

## **Permanent (and Soft) Magnetic Materials for Accelerators**

Workshop on Special Compact and Low Consumption Magnet  
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## Outline

- **Homogeneous magnets for undulators**
- **Cryogenic applications: PrFeB**
- **Improvements of actual NdFeB alloys**
  - **by alloy composition**
  - **by grain boundary diffusion**
- **New soft magnetic alloys**

## Magnets for scientific applications on industrial scale

- Undulator applications need extreme homogeneities
- actual FEL-projects request material quantities on industrial scale
- Vacuumschmelze delivers:
  - Soft magnetic components
  - Precise permanent magnets
  - Assemblies

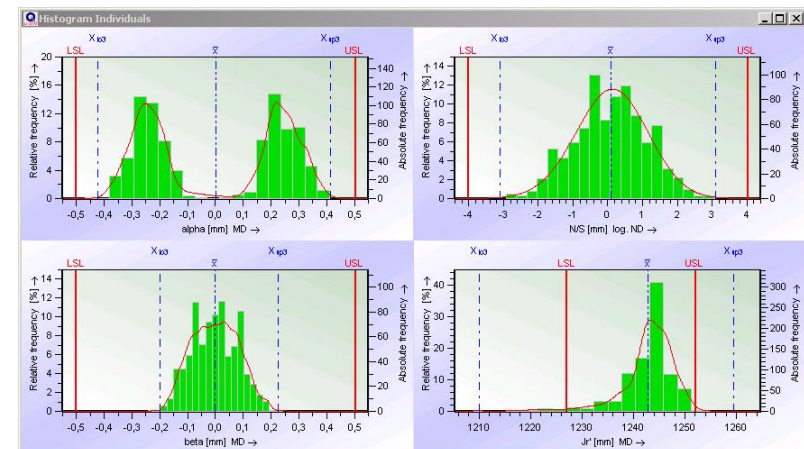


## Permanent magnet structures for E-XFEL U40 and U68

- 70 undulators U40, 21 undulators U68, each 5m long in 10 substructures of 1 m length
- Total of more than 35000 permanent magnets and VACOFLUX® pole-pieces

### Homogeneity of the permanent magnets:

- Variation of magnetic moment:  $\leq \pm 1\%$  for the whole order (more than 10 tons of PM-material)
- Angular deviation Alpha, Beta:  $\leq \pm 0.5^\circ$
- h/c-effect:  $\leq \pm 2\%$



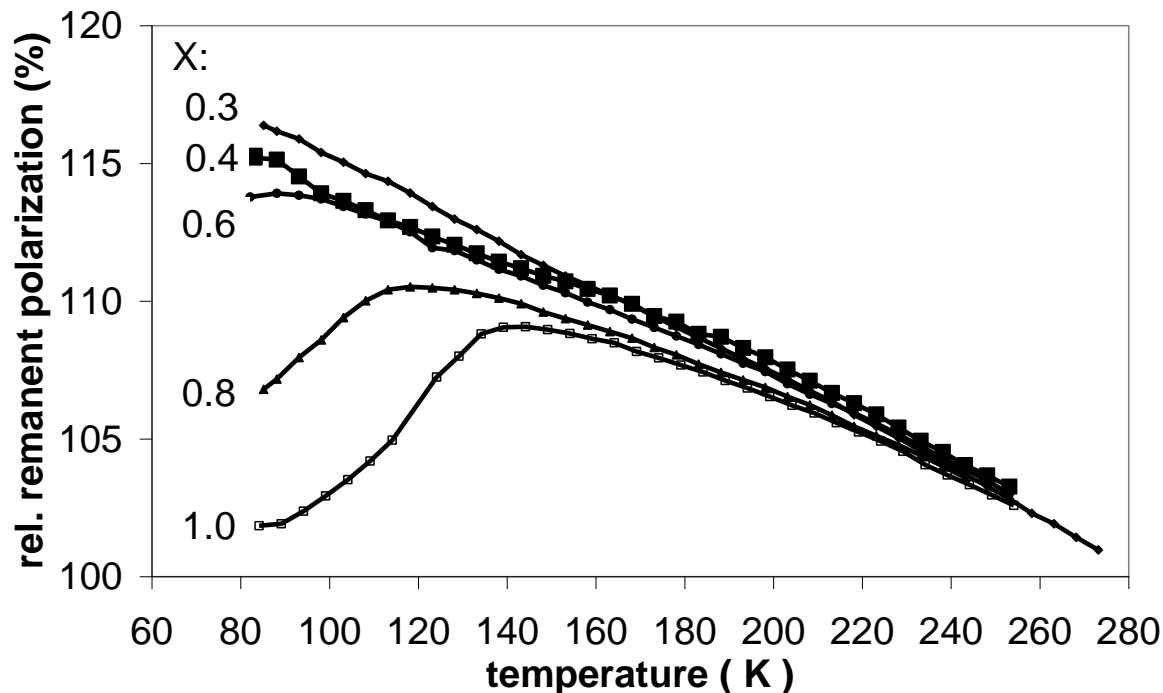
## Material properties for cryogenic applications

