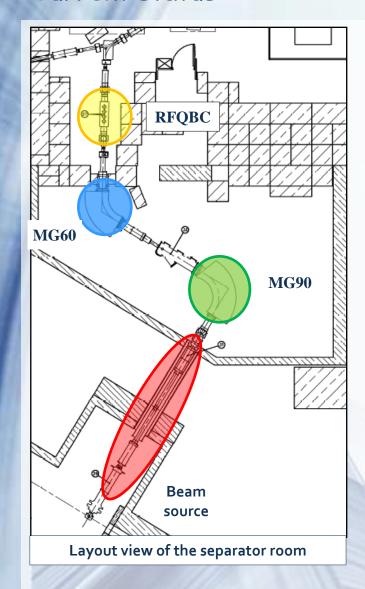
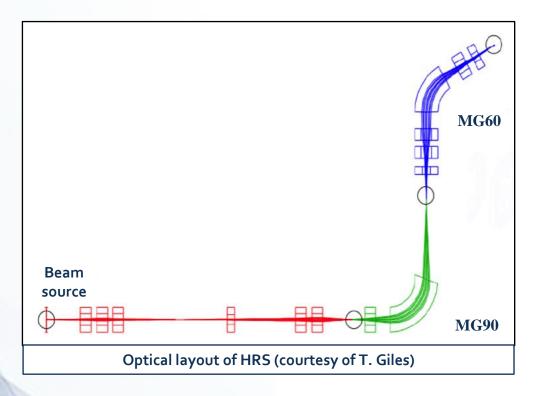


## Outline

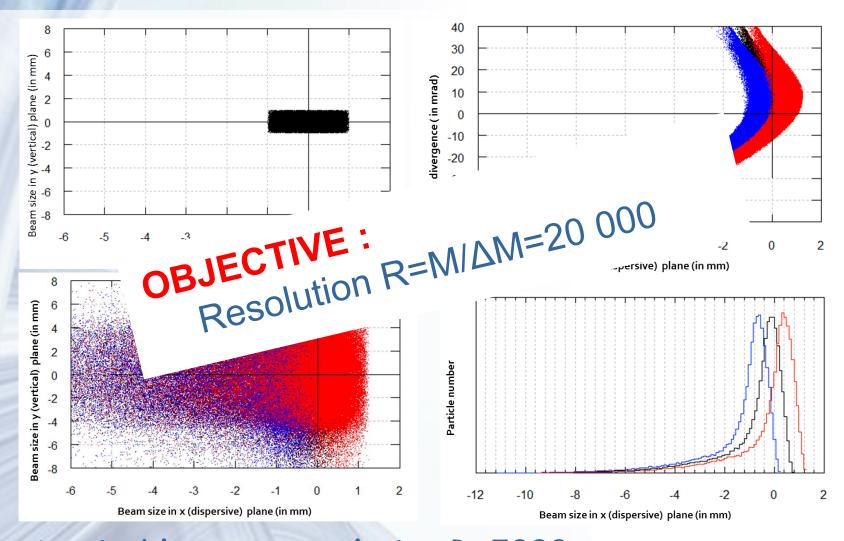
- √ The High Resolution Separator and its current situation
- √ The new constraints
- ✓ Design proposals
- √ Magnet features
- √ The technology: pole face winding coils
- √ The testbench

#### Current status





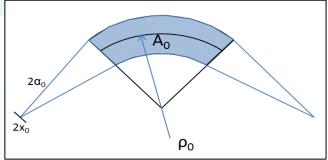
Current HRS optical performances



Attainable mass resolution R=5000 for beam source of emittance  $\epsilon$ =20 $\pi$ .mm.mrad

How to reach high resolution?

