Iterative Schemes for Coupled Multiphysical Problems in Electrical Engineering



TECHNISCHE UNIVERSITÄT DARMSTADT

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Outline of the Talk



NAAAA

- 2 Coupled systems in time domain
- 3 Low-Frequency field-circuit coupling
- 4 Conclusions

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Outline of the Talk







- DAE Index
- 2 Coupled systems in time domain
- 3 Low-Frequency field-circuit coupling
- 4 Conclusions

Motivation: Coupling

multiphysics: 'EM + X'

- electromagnetics
- solid-body motion
- thermodynamics
- fluid dynamics

multiscale modeling: 'EM + EM'

- effects on multiple scales (m to nm)
- elevated frequencies in some devices
- focus is on particular device or domain

hybrid formulations

- formulation (e.g. variables)
- discretization (e.g. FEM & FDM)
- models (e.g. network vs. spatially resolved)



VPI dry type transformer, ABB



smart grid power semiconductors, Infineon

Coupled systems I



Monolithic solution of a single system

$$\mathbf{u} \longrightarrow \mathbf{y} = \mathbf{f}(\mathbf{u}) \longrightarrow \mathbf{y}$$

with inputs u and e.g. two outputs $y = [y_1, y_2]$

Coupled systems I



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with inputs u and e.g. two outputs $y = [y_1, y_2]$

Two coupled (sub-)systems

$$u_2 \xrightarrow{\qquad } y_1 = f_1(u_2) \xrightarrow{\qquad } u_1 = y_1 \xrightarrow{\qquad } y_2 = f_2(u_1) \xrightarrow{\qquad } u_2 = y_2$$

Coupled systems I



Monolithic solution of a single system

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Two coupled (sub-)systems

$$u_2 \xrightarrow{\qquad \qquad } y_1 = f_1(u_2) \xrightarrow{\qquad \qquad } u_1 = y_1 \xrightarrow{\qquad \qquad } y_2 = f_2(u_1) \xrightarrow{\qquad \qquad } u_2 = y_2$$

Inputs and outputs can depedent on space and time, i.e.,

$$\mathbf{u} = \mathbf{u}(\mathbf{r}, t)$$
 and $\mathbf{y} = \mathbf{y}(\mathbf{r}, t)$

Coupled systems II





J. Bastian, C. Clauß, S. Wolf, and P. Schneider. Master for co-simulation using FMI. In C. Clauß, editor, *Proceedings of the 8th International Modelica Conference*, Dresden, Germany, 2011.

Example: Pendulum as one Block





Each pendulum as Ordinary Differential Equation (ODE)

$$\ddot{\theta} = -\frac{q}{L} \cdot \sin(\theta) + \dots$$

with coordinates

 $x_1 = L \cdot \cos(\theta)$ $x_2 = L \cdot \sin(\theta)$

more general: Differential-Algebraic Equations (DAEs)

 $m \cdot \ddot{x_1} + 2\lambda \cdot x_1 = \dots,$ $m \cdot \ddot{x_2} + 2\lambda \cdot x_2 = \dots,$ $x_1^2 + x_2^2 = L^2$

Example: Cartesian Pendulum in Modelica





model PendulumIndexXX "PendulumIndexXX.mo"

```
emph/*emph emphConstantsemph emphandemph emphParametersemph emph*/
constant Modelica.Slunits.Acceleration g=9.81;
parameter Modelica.Slunits.Length 1(min=0)=1;
parameter Modelica.Slunits.Mass m=1;
```

```
emph/*emph emphVariablesemph emph*/
```

```
Modelica.Slunits.Position x1(start=0) ;
Modelica.Slunits.Position x2(start=-1) ;
Modelica.Slunits.Velocity v(start=1) ;
Modelica.Slunits.Velocity w(start=0) ;
Modelica.Slunits.Length lambda(start=(m*(i+1*g))/(2*1*1));
```

```
emph/*emph emphInputemph emphandemph emphOutputemph emphModelicaemph
emphinterfacesemph emph*/
```

```
output Modelica.Blocks.Interfaces.RealOutput xValue;
output Modelica.Blocks.Interfaces.RealOutput yValue;
```

equation

```
empl/*emph emphRESTRICTIONemph emphEQUATIONemph emphHEREemph emph*/
der(x1) = v;
der(x2) = u;
m * der(v) = -2 * x1 * lambda;
m * der(w) = -m * g - 2 * x2 * lambda;
xValue = x1;
yValue = x2;
```

