

# ***FTIR spectroscopy at grazing incidence for surface chemical analysis***

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Internship in the Chemistry Laboratory of TE-VSC-SCC



- Introduction
- FTIR spectroscopy at grazing incidence
- Experiments on Stainless Steel
  - Baseline Distortions
  - Detection Limit
- Conclusion



- **Introduction**
- FTIR spectroscopy at grazing incidence
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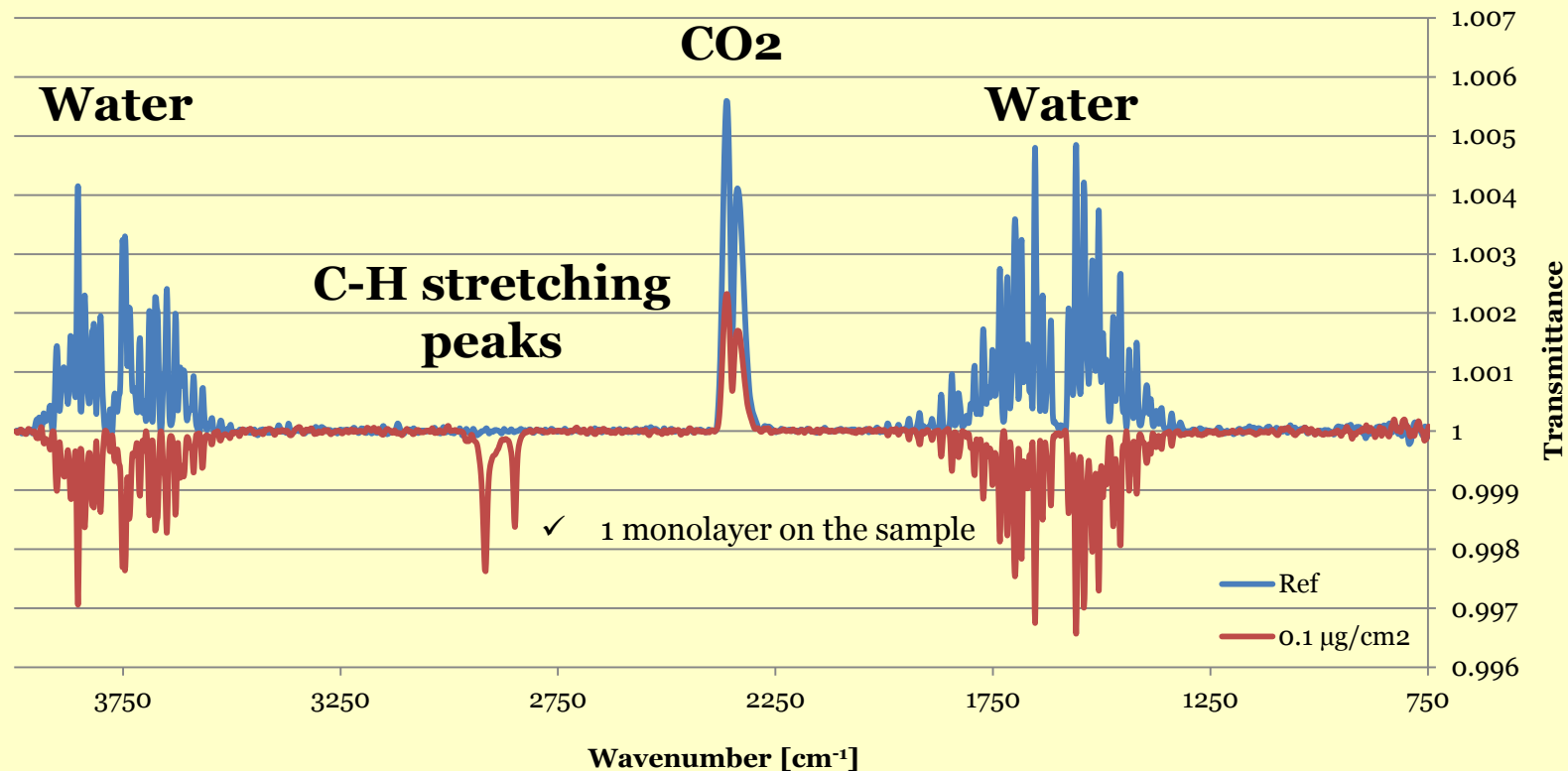


- Current procedure for organic contamination:
  - Extraction with n-Hexane (304 ml/m<sup>2</sup>)
  - Deposition of 2 drops of extraction solution on a ZnS cell
  - The n-Hexane evaporates from the cell
  - The organic contamination remains on the surface of the cell and is analysed with FTIR (in transmission)





- Transmission spectrum for an organic contaminant





- Disadvantages:
  - n-Hexane is toxic

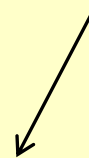


- The sample has to be dismantled and transported to the chemistry laboratory
- Complex geometries can cause problems
- Only the average surface contamination
- Solubility in n-Hexane

- The portable Agilent 4100 ExoScan FTIR

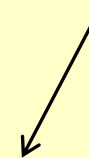


Diamond  
ATR



For the  
identification  
of polymers,  
powders

Diffuse  
Reflectance



For the  
measurement of  
rough surfaces

Grazing  
Angle 82°



For the  
measurement  
of thin films  
( $d < \lambda$ )



- Detection of *Silicones* down to  $0.1 \mu\text{g}/\text{cm}^2$ 
  - Stainless Steel
  - Copper
  - Aluminum



$0.1 \mu\text{g}/\text{cm}^2 = 1 \text{ monolayer}$

- Detection of *Hydrocarbons* down to  $0.1 \mu\text{g}/\text{cm}^2$ 
  - Copper
  - Aluminum



– Stainless Steel → **Problems**

**$1 \mu\text{g}/\text{cm}^2 \text{ not visible!}$   
 $= 10 \text{ monolayers}$**

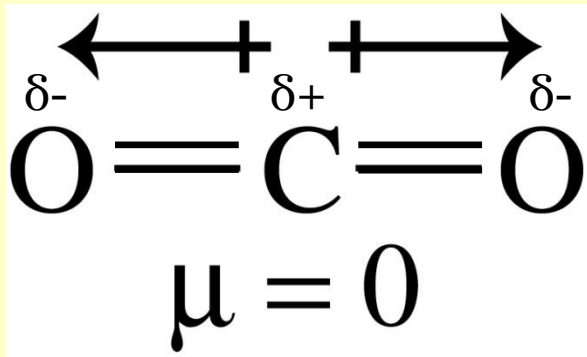




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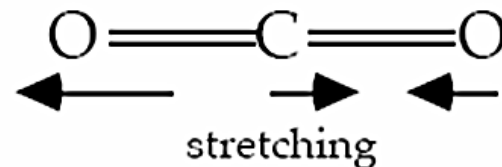
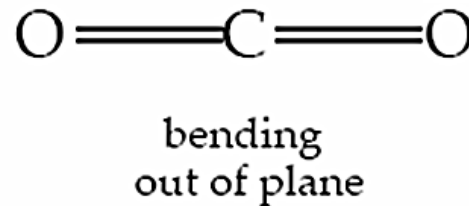
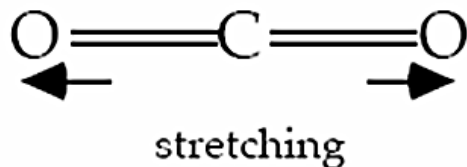
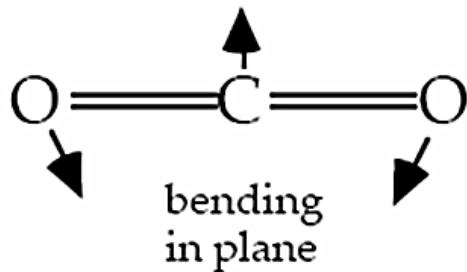
## Vibrational Spectroscopy



