

Improved method for quark polarization in non-central nuclear collisions

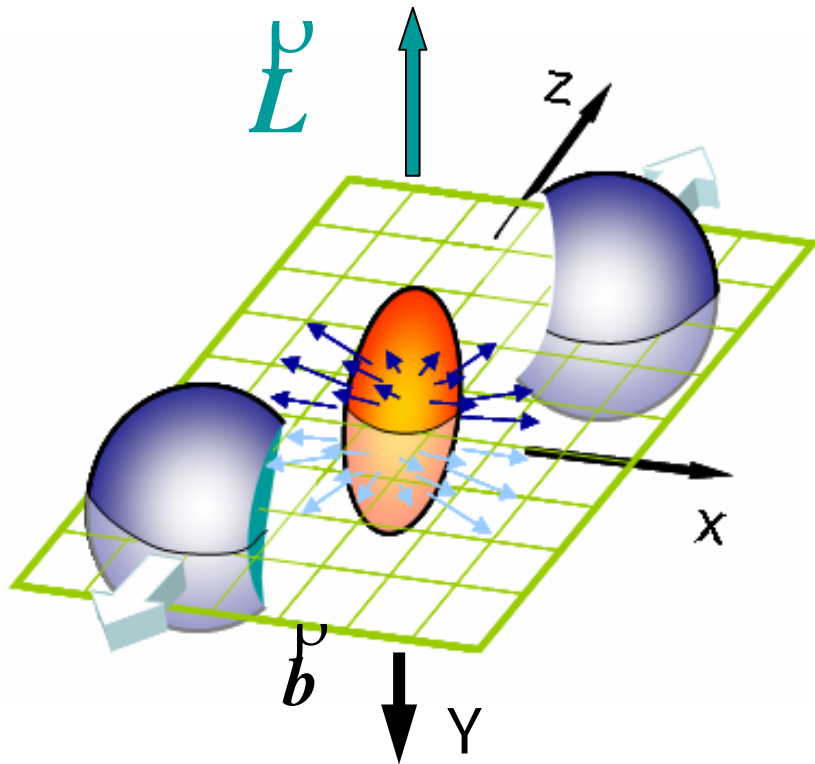
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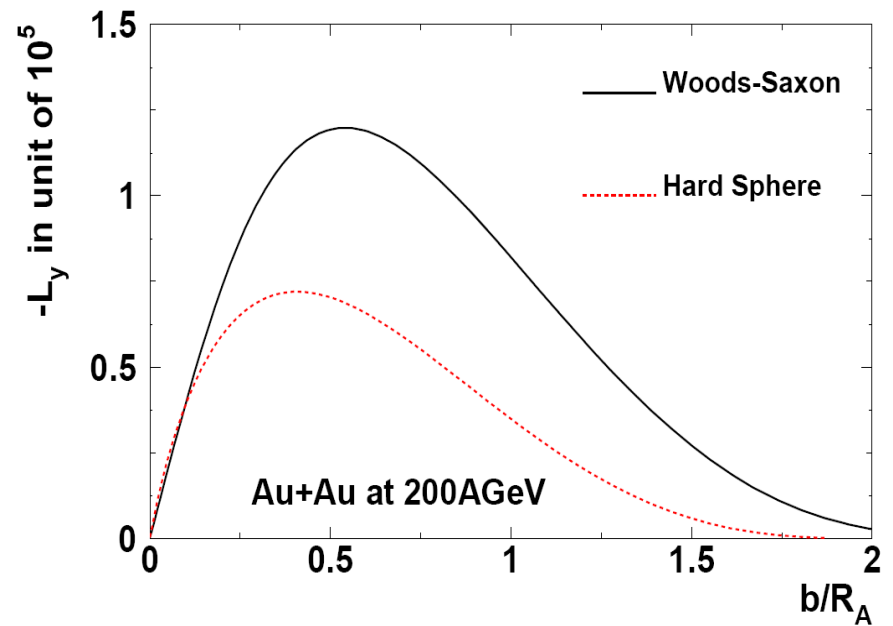
- ❖ Introduction
 - ❖ Calculation method of global quark polarization
 - ❖ Improved treatment
 - ❖ Conclusion
-
- J.H. Gao, S.W. Chen, W.T. Deng, Z.T. Liang, QW, X.N. Wang, Phys.Rev.C77:044902,2008.
 - S.W. Chen, J. Deng, J.H. Gao, QW, arXiv:0803.4360