With decreasing application temperature:

- Large increase of coercivity of REFeB-material → enhanced stability
- Remanence of REFeB-material increases → more flux for the application
- But: We need to overcome the spin-flip-transition of NdFeB at 140 K

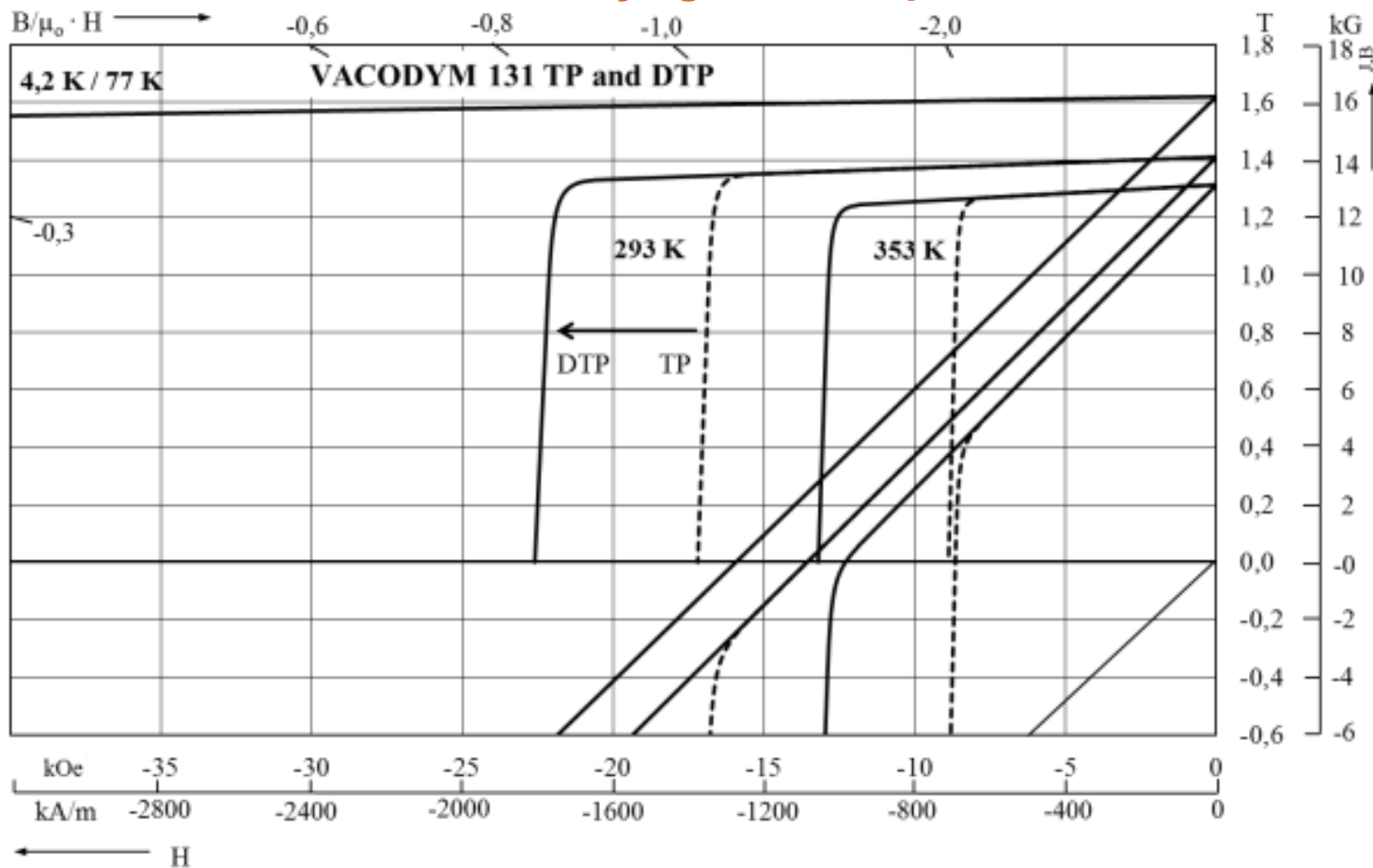
→ Solution: use PrFeB-material !