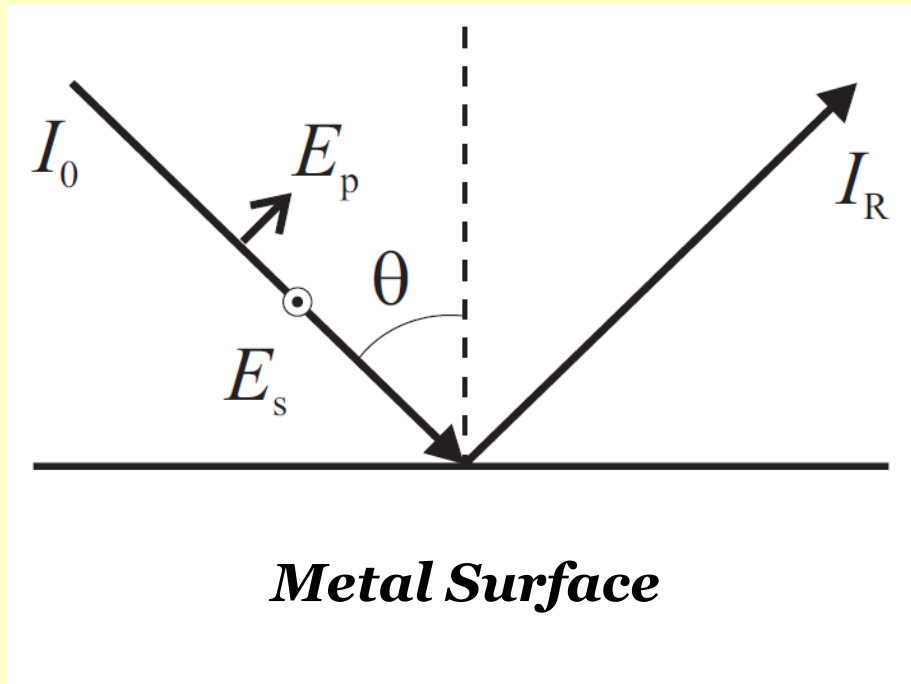
### Requirements for excitation:

- Oscillating dipole moment  $\mu$
- Alignment of the electric field vector of the radiation with the oscillating dipole

For  $\text{CO}_2$ , which is a linear molecule, there are  $3(3) - 5 = 4$  fundamental vibrations:

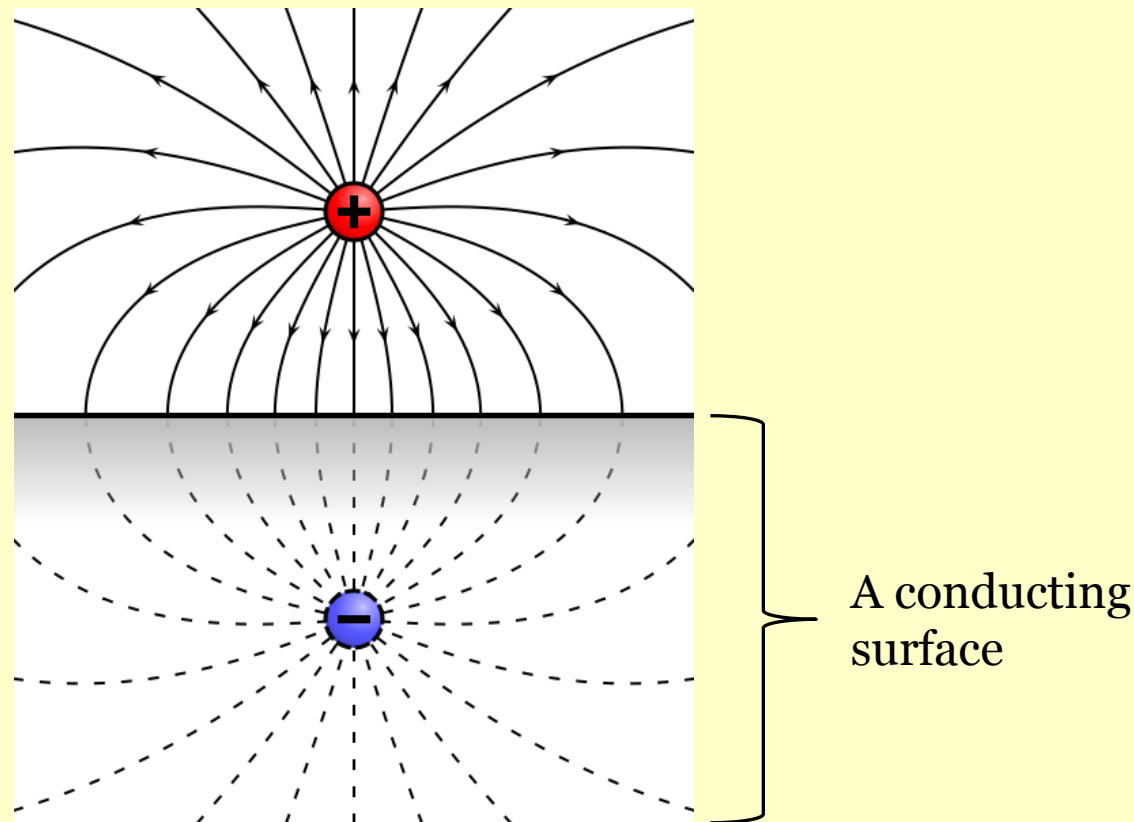


- Polarization of light

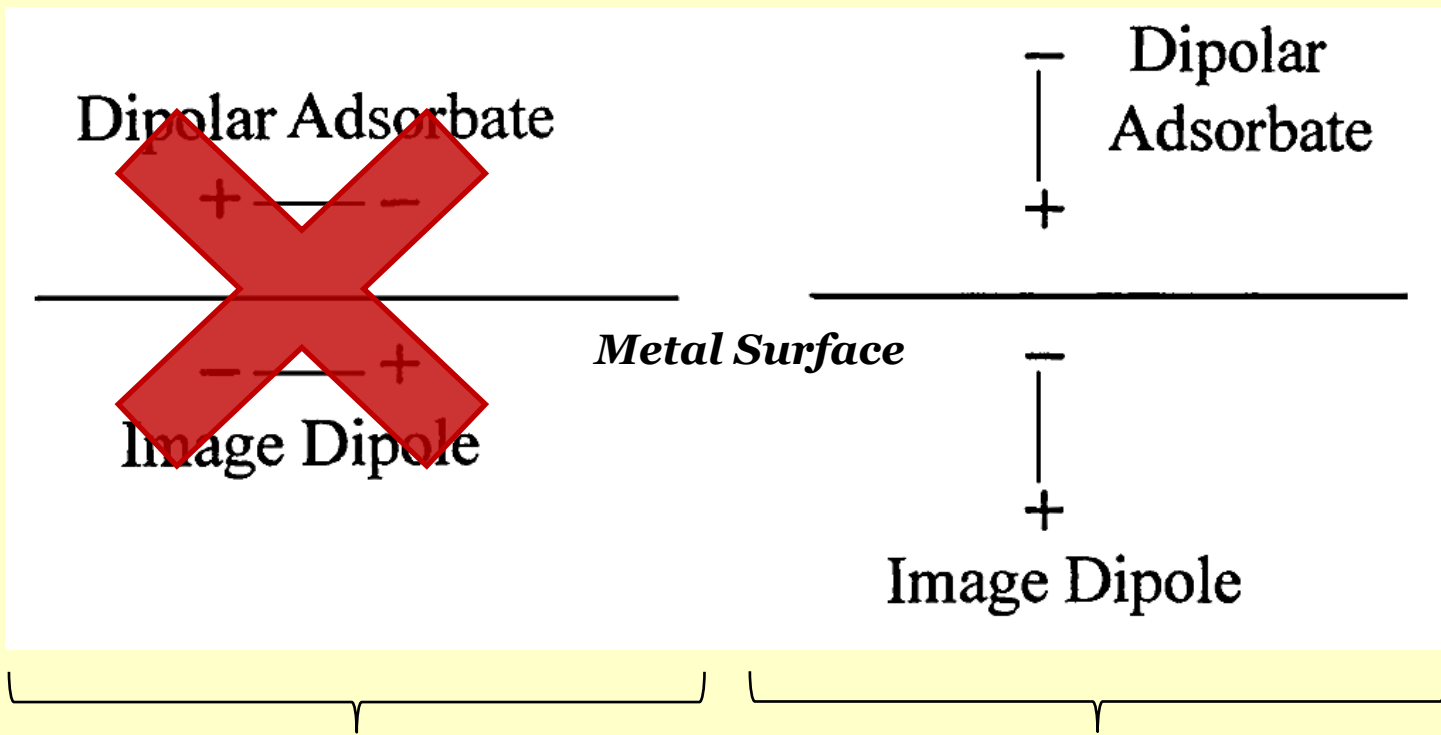


- P-polarized light → **parallel** to the plane of incidence
- S-polarized light → **perpendicular** to the plane of incidence