International workshop on heavy ion physics at LHC, May 21-24, 2008

Global Orbital Angular Momentum

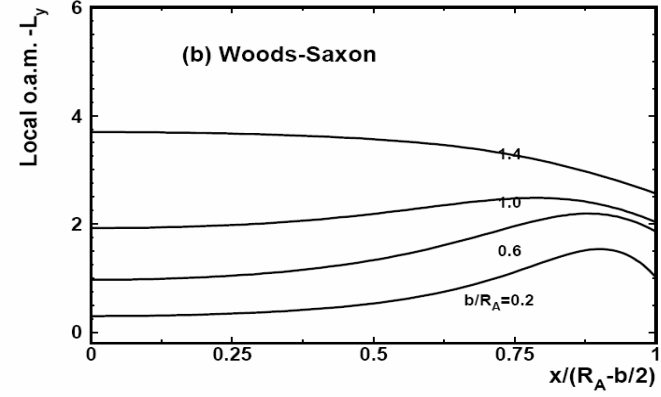
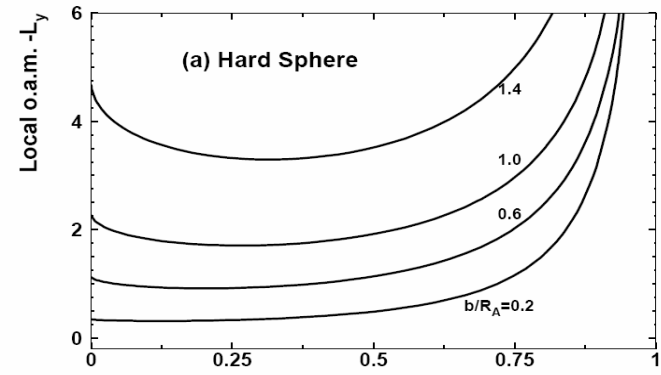
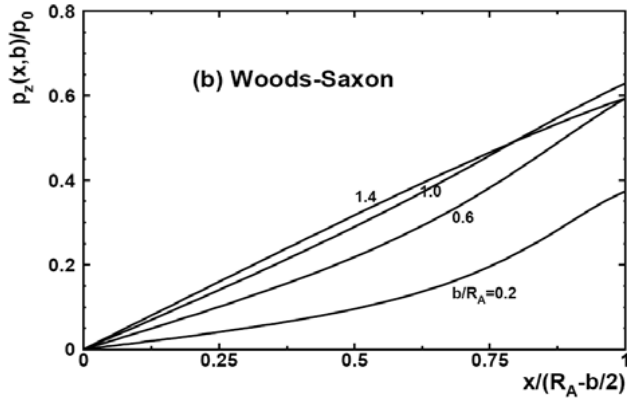
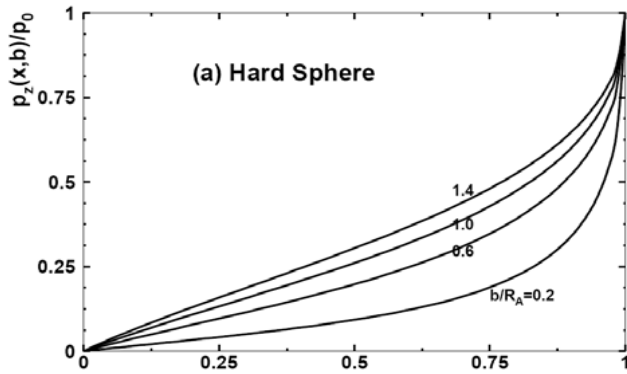
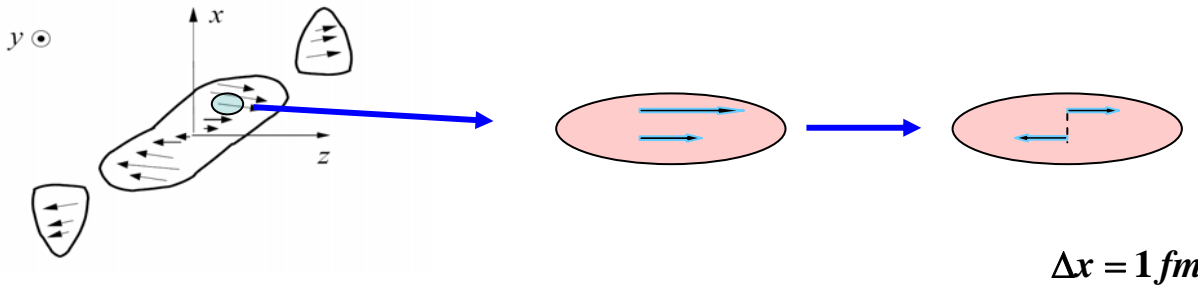


reaction plane $\mathbf{n}_b = \frac{\mathbf{p} \times \mathbf{b}}{|\mathbf{p} \times \mathbf{b}|}$