DAEs and the Index



 many problems are not characterized by ODEs but differenital algebraic equations (DAEs), i.e.,

 $\dot{\mathbf{y}} = \mathbf{f}(t, \mathbf{y}, \mathbf{z})$

with an additional algebraic constraint

 $0 = \mathbf{g}(t, \mathbf{y}, \mathbf{z})$

with unknown $\mathbf{x} = [\mathbf{y}, \mathbf{z}]$.

DAEs and the Index



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the DAE index is the number of derivatives with respect to time that are needed to obtain an ODE from an DAE.

DAEs and the Index



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 $\dot{\mathbf{y}} = \mathbf{f}(t, \mathbf{y}, \mathbf{z})$

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 $0 = \mathbf{g}(t, \mathbf{y}, \mathbf{z})$

with unknown $\mathbf{x} = [\mathbf{y}, \mathbf{z}]$.

- the DAE index is the number of derivatives with respect to time that are needed to obtain an ODE from an DAE.
- high index problems are difficult to solve because errors are amplified (integration and differentiation).

Outline of the Talk





Introduction

- Coupled systems in time domain
 Double Pendulum
 Dynamic iteratation
- 3 Low-Frequency field-circuit coupling
- 4 Conclusions

Coupled systems in time domain





Coupled systems in time domain



Dynamic iteration / waveform relaxation



(requires synchronization points, inter and extrapolation!)

Simple Example: Double Pendulum (ODEs)



System of 2nd order Ordinary Differential Equations:

$$\ddot{\theta}_{1} = \frac{kl_{2}\sin(\theta_{2}) - kl_{1}\sin(\theta_{1}) + l_{1}m_{1}\dot{\theta}_{1}^{2}\sin(\theta_{1}) + gm_{1}\tan(\theta_{1})}{l_{1}m_{1}\cos(\theta_{1})}$$
$$\ddot{\theta}_{2} = \frac{kl_{1}\sin(\theta_{1}) + l_{2}m_{2}\dot{\theta}_{2}^{2}\sin(\theta_{2}) - \tan(\theta_{2})(gm_{2} + kl_{2}\cos(\theta_{2}))}{l_{2}m_{2}\cos(\theta_{2})}$$



- **unknowns**: angles θ_{\star}
- **parameters**: masses m_{\star} , length I_{\star} and gravitation *g*.
- **initial values**: θ_{\star} and $\dot{\theta}_{\star}$

Simple Example: Double Pendulum (ODEs)



System of 2nd order Ordinary Differential Equations:

 $\ddot{\theta}_{1}^{(k)} = \frac{k l_{2} \sin \left(\theta_{2}^{(k-1)}(t)\right) - k l_{1} \sin \left(\theta_{1}\right) + l_{1} m_{1} \dot{\theta}_{1}^{2} \sin \left(\theta_{1}\right) + g m_{1} \tan \left(\theta_{1}\right)}{l_{1} m_{1} \cos \left(\theta_{1}\right)}$ $\ddot{\theta}_{2}^{(k)} = \frac{k l_{1} \sin \left(\theta_{1}^{(k)}(t)\right) + l_{2} m_{2} \dot{\theta}_{2}^{2} \sin \left(\theta_{2}\right) - \tan \left(\theta_{2}\right) \left(g m_{2} + k l_{2} \cos \left(\theta_{2}\right)\right)}{l_{2} m_{2} \cos \left(\theta_{2}\right)}$



- **unknowns**: angles θ_{\star}
- **parameters**: masses m_{\star} , length I_{\star} and gravitation *g*.
- **initial values**: θ_{\star} and $\dot{\theta}_{\star}$
- dynamic iteration: Gauss-Seidel scheme with k = 1, ..., N sweeps for a single time window

Simple Example: Double Pendulum (ODEs)