- Image charge



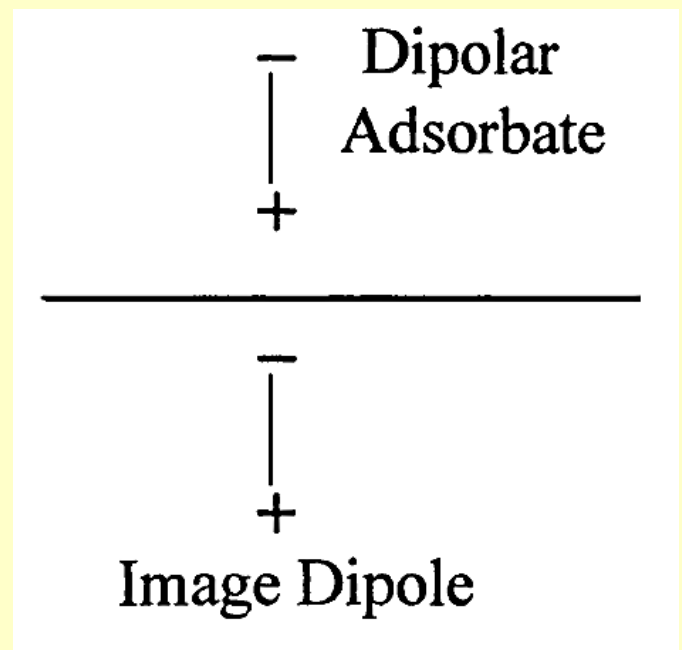
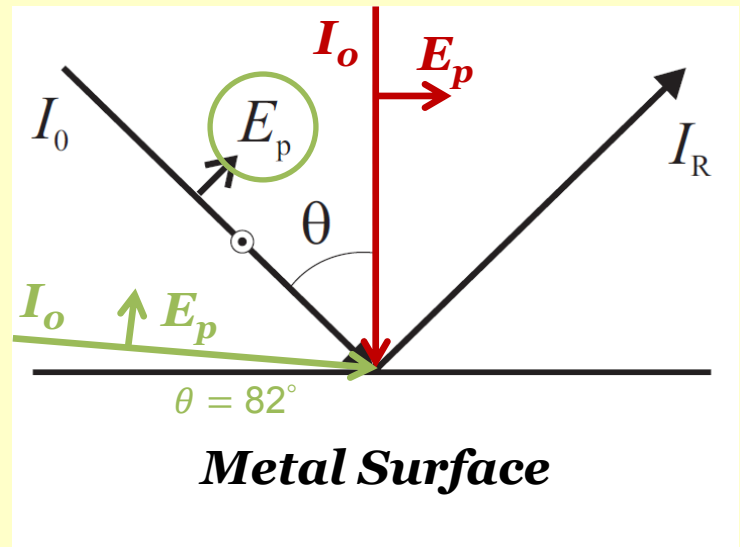
- The effect of the image charge



No net dipole oscillation  
No absorption

The dipole oscillation  
is amplified

- How to excite this vibration?



But... You need an angle  $\theta > 0$

*In conclusion:  
Good absorbance only for a large angle of incidence  $\theta$*



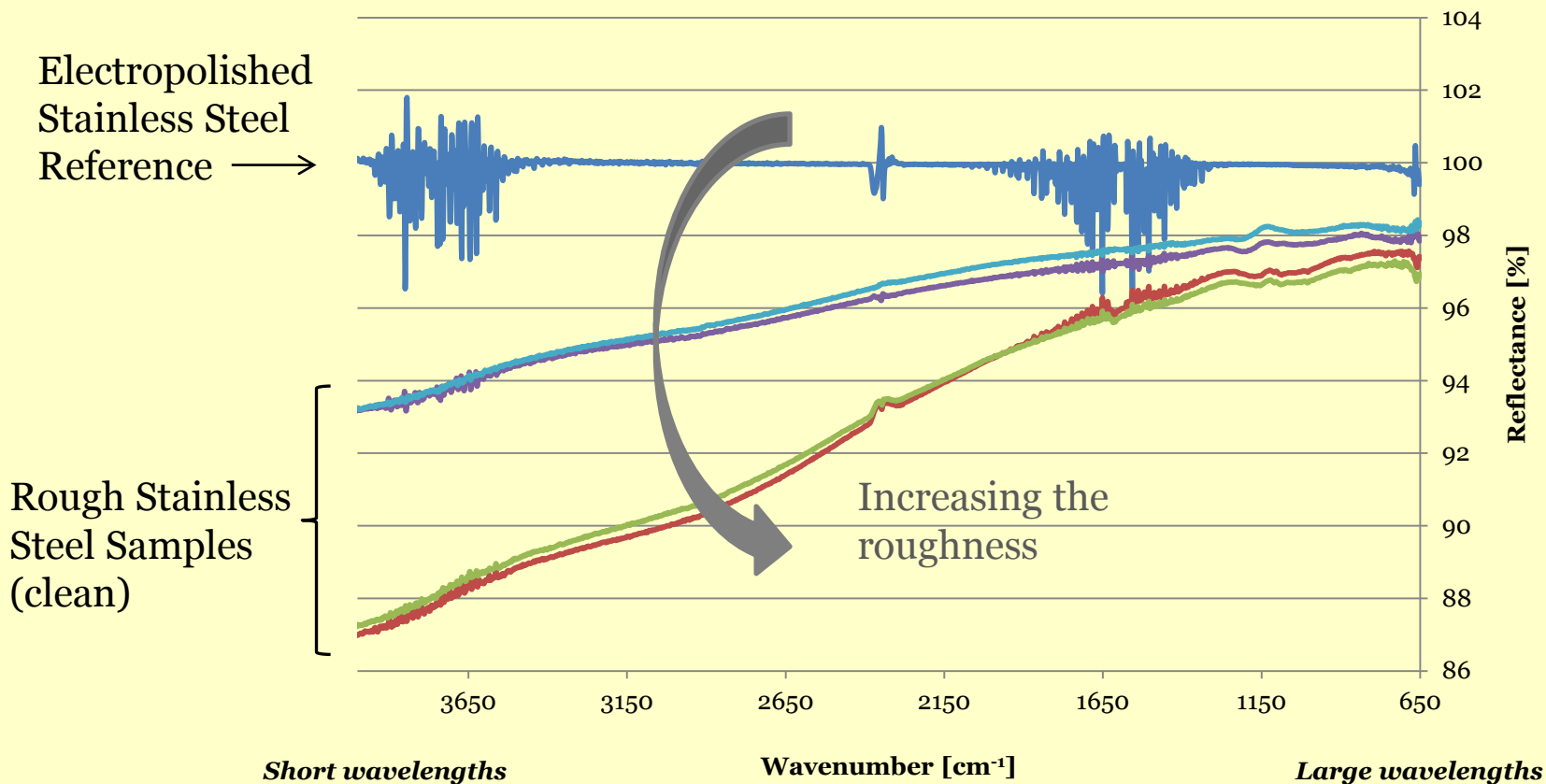
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- **Experiments on Stainless Steel**
  - Baseline Distortions
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- Roughness Induced Baseline Distortions
- Film Induced Baseline Distortions





