



# HOM studies for DQWCCs and HOM filter design

Binping Xiao, BNL

BNL

Sergey Belomestnykh, Ilan Ben-Zvi, Carlos Marques, John Skaritka, Silvia Verdú-Andrés, Qiong Wu

CERN

Luis Alberty, Said Atieh, Rama Calaga, Ofelia Capatina, Teddy Capelli, Federico Carra, Norbert Kuder, Raphael Leuxe, Thierry Renaglia

Lancaster University/Cockcroft Institute

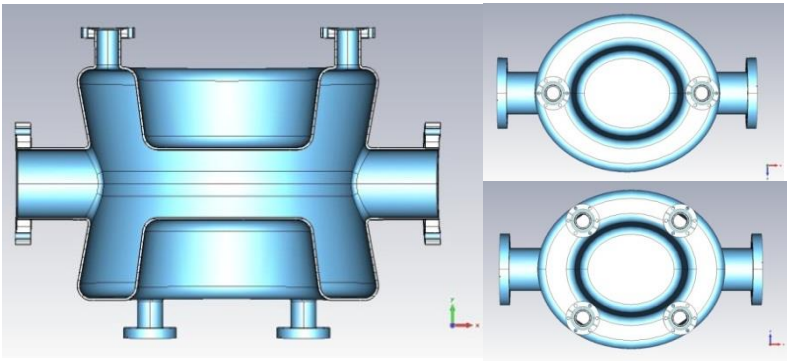
Graeme Burt, Ben Hall, Tom Jones

SLAC

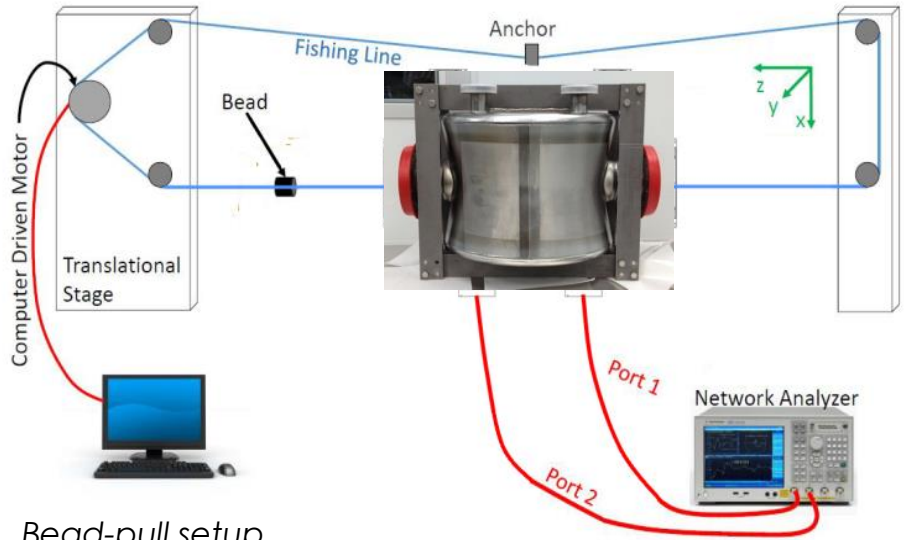
Zenghai Li

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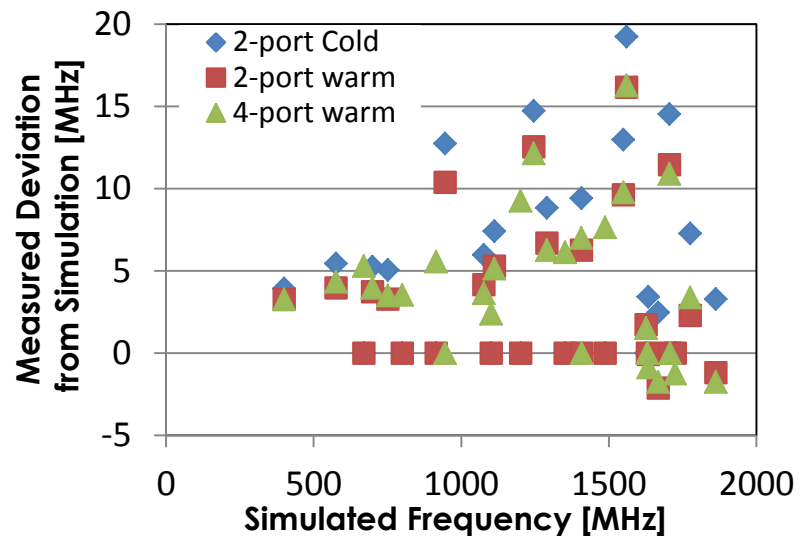
# PoP DQW: Bead Pulling



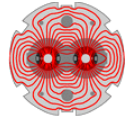
Proof-of-Principle (PoP)  
Double-Quarter Wave Crab Cavity (DQWCC)



Bead-pull setup

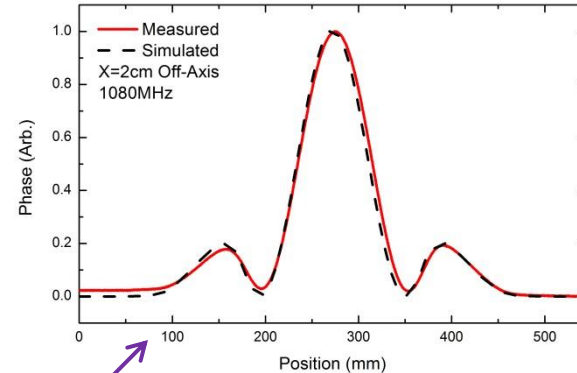
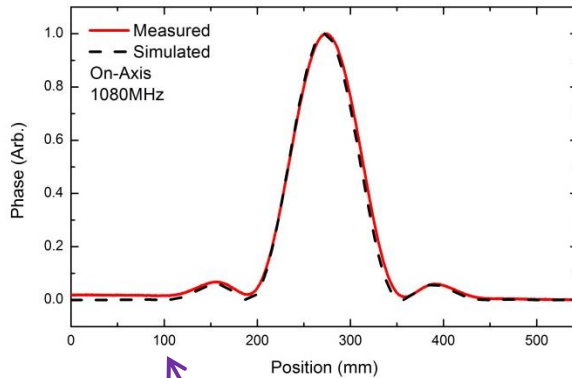
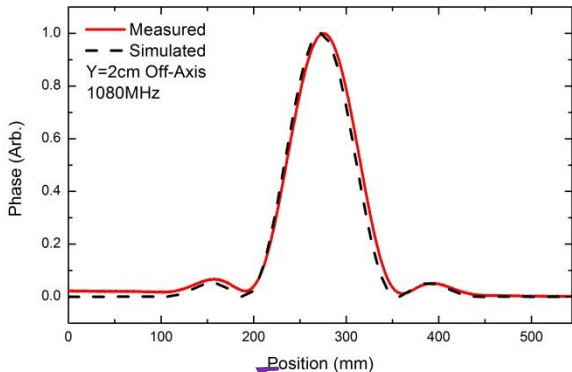


- Cavity prototype smaller than RF model cause frequencies shifting up.
- HOM frequencies deviated from designed values due to unspecified tolerances for PoP cavity.