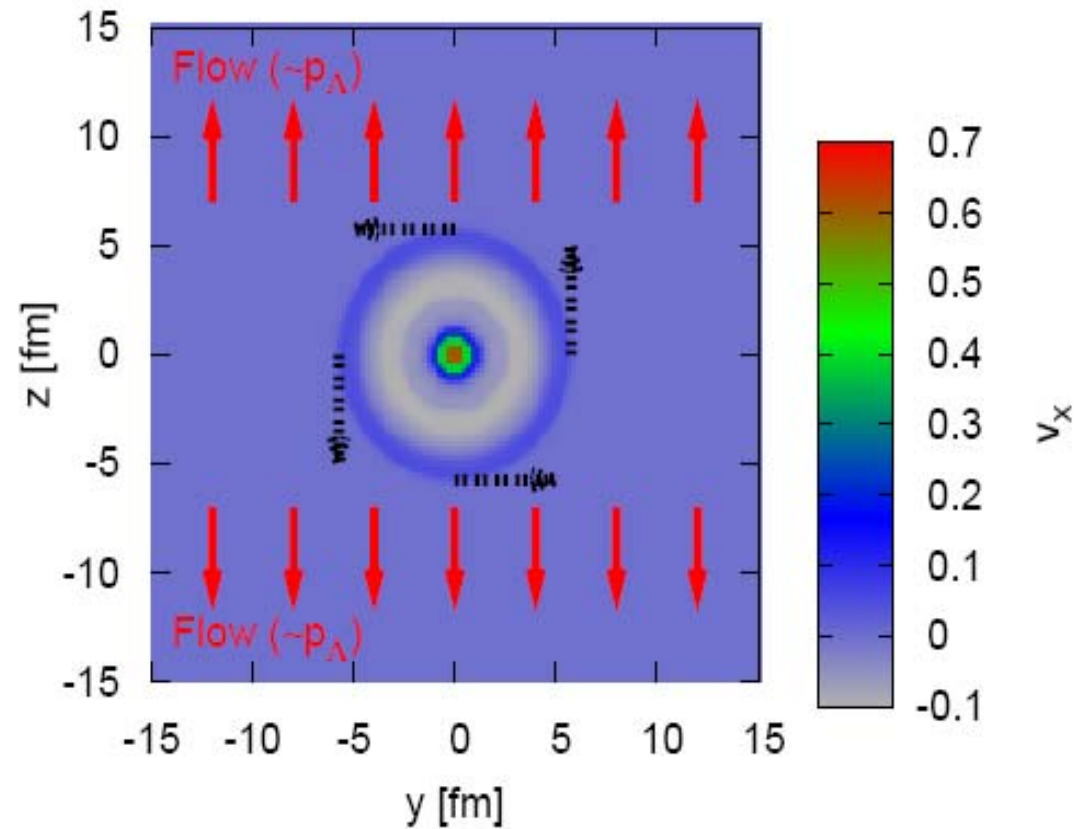
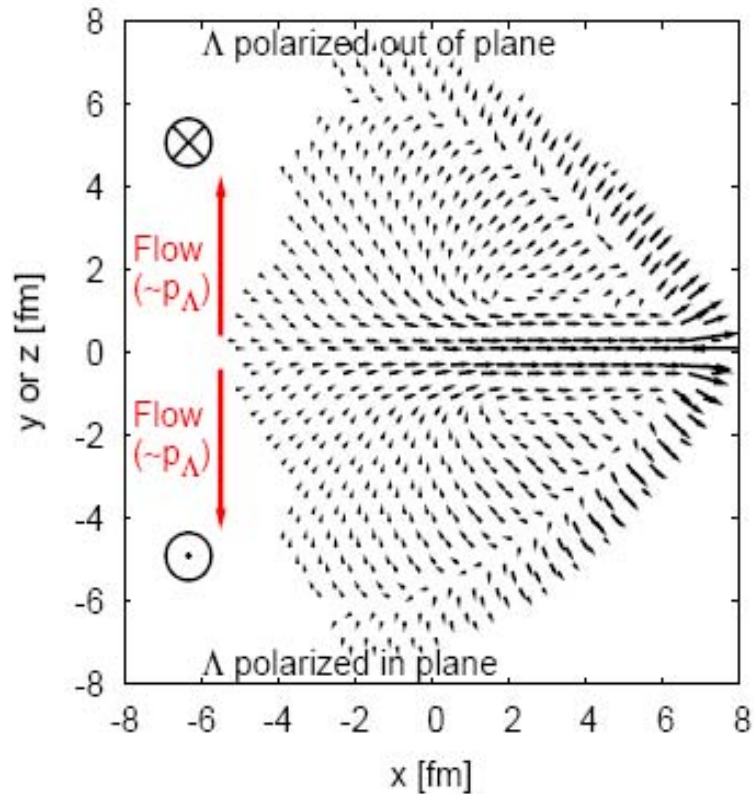