## Permanent Magnets for Undulators at Cryogenic temperatures



Open circuit remanent polarization of  $(\text{Nd}_x\text{Pr}_{1-x})_2\text{Fe}_{14}\text{B}$  relative to the remanent polarization at 283 K, as a function of temperature, measured parallel to the alignment direction on samples of  $B/\mu_0H = -1.78(\pm 0.04)$  for various  $x$  values. [2]

## VACODYM<sup>®</sup> 131 for use at Cryogenic temperatures



Demagnetization curves of VACODYM<sup>®</sup> 131 TP and DTP at cryogenic temperatures, room temperature and elevated temperature

## Improvements of actual NdFeB-based alloys

- Radiation damage of permanent magnets correlates to temperature stability over large ranges of potential radiation doses
- Stability at elevated temperatures depends on
  - Load line (depends on geometry and external fields)
  - Coercivity of the material
- Coercivity is increased by heavy rare-earth (HRE-) content

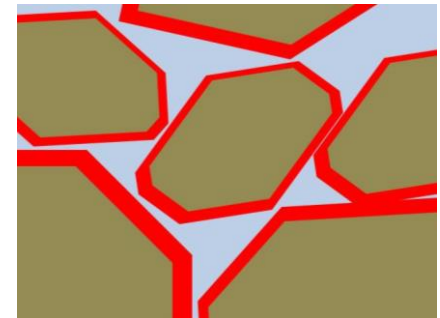
### Possible solutions:

- Place the HRE at the location, where it works most effectively
- Use of more effective HRE-elements



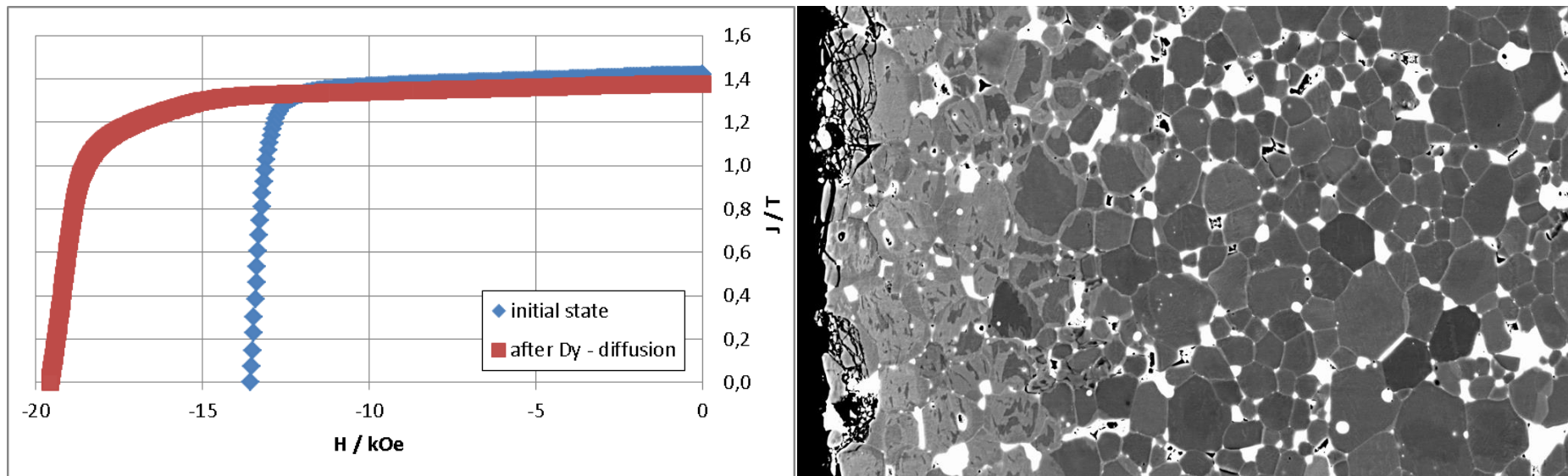
## Optimised coercivity by Dy-diffusion-process