## Dispersion D



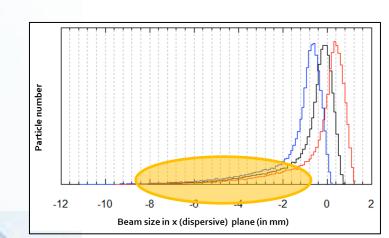
$$R = \frac{D}{2.x_0.M_x}$$

$$\varepsilon = \pi \cdot x_0 \cdot a_0$$

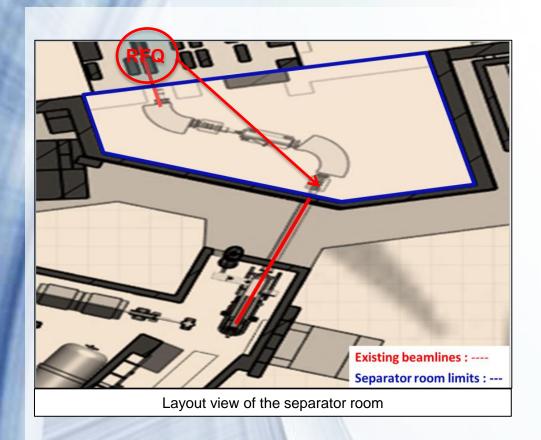
Beam emittance

 $M_x$  magnif. Factor  $x_0$  beam size at source

Eliminate higher order terms (=aberrations)