Z.T. Liang, X.N. Wang,
Phys. Rev. Lett. 94,102301(2005)

Longitudinal Fluid Shear

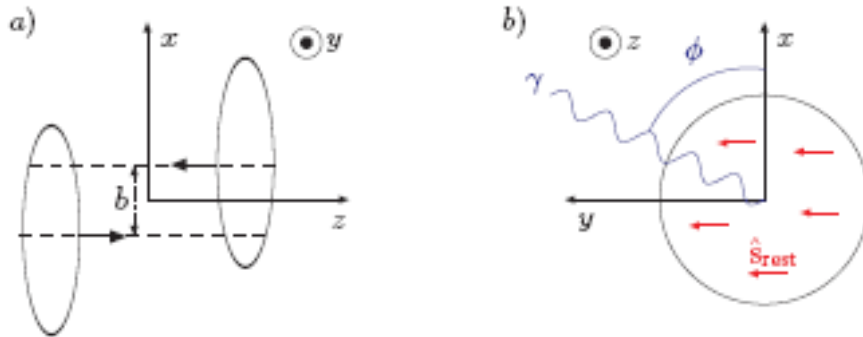
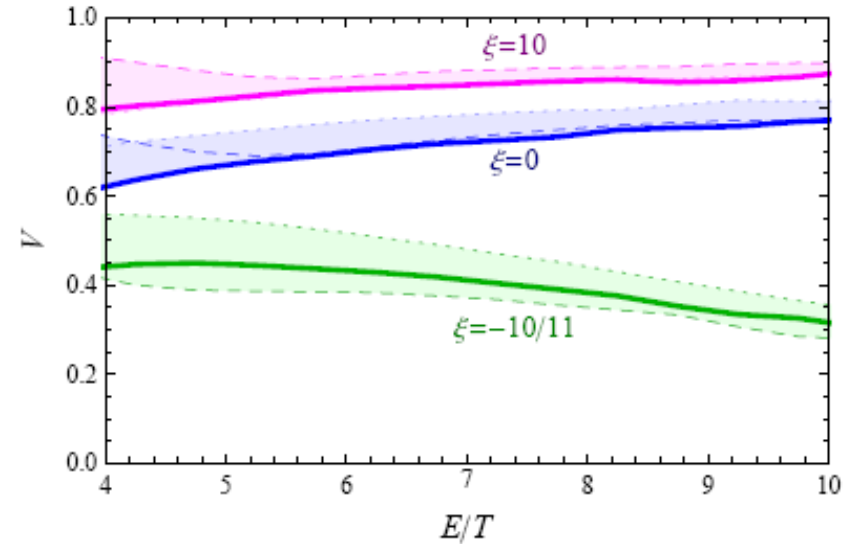
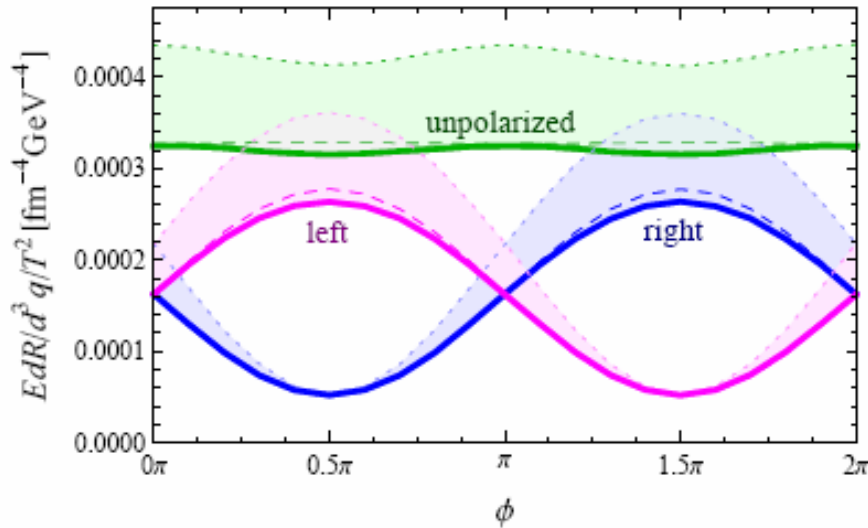


Related problem: Jet induced polarization



B.Betz, M.Gyulassy, G.Torrieri, Phys.Rev.C76:044901,2007

Induced photon Polarization