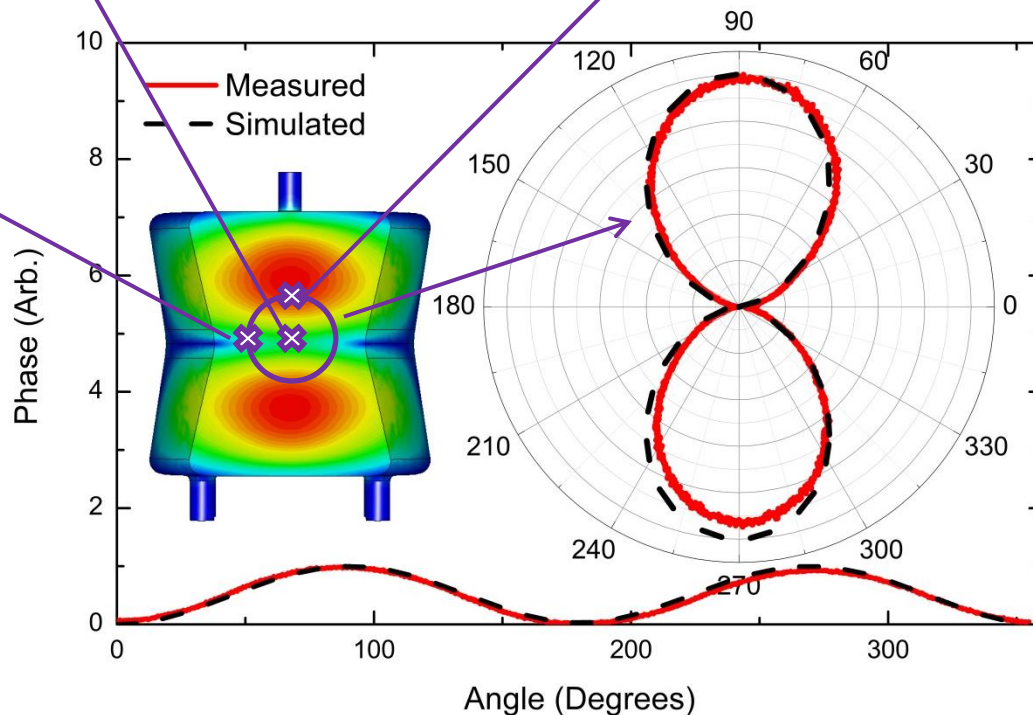
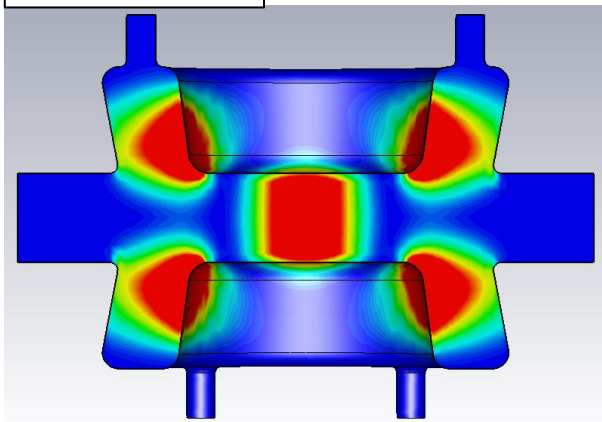