- Additions of Dy to pure NdFeB are used to increase coercivity
- They slightly reduce remanence
- The use of Dy is optimised by placing it to the grain boundaries in a diffusion process instead of additions to the base alloy
- For a given coercivity and remanence the amount of Dy needed is minimised
- The effectiveness is restricted to limited dimensions (thickness of the magnet)



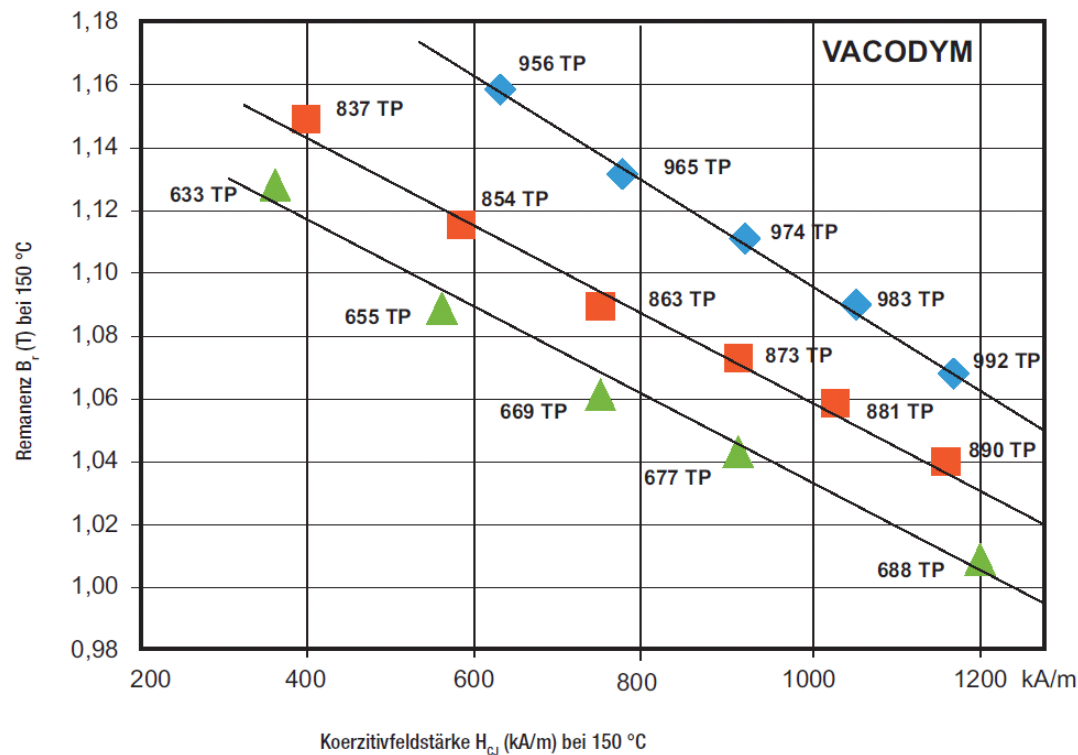
## Optimised coercivity by Dy-diffusion-process