- Roughness Induced Baseline Distortions



*Light only 'sees' objects larger or approximately equal to its wavelength*

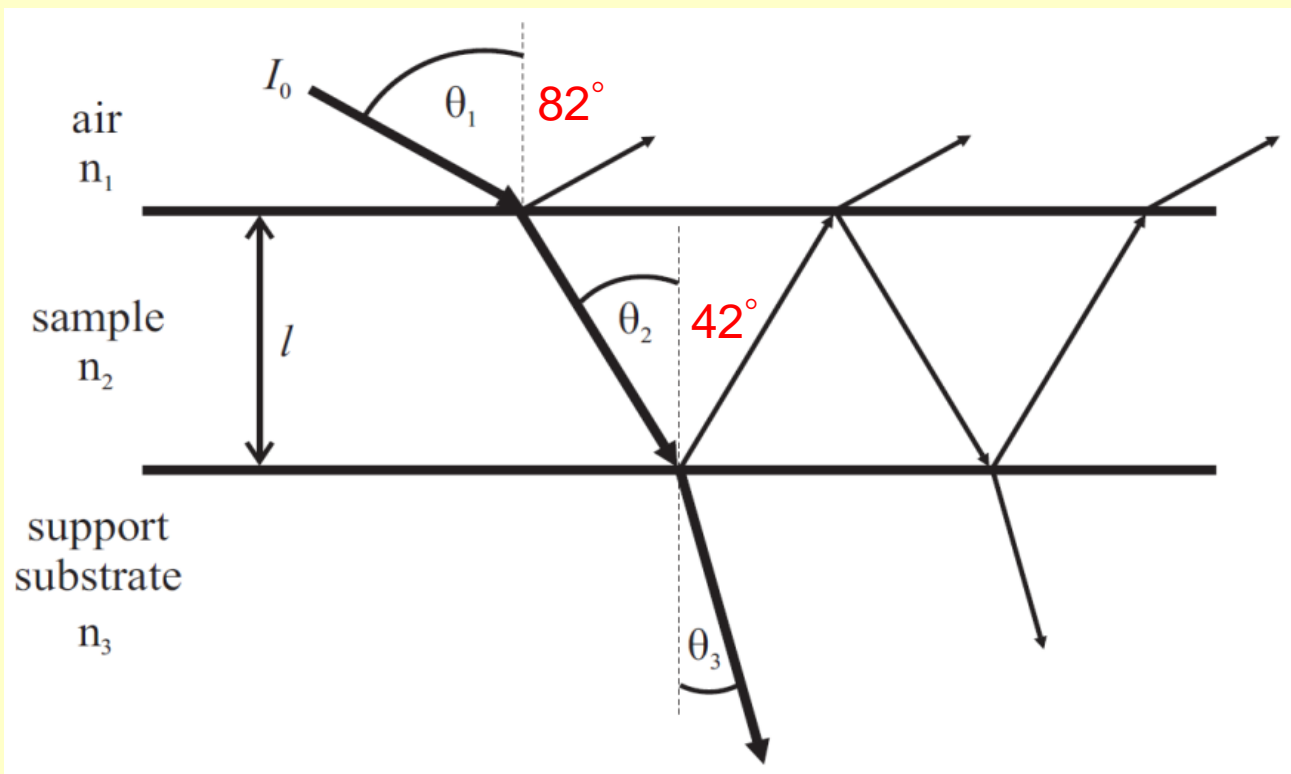


- Film Induced Baseline Distortions

Air  
 $n_1 = 1$

Paraffin  
 $n_2 = 1.473$

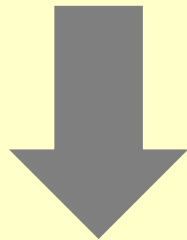
Stainless Steel



- The angle of incidence for the metal surface changes
- Higher refractive index



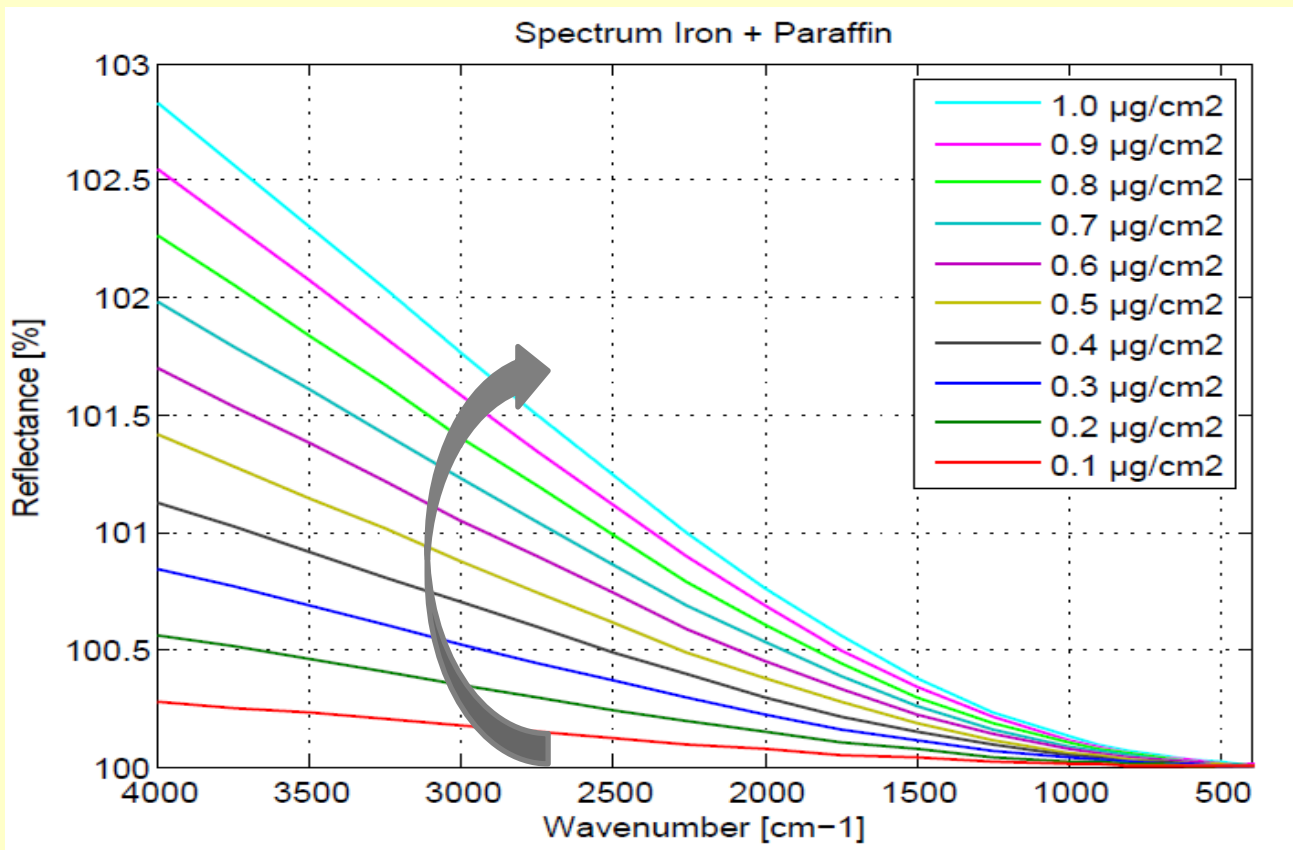
- Calculation of the baseline (MATLAB)
  - Approximations:
    - The complex refractive index of **iron** as a function of wavenumber
    - The refractive index of Paraffin:  
 $n_2 = 1.473$  (n<sub>20/D</sub>)



**The calculation will yield:**

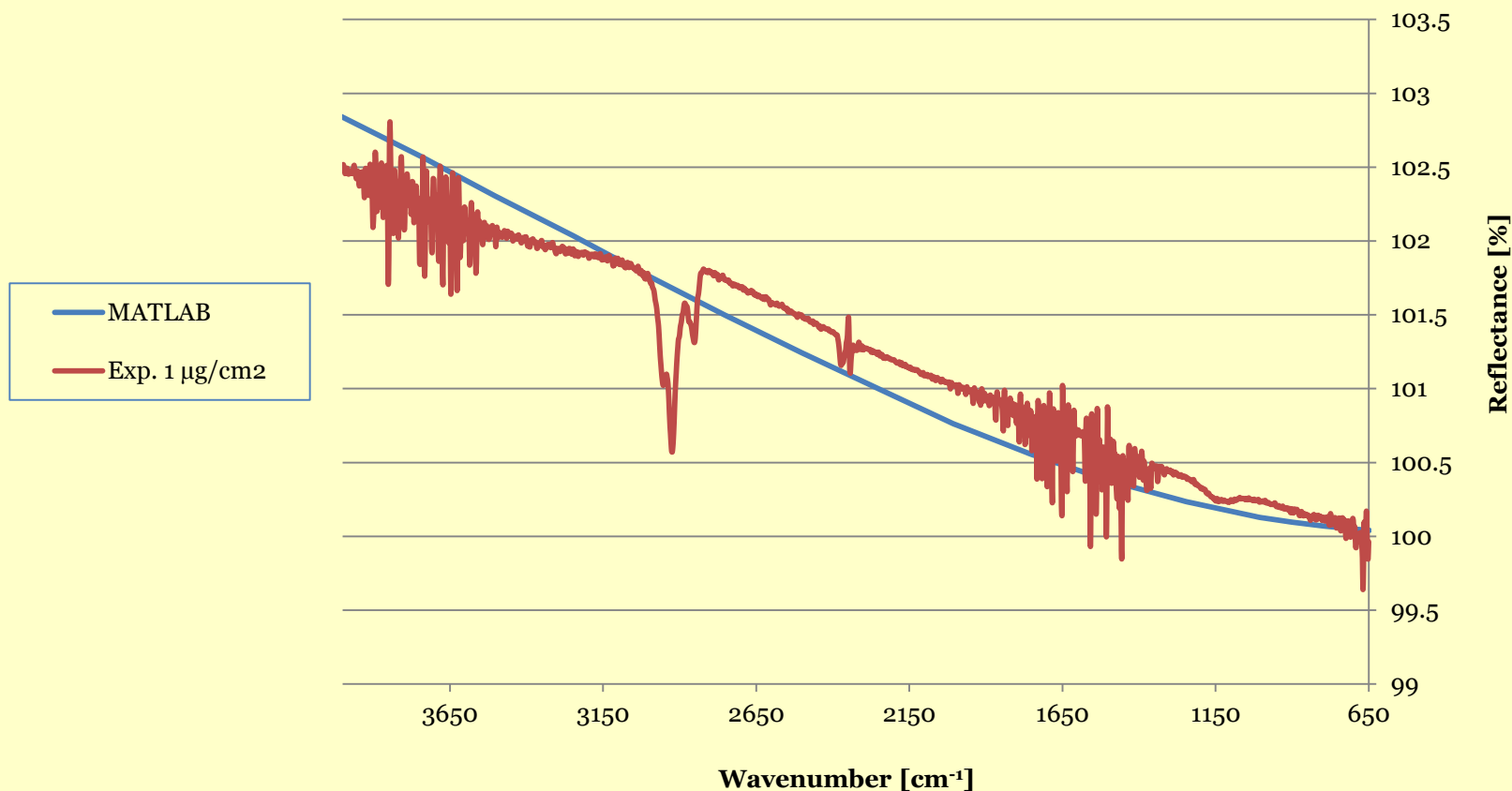
Only the baseline, not the carbon-hydrogen stretching peaks