## The High Resolution Separator RFQ-CB displacement



#### Moving of the RFQ-CB

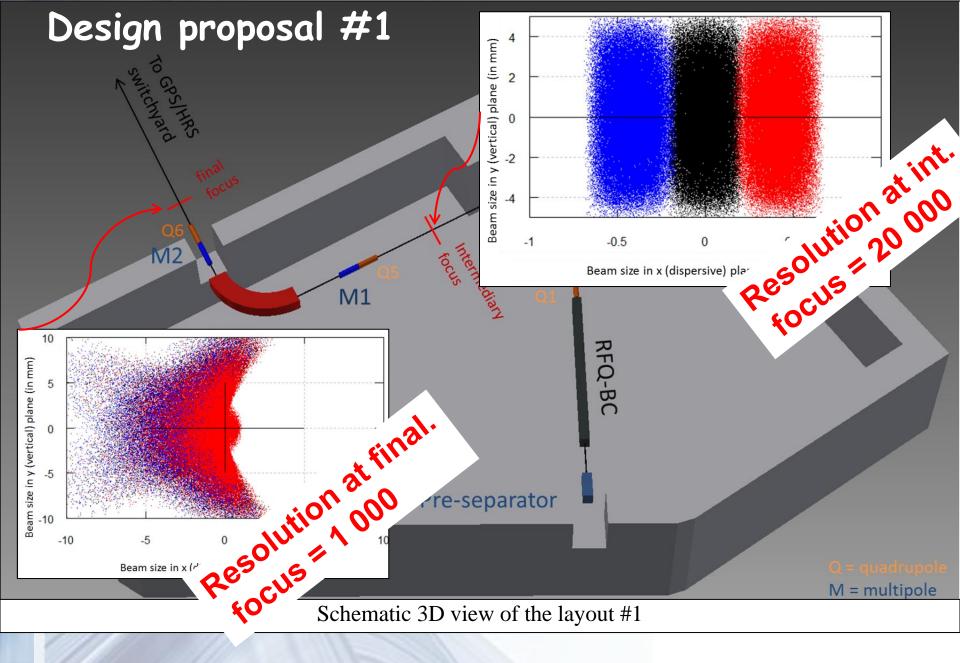


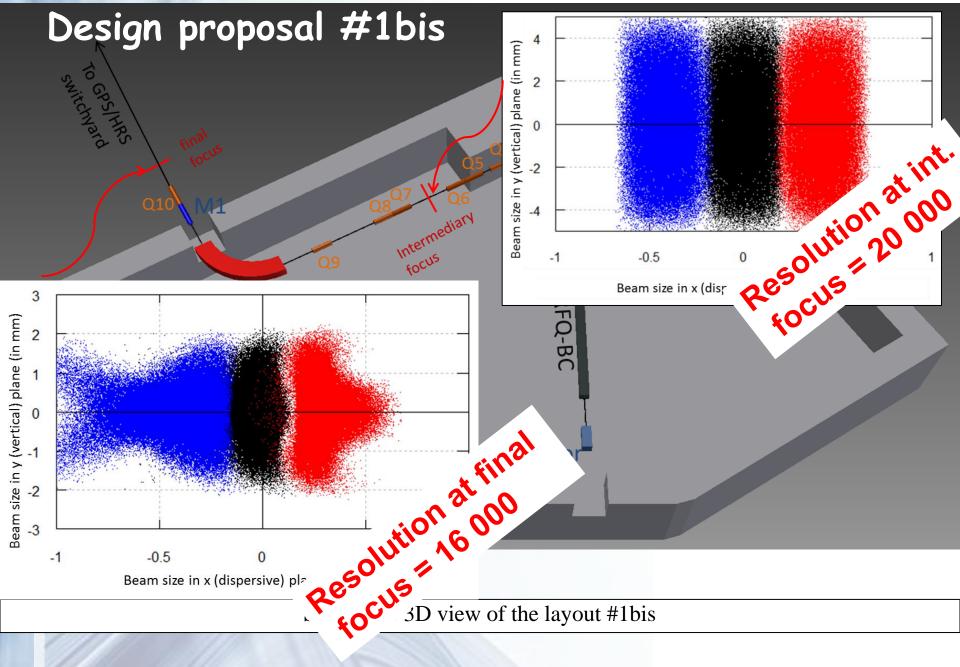
### **Ensuing constraints:**

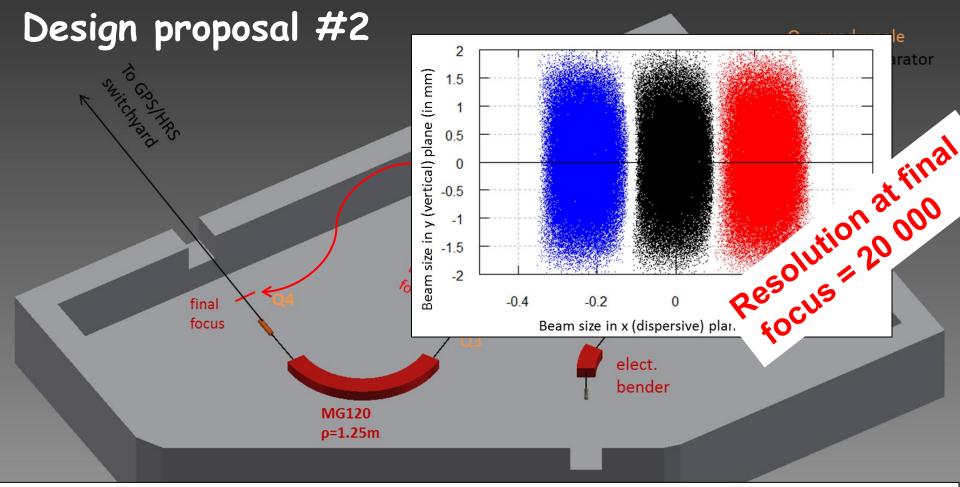
- Beamlines installations and positioning
- Separator room size

#### **OBJECTIVE:**

Resolution R=M/ $\Delta$ M=20 000 for a beam source emittance  $\epsilon$ =3 $\pi$ .mm.mrad







