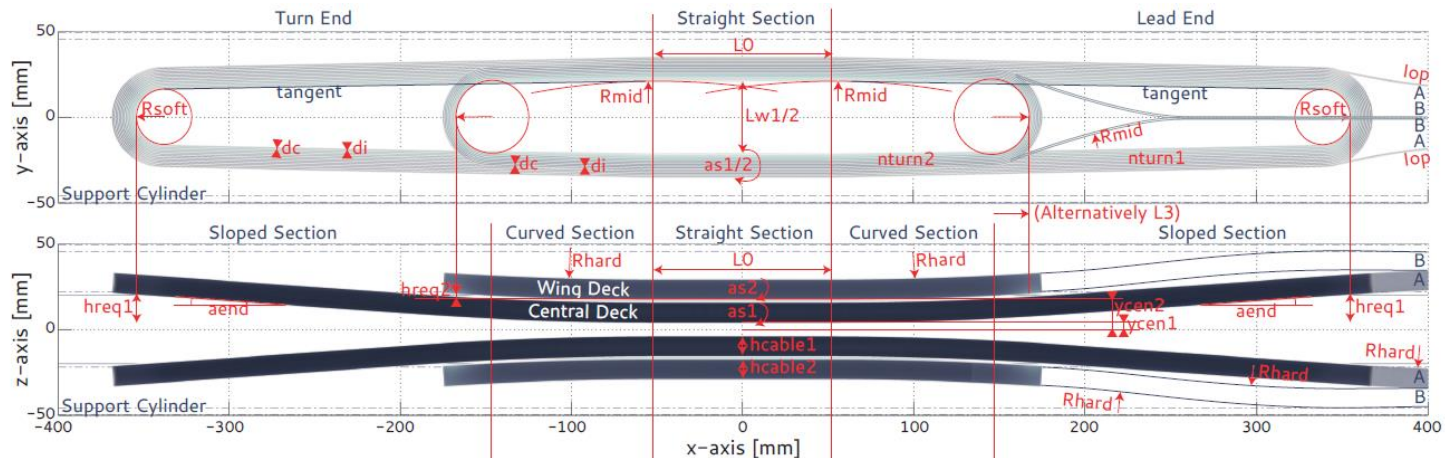


Electrical Network Model for ReBCO Cables and Coils

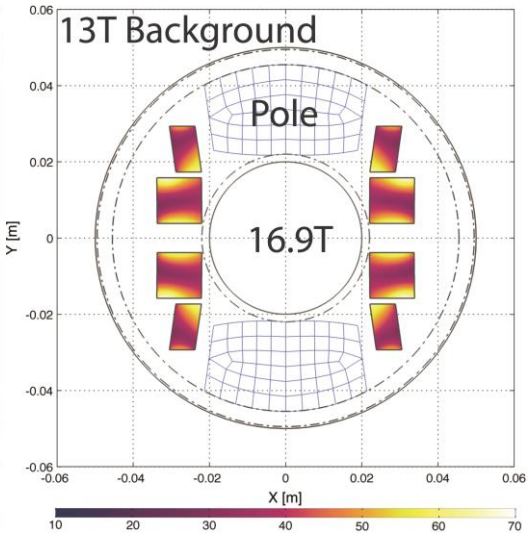
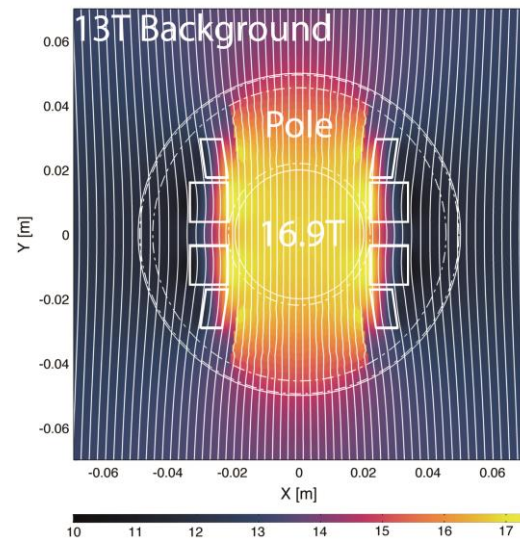
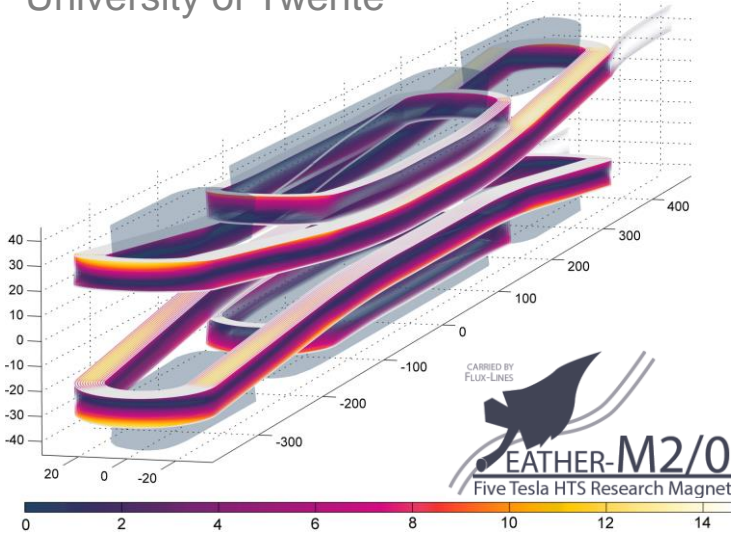
WAM-HTS Kyoto Japan 14-15 November 2014

Work performed at CERN, Technology Department, Magnets, Superconductors and Cryostats group as part of the EuCARD-2 project, within the framework of a PhD. At the University of Twente, Energy Materials and Systems group.

*J. van Nugteren, G. Kirby, G. de Rijk, L. Rossi, H.H.J. Ten Kate (CERN),
A. Nijhuis, K. Yagotintsev and M.M.J. Dhalle (Twente)*



- Feather-M0/2 EuCARD-2 Magnets (presented at ASC 2014)
- Two of the present concerns with **ReBCO** HTS accelerator magnets
 1. Magnetization and Field Quality
 2. Quench Detection and Protection
- This lead to the development of an Electrical Network model of ReBCO cables (and coils)
- The model follows the **JackPot-AC** model for Cable in Conduit Conductors from the University of Twente



- Part of **ITER** project
- Calculation of current distribution in Cable in Conduit Conductors (CiCC)
- Accurate prediction of coupling losses of such cables and joints
- Allows for large number of elements
- Idea is to start from same solver setup because it is fast and solid
- Many new features needed implementation

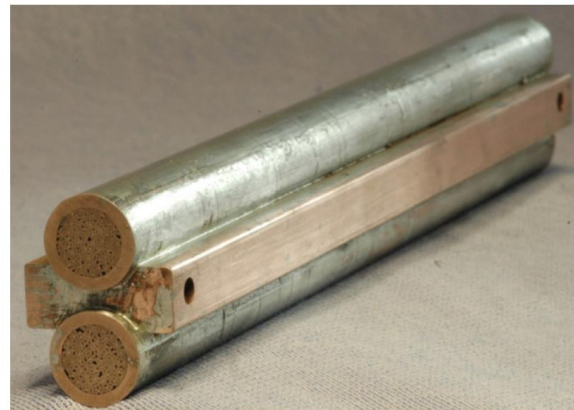
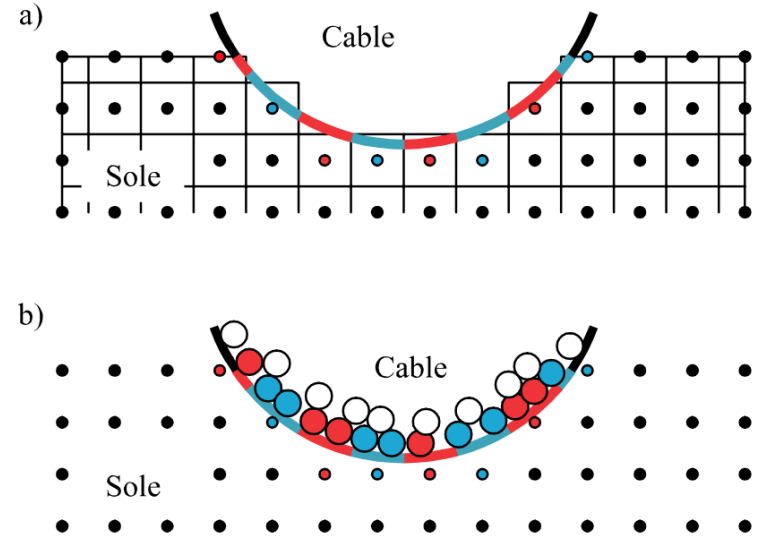


Figure 9. The mock-up joint assembly.