- Calculation of the baseline (MATLAB)



*The higher the concentration, the bigger the baseline distortion  
But negligible compared to the effect of the roughness*

- Calculation of the baseline (MATLAB)



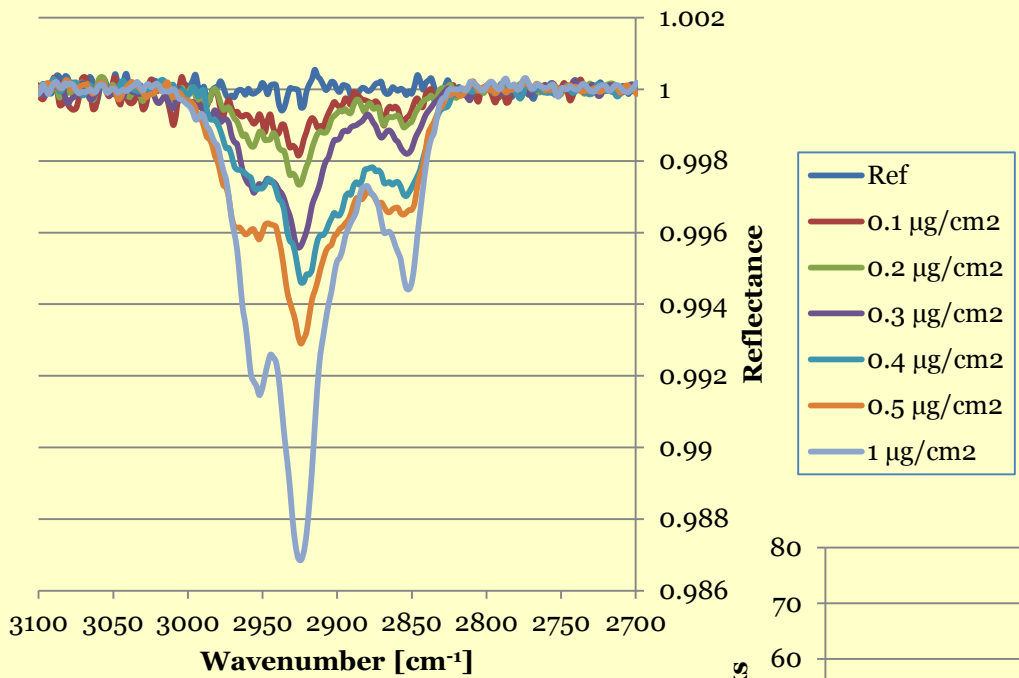
Comparison with a Paraffin film on a *electropolished* Stainless Steel surface (experiment)



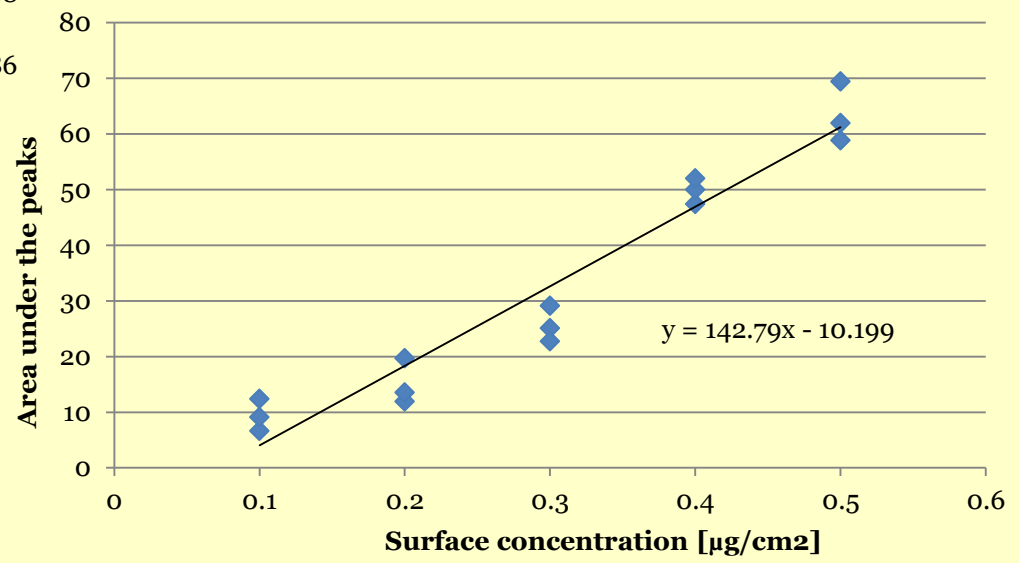
- The contamination standard for hydrocarbons:
  - Cutting oil: *Blasocut BC 35 LF SW* (33 vol%)
  - Machine oil: *Shell Vitrea 150* (33 vol%)
  - Bearing grease: *Kluber Isoflex NBU 15* (33 vol%)
  
- Dissolve in n-Hexane (for spectroscopy)
  
- Switch to Paraffin (for spectroscopy)



- Electropolished Stainless Steel Surface



Stainless Steel is *not* the cause of the problems!