Schematic 3D view of the layout #2

Beam emittance  $\varepsilon=3\pi$ .mm.mrad

R = 20 000 for more than 99% transmission of pure beam

R ~ 23 000 for 90% transmission of pure beam

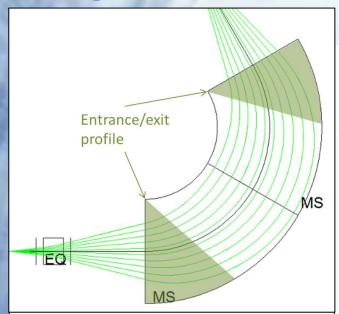
## Magnet features Optical parameters

Beam energy	60 keV
Maximum mass	300
Magnetic rigidity	0.6125
Bending radius	1.25 meter
Nominal magnetic field B	0.49
Bending angle	120 degrees
Vacuum chamber size on x-plane (dispersive)	350 mm
Vacuum chamber size on y-plane (vertical)	25 mm
Inhomogeneous field parameters	
α (quadrupole component)	0.25 (tolerable between 0.21 and
	0.31)
β (hexapole component)	4.245e-2< 4.32E-2< 4.40E-2
Γ (octopole component	4.00E-3< 8.38E-3 < 1.30e-2



## List of parameters for the mechanical design of the magnet

## Magnet features: optical parameters

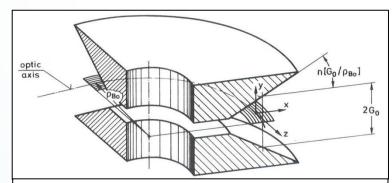


Beam enveloppe for design #2 in lab coordinates (x,z), featuring a magnet using entrance/exit profiles (producing a quadrupole component)

- > No entrance/exit angular profile
- > Radially Inhomogeneous Magnetic field:

$$B = B_0 \left( 1 - \alpha \cdot \frac{r - r_0}{r_0} + \beta \cdot \left( \frac{r - r_0}{r_0} \right)^2 - \gamma \cdot \left( \frac{r - r_0}{r_0} \right)^3 \right)$$
 (with a,  $\beta$  and  $\gamma$  respectively being the

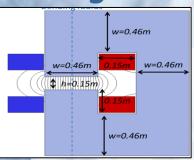
quadrupole, sextupole and octopole components)



Example of magnet design, producing a radial inhomogeneous field, using inclined pole faces.

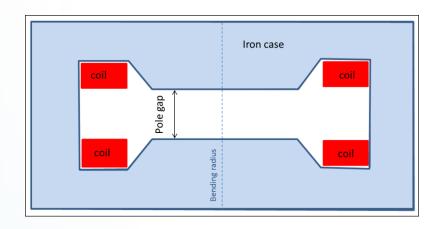
- > Plane pole faces > easier to machine
- > Inhomogeneous field produced with pole face windings

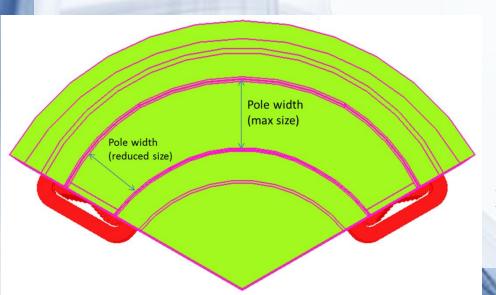
### Magnet features



→ H type magnet → mechanically more stable, possibility of better pole face machining

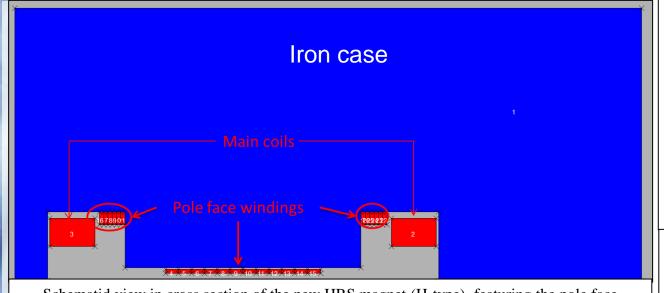
Yoke made of laminated steel
 → reduction of eddy currents,
 allowing an increase in cycling speed
 (~1min VS 15min)



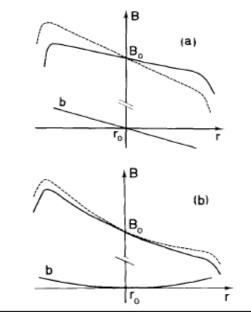


- Changing pole face width
  - → saving of material (~8%)