System of 2nd order Ordinary Differential Equations:

$$\ddot{\theta}_{1} = \frac{kl_{2}\sin(\theta_{2}) - kl_{1}\sin(\theta_{1}) + l_{1}m_{1}\dot{\theta}_{1}^{2}\sin(\theta_{1}) + gm_{1}\tan(\theta_{1})}{l_{1}m_{1}\cos(\theta_{1})}$$

$$\ddot{\theta}_{2} = \frac{kl_{1}\sin(\theta_{1}) + l_{2}m_{2}\dot{\theta}_{2}^{2}\sin(\theta_{2}) - \tan(\theta_{2})(gm_{2} + kl_{2}\cos(\theta_{2}))}{l_{2}m_{2}\cos(\theta_{2})}$$



- **unknowns**: angles θ_{\star}
 - **parameters**: masses m_{\star} , length I_{\star} and gravitation *g*.
- **initial values**: θ_{\star} and $\dot{\theta}_{\star}$
- dynamic iteration: Gauss-Seidel

Convergence

Super-linear convergence for ODEs (bounded right-hand-sides *f*).

Waveform Relaxation: Playing with the loops



possible application to CUDI (Arjan Verweij's talk):

- Loop for parametric sweep
 - Iterate with different h_{ext} to calculate the Minimum Quench Energy
 - Loop through all time steps

each problem gets it's own time step terate until the time step is small enough

- Iterate until the electrical module has converged
 - Iterate until the thermal module has converged
 - Loop over all the bands of the cable

move[´]time Loop here

- Loop over all the strand sections of a band
 - Iterate until the temperatures of the section and the adjacent helium have converged

ecouple



Index-1 systems

$$\dot{\mathbf{y}}_i = \mathbf{f}_i(\mathbf{y}, \mathbf{z}), \quad 0 = \mathbf{g}_i(\mathbf{y}, \mathbf{z}) \text{ with } \det \partial_{\mathbf{z}_i} \mathbf{g}_i \neq 0, \qquad i = 1, \dots, n$$



Index-1 systems

Errors

$$\dot{\mathbf{y}}_{i}^{(k+1)} = \mathbf{F}_{i}(\mathbf{y}^{(k+1)}, \mathbf{z}^{(k+1)}, \mathbf{y}^{(k)}, \mathbf{z}^{(k)}), \quad 0 = \mathbf{G}_{i}(\mathbf{y}^{(k+1)}, \mathbf{z}^{(k+1)}, \mathbf{y}^{(k)}, \mathbf{z}^{(k)})$$

differential splitting error $\delta_v^{(k)}$

■ algebraic splitting error $\delta_z^{(k)}$



Index-1 systems

$$\dot{\mathbf{y}}_{i}^{(k+1)} = \mathbf{F}_{i}(\mathbf{y}^{(k+1)}, \mathbf{z}^{(k+1)}, \mathbf{y}^{(k)}, \mathbf{z}^{(k)}), \quad \mathbf{0} = \mathbf{G}_{i}(\mathbf{y}^{(k+1)}, \mathbf{z}^{(k+1)}, \mathbf{y}^{(k)}, \mathbf{z}^{(k)})$$

Errors

differential splitting error $\delta_{V}^{(k)}$

algebraic splitting error $\delta_z^{\scriptscriptstyle (k)}$

Fixed point iteration

$$\begin{bmatrix} \delta_{y}^{(k+1)} \\ \delta_{z}^{(k+1)} \end{bmatrix} \leq \begin{bmatrix} \mathcal{O}(H) & \mathcal{O}(H) \\ \beta + \mathcal{O}(H) & \alpha + \mathcal{O}(H) \end{bmatrix} \begin{bmatrix} \delta_{y}^{(k)} \\ \delta_{z}^{(k)} \end{bmatrix} + \text{"error in initial values"}$$



Index-1 systems

$$\dot{\mathbf{y}}_{i}^{(k+1)} = \mathbf{F}_{i}(\mathbf{y}^{(k+1)}, \mathbf{z}^{(k+1)}, \mathbf{y}^{(k)}, \mathbf{z}^{(k)}), \quad 0 = \mathbf{G}_{i}(\mathbf{y}^{(k+1)}, \mathbf{z}^{(k+1)}, \mathbf{y}^{(k)}, \mathbf{z}^{(k)})$$