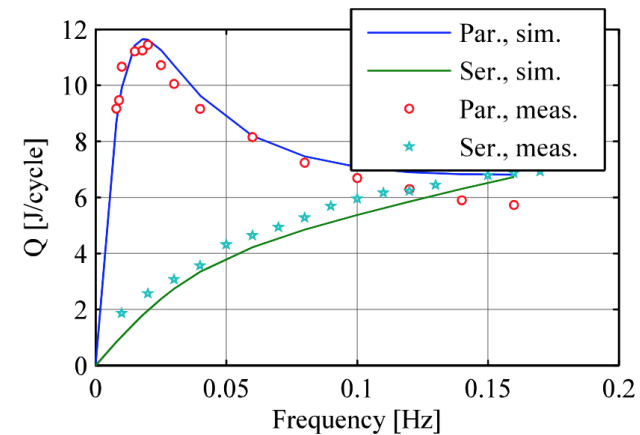
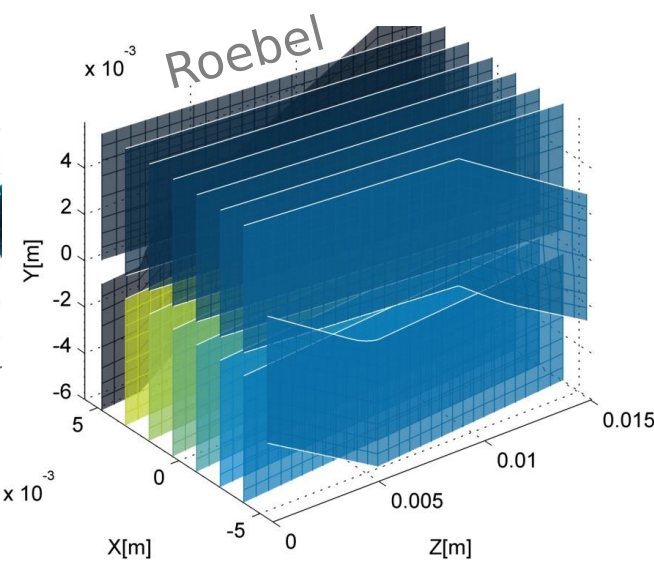
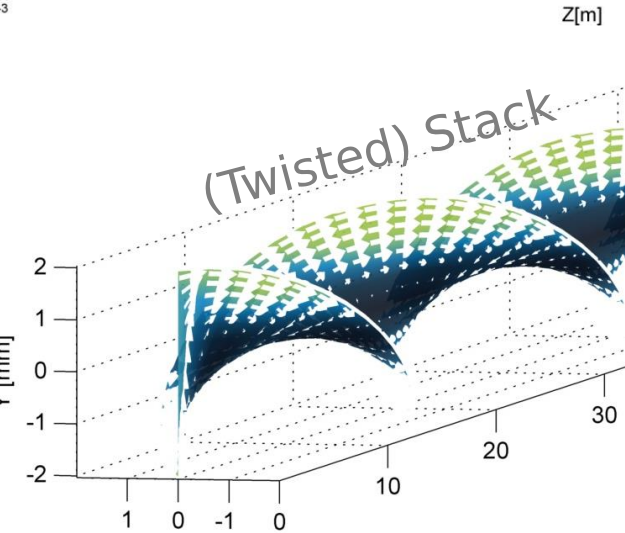
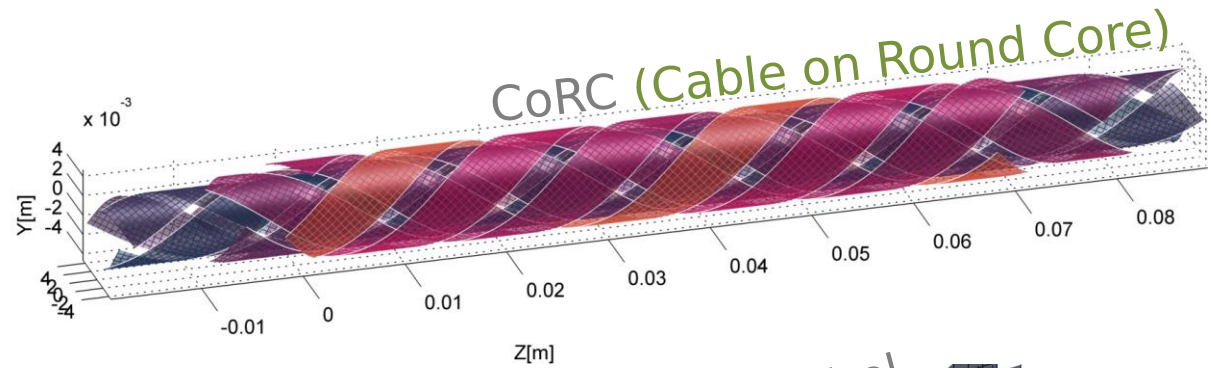


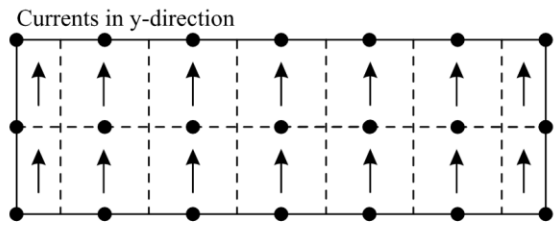
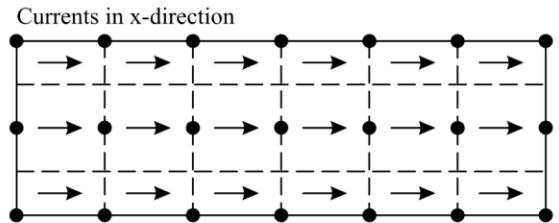
Figure 10. Measured and simulated AC loss of the joint versus frequency, under different angles of the applied AC field.

E P A van Lanen, J van Nugteren and A Nijhuis, "Validation of a strand-level CiCC-joint coupling loss model" Superconducting Science and Technology 2012, vol 25

- To be able to model the hysteresis the superconducting tapes are modeled as ribbon shaped meshes of elements (PEEC)
- At this moment there are three cable geometries implemented.



Network Elements



- Voltage node
- Current

Figure 1. Schematic representation of a 2D rectangular object modelled with the PEEC method.

- Geometry consists of
 - Voltage nodes
 - Current elements



- Baseline cable geometry for EuCARD2 Feather-M2 magnet
 - 15 tapes
 - 226 mm twist pitch
- The positions of some nodes along the length of the cable are fixed
- Trajectories of tapes are calculated from unit cell