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# PoP DQW: Bead Pulling

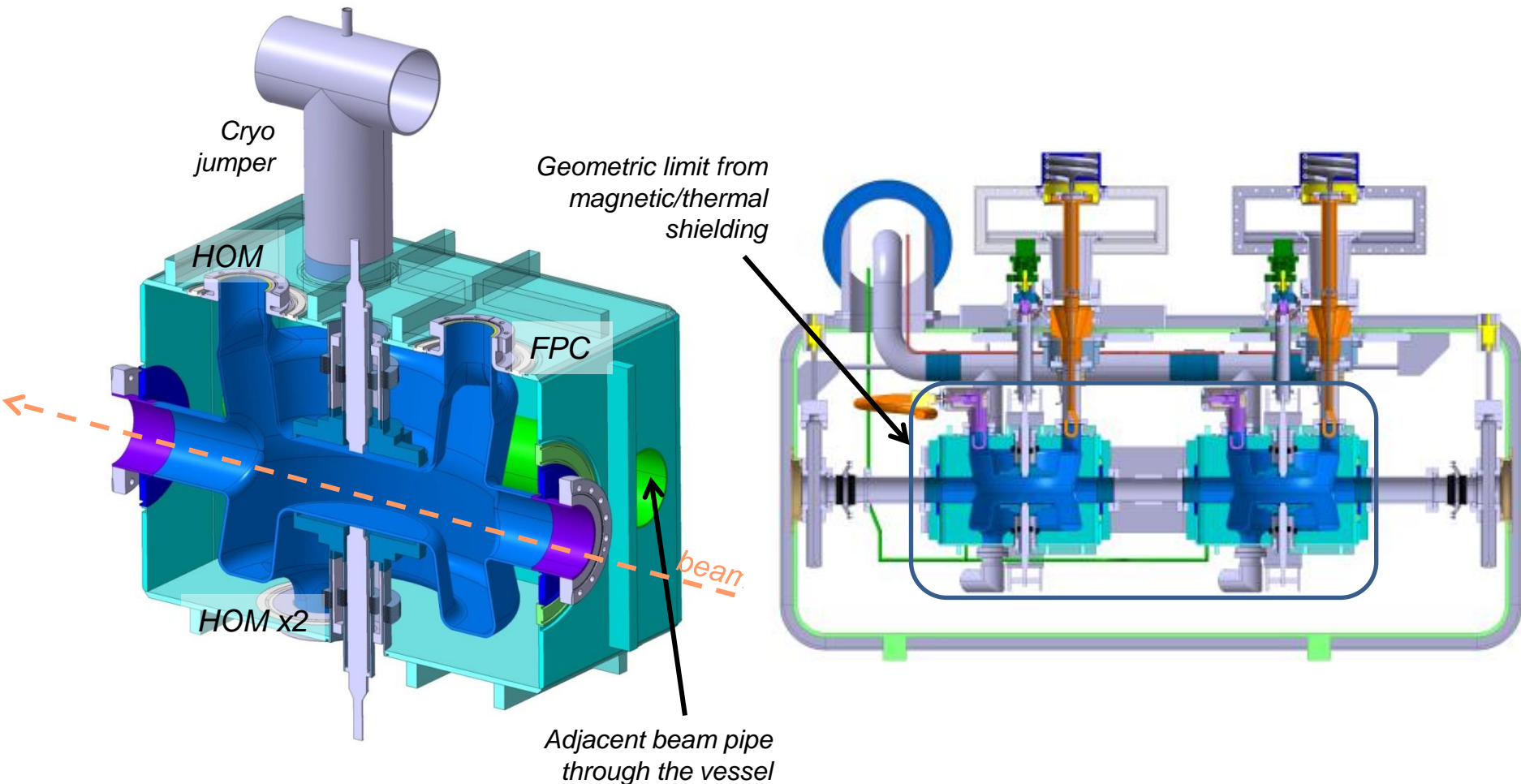


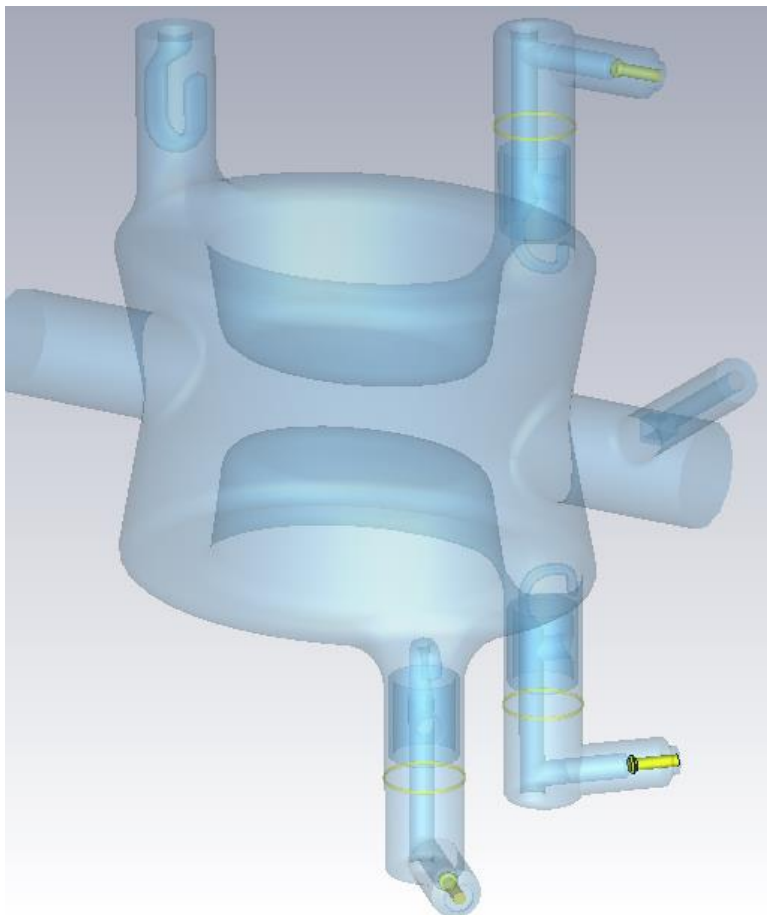
1080 MHz



© Carlos Marques (Master thesis)

# SPS double quarter wave





- 3 HOM filters per cavity, with two 60-degree away from the center to give *clearance to the other beam pipe* in horizontal kick scheme
- *Symmetrical* design to minimize multipolar components.
- 60 degree is chosen to provide more coupling to HOMs.
- *Compact* to fit into cryomodule.
- Longer RF cables can be easily attached to the L shape filter to *reduce static heating*.

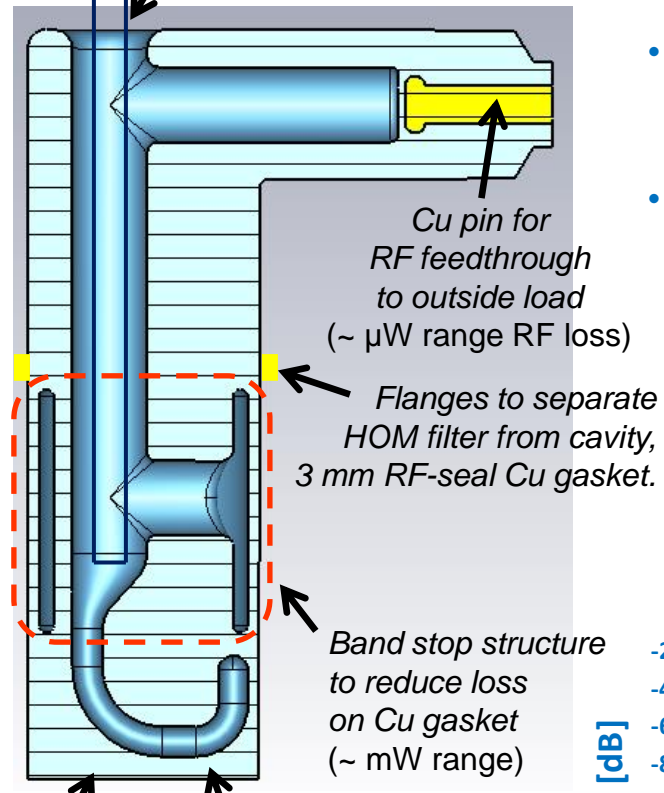


# SPS DQW: L-shape Filter



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>  $\varnothing$  10mm cooling channel capable of extracting 0.8W (~30 mW dynamic loss per filter for 20n $\Omega$  resistance)



Cu pin for RF feedthrough to outside load (~  $\mu$ W range RF loss)

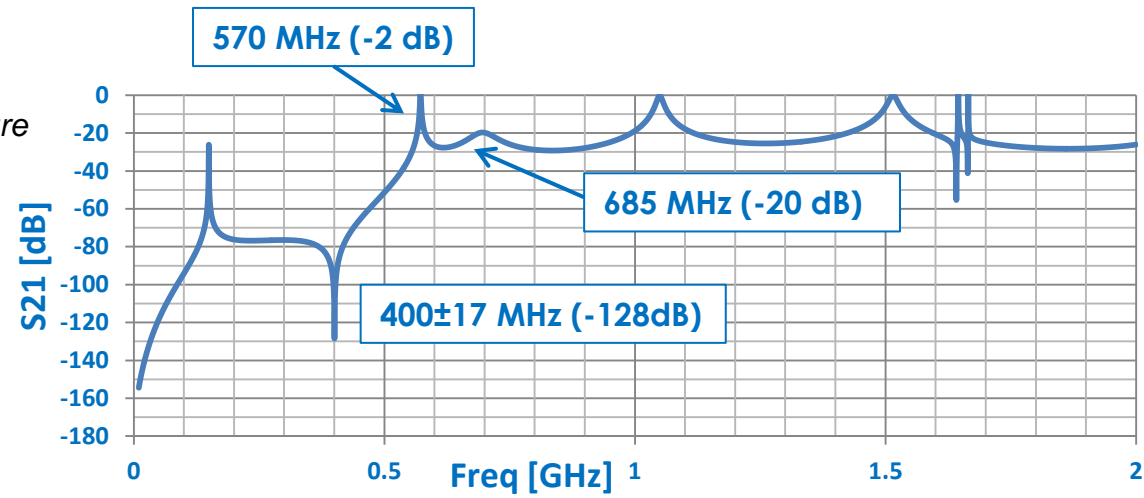
Flanges to separate HOM filter from cavity, 3 mm RF-seal Cu gasket.