Errors

differential splitting error $\delta_{V}^{(k)}$

algebraic splitting error $\delta_z^{(k)}$

Fixed point iteration

$$\begin{bmatrix} \delta_{y}^{(k+1)} \\ \delta_{z}^{(k+1)} \end{bmatrix} \leq \begin{bmatrix} \mathcal{O}(H) & \mathcal{O}(H) \\ \beta + \mathcal{O}(H) & \alpha + \mathcal{O}(H) \end{bmatrix} \begin{bmatrix} \delta_{y}^{(k)} \\ \delta_{z}^{(k)} \end{bmatrix} + \text{"error in initial values"}$$

Theorem (Contraction)

The iteration converges if the coupling between old and new algebraic variables is weak: $\alpha = \left\| \left(\frac{\partial G}{\partial z^{(k+1)}} \right)^{-1} \frac{\partial G}{\partial z^{(k)}} \right\| < 1$ because "convergence rate" = "spectral radius" r < 1

Optimal Time Discretization Order



The splitting error on the *i*-th time window is

$$\delta_{\mathbf{y},i}^{k} = \mathcal{O}(H^{pk})$$

where *p* is:

- (a) for a coupled system of 2 DAEs with only differential coupling
- (b) for a DAE with no algebraic-to-algebraic coupling
- (c) for a general DAE

Thus the optimal order for the numerical time integration is:

$$q \ge p \cdot k$$
.

with the total error (splitting + time discretization)

$$\left\|\tilde{\mathbf{x}}^{(k)}-\mathbf{x}\right\|=\mathcal{O}(H^{pk})+\mathcal{O}(m\cdot h^q)=\mathcal{O}(H^{pk}).$$

where $m < \infty$ is the number of (local) time steps.

p = 2,p = 1,p = 0.

Outline of the Talk

MaxwellCircuit couplingExample

3 Low-Frequency field-circuit coupling



MANN

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 \vec{J} [A/m²]

 \vec{H} [A/m]







where $\mu^{-1} = \nu(|\mathbf{B}|)$ is nonlinear.

■ introduction of potentials, e.g. magnetic vector potential B = ∇ × A





differential formulation $\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} ,$ $\nabla \cdot \mathbf{B} = 0 ,$ $\nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t} + \mathbf{J} ,$ $\nabla \cdot \mathbf{D} = \rho .$ with material laws

 $\mathbf{J} = \sigma \mathbf{E}$, $\mathbf{D} = \varepsilon \mathbf{E}$, $\mathbf{H} = \mu^{-1} \mathbf{B}$ where $\mu^{-1} = \nu(|\mathbf{B}|)$ is nonlinear.

■ introduction of potentials, e.g. magnetic vector potential B = ∇ × A







■ reformulate Maxwell in terms of magnetic vector potential A with B = ∇ × A

hyperbolic curl-curl equation on Ω

$$\varepsilon \frac{\partial^2}{\partial t^2} \mathbf{A} + \sigma \frac{\partial}{\partial t} \mathbf{A} + \nabla \times \left(\nu \left(|\nabla \times \mathbf{A}| \right) \nabla \times \mathbf{A} \right) = -\sigma \nabla \varphi \ - \ \varepsilon \frac{\partial}{\partial t} \nabla \varphi$$





■ reformulate Maxwell in terms of magnetic vector potential A with B = $\nabla \times A$

Iow frequency: max |∂/∂t D| ≪ max |J| → disregard displacement currents

parabolic / elliptic curl-curl equation on Ω

$$\frac{\partial^{2}}{\partial t^{2}} \mathbb{A} + \sigma \frac{\partial}{\partial t} \mathbf{A} + \nabla \times \left(\nu \left(|\nabla \times \mathbf{A}| \right) \nabla \times \mathbf{A} \right) = -\sigma \nabla \varphi - \varepsilon \frac{\partial}{\partial t} \nabla \varphi$$





- reformulate Maxwell in terms of magnetic vector potential A with B = $\nabla \times A$
- Iow frequency: max |∂/∂t D| ≪ max |J| → disregard displacement currents
- homogeneous Dirichlet BC on Γ

parabolic / elliptic curl-curl equation on Ω

$$\sigma \frac{\partial}{\partial t} \mathbf{A} + \nabla \times \left(\nu \left(|\nabla \times \mathbf{A}| \right) \nabla \times \mathbf{A} \right) = -\sigma \nabla \varphi \qquad \mathbf{A}_t|_{\Gamma} = \mathbf{0}$$