## The High Resolution Separator Pole face windings



Schematid view in cross section of the new HRS magnet (H-type), featuring the pole face windings technology (picture credit to M. Breitenfeldt



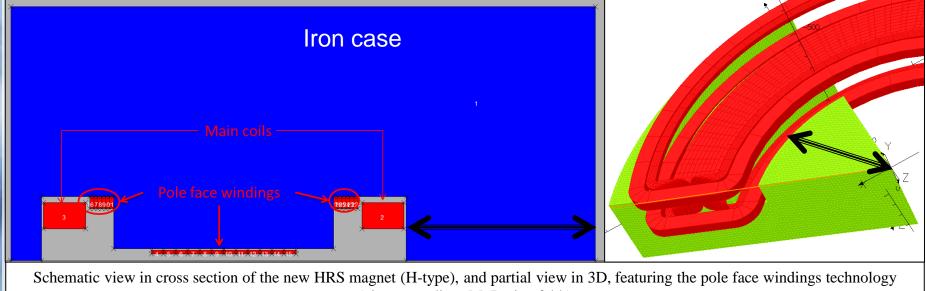
Effect of pole face winding for  $\alpha$  and  $\beta$  component in the main field distribution. Dashed curves represent the additional field necessary to modify  $\alpha$  and  $\beta$ 

#### > Optimize currents in the conductors to match the field composition

$$I = I_{quad} + I_{hex} \left( \frac{r - r_0}{r_0} \right)^2 + I_{octo} \left( \frac{r - r_0}{r_0} \right)^3 \implies B = B_0 \left( 1 - \alpha \cdot \frac{r - r_0}{r_0} + \beta \cdot \left( \frac{r - r_0}{r_0} \right)^2 - \gamma \cdot \left( \frac{r - r_0}{r_0} \right)^3 \right)$$

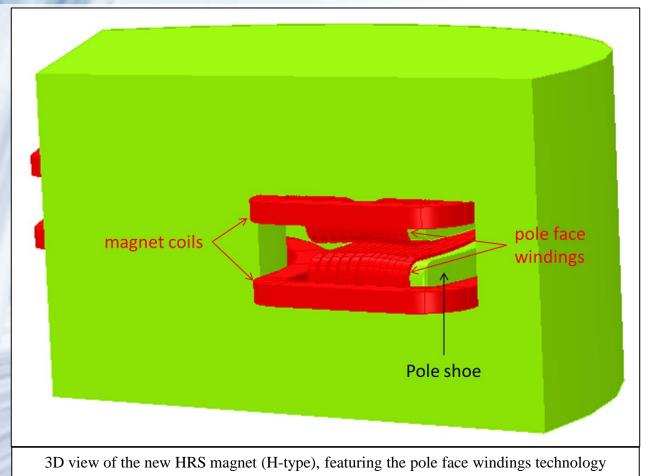
- > Current density in the conductor : up to 1A/mm2 (with air cooling)
  - → for the studied magnet: 0.2 A/mm2 were necessary
- → Higher order term coefficients are adjustable by changing current
  → High degree of freedom

## The High Resolution Separator Pole face windings

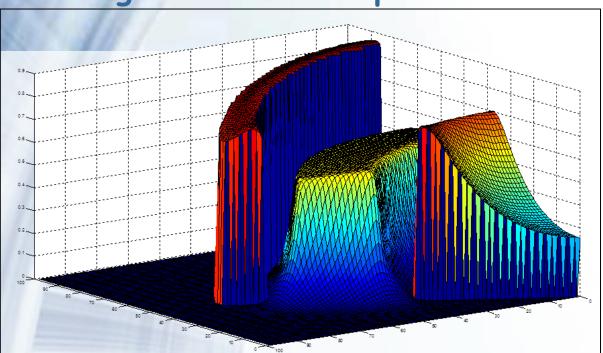


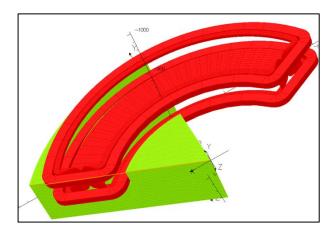
(picture credit to M. Breitenfeldt)

