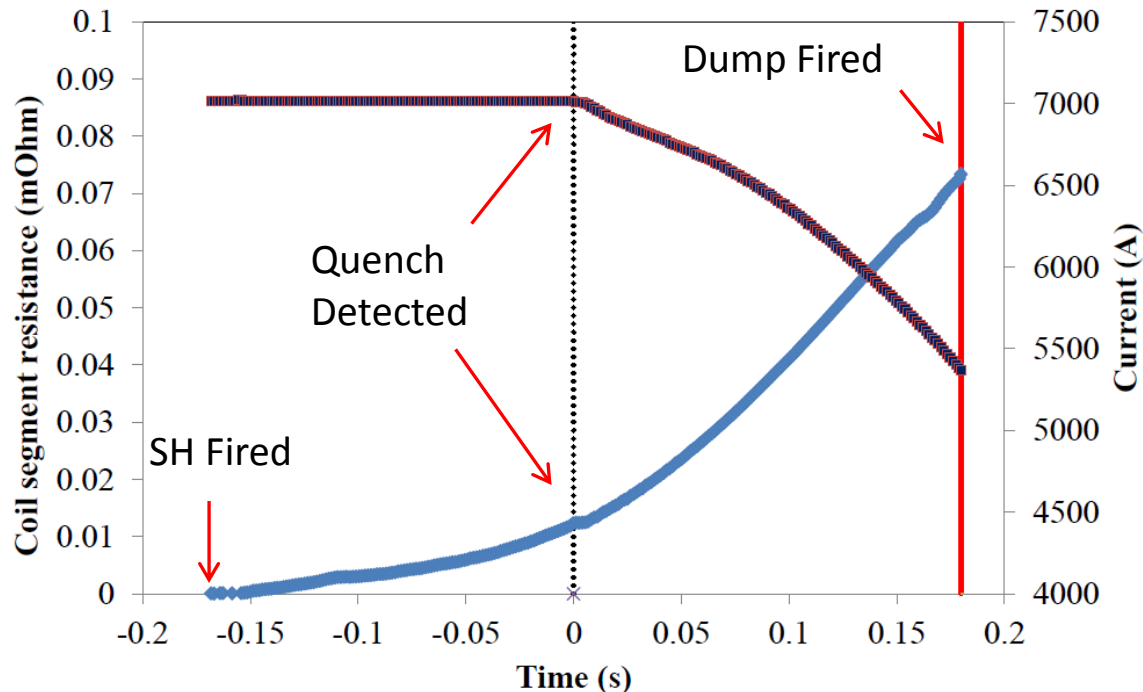


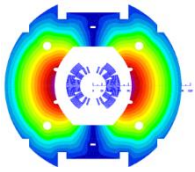
Spot Heater Tests at 4.5 K



Only OL spot heater was available for testing:

- Peak power density of $\sim 26 \text{ W/cm}^2$ was deposited at different currents
- Dump was delayed for 70-250 ms to increase accumulated QI
- Coil temperature was measured during the warm-up from 4.5 K to 200 K to calibrate the coil resistance change during the quench