- reformulate Maxwell in terms of magnetic vector potential A with B = ∇ × A
- Iow frequency: max |∂/∂t D| ≪ max |J| → disregard displacement currents
- homogeneous Dirichlet BC on Γ
- **excitation** by spatially distributed current density $\mathbf{J}_{\text{src}} := -\sigma \nabla \varphi$

parabolic / elliptic curl-curl equation on Ω

$$\sigma \frac{\partial}{\partial t} \mathbf{A} + \nabla \times \left(\nu \left(|\nabla \times \mathbf{A}| \right) \nabla \times \mathbf{A} \right) = \mathbf{J}_{\text{src}} \qquad \mathbf{A}_t|_{\Gamma} = \mathbf{0}$$





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- exhibits eddy currents where $\sigma > 0$

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$$\sigma \frac{\partial}{\partial t} \mathbf{A} + \nabla \times \left(\nu \left(|\nabla \times \mathbf{A}| \right) \nabla \times \mathbf{A} \right) = \mathbf{J}_{\text{src}} \qquad \mathbf{A}_t |_{\Gamma} = \mathbf{0}$$

the system is elliptic in subdomains where σ = 0





- reformulate Maxwell in terms of magnetic vector potential A with B = ∇ × A
- Iow frequency: max |∂/∂t D| ≪ max |J| → disregard displacement currents
- homogeneous Dirichlet BC on Γ
- excitation by spatially distributed current density $\mathbf{J}_{\mathrm{src}} \coloneqq -\sigma \nabla \varphi$
- exhibits eddy currents where $\sigma > 0$
- **2**D reduction: **A** = $[0, 0, u(x_1, x_2)]^{\top}$

parabolic / elliptic curl-curl equation on Ω

$$\sigma \frac{\partial}{\partial t} u - \nabla \cdot \left(\nu \left(|\nabla u| \right) \nabla u \right) = J_{z} \qquad u|_{\Gamma} = 0$$

the system is elliptic in subdomains where σ = 0

Field-Circuit Coupling





Weak formulation: find $u(\mathbf{x}) \in H_0^1(\Omega)$ with $u_i = u|_{\Omega_i}$ such that $\forall v \in H_0^1(\Omega)$

$$\int_{\Omega_1} \left(\sigma_1 \frac{\partial u_1}{\partial t} \mathbf{v} + \nu_1 \nabla u_1 \cdot \nabla \mathbf{v} \right) d\mathbf{x} + \int_{\Omega_0} \nu_0 \nabla u_0 \cdot \nabla \mathbf{v} \, d\mathbf{x} = \int_{\Omega_0} \mathbf{\chi}^{\mathsf{T}} \mathbf{i}_{\mathsf{M}} \mathbf{v} \, d\mathbf{x},$$

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Introduction to electric circuits from differenial forms perspective

P. Bamberg and S. Sternberg, A course in mathematics for students of physics, Volume 2.



$$\mathbf{L}_{\mathsf{M}}\frac{\mathsf{d}}{\mathsf{d}t}\mathbf{i}_{\mathsf{M}} + \mathbf{R}_{\mathsf{M}}\mathbf{i}_{\mathsf{M}} + \mathbf{v}_{\mathsf{M}}(u_1) = \mathbf{v}_{\mathsf{M}}$$



[De Gersem, S., 2013]



$$\mathbf{L}_{\mathsf{M}}\frac{\mathsf{d}}{\mathsf{d}t}\mathbf{i}_{\mathsf{M}} + \mathbf{R}_{\mathsf{M}}\mathbf{i}_{\mathsf{M}} + \mathbf{v}_{\mathsf{M}}(u_{1}) = \mathbf{v}_{\mathsf{M}}$$

with constant inductance

$$\mathbf{L}_{\mathsf{M}} \coloneqq \int_{\Omega_0} \boldsymbol{\chi} \left(\nabla \cdot \boldsymbol{\nu} \nabla \right)^{-1} \boldsymbol{\chi} \, \, \mathrm{d} \mathbf{x}$$

Primary Side Dual Side -grad div ε, σ \vec{J}, \vec{D} AM curl curl +L Ĥ \mathbf{B}_{M} $\mathbf{B}_{\mathrm{M}}^{\mathsf{T}}$ div -grad 0 0