- $\Delta H_cJ$  as high as by diffusion treatment after sputter coating
- Micrograph depicts Dy rich grains near surface which are responsible for the loss of  $B_r$

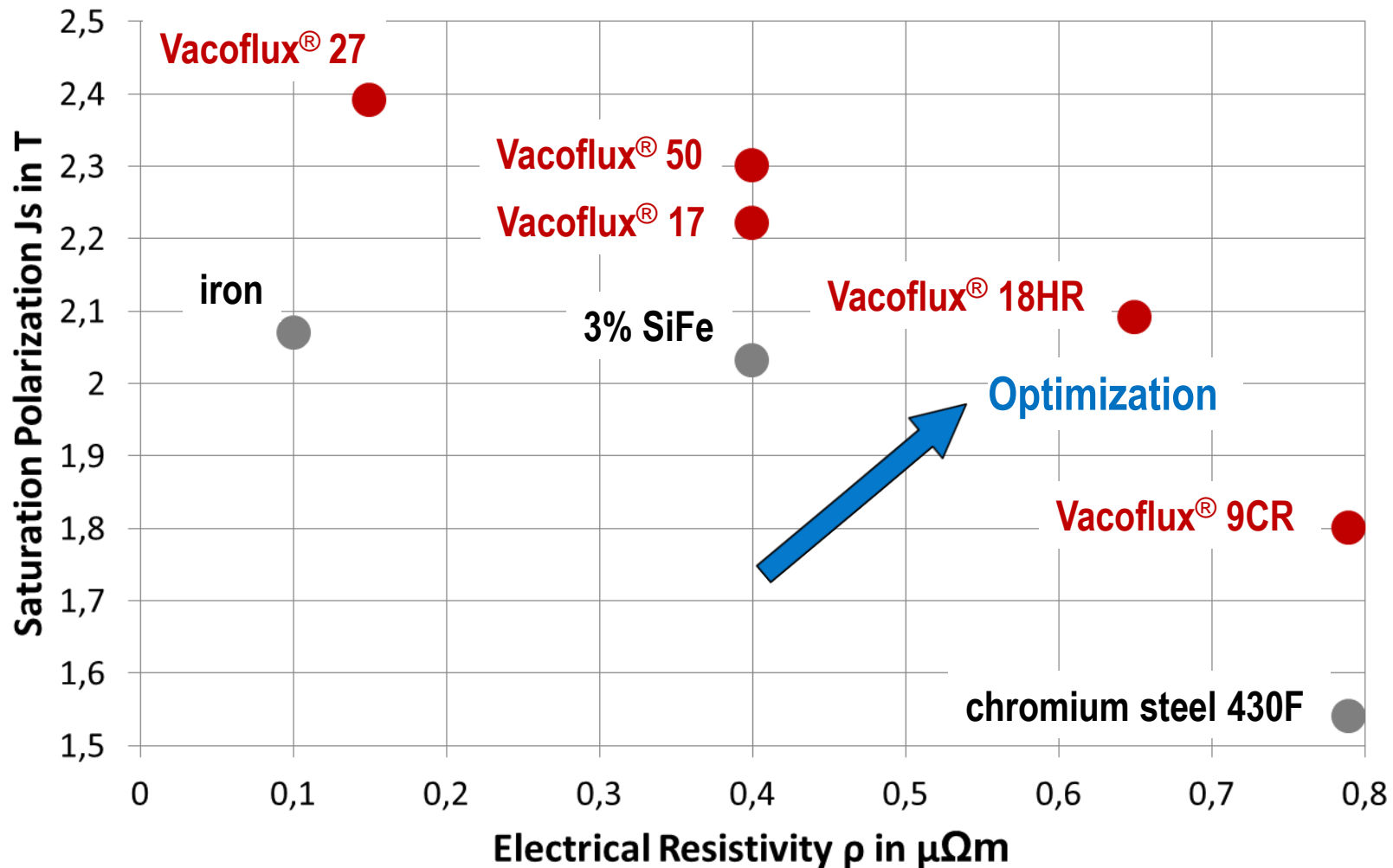