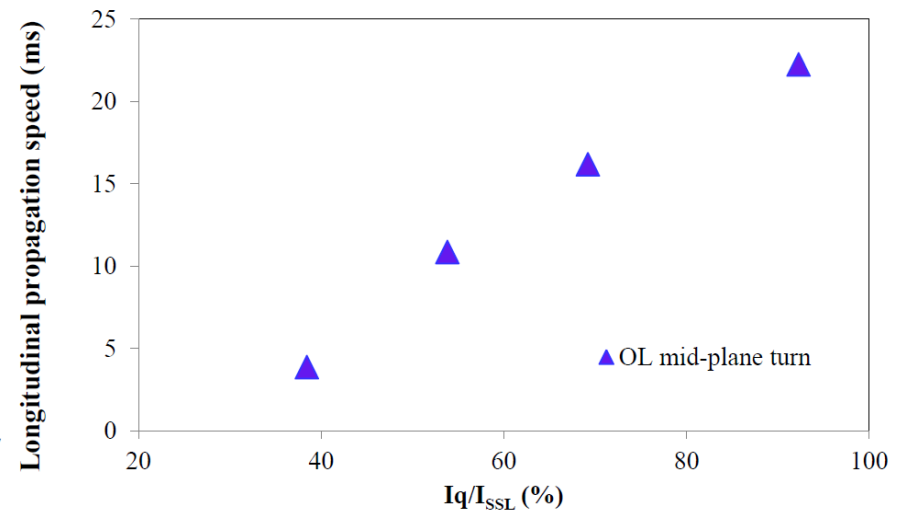
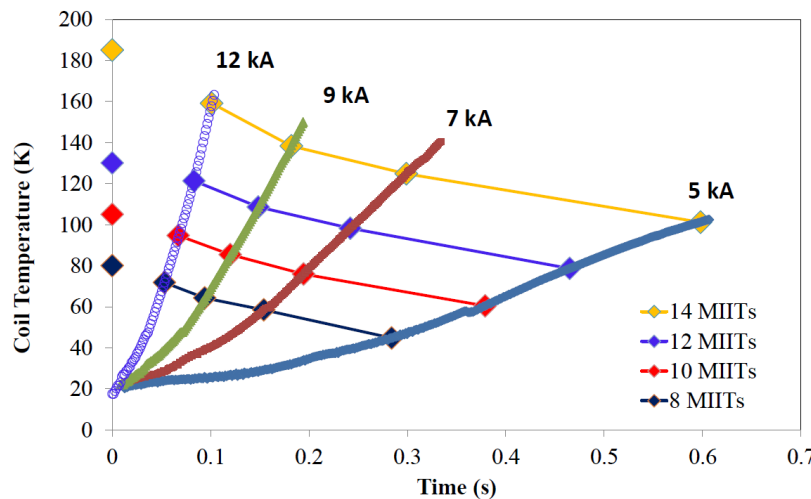
Spot Heater Tests at 4.5 K



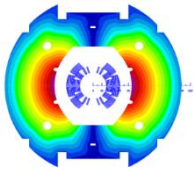
Coil temperature as a function of time was estimated in the OL mid-plane turn at different currents. Data point with the same QI are also shown in the plot

Adiabatic coil temperature estimations for different QI are shown at $t=0$

- Cable insulation, epoxy inside the cable and bronze inside sub-elements were included in calculations
- Current decays almost fully in 0.1-0.2 s, i.e. measured $T_{\max} = \sim 0.8 T_{\text{calc}}$



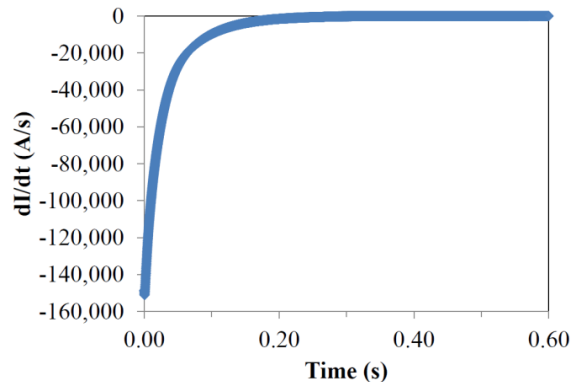
Longitudinal quench propagation velocity estimated only in the OL mid-plane turn