Band stop structure to reduce loss on Cu gasket (~ mW range)

Bend to lower peak magnetic field (hook: 61.3mT) (on cavity: 71.3mT)

Hook length tuned to minimize Hpk on hook surface.

- Designed to handle kW range HOM power per cavity
- Coupling to 400 MHz:  $7.9 \times 10^9$  (1.1 W at each port to outside load)
- RF losses estimated for crabbing mode with  $V_t = 3.34$  MV  
Estimation of RF losses from HOMs will follow.

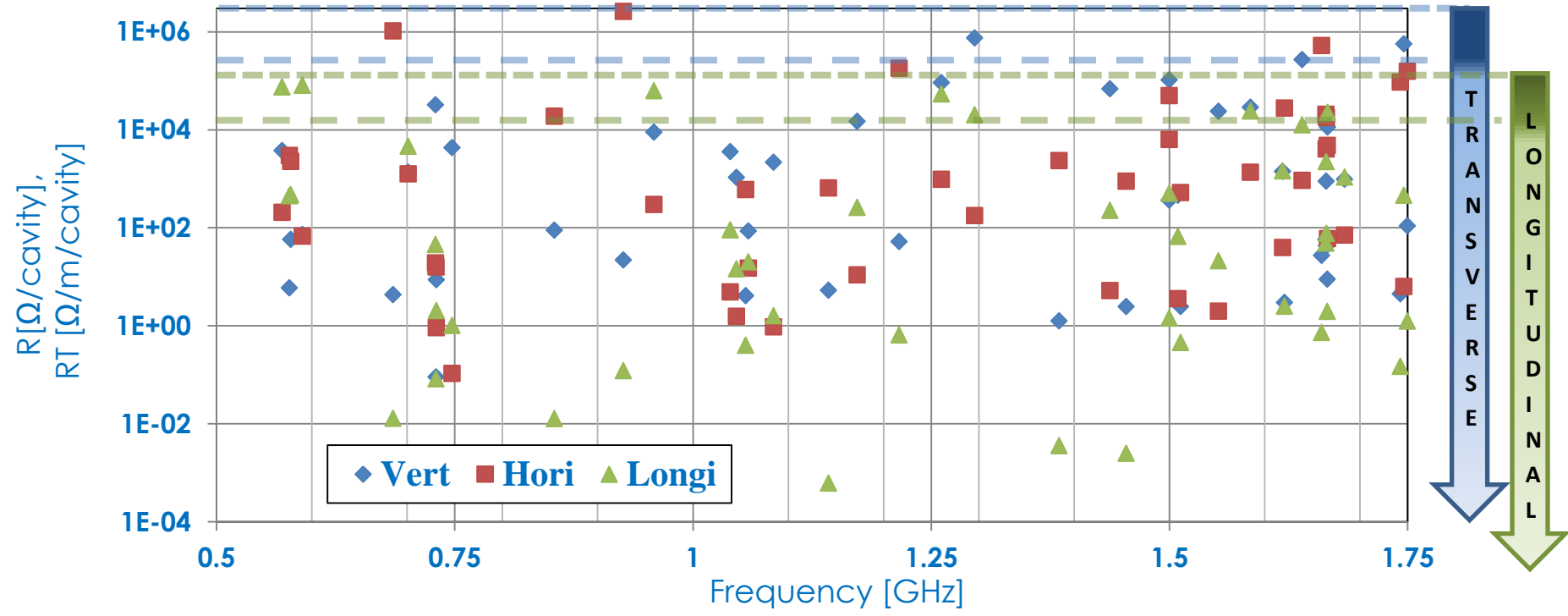




# Budget Limit

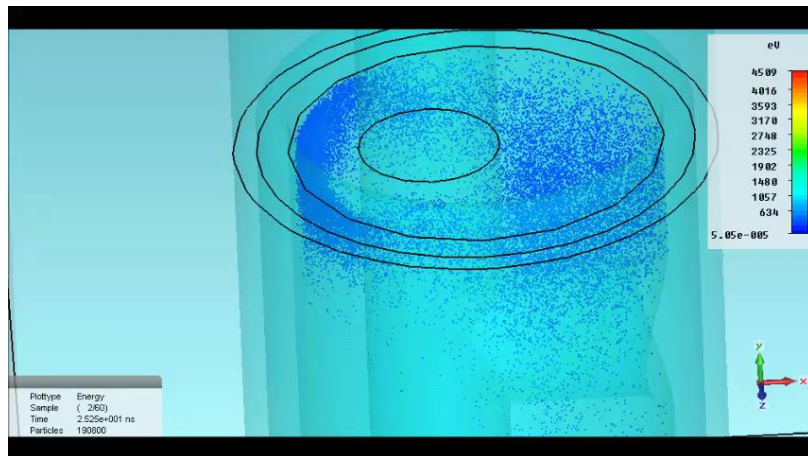
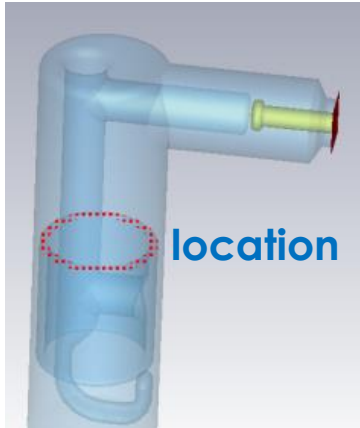


Impedance limits		Lower	Upper/2	Upper
[Ref: Ranking Criteria, May 2014]				
Longitudinal	(kΩ/cavity)	12.5	62.5	125
Transverse	(MΩ/m/cavity)	0.3	1.5625	3.125



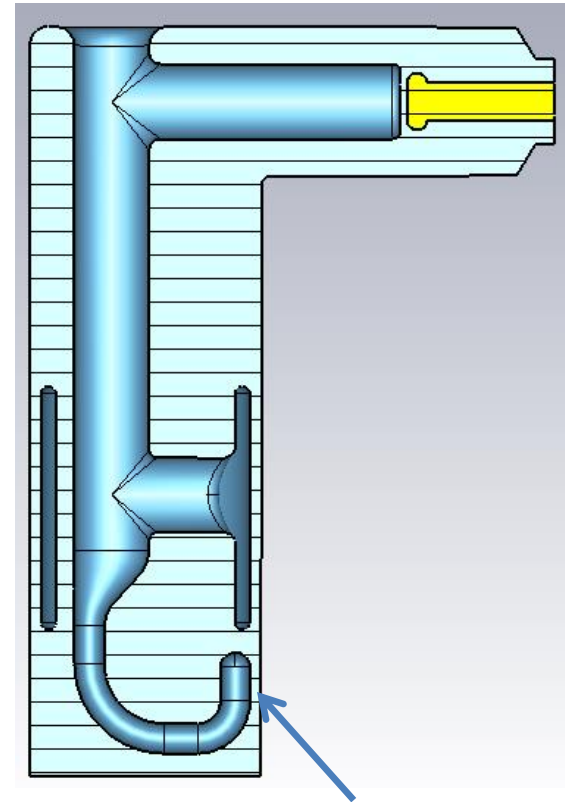
- Below upper limit: *all*
- Higher than half-upper limit: *0.569, 0.590, 0.927 GHz*
- Higher than lower limit: *0.685, 0.959, 1.261, 1.296, 1.585, 1.639, 1.660, 1.666, 1.746 GHz + abovementioned*