## VACODYM<sup>®</sup> 9xx-series

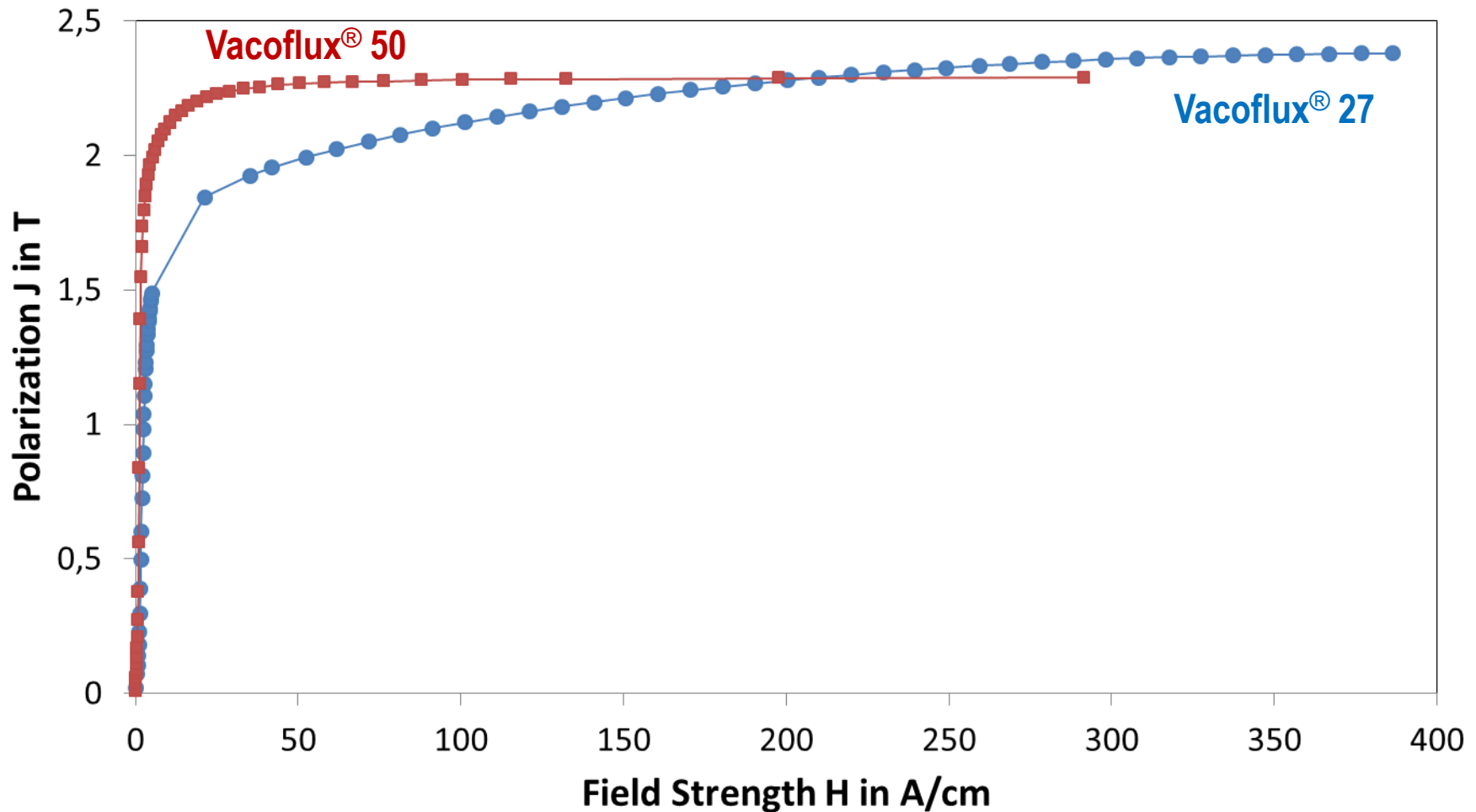
- use Tb instead of Dy as HRE-element (in the base alloy)
- optional: additional enhancements by grain boundary diffusion at the surfaces