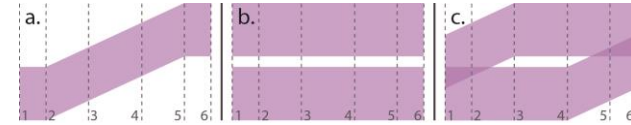
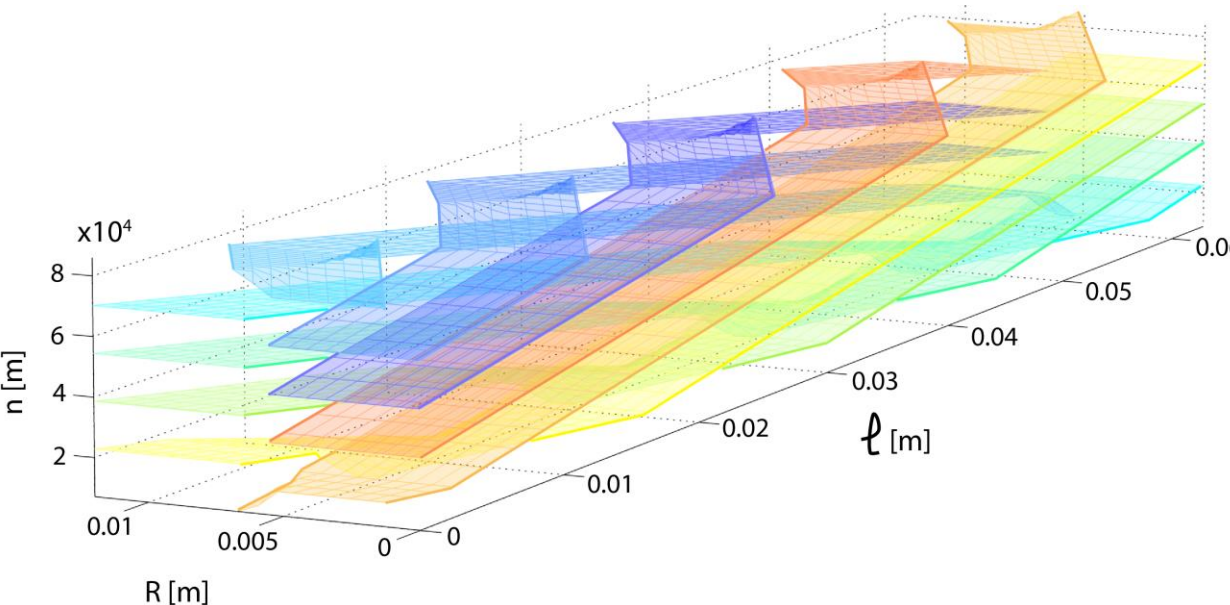
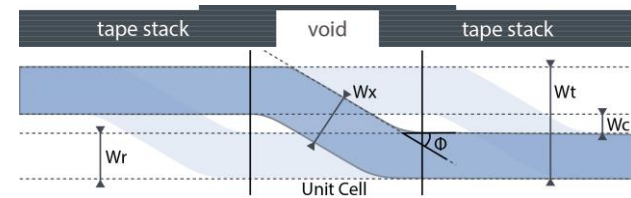
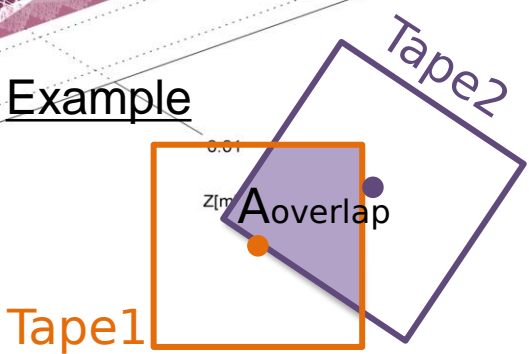
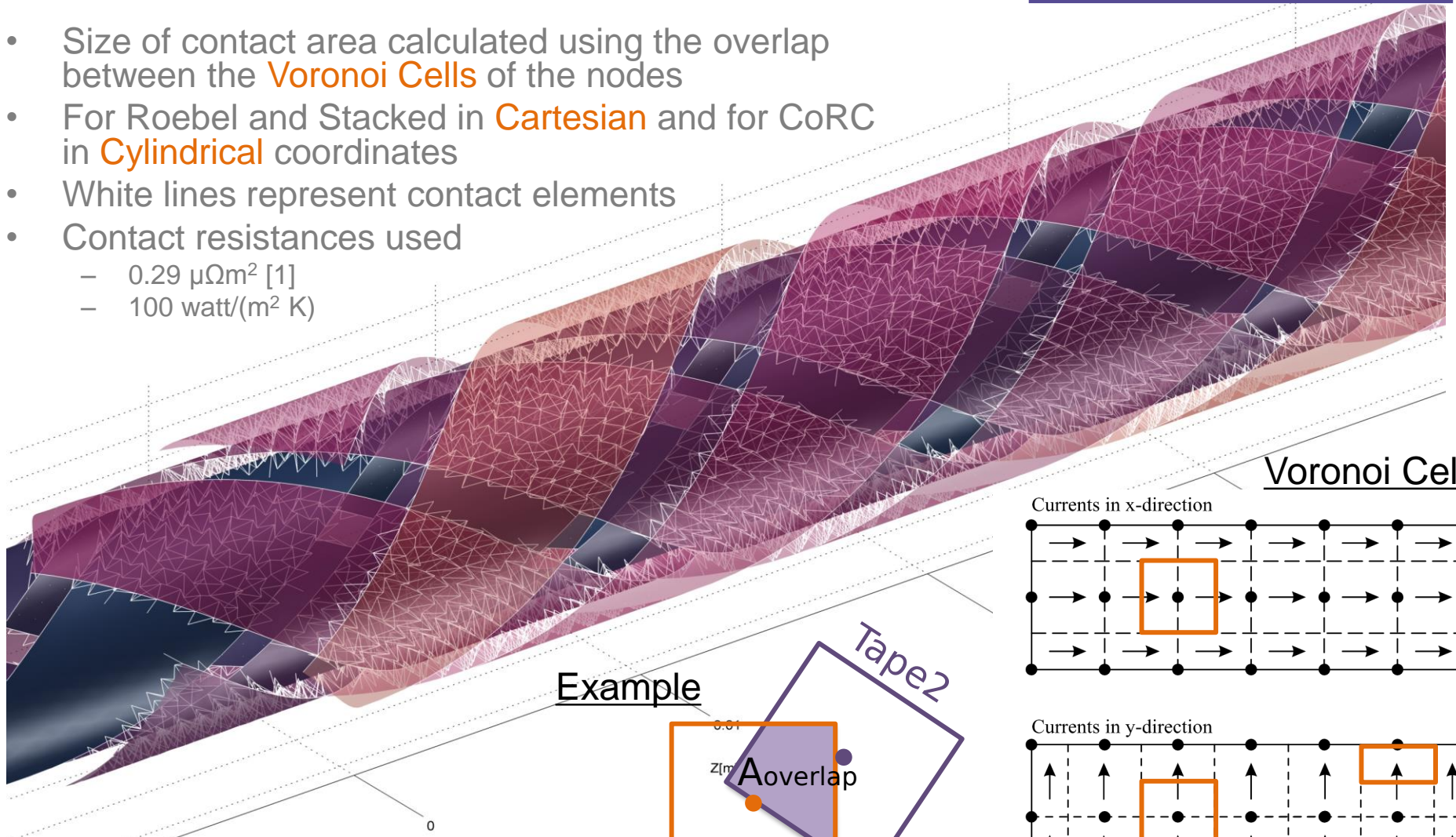


TABLE I
PARAMETER VALUES OF THE COATED CONDUCTOR AND ROEBEL CABLE.

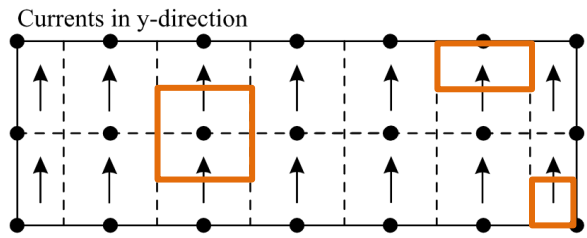
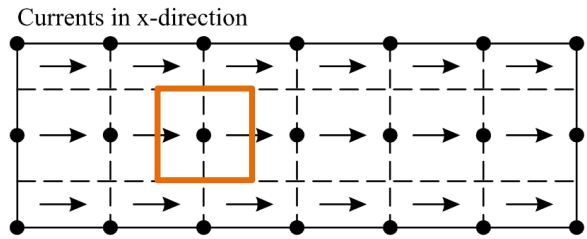
Symbol	FM0	FM2	Description
N_s	15	15	number of strands
ds	0.10 mm	0.10 mm	strand thickness
dc	0.8 mm	0.8 mm	cable total thickness
di	0.1 mm	0.1 mm	insulation thickness
Wr	5.50 mm	5.50 mm	strand width
Wt	12.0 mm	12.0 mm	cable width
Wx	5.50 mm	5.50 mm	cross over width
Wc	1.0 mm	1.0 mm	channel width
Φ	30 degree	30 degree	cross over angle
Ltp	226 mm	226 mm	transposition pitch
ri	6.0 mm	6.0 mm	inner radius
ro	0.0 mm	0.0 mm	outer radius
$fimp$	1.0	1.5	improvement factor
$J_{20T\perp}$	400 A/mm ²	600 A/mm ²	tape J_e at 20 T \perp
A_{bare}	9.6 mm ²	9.6 mm ²	bare cable area
A_{insu}	12.2 mm ²	12.2 mm ²	total cable area
f_{void}	~ 0.10	~ 0.10	void factor
f_{insu}	~ 0.20	~ 0.20	insulation factor



- Size of contact area calculated using the overlap between the **Voronoi Cells** of the nodes
- For Roebel and Stacked in **Cartesian** and for CoRC in **Cylindrical** coordinates
- White lines represent contact elements
- Contact resistances used
 - $0.29 \mu\Omega\text{m}^2$ [1]
 - $100 \text{ watt}/(\text{m}^2 \text{ K})$