## Multipacting



Preliminary multipacting analysis

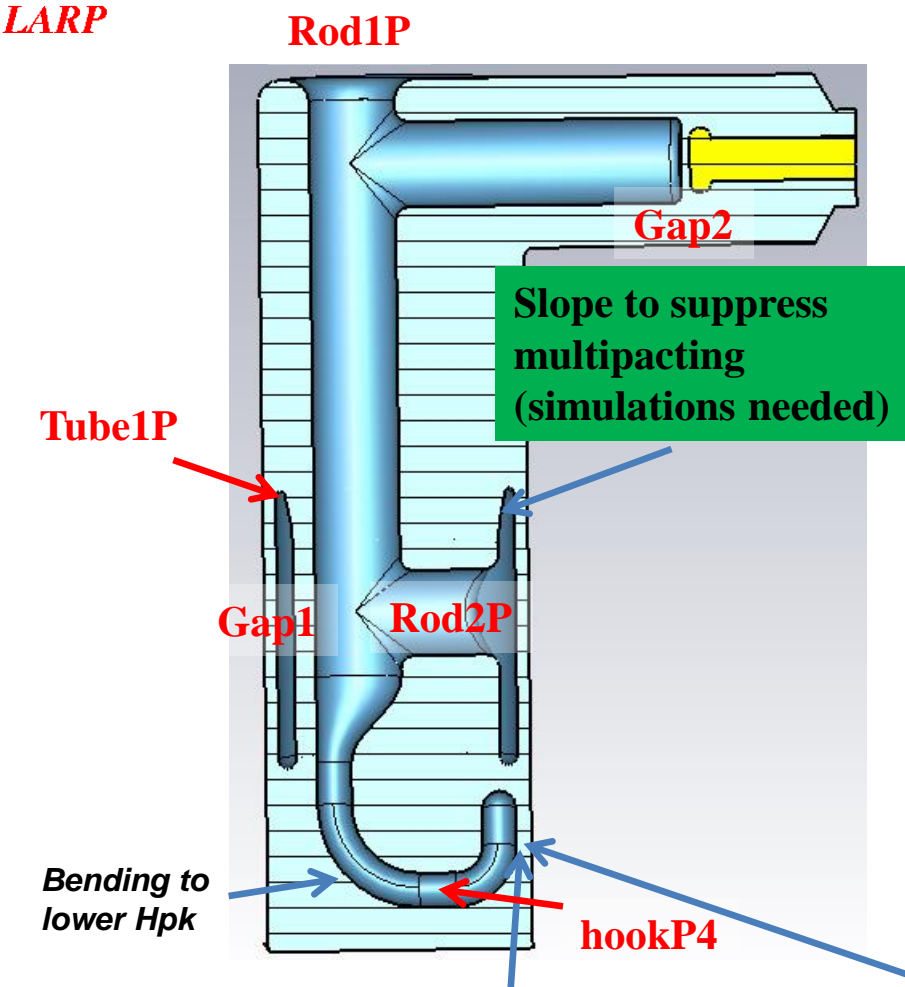
## Peak E field



High Epk of 40.3MV/m.  
(cavity: 36.7MV/m)

© Graeme Burt & Ben Hall using CST, confirmed by Z. Li using ACE3P





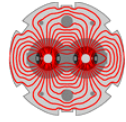
Evaluate the red numbers in  $\pm 0.3\text{mm}$  range  
 Tube1P and Rod2P will not affect RF performance

Freq [GHz]	S21 [dB]		$\Delta S21$ [dB]			
	orig. model		Gap1	Gap2	hookP4	Rod1P
0.569	-22.3		-1.4	-0.8	-2.9	-0.4
0.590	-6.2		-3.15	-1.0	-8.7	-7.3
0.927	-26.5		-0.1	-0.7	-0.2	-0.5

On-going: slightly modify the filter to suppress the fabrication error induced performance degradation.

This gap will affect the damping of first several modes significantly, possible to **tune**?

Changing the gap 0.5mm bigger, peak electric field reduced to 19.3MV/m. (To be cross checked with ACE3P)



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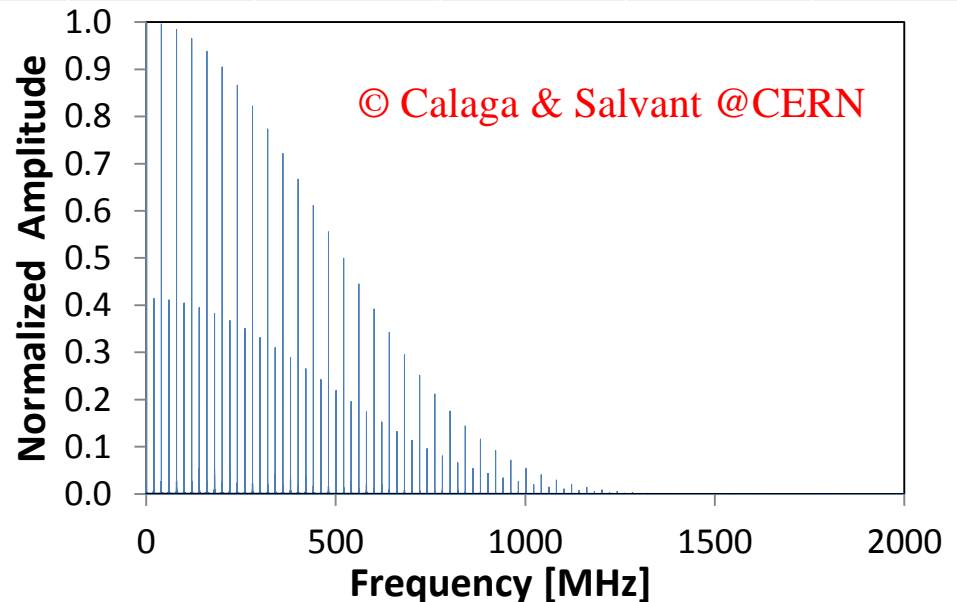
# DQW: Power Estimation



	F (MHz)	558.4	588.3	685.3	701.5	926.7	958.7
	Mode Type	M	M	h	mix	h	M
	Qext	3850	4700	1840	569	5450	4190
Impedance	Longitudinal [Ω/cavity]	49900	207000		3563		40400
	Horizontal [Ω/m/cavity]			911000	1234	1740000	
	Vertical [Ω/m/cavity]				748	287	
	HOM Power [Watt]	4.5	1.4	<0.1	57.8	<0.1	0.2
	HOM Power with freq shift in ±2MHz [Watt]	8.6	5.9	17.6	58.7	4.4	128.0

- HOM power is about 65 Watts per cavity
- The power increased to 225 Watts if HOM frequencies shift in ±2 MHz range.