## Soft magnetic materials: saturation vs. resistivity

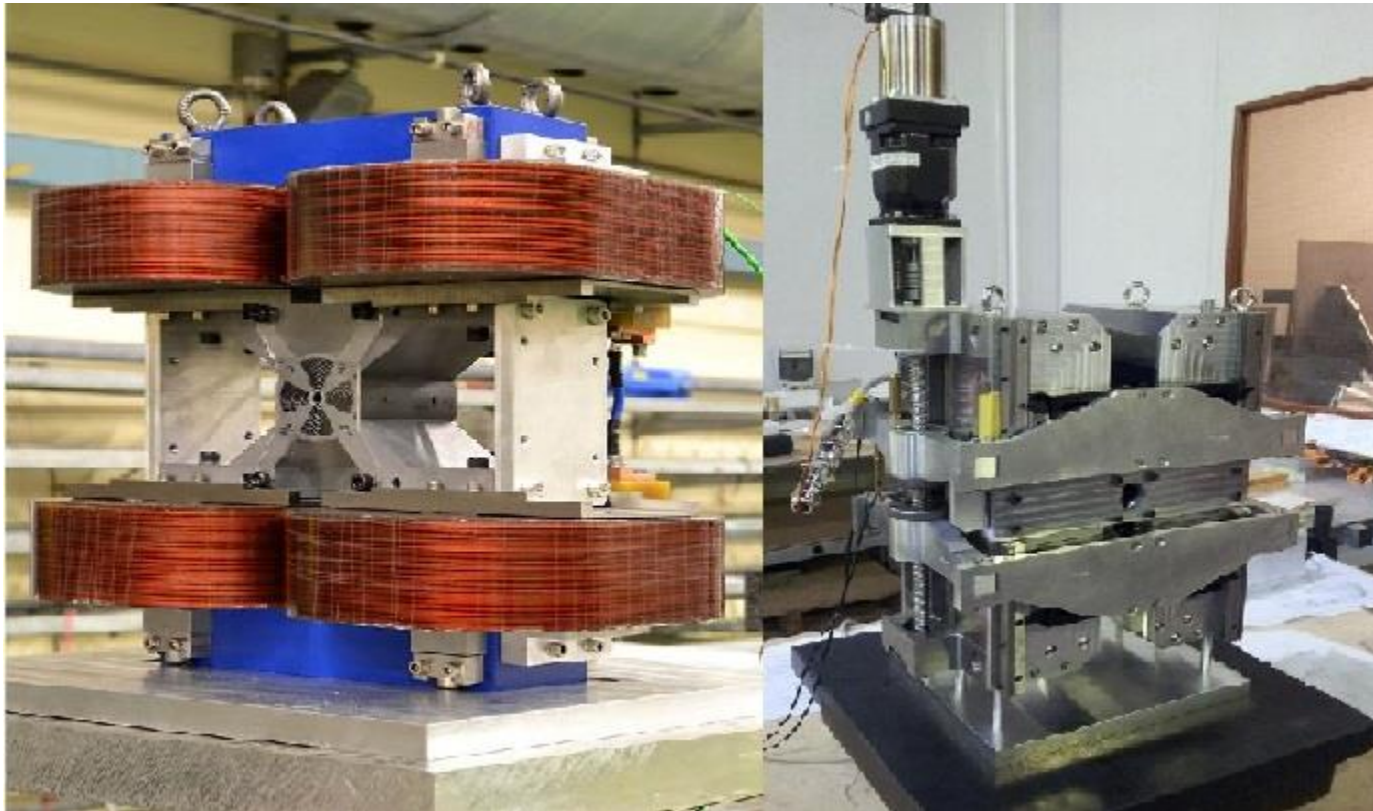


# Comparison of Static Initial Magnetization Curves VACOFLUX<sup>®</sup>50 vs. VACOFLUX<sup>®</sup>27



## Outlook

- Vacuumschmelze material is already implemented in various designs
- We are looking forward to your discussions on further optimisation



**Thanks for your attention!**