Electropolished



Rough Surface



Sandblasted

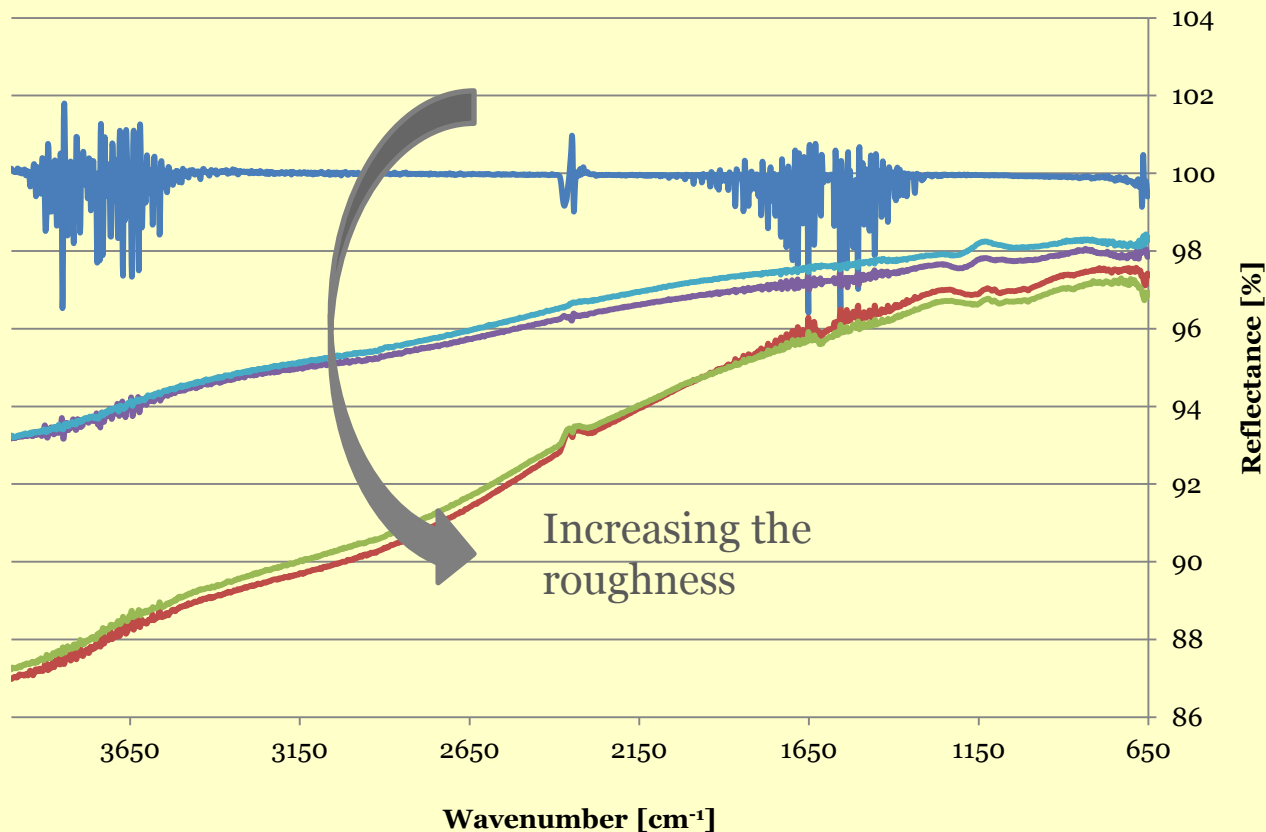


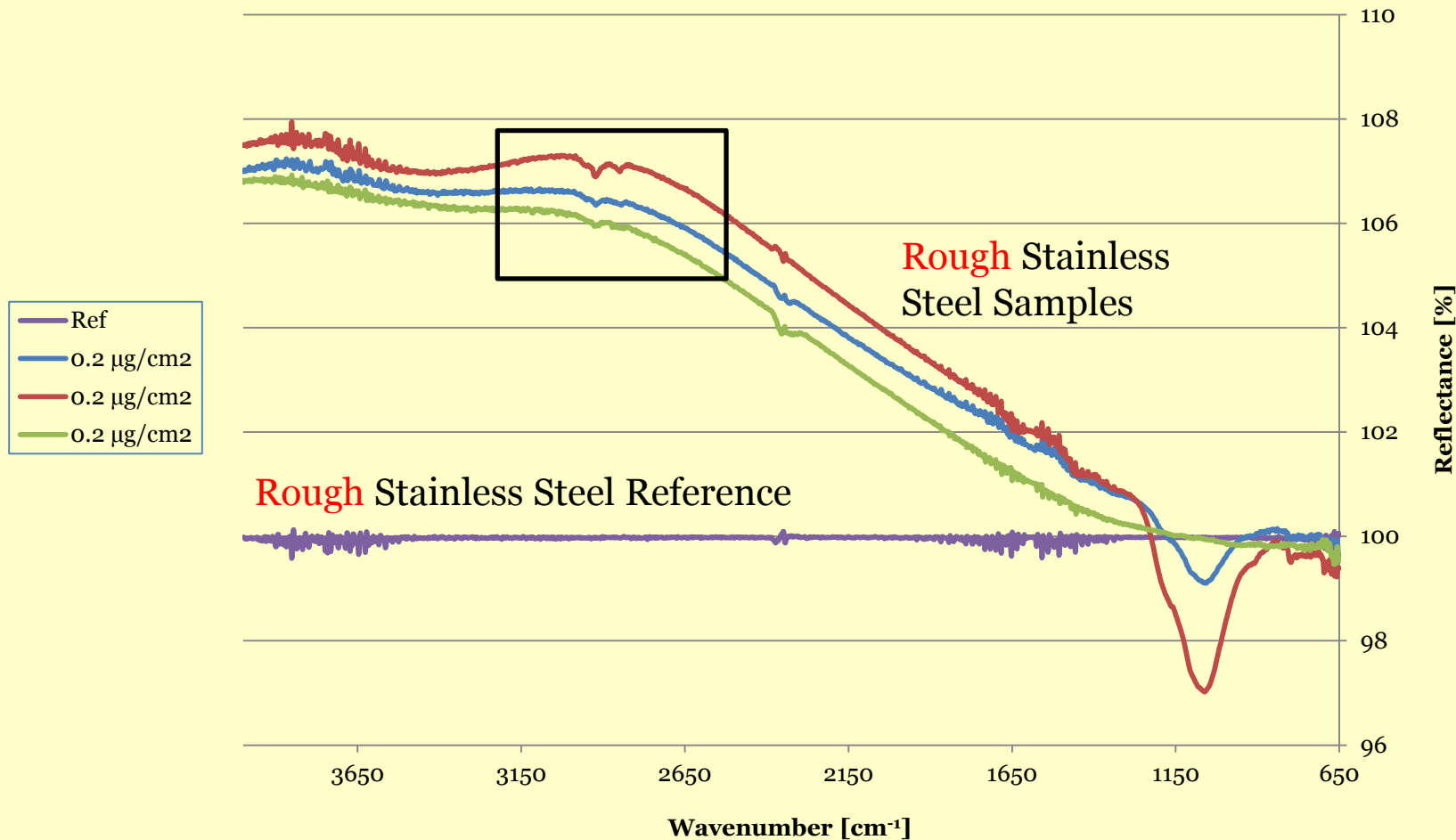




Electropolished  
Stainless Steel  
Reference →

Rough Stainless  
Steel Samples  
(clean)





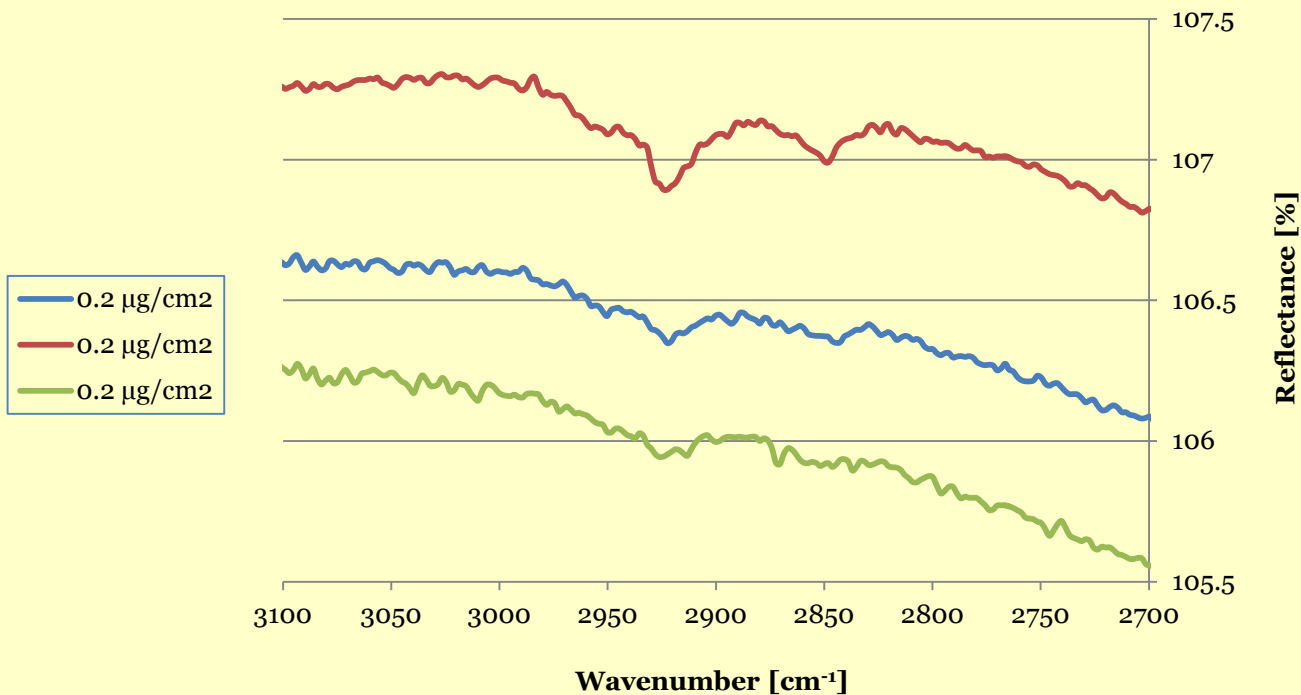
Rough Stainless Steel Reference

Rough Stainless Steel Samples

*The samples are rougher than the reference*



- Rough Stainless Steel Sample & Rough Stainless Steel Reference



*The more signal is lost, the smaller the peaks become.*



- Detection of *Hydrocarbons* on *smooth Stainless Steel* surfaces is possible down to  $0.1 \mu\text{g}/\text{cm}^2$  (= 1 monolayer)
- Detection on rough surfaces is an issue for
  - Stainless Steel