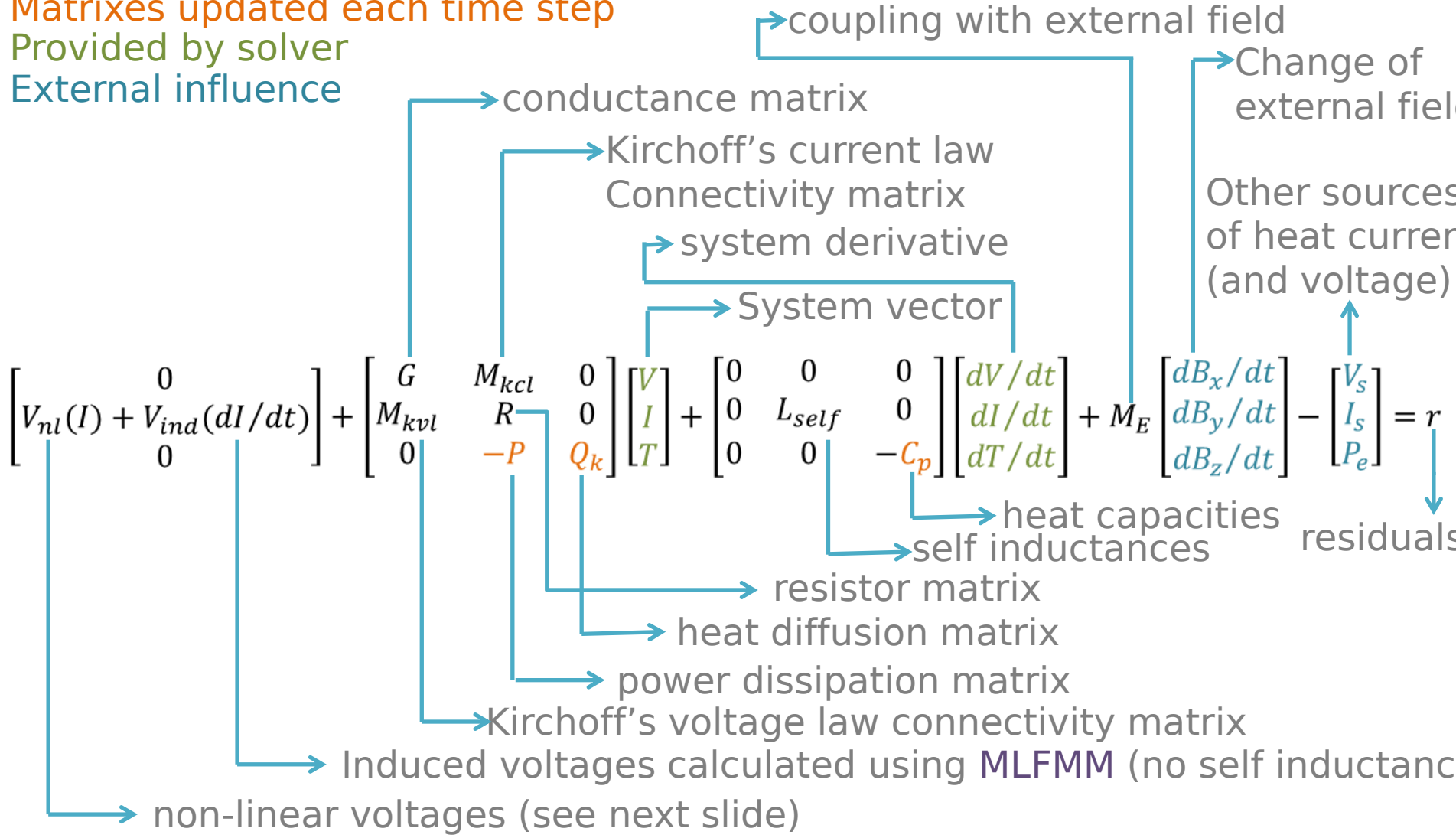
Voronoi Cell



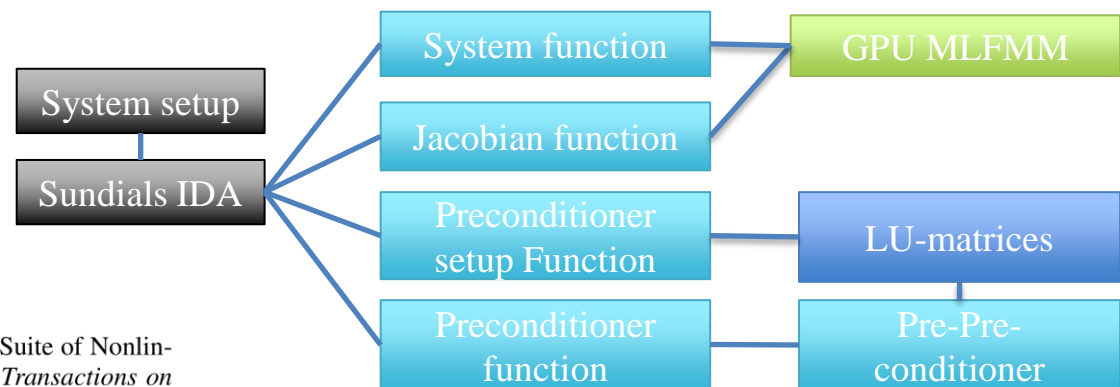
[1] K. Yagotintsev, P. Gao, M. Dhalle *et al.*, "AC loss tests on CORC and stacked tape ReBCO cables," Poster presented at ASC 2014, August 2014, charlotte (SC) USA.



Matrixes updated each time step
 Provided by solver
 External influence



- The system is solved using the **Sundials IDA** solver from LLNL [1]
- **Jacobian Function**
 - Most derivatives are approximated using finite difference
 - The system
- **Preconditioner**
 - Using stabilized bi-conjugent gradient method (**BICGSTAB**) or generalised minimal residual method (**GMRES**) preconditioned by LU-matrices
 - The LU-decomposition of the system matrix is performed only when requested by IDA
 - Only for the LU the mutual inductances from the MLFMM can not included in the system



[1] A. Hindmarsh, P. Brown, K. Grant *et al.*, "SUNDIALS: Suite of Nonlinear and Differential/Algebraic Equation Solvers," *ACM Transactions on Mathematical Software*, vol. 31, no. 3, pp. 363–396, September 2005.

Non-Linear Current Sharing Model

- Current sharing refers to the current distribution between the matrix material and the superconductor provides $VnI(I)$
- In the model three options are available:
 1. Pure power law (not useable for quench analysis because only valid below or just above T_{cs})
 2. Linear transition between T_{cs} and T_c

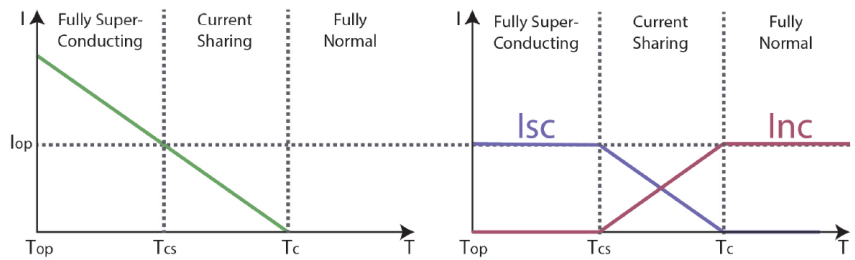
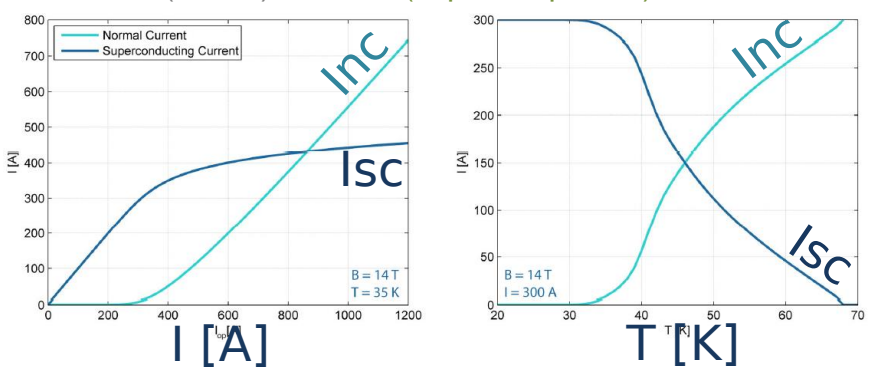
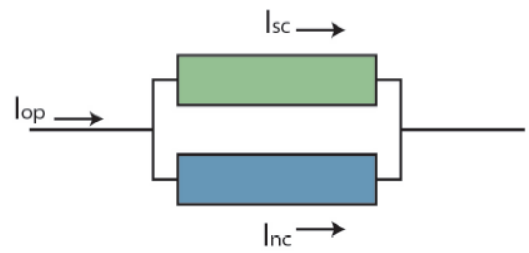


Figure 4.1: Schematic representation of current sharing in a practical superconductor (adapted from Bellis [35]).

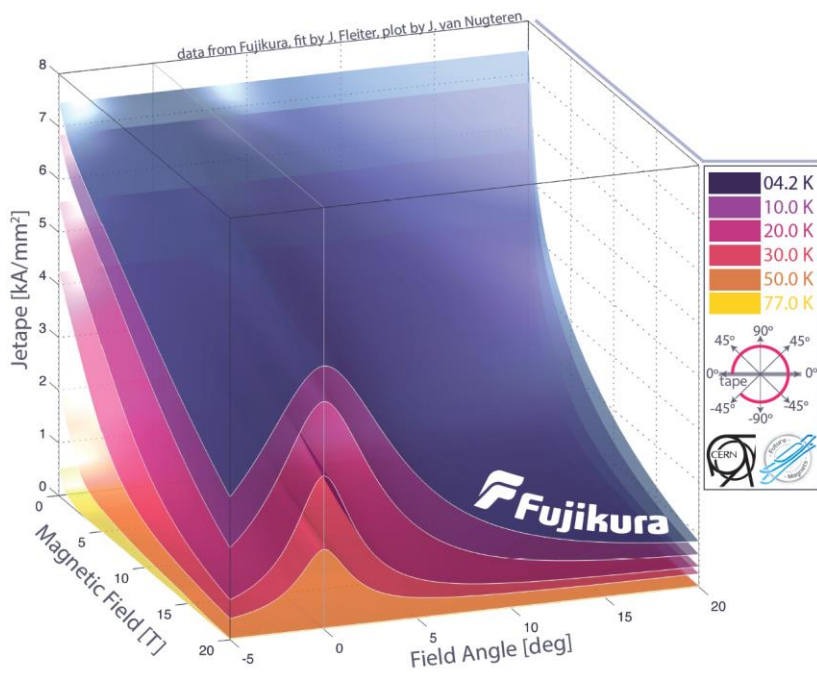
3. Superconducting power law element in parallel with resistive (matrix) element (implicit equation)