(s.p.d.) $\mathbf{A}_{\mathrm{M}}^{\mathsf{T}}$ VM



Primary Side -grad (s.p.d.) ε. σ $\mathbf{A}_{\mathrm{M}}^{\mathsf{T}}$ \mathbf{A}_{M} curl VM (diag.) \mathbf{B}_{M}^{T} \mathbf{B}_{M} div 0 0

Interface equation in matrix-form

$$\mathbf{L}_{\mathsf{M}}\frac{\mathsf{d}}{\mathsf{d}t}\mathbf{i}_{\mathsf{M}} + \mathbf{R}_{\mathsf{M}}\mathbf{i}_{\mathsf{M}} + \mathbf{v}_{\mathsf{M}}(u_{1}) = \mathbf{v}_{\mathsf{M}}$$

$$\mathbf{L}_{\mathsf{M}} \coloneqq \int_{\Omega_0} \boldsymbol{\chi} \left(\nabla \cdot \boldsymbol{\nu} \nabla \right)^{-1} \boldsymbol{\chi} \, \, \mathrm{d} \mathbf{x}$$

constant resistance

$$\mathbf{R}_{\mathrm{M}} \coloneqq \int_{\Omega_0} \boldsymbol{\chi} \sigma^{-1} \boldsymbol{\chi}^{\mathrm{T}} \, \mathrm{d} \mathbf{x},$$

with constant inductance

[De Gersem, S., 2013] Dual Side

div

 \vec{J}, \vec{D}

curl

Ĥ

-grad





[De Gersem, S., 2013]

Numerical Example – Rectifier

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Conclusions

- dynamic iteration is the justification of many ad-hoc approaches
- Iterative coupling schemes ensure stability and are essential for high accuracy (→ splitting error)
- You can play with the time stepping loop (sometimes it can be skipped...)
- Implementation effort of iterative coupling is only one additional loop
- Convergence cannot be taken for granted
- Mathematical verification by fixed point analysis
- Clever modeling can overcome divergence (similar to sophisticated interface conditions in Domain Decomposition)





Conclusions

- dynamic iteration is the justification of many ad-hoc approaches
- Iterative coupling schemes ensure stability and are essential for high accuracy (→ splitting error)
- You can play with the time stepping loop (sometimes it can be skipped...)
- Implementation effort of iterative coupling is only one additional loop
- Convergence cannot be taken for granted
- Mathematical verification by fixed point analysis
 Final question

When to update which model?







[any DAE textbook, Mattsson 1993]

"Physical" model

DAE INDEX 3

$\begin{aligned} x_1^2 + x_2^2 &= l^2 \\ m\ddot{x}_1 &= -(\lambda/L)x_1 \\ m\ddot{x}_2 &= -(\lambda/L)x_2 \ mg \end{aligned}$

g force of gravity, λ is a Lagrange multiplier; $(\lambda/L)x_i$ represent the force which holds the solution onto the constraint



[any DAE textbook, Mattsson 1993]

"Physical" model

DAE index 3

$$x_1^2 + x_2^2 = l^2$$

$$m\dot{x}_3 = -(\lambda/L)x_1$$

$$m\dot{x}_4 = -(\lambda/L)x_2 mg$$

$$\dot{x}_1 = x_3$$

$$\dot{x}_2 = x_4$$

g force of gravity, λ is a Lagrange multiplier; $(\lambda/L)x_i$ represent the force which holds the solution onto the constraint



[anv DAE textbook, Mattsson 1993]

"Physical" model DAF index 3

Manual reduction DAF index 2



$$2x_1 \cdot x_3 = -2x_2 \cdot x_4$$

$$m\dot{x}_3 = -(\lambda/L)x_1$$

$$m\dot{x}_4 = -(\lambda/L)x_2 mg$$

$$\dot{x}_1 = x_3$$

$$\dot{x}_2 = x_4$$

derviative w.r.t. time

g force of gravity, λ is a Lagrange multiplier; $(\lambda/L)x_i$ represent the force which holds the solution onto the constraint



[any DAE textbook, Mattsson 1993]



g force of gravity, λ is a Lagrange multiplier; $(\lambda/L)x_i$ represent the force which holds the solution onto the constraint

Example: Pendulum (Drift-Off)