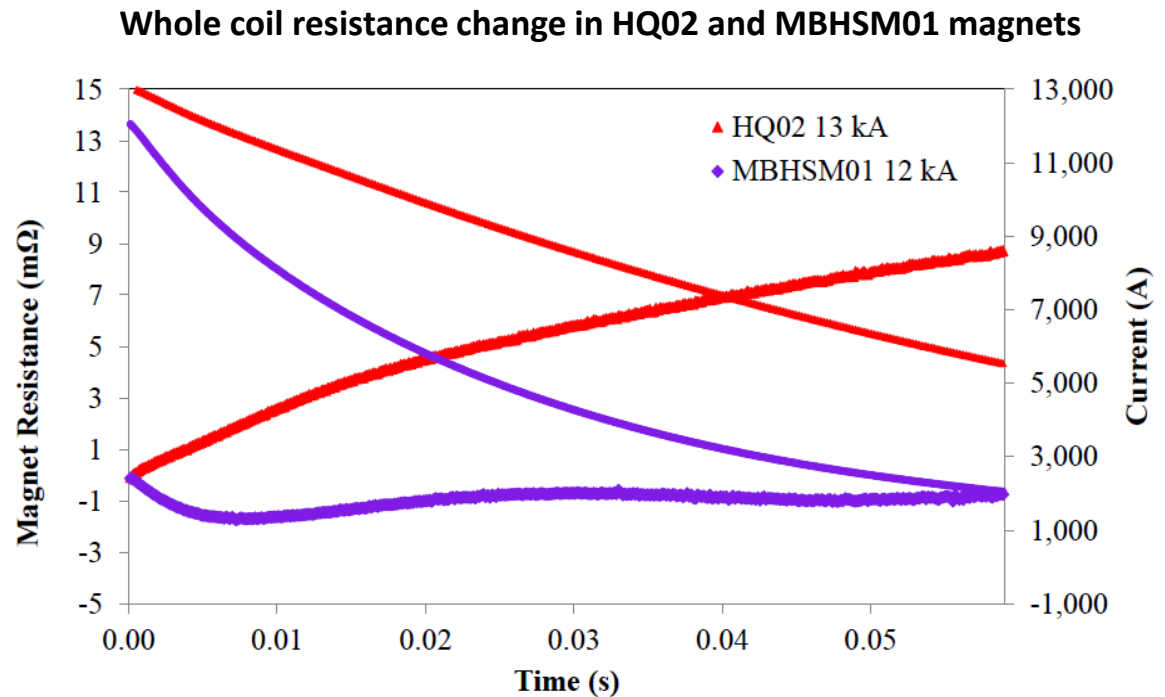
Fast extraction tests

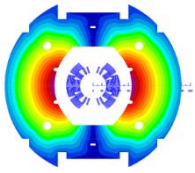


- The extraction dump is initiated at different currents w/o protection heaters.
No resistance increase was observed in the coil for the fast extraction at 12 kA
- Effect of cored cable and small filament size



Ramp rate for the fast extraction test





Summary



Quench protection study was performed at currents up to 92% of SSL and for different external dump resistors in 2 dipole and 1 mirror models

Minimum peak power density of $\sim 55 \text{ W/cm}^2$ is required to quench magnet at currents $I_{inj} < I < I_{nom}$

Azimuthal and Radial quench propagation was measured at different currents and temperatures

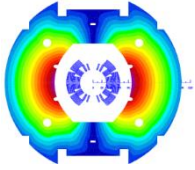
- Quite small quench delay helps to spread energy in the coil

Longitudinal quench propagation velocity was estimated in the mid-plane turn at different currents

- Quite large velocity helps to spread energy in the long magnet coils

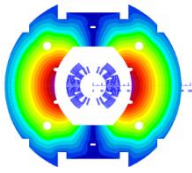
Coil temperature increase as a function of time was studied at different currents

- T_{max} measured is $\sim 20\%$ lower than the calculated one due to the cable cooling