Current Sharing

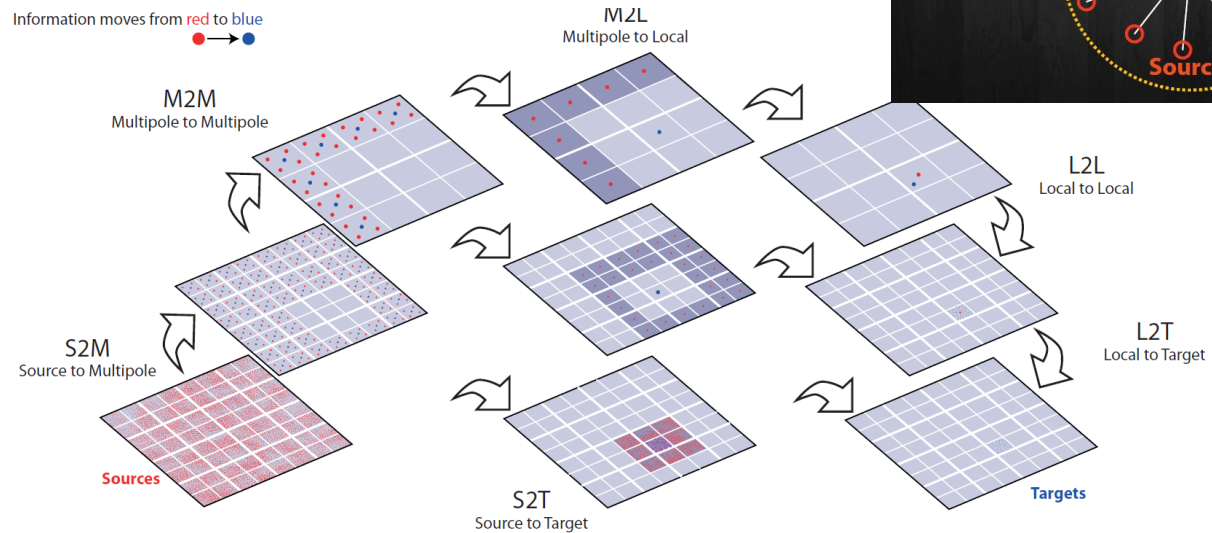
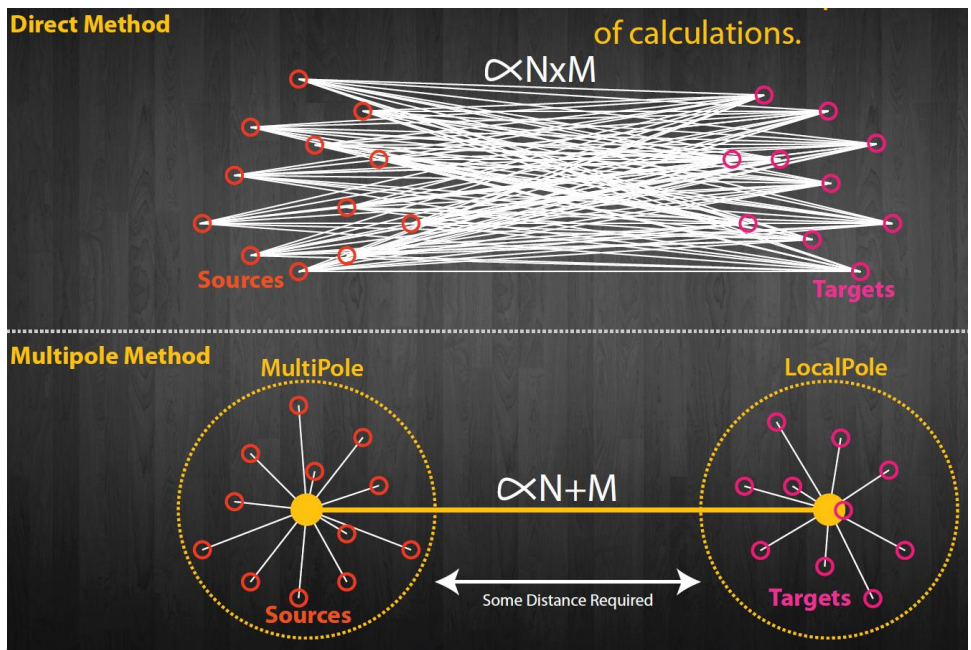


Angular Dependent Critical Current



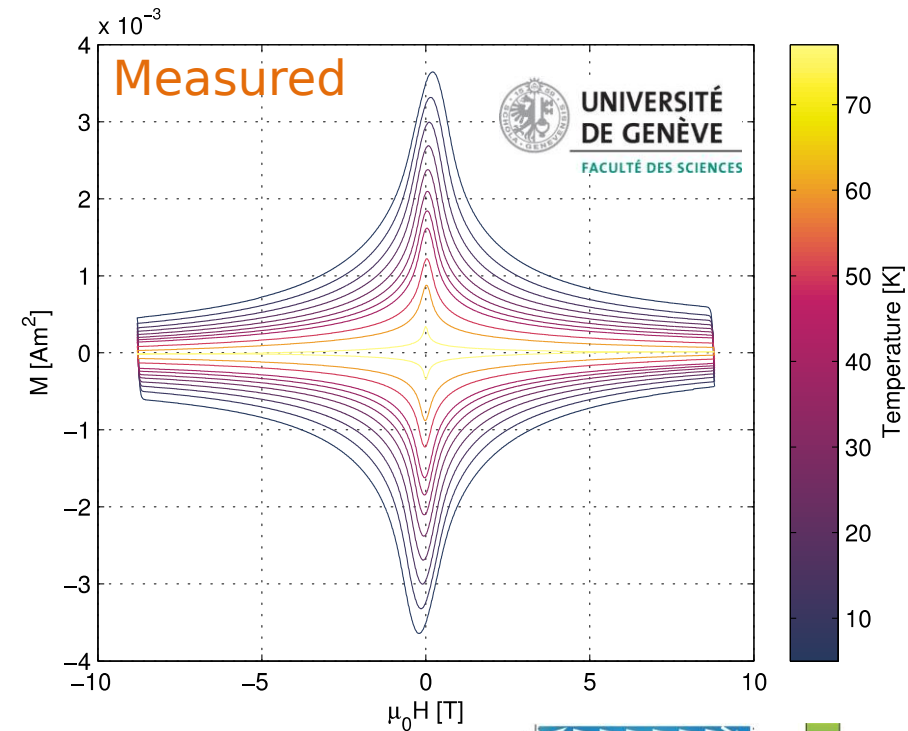
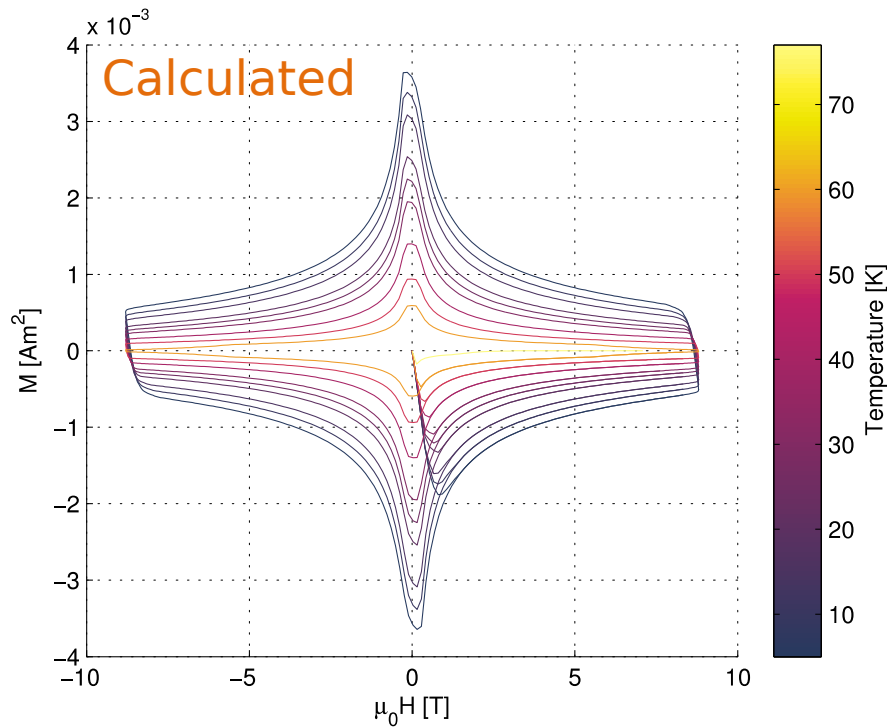
Multi-Level Fast Multipole Method

- Multi-Level Fast Multipole Method (MLFMM) developed by Greengard and Leslie (one of the top 10 algorithms of the previous century)
- Instead of using a dense matrix the induced voltages can be calculated at each element every time step using MLFMM
- Uses spherical harmonics (multipoles) as a "middle man" to reduce the computational complexity from $O(N \times M)$ to $O(N+M)$
- An octtree-grid ensures that all the interactions are included
- Implemented using highly parallelized code using NVIDIA CUDA GPU programming language

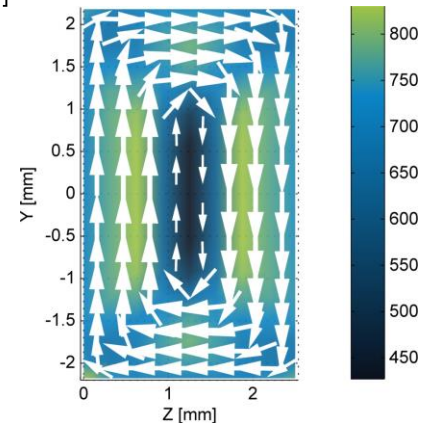


L. Greengard, "The rapid evaluation of potential fields in particle systems," tech. rep., Cambridge, 1988.
 J. Kurzak and B. M. Pettitt, "Fast multipole methods for particle dynamics," Molecular Simulation, vol. 32, no. 10-11, pp. 775-790, 2006.