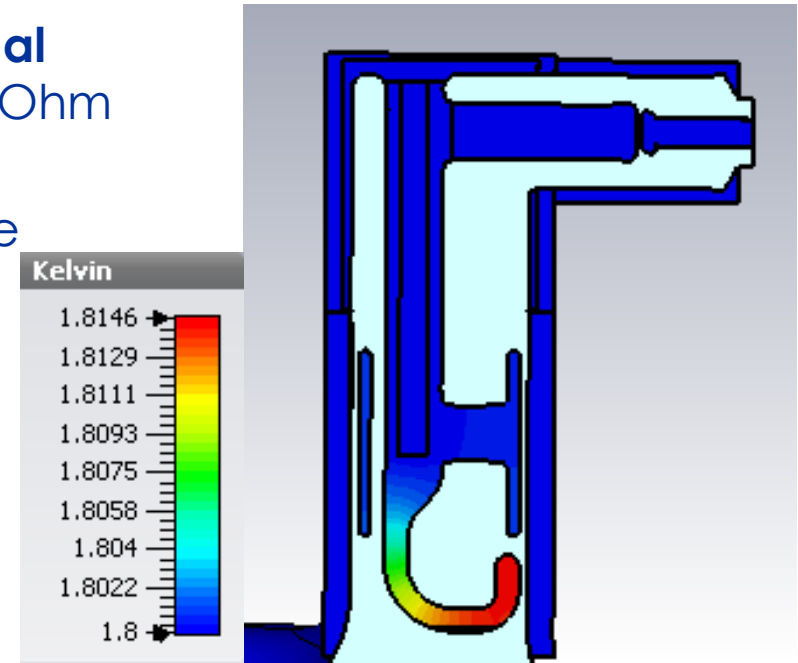
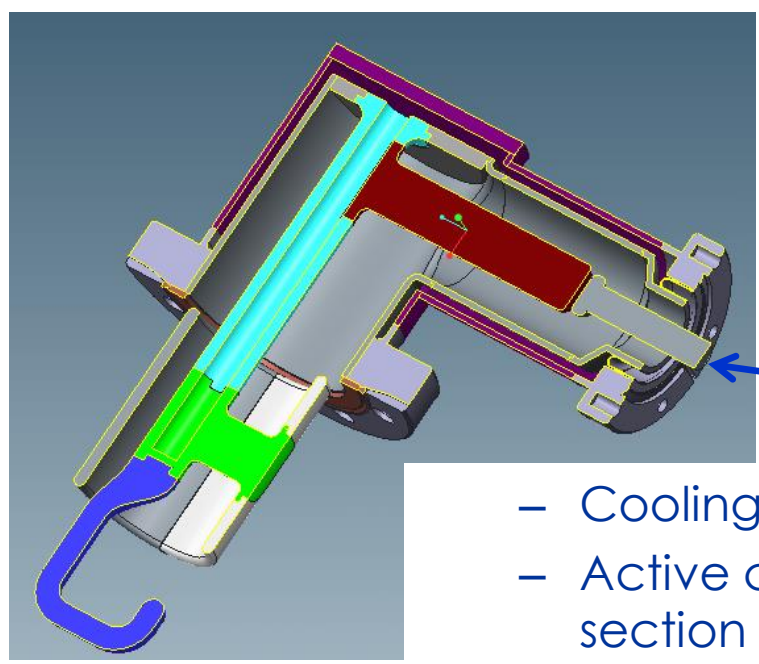
Power of transverse modes estimated based on 5mm offsets.



# DQW: Thermal Analysis

CERN and Cockcroft

- Assumes cavity operating **at nominal deflecting voltage** of 3 MV with 5 nOhm surface resistance.
- Assumes active cooling through the center cooling channel **at 1.8 K**



Feed-through to a coax cable to an outside load

- Cooling channel larger than the previous version.
- Active cooling will be applied in the straight section of the HOM hook, and it is possible to extend it till the end of the tip.

# DQW: Prototyping

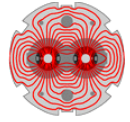
- 3-D printing (BNL) + Cu coating (Epner Technology Inc.).
- Acetone etching for smoother surface.
- Evaluating different ways to deal with joint loss.
- Will figure out the ports connection based on new design.



**Prototyping of updated version will start soon**



SPL HOM filter  
(K. Papke, CERN)



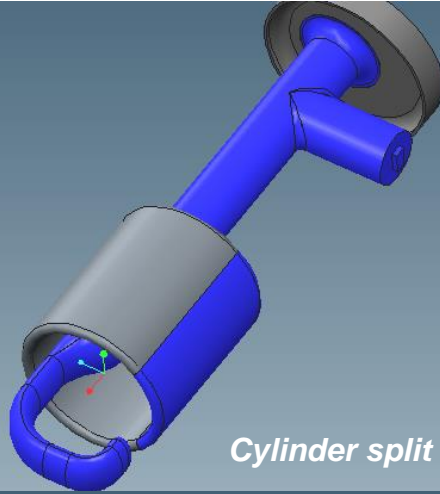
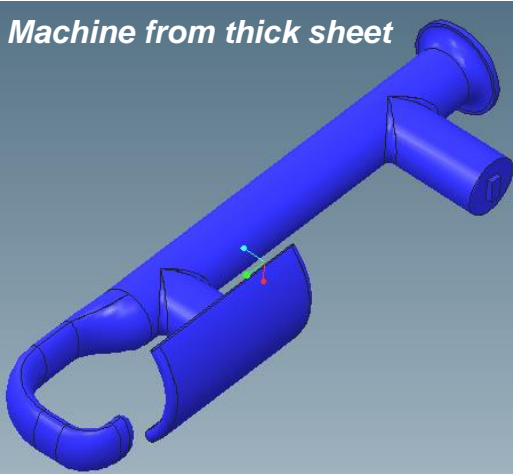
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# Assembly ideas (UK, CERN)