BACKUP SLIDES

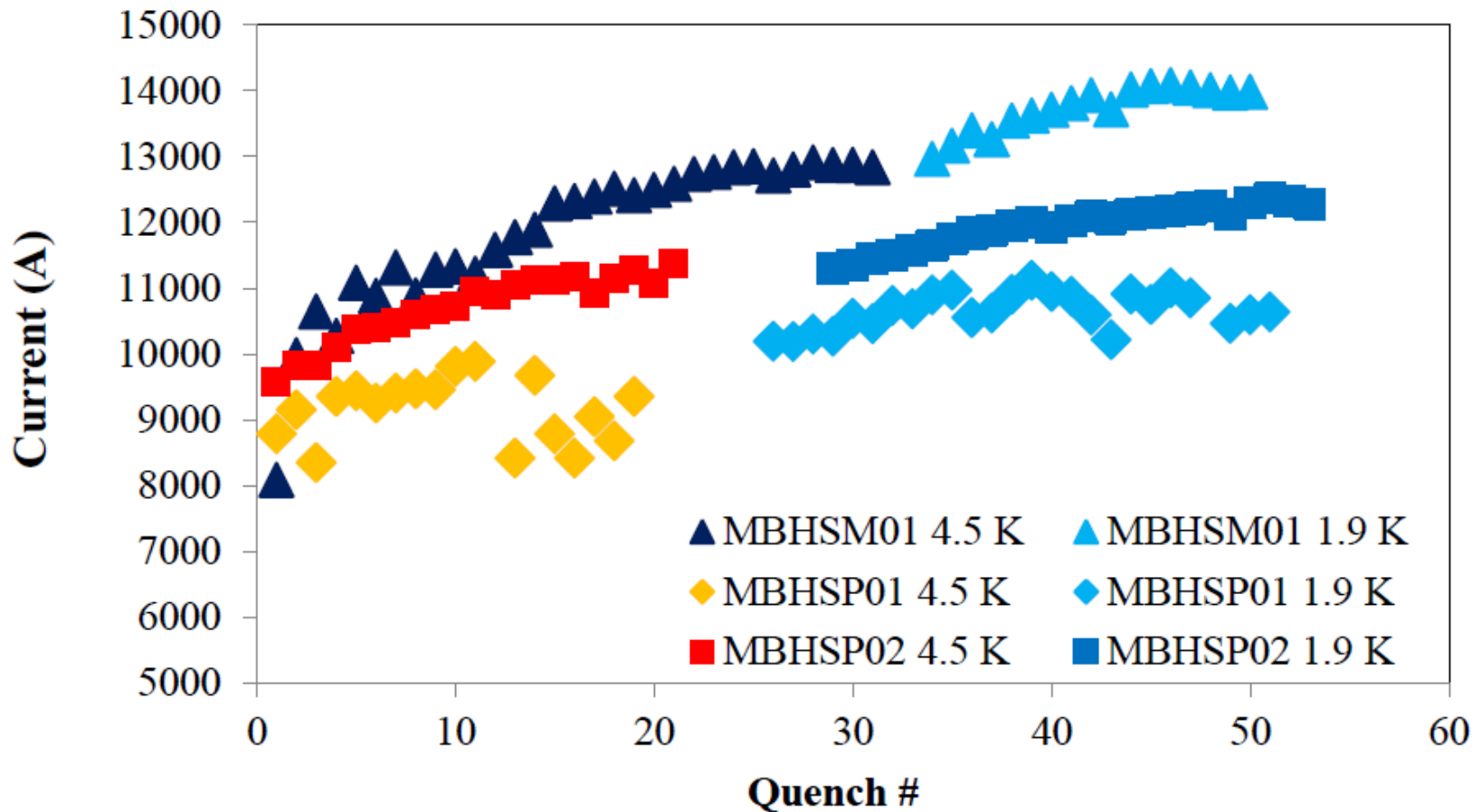


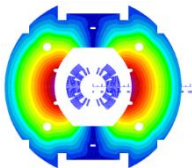


MBHSM01 vs. MBHSP01/02



Quench training in all 11 T magnets