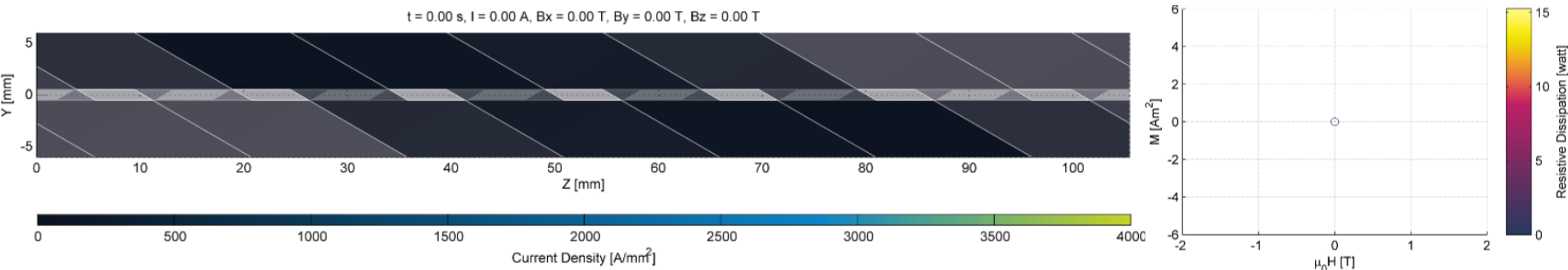




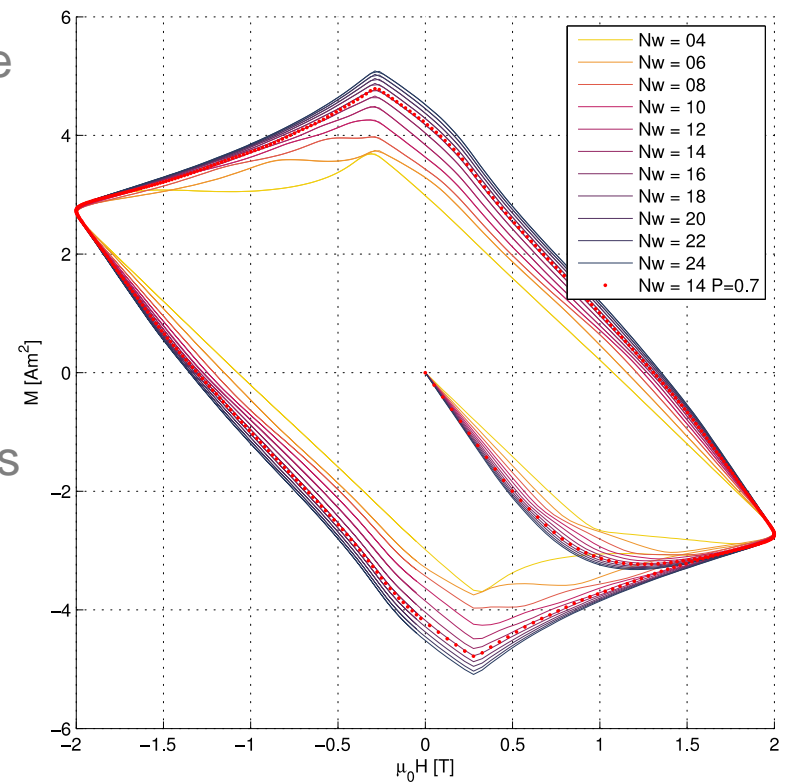
- Comparison University of Geneva Data taken with VSM
- sample size **4.4 mm x 5.1 mm x 0.16 mm** but edges near cut suspected to be damaged during sample preparation
- For the calculation critical current scaled to **50 A/mm** in **4.2K**, **19 T** perpendicular field
- Considering scaling relation used. Reasonable agreement is found between measurement and experiment.



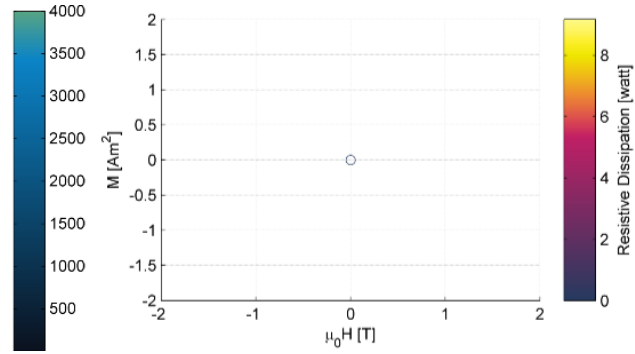
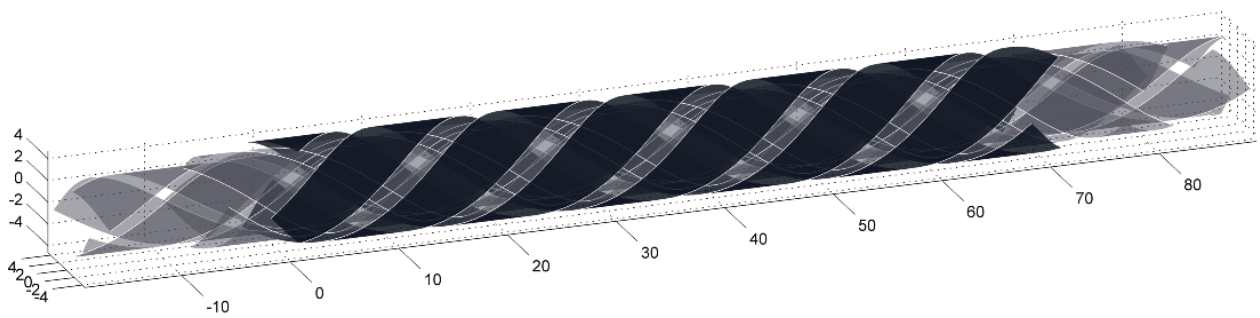
Special thanks to Carmine Senatore and the university of Geneva for sharing their measurement data!



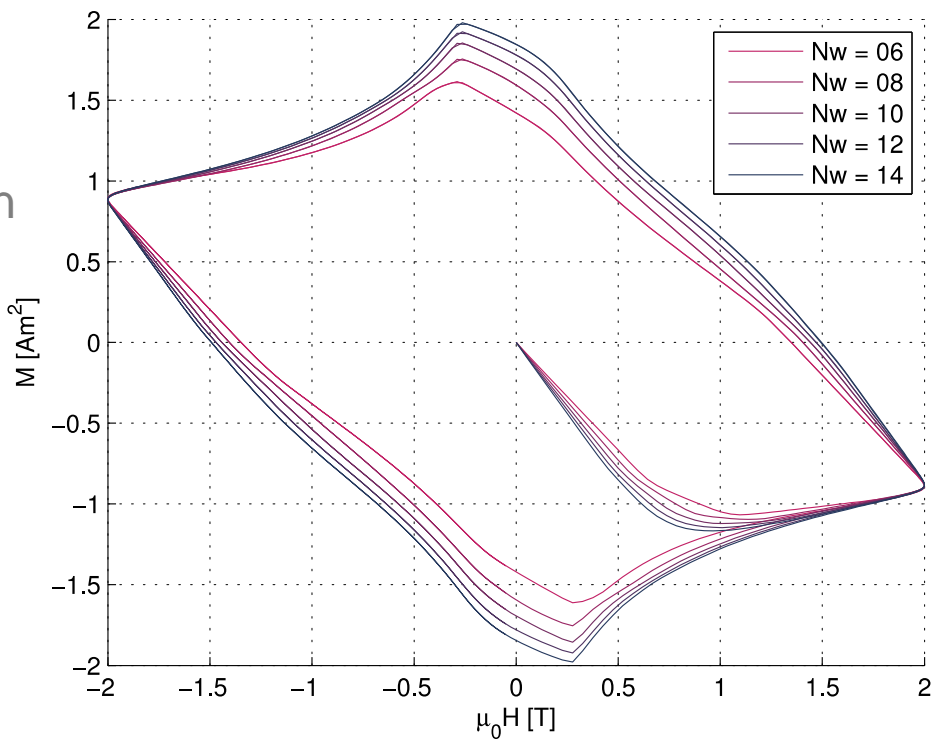
- The calculated magnetisation of a Roebel cable in -2 to 2 T sinusoidal applied field in the perpendicular direction
- Only hysteresis, almost no coupling currents observed
- Hysteresis curve as function of number of elements along width of tapes
- Studied the influence of the number of elements across the width of the tape (decided to use 14 or more)
- Measurement of hysteresis and AC-losses is on-going at the University of Twente