But possibly also for

- Copper
- Aluminum

# Questions ?

## **Acknowledgements:**

Paolo Chiggiato & Mauro Taborelli

### The Chemistry Laboratory:

Benoit Teissandier, Colette Charvet, Laetitia Bardo & Radu Setnescu

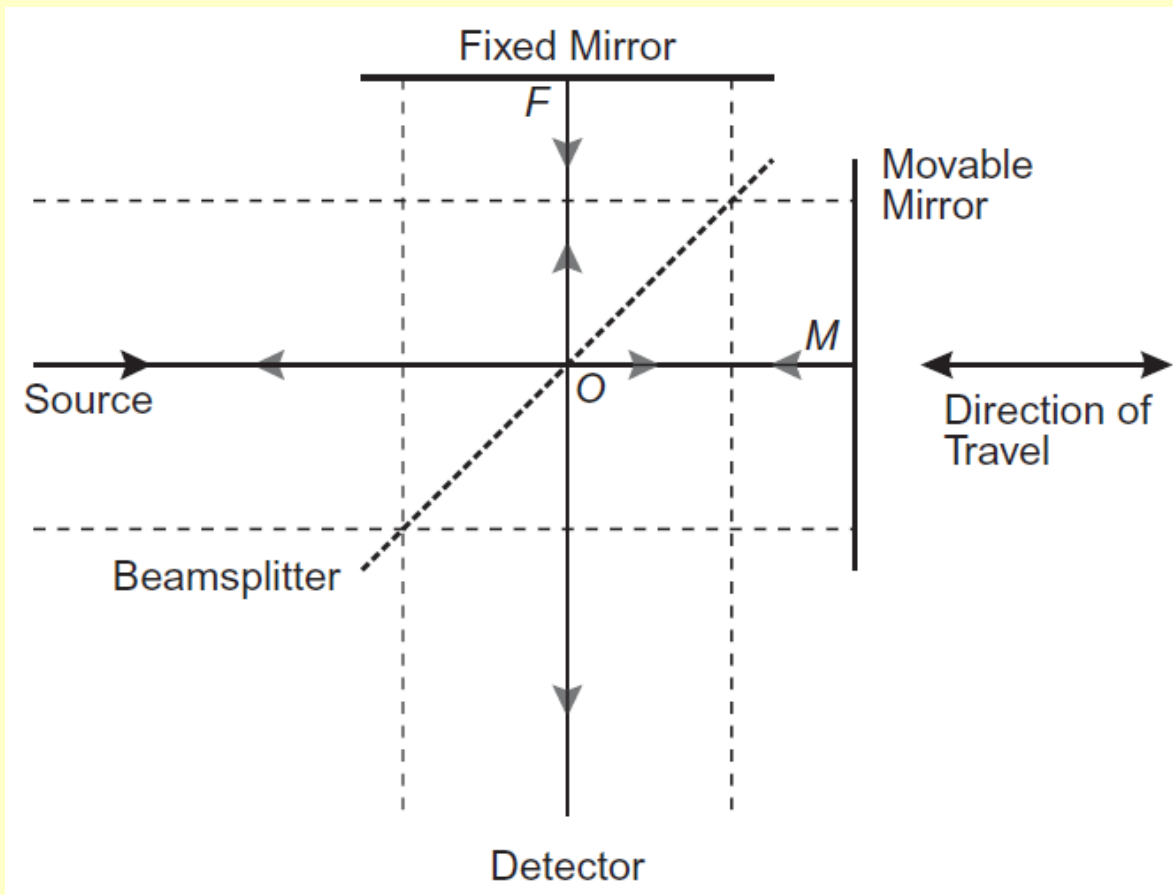
### The Surface Treatment Workshop:

Florent Fesquet, Pierre Maurin & Jacky Carosone

### The Polymer Laboratory

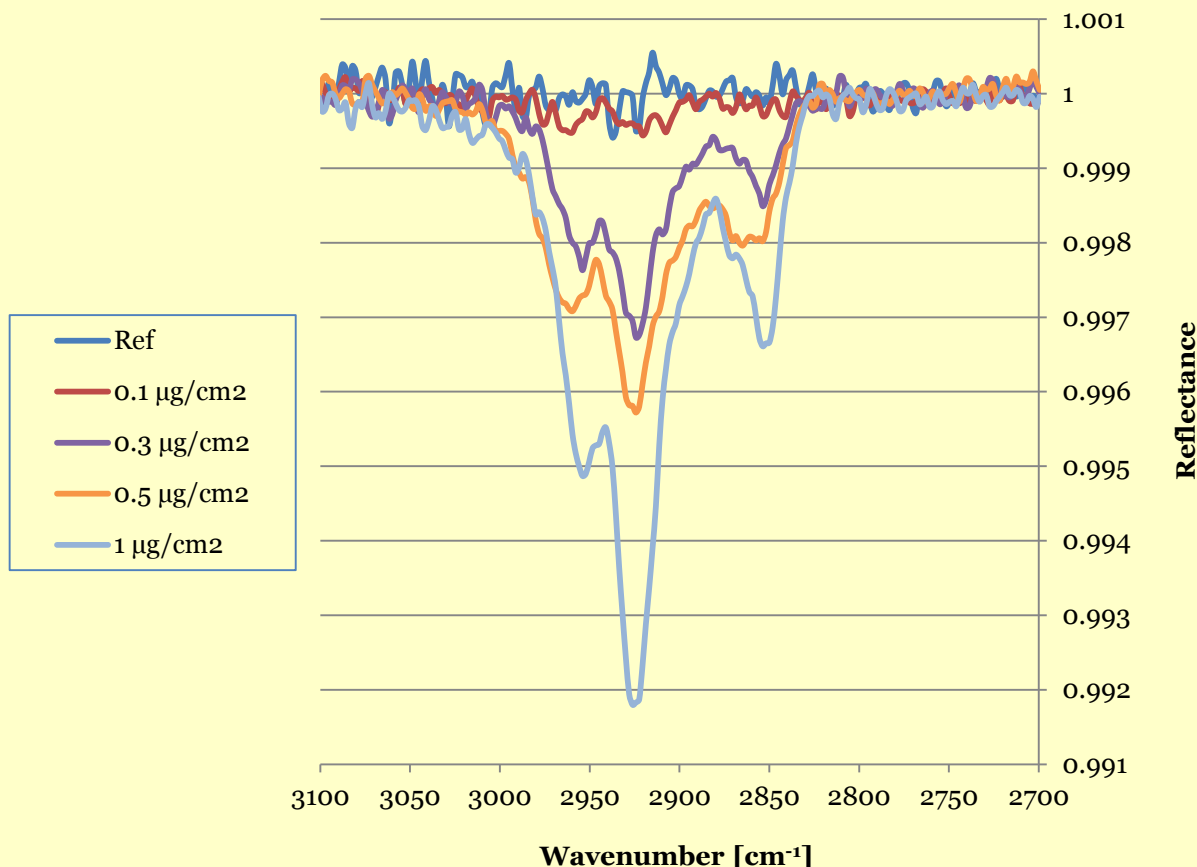


- Why *Fourier Transform*?





- Electropolished stainless steel plates
- 300°C for 2.5 days





- The Fresnel equations

$$r_p = \frac{(n_2 \cdot \cos(\theta_1) - n_1 \cdot \cos(\theta_2))}{(n_2 \cdot \cos(\theta_1) + n_1 \cdot \cos(\theta_2))}$$

$$r_s = \frac{(n_1 \cdot \cos(\theta_1) - n_2 \cdot \cos(\theta_2))}{(n_1 \cdot \cos(\theta_1) + n_2 \cdot \cos(\theta_2))}$$

- Snell's law

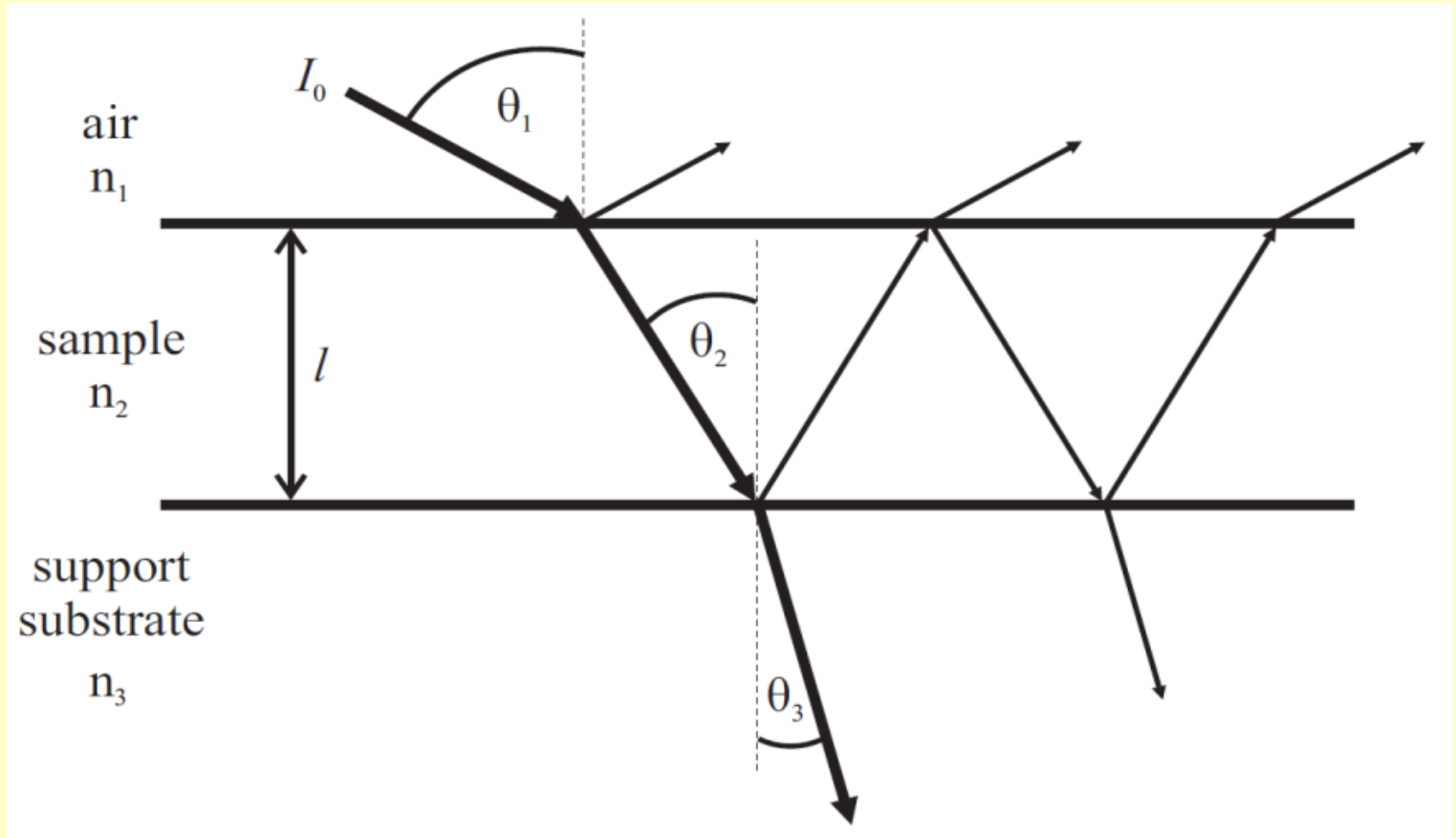
$$n_1 \cdot \sin(\theta_1) = n_2 \cdot \sin(\theta_2)$$