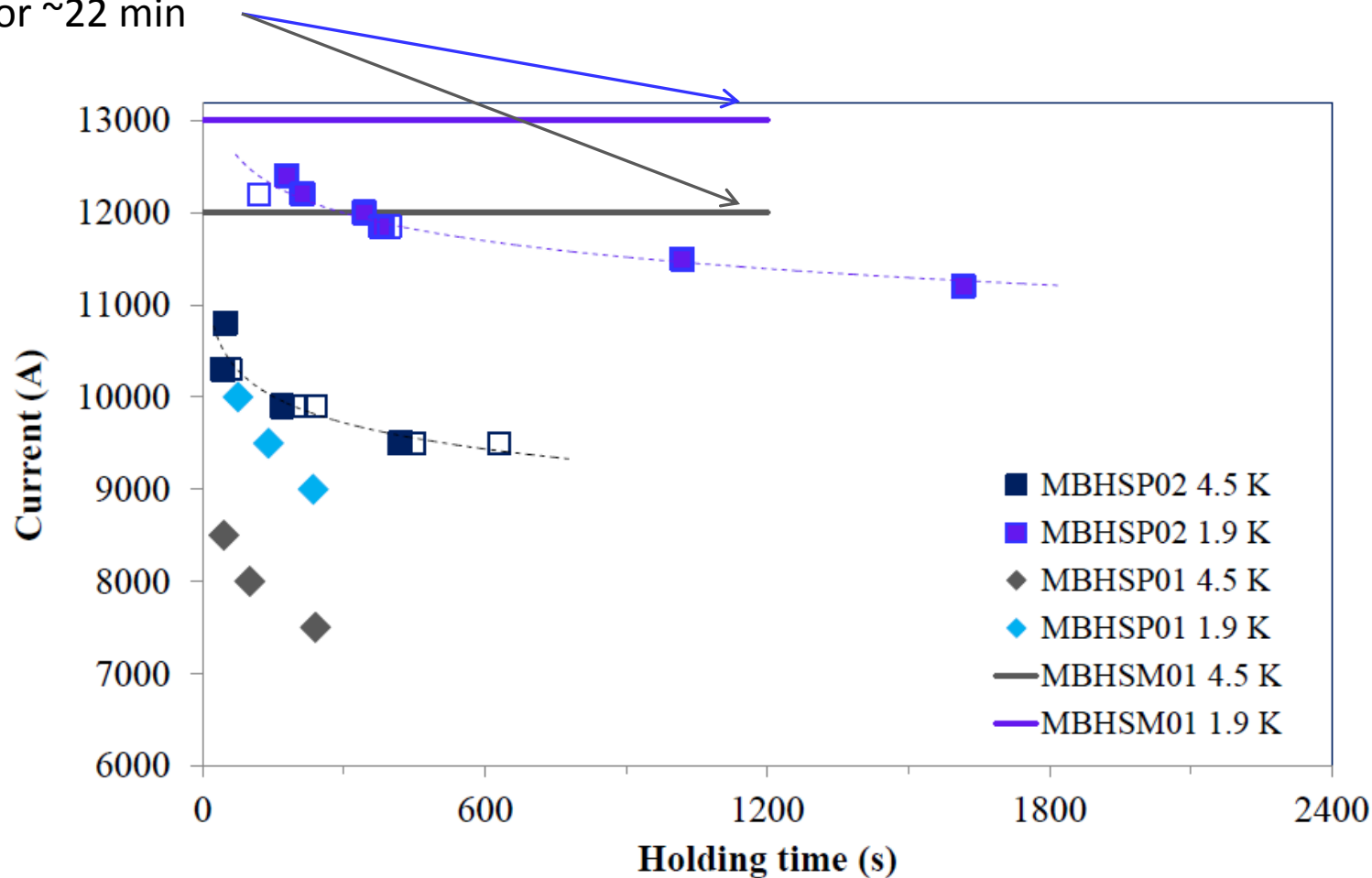


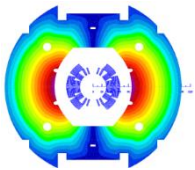


“Holding quenches”



No quenches in MBHSM01 after “holding” 13 kA at 1.9 K and 12 kA at 4.5 K for ~22 min