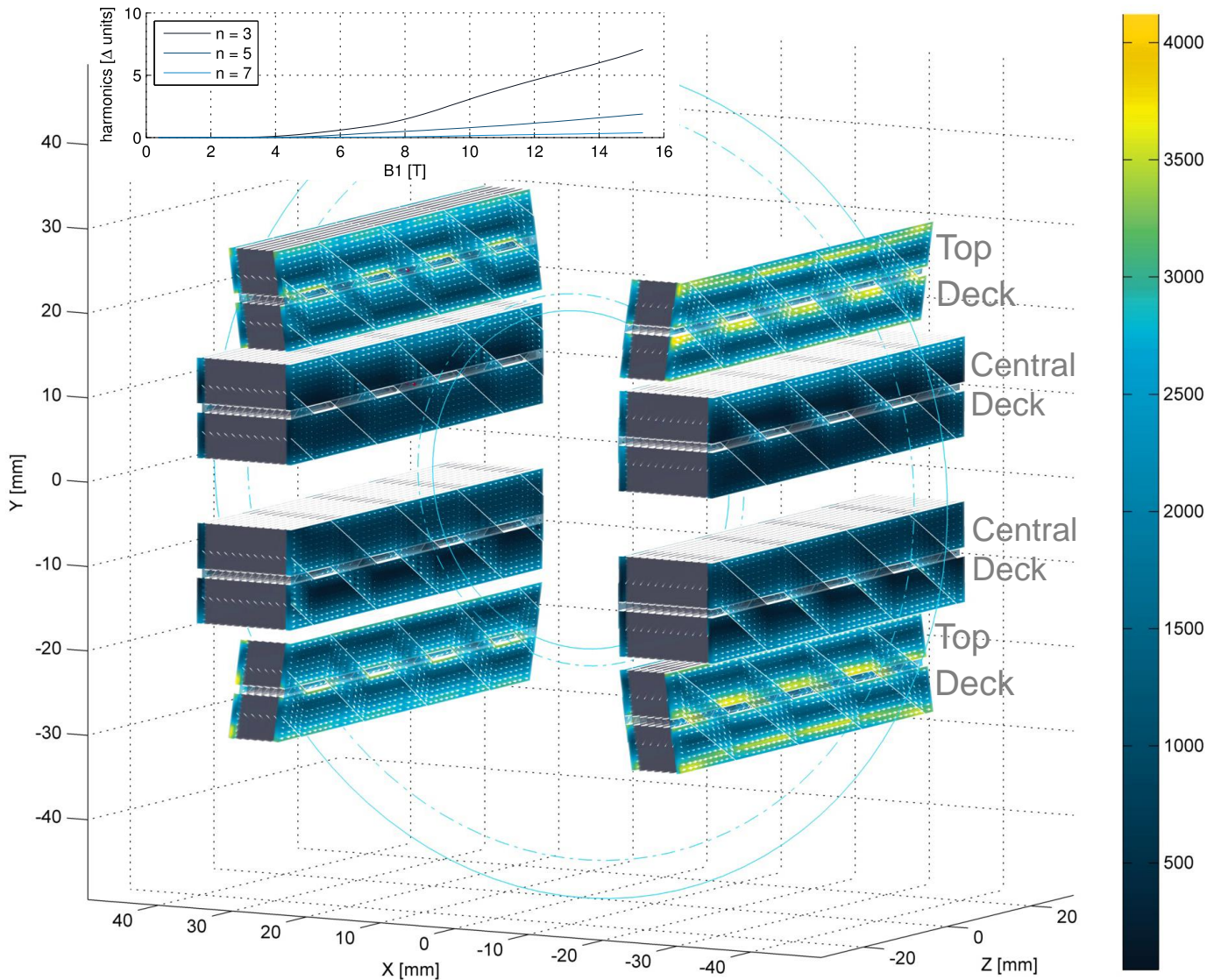
t = 0.00 s, I = 0.00 A, Bx = 0.00 T, By = 0.00 T, Bz = 0.00 T



- The calculated shielding currents of a CoRC cable in **-2 to 2 T** sinusoidal applied field in the perpendicular direction
- Almost only hysteresis observed
- CoRC strands are twisted therefore less magnetisation than Roebel in perpendicular field direction
- Similar behaviour with number of elements observed as for Roebel

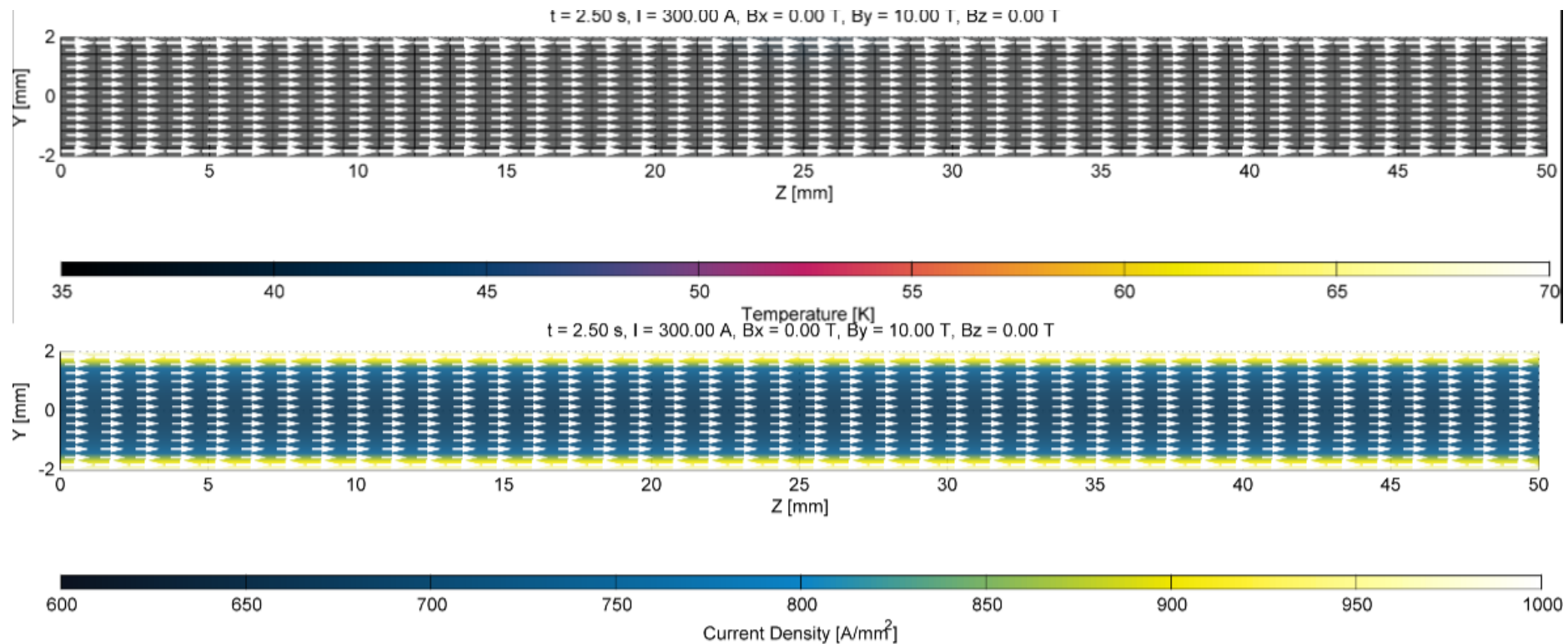


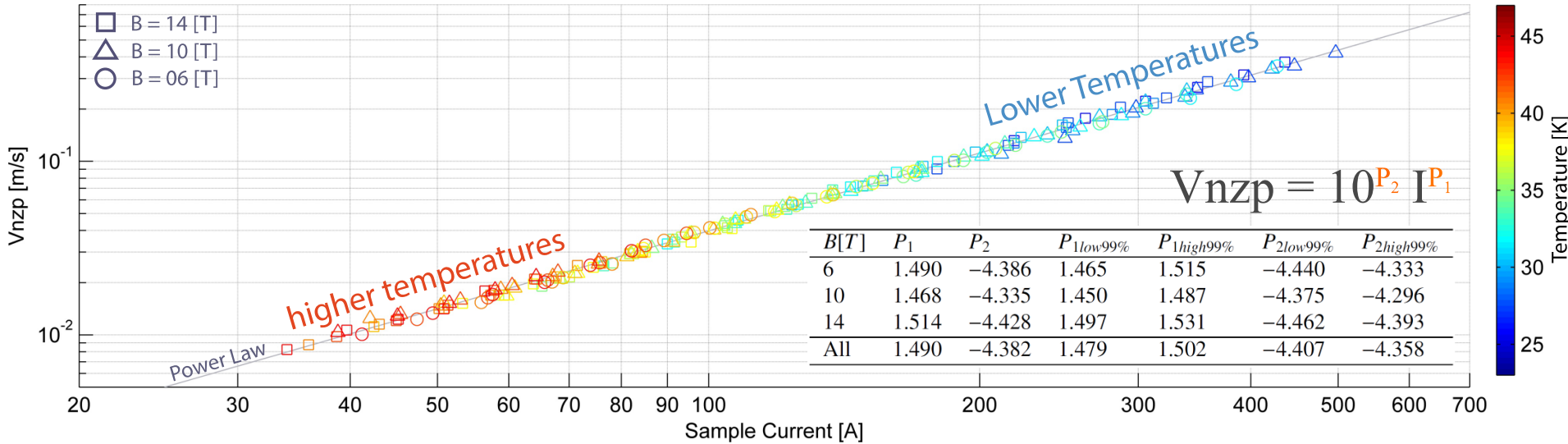
$t = 1200.00$ s, $I = 7993.33$ A, $B_x = 0.00$ T, $B_y = -12.99$ T, $B_z = 0.00$ T



- Due to limitations of the BemFem no Iron pole (yet)
- Simultaneous ramp of Fresca2 and insert over 20 minutes (1200 s)
- Top deck generates more shielding currents due to field angle
- Harmonics at $2/3$ aperture less than **10 units**
- Keeping alignment during ramping could reduce the field error by a great deal

- Comparison University of Twente normal zone propagation measurement data (master assignment JvN).
- As an example a quench at 35 K, 10 T parallel, 300 A in a 4 mm wide tape
- Quench was purposely initiated at edge of tape to show redistribution of current
- Propagation is, due to the redistribution of the current, much faster in width direction than longitudinal direction!