[any DAE textbook, Mattsson 1993]



Example: Pendulum (Drift-Off)



[any DAE textbook, Mattsson 1993]





Find magnetic vector potential A and temperature T

$$\int_{\Omega} \left(\left(\epsilon \frac{\partial^2 \mathbf{A}}{\partial t^2} + \sigma(T) \frac{\partial \mathbf{A}}{\partial t} \right) \cdot \mathbf{w} + \nu \nabla \times \mathbf{A} \cdot \nabla \times \mathbf{w} \right) d\mathbf{x} - \int_{\Omega} \mathbf{J}_{\text{src}} \cdot \mathbf{w} \, d\mathbf{x} = 0$$
$$\forall \mathbf{v} \in H_0^1(\Omega)$$

$$\int_{\Omega} \left(\rho c \frac{\partial T}{\partial t} \mathbf{v} - k \nabla T \cdot \nabla \mathbf{v} \right) d\mathbf{x} - \int_{\Omega} Q \left(T, \frac{\partial \mathbf{A}}{\partial t} \right) \mathbf{v} \, d\mathbf{x} = 0$$



Find magnetic vector potential A and temperature T

 $\forall w \in H_0(curl; \Omega)$

$$\int_{\Omega} \left(\left(\epsilon \frac{\partial^2 \mathbf{A}^{(k)}}{\partial t^2} + \sigma (\mathcal{T}^{(k-1)}) \frac{\partial \mathbf{A}^{(k)}}{\partial t} \right) \cdot \mathbf{w} + \nu \nabla \times \mathbf{A}^{(k)} \cdot \nabla \times \mathbf{w} \right) d\mathbf{x} - \int_{\Omega} \mathbf{J}_{\text{src}} \cdot \mathbf{w} \, d\mathbf{x} = 0$$
$$\forall \mathbf{v} \in H_0^1(\Omega)$$

$$\int_{\Omega} \left(\rho c \frac{\partial T^{(k)}}{\partial t} v - k \nabla T^{(k)} \cdot \nabla v \right) d\mathbf{x} - \int_{\Omega} Q \left(T^{(k-1)}, \frac{\partial \mathbf{A}^{(k)}}{\partial t} \right) v \, d\mathbf{x} = 0$$

apply dynamic iteration scheme



Find magnetic vector potential A and temperature T

$$\int_{\Omega} \left(\left(\epsilon \frac{\partial^2 \mathbf{A}^{(k)}}{\partial t^2} + \sigma^{(k-1)} \frac{\partial \mathbf{A}^{(k)}}{\partial t} \right) \cdot \mathbf{w} + \nu \nabla \times \mathbf{A}^{(k)} \cdot \nabla \times \mathbf{w} \right) d\mathbf{x} - \int_{\Omega} \mathbf{J}_{\text{src}} \cdot \mathbf{w} \, d\mathbf{x} = 0$$

$$\forall \nu \in H_0^1(\Omega)$$

$$\int_{\Omega} \left(\rho c \frac{\partial T^{(k)}}{\partial t} v - k \nabla T^{(k)} \cdot \nabla v \right) d\mathbf{x} - \int_{\Omega} Q \left(T^{(k-1)}, \frac{\partial \mathbf{A}^{(k)}}{\partial t} \right) v \, d\mathbf{x} = 0$$

- apply dynamic iteration scheme
- average conductivity $\bar{\sigma}^{(k-1)} := \frac{1}{T} \int_T \sigma(T^{(k-1)}(t)) dt$ for each sweep k



Find magnetic vector potential \mathbf{A} and temperature \mathcal{T}

$$\int_{\Omega} \left(\left(\omega^2 \epsilon \frac{\partial^2 \mathbf{A}^{(k)}}{\partial t^2} \mathbf{A}^{(k)} + j \omega \sigma^{(k-1)} \mathbf{A}^{(k)} \right) \cdot \mathbf{w} + \nu \nabla \times \mathbf{A}^{(k)} \cdot \nabla \times \mathbf{w} \right) d\mathbf{x} - \int_{\Omega} \mathbf{J}_{\text{src}} \cdot \mathbf{w} \, d\mathbf{x} = 0$$
$$\forall \mathbf{v} \in H_0^1(\Omega)$$

$$\int_{\Omega} \left(\rho c \frac{\partial T^{(k)}}{\partial t} v - k \nabla T^{(k)} \cdot \nabla v \right) d\mathbf{x} - \int_{\Omega} Q \left(T^{(k-1)}, \mathbf{A}^{(k)} \right) v \, d\mathbf{x} = 0$$