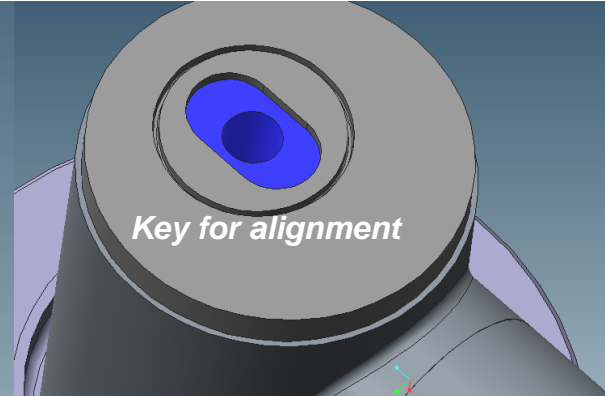


*In evolution...*

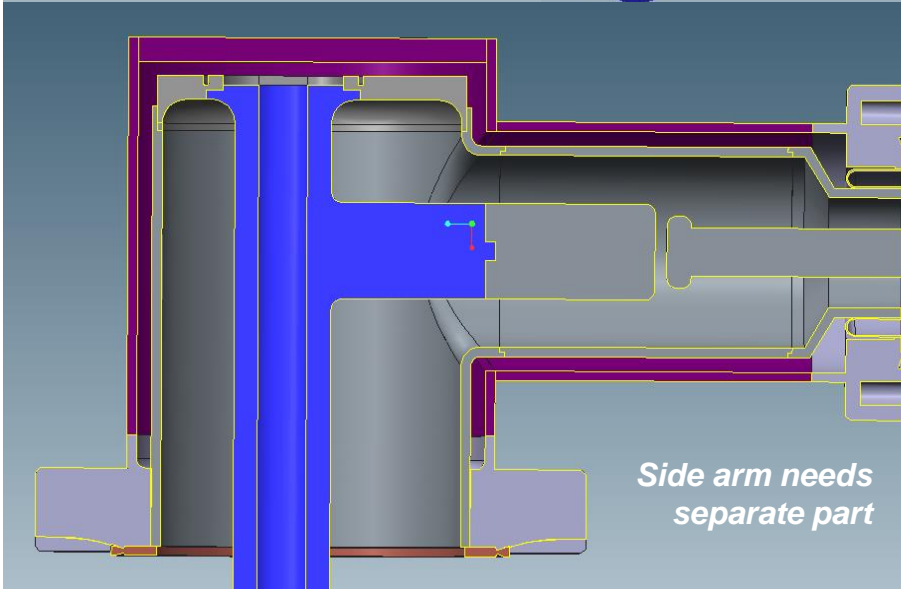
*Machine from thick sheet*



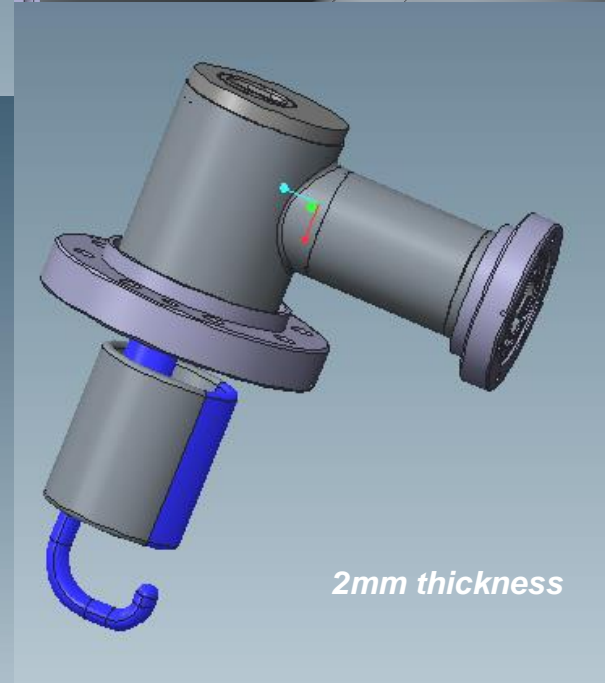
*Cylinder split*



*Key for alignment*



*Side arm needs separate part*



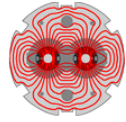
*2mm thickness*



# Summary



- **Peak electric/magnetic fields** on filter smaller than on cavity. Calculations are cross-checked between CST MWS and ACE3P.
- Tolerance calculation is on-going, current results suggest that tuning at room temperature (before or after mounting onto cavity) might be necessary.
- Methodology for **R/Q calculation** has been established (UK). Values cross checked by UK and BNL using CST MWS. Additional check by SLAC with ACE3P is on going.
- Qext calculations of HOMs using two methods: eigenmode Q and S parameter Q.
- HOM filter is designed to meet the current “upper limit” and to try to achieve the current “lower limit” of impedance budget with HOM frequency up to 1.75 GHz.
- Impedance evaluation up to 2 GHz is on going.
- **Multipacting** simulations are cross-checked between CST MWS (UK) and ACE3P/TRACK3P (SLAC).
- HOM filter **assembly** is under discussion. Ideas proposed by UK and CERN.



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Thank you!