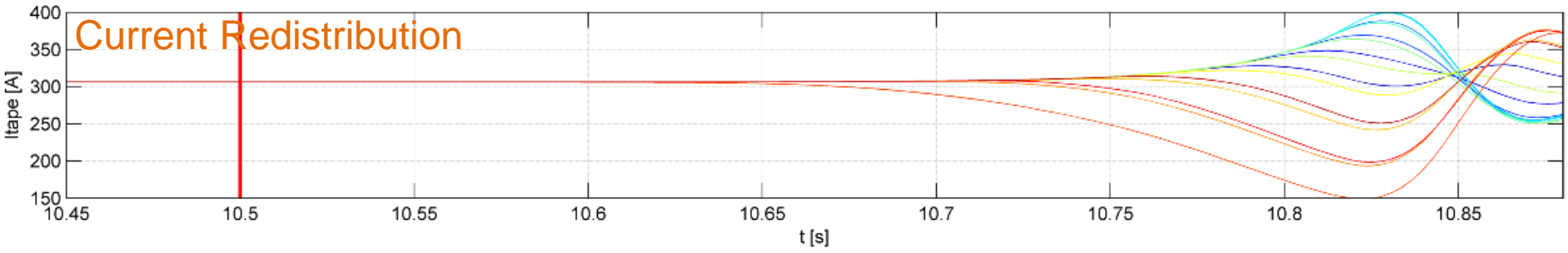
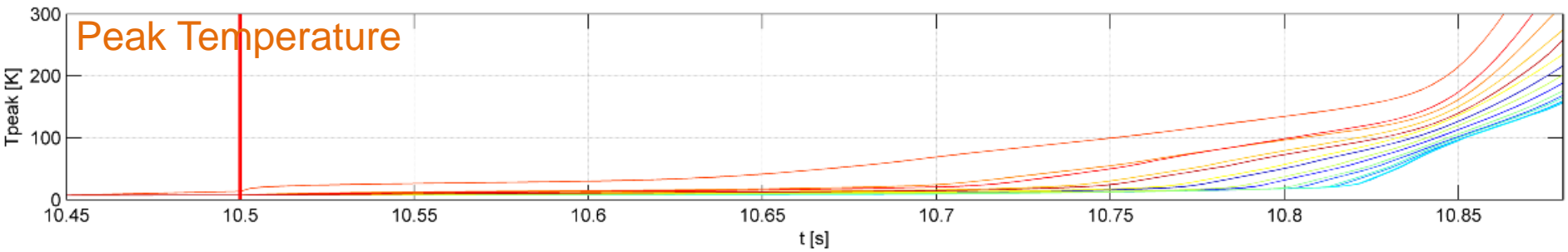
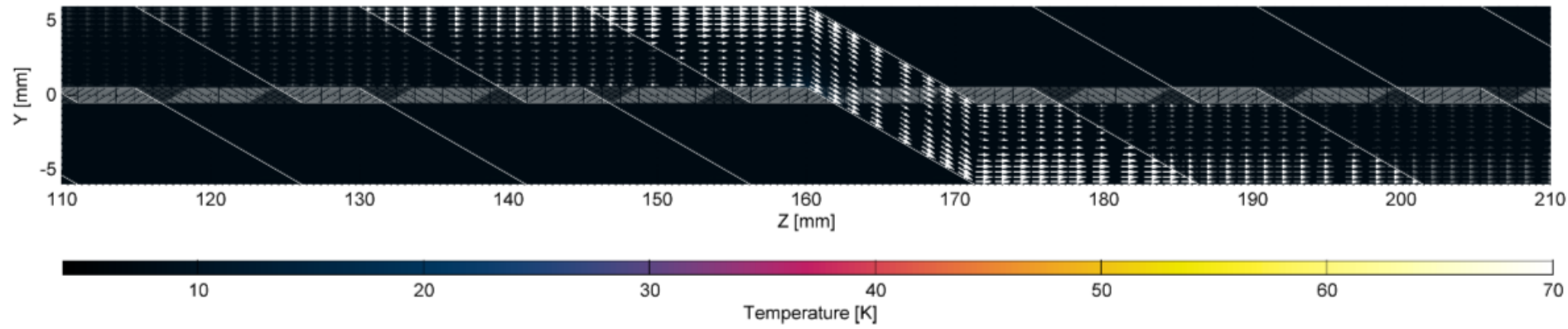




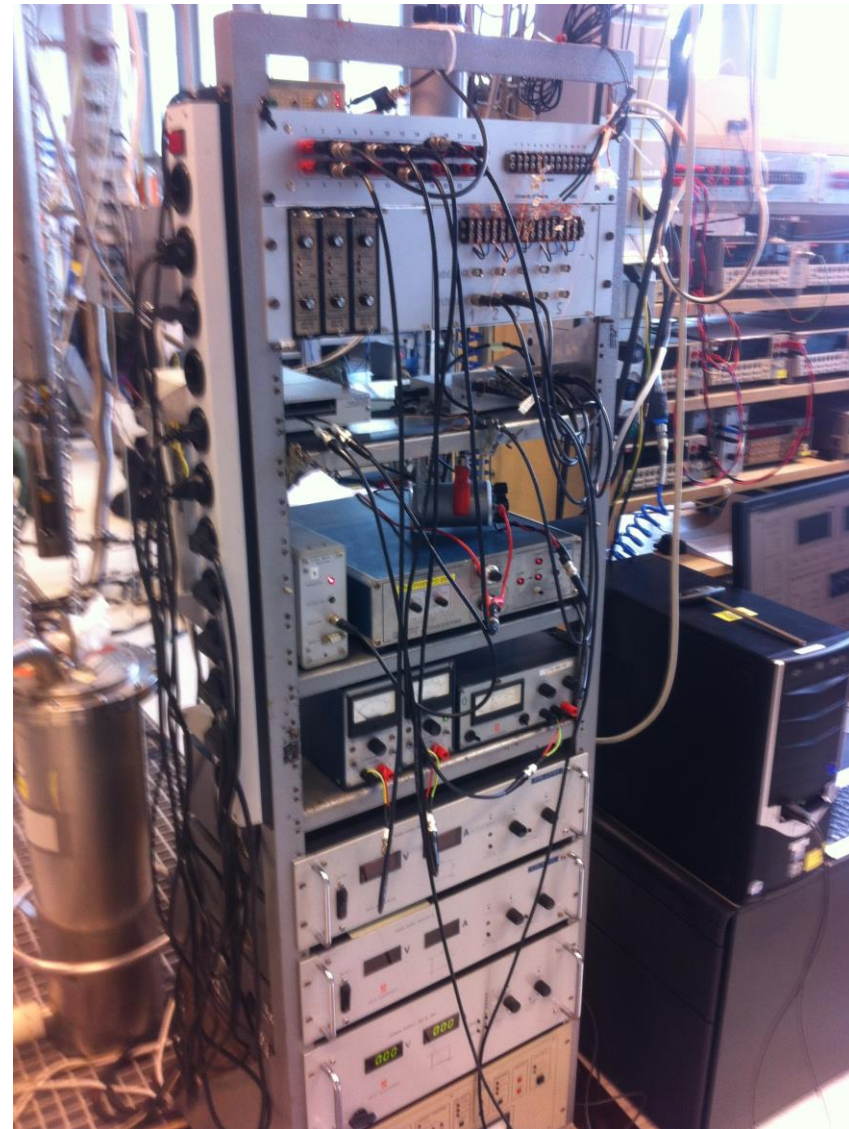
Normal Zone Propagation inside Roebel cable

- 0.4 watt heating on point after 10.5 s

$t = 10.50 \text{ s}$, $I = 4593.80 \text{ A}$, $B_x = 10.00 \text{ T}$, $B_y = 0.00 \text{ T}$, $B_z = 0.00 \text{ T}$



- Additional validation of the model
 - Magnetisation and AC-losses of different cable structures, pressures and orientations
 - Quench propagation and corresponding current redistribution of different cable structures
- Electrical contact resistances
- Thermal contact resistances



- An electrical network model representing the tapes in ReBCO cables has been introduced
- In the model the following physics are available
 - Electrical voltages and currents
 - Heat generation and conduction
- Initial validation seems promising but waiting for more measurement data (from the University of Twente)
- Some examples were calculated for this conference but real data mining is yet to start (need validation first)
- Intend to get
 - Further analysis of the magnetisation currents and their effect on the coil harmonics.
 - Possible ramp scenarios for Feather-M2 magnet
 - Quench analysis and comparison between the different cable types