- apply dynamic iteration scheme
- average conductivity $\bar{\sigma}^{(k-1)} := \frac{1}{T} \int_T \sigma(T^{(k-1)}(t)) dt$ for each sweep k
- **assume sinusoidal current exication** $\mathbf{J}_{src} \sim \sin(\omega t) \rightarrow \mathbf{frequency}$ domain



Find magnetic vector potential A and temperature T

$$\int_{\Omega} \left(\left(\epsilon \mathbf{A}^{(k)} + j\omega\sigma^{(k-1)}\mathbf{A}^{(k)} \right) \cdot \mathbf{w} + \nu\nabla \times \mathbf{A}^{(k)} \cdot \nabla \times \mathbf{w} \right) d\mathbf{x} - \int_{\Omega} \mathbf{J}_{\text{src}} \cdot \mathbf{w} \, d\mathbf{x} = 0$$
$$\forall \mathbf{v} \in H_0^1(\Omega)$$

$$\int_{\Omega} \left(\rho c \frac{\partial T^{(k)}}{\partial t} v - k \nabla T^{(k)} \cdot \nabla v \right) d\mathbf{x} - \int_{\Omega} Q \left(T^{(k-1)}, \mathbf{A}^{(k)} \right) v \, d\mathbf{x} = 0$$

- apply dynamic iteration scheme
- average conductivity $\bar{\sigma}^{(k-1)} := \frac{1}{T} \int_T \sigma(T^{(k-1)}(t)) dt$ for each sweep k
- **a** assume sinusoidal current exication $\mathbf{J}_{\mathrm{src}} \sim \sin(\omega t) \rightarrow$ frequency domain
- space and time discretization (FIT, Cell Method, FEM; implicit Euler, RK, ...)



Find magnetic vector potential A and temperature T

 $\forall w \in H_0(curl; \Omega)$

$$\int_{\Omega} \left(\left(\epsilon \mathbf{A}^{(k)} + j\omega\sigma^{(k-1)}\mathbf{A}^{(k)} \right) \cdot \mathbf{w} + \nu\nabla \times \mathbf{A}^{(k)} \cdot \nabla \times \mathbf{w} \right) d\mathbf{x} - \int_{\Omega} \mathbf{J}_{\text{src}} \cdot \mathbf{w} \, d\mathbf{x} = 0$$
$$\forall \mathbf{v} \in H_0^1(\Omega)$$

$$\int_{\Omega} \left(\rho c \frac{\partial T^{(k)}}{\partial t} v - k \nabla T^{(k)} \cdot \nabla v \right) d\mathbf{x} - \int_{\Omega} Q \left(T^{(k-1)}, \mathbf{A}^{(k)} \right) v \, d\mathbf{x} = 0$$

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P. Alotto, F. Freschi, M. Repetto. Multiphysics Problems via the Cell Method: The Role of Tonti Diagrams, 2010.

Motivation: Inductive Charging of Electric Cars



ICNIRP based recommendation

[Kaufmann et al. (with KOSTAL), 2014]



Source: Elektrische Ausrüstung von Elektro-Straßenfahrzeugen Induktive Ladung von Elektrofahrzeugen - Teil 4-2: Niedriger Leistungsbereich. German. VDE-AR-E 2122-4-2. 2011.

Public area: $|\mathbf{B}| \le 6.25 \,\mu\text{T}$ Functional area: test object must not heat up above 80°C.

Coupling in time domain (2 systems)





Coupling in time domain (2 systems)



Dynamic iteration / waveform relaxation



(requires synchronization points, inter and extrapolation!)

Numerical Example with Comsol





simulation time (20 min):

- frequency-transient model: 7 s
- purely transient model: ca. 2 years

time steps (for 20 min):

- frequency-transient model: 17
- purely transient model: ca. 250 · 10⁶
- without window iteration: 290° C, i.e., $\leq 3\%$ error.
- when using implicit Euler: one iteration is sufficient for $\mathcal{O}(H)$