> Avoid field lines saturation > adapting the design



(picture credit to M. Breitenfeldt)





3D magnetic field map of the new HRS magnet for a section of a magnet, computed with Opera software (picture credit to M. Breitenfeldt)

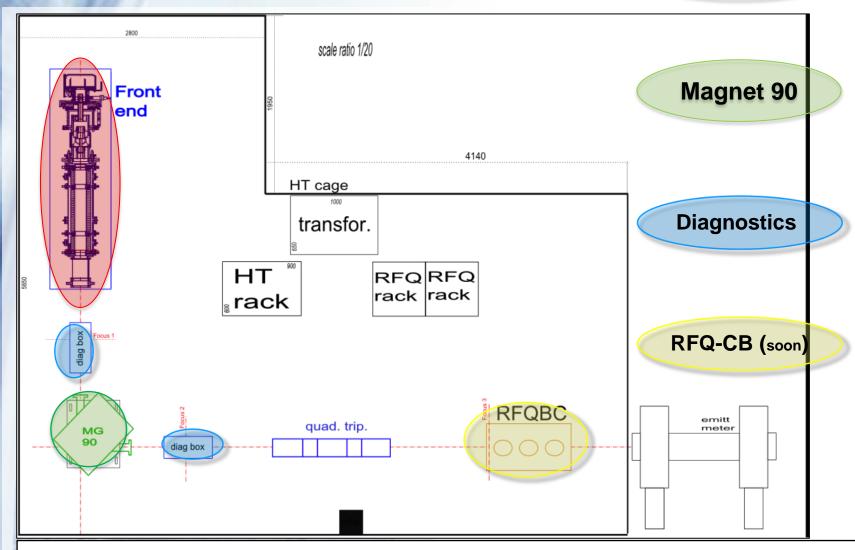
- Poleface windings allow the adjustment of the magnetic field along the beam axis.
- Rogovski profile at pole entrance and exit adjusts magnetic length.
- Excitation of return yoke is not exceeding 0.9T for max field at beam axis (0.5T)
  - > the excitation is in the linear regime.

## The Offline Separator



## The Offline Separator



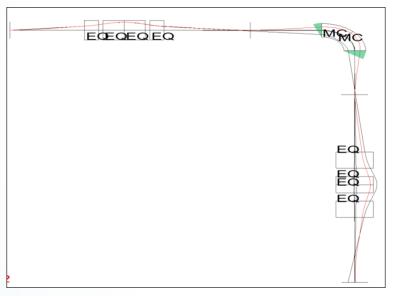


October 2013 : FE8 made its first beam : 30 nA at 40 kV with surface ion source !

March 2014 : First separation tests successful

## The Offline Separator Objectives





- Current magnet is of flat pole type, with entrance/exit profile (later used as pre-separator?)
- Design of a new offline magnet ongoing, featuring pole face windings

> Objective : validate the technology

## The Offline Separator Objectives

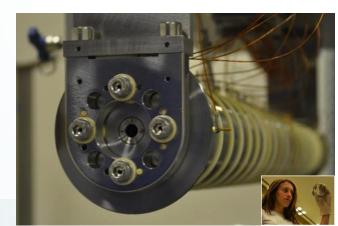


#### **ISOLDE FRONT END 8**

- Beam production
- Tests and characterization of different ion sources

## THE RFQ-CB

- > Investigation of functional parameters :
  - injection/extraction system efficiency
  - > Emittance and beam parameters



## Conclusion

### ON THE ROAD TO A NEW HIGH RESOLUTION MAGNET...

- > A workable layout, including all necessary items
- Design choice for the magnet features
- Functional test bench for validating the technology

Pole face winding



source parameters

## Acknowledgements





## My supervisor Tim Giles

# All the Marie Curie Fellows, and CERN staff

## The Marie Curie Actions

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## Thank you for your attention