- The reflectance of a thin film on a metal surface (= stratified medium)

$$r_j = \frac{r_{12,j} + r_{23,j} \cdot e^{2 \cdot i \cdot \beta}}{1 + r_{12,j} \cdot r_{23,j} \cdot e^{2 \cdot i \cdot \beta}} \quad \text{with } (j = p \text{ or } s)$$

$$\beta = \frac{2\pi}{\lambda_0} \cdot n_2 \cdot l \cdot \cos(\theta_2)$$





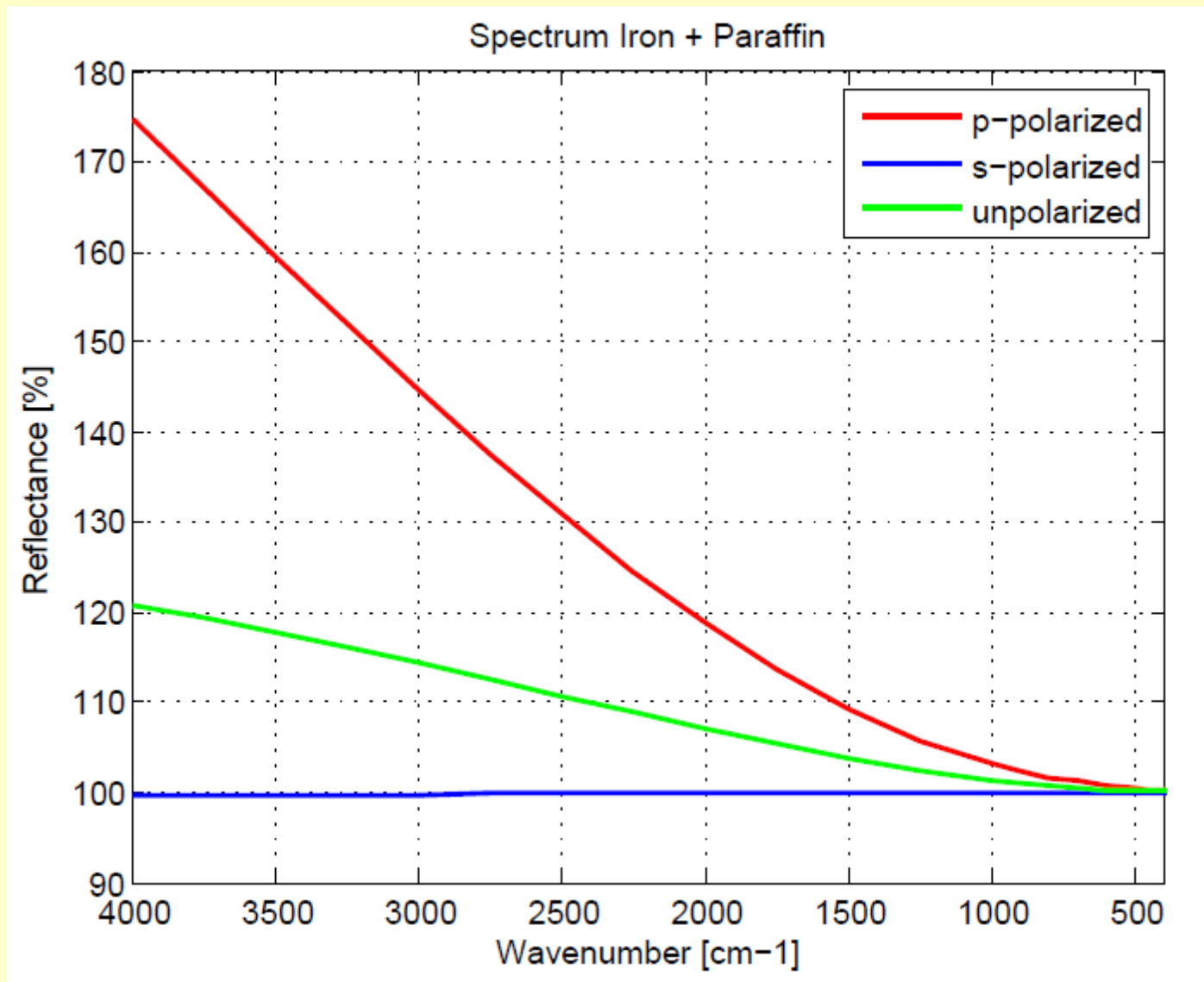
- The reflectance

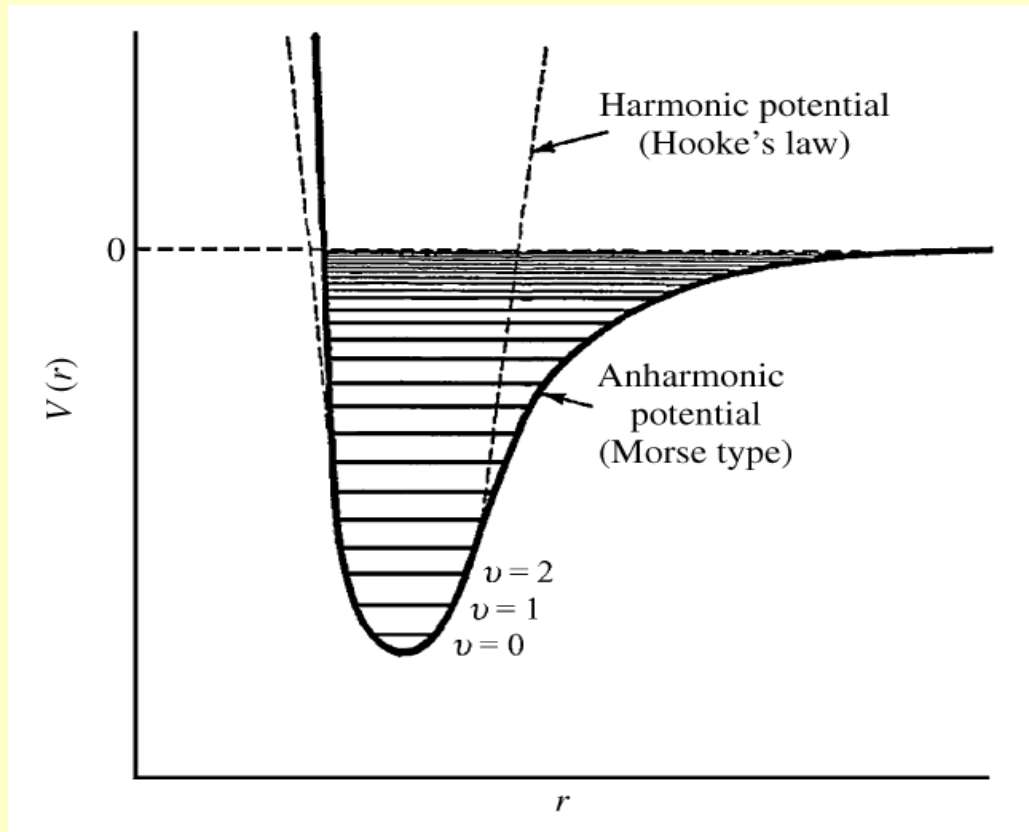
$$R_j = |r_j|^2$$

$$R_u = \frac{R_p + R_s}{2}$$

$$\text{Spectrum} = \frac{R_{p,\text{film}} + R_{s,\text{film}}}{R_{p,\text{no film}} + R_{s,\text{no film}}}$$

# The Calculation





$$V_{iv} = h\nu_i \left( v_i + \frac{1}{2} \right) + h\nu_i x_i \left( v_i + \frac{1}{2} \right)^2$$



- Bruker Vertex 70