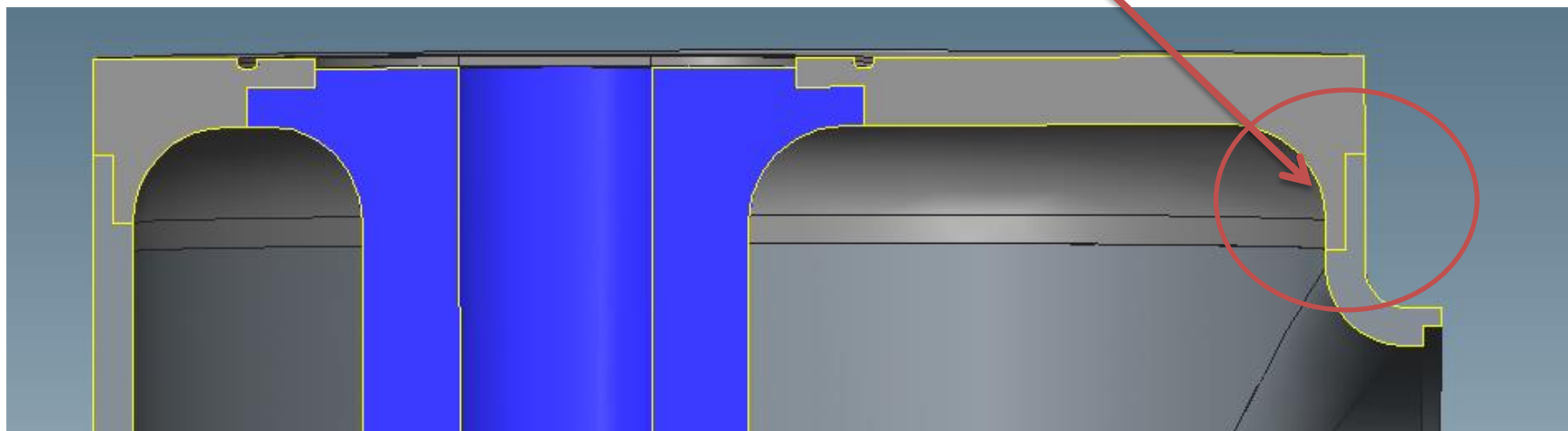




# Awaiting further RF design update

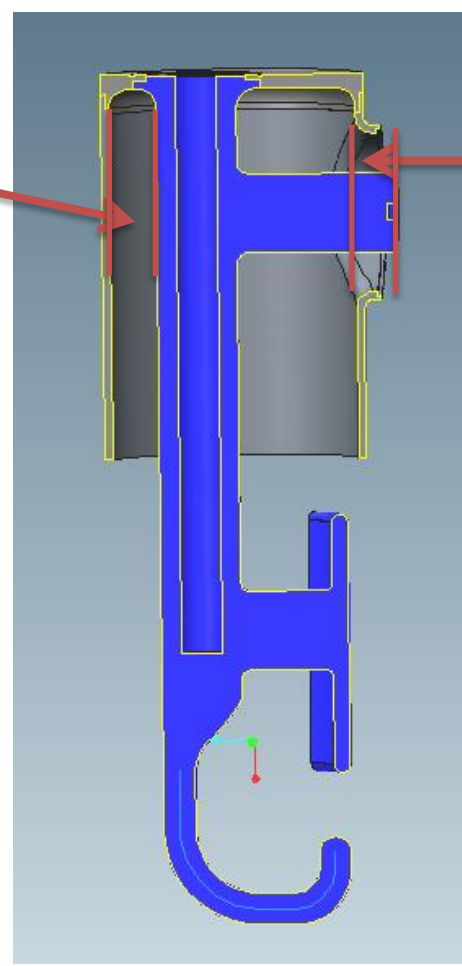


Exact height of step to be determined by RF simulations



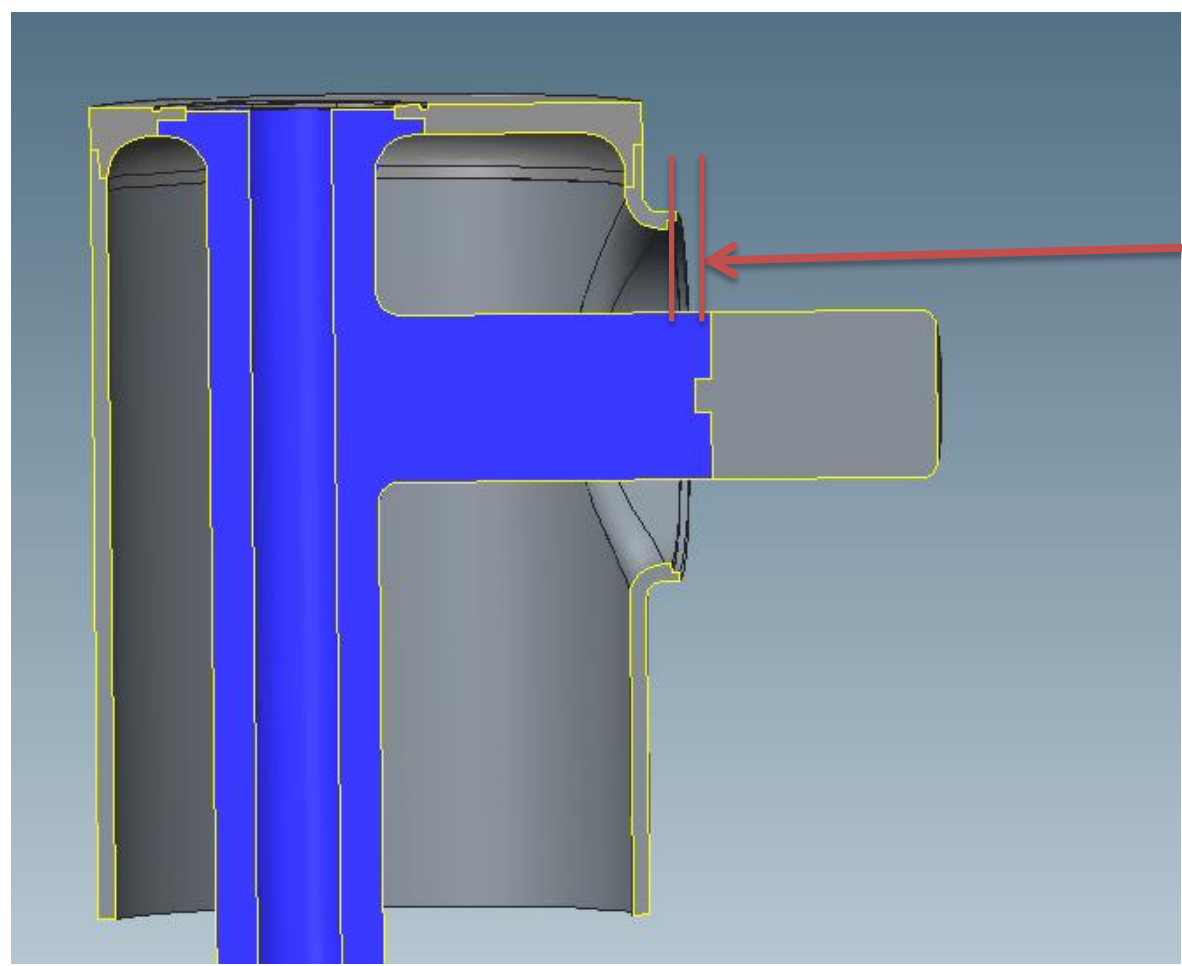
# Assembled first

12 mm gap



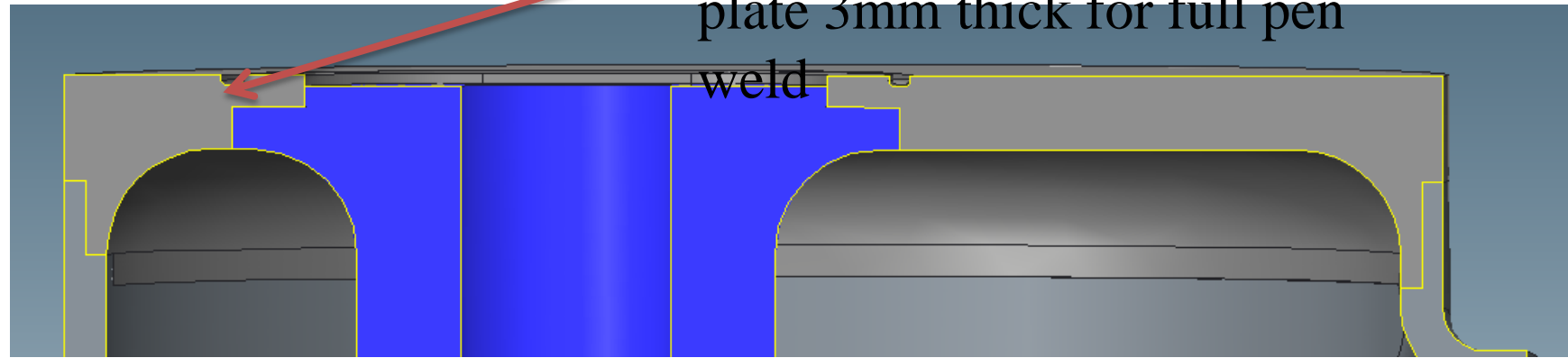
10 mm overlap,  
2 mm of play  
when  
assembling

Then rest of stub attached,



3mm  
space for  
EB weld

Small groove to make top plate 3mm thick for full pen weld



Locating point.