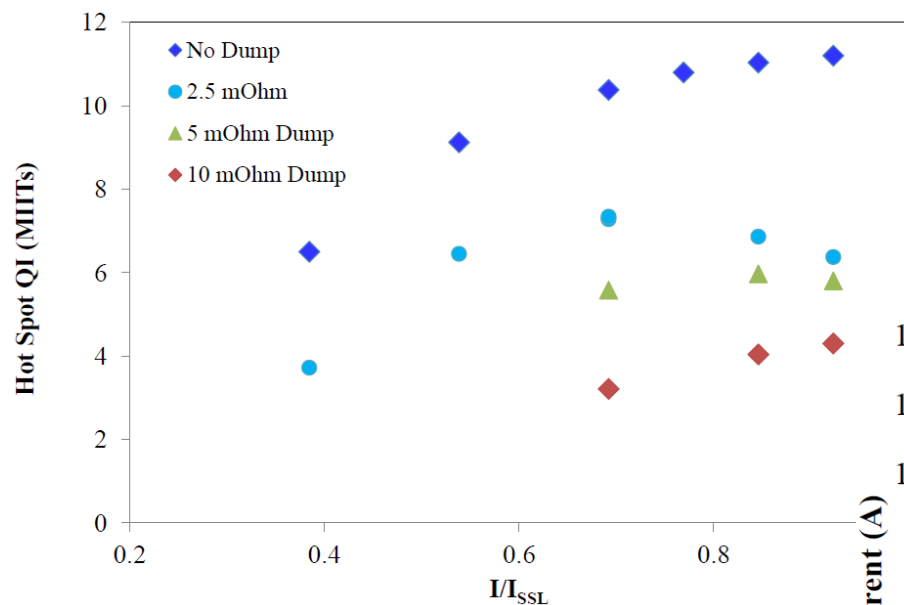




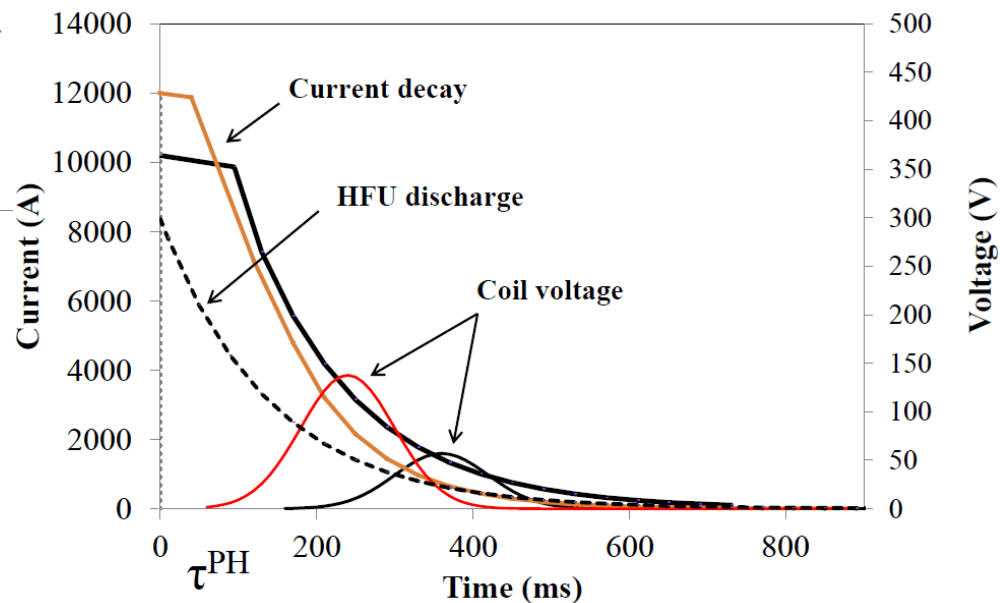
QI Study in 11T magnets

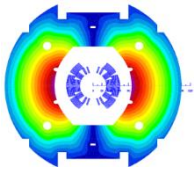


QI ($t > t_q$) exhibited similar current dependence in MBHSM01



QP tests at 10 kA and 12 kA





RRR Measurements



Average RRR in MBHSM01: ~220

- All segments shown for MBHSM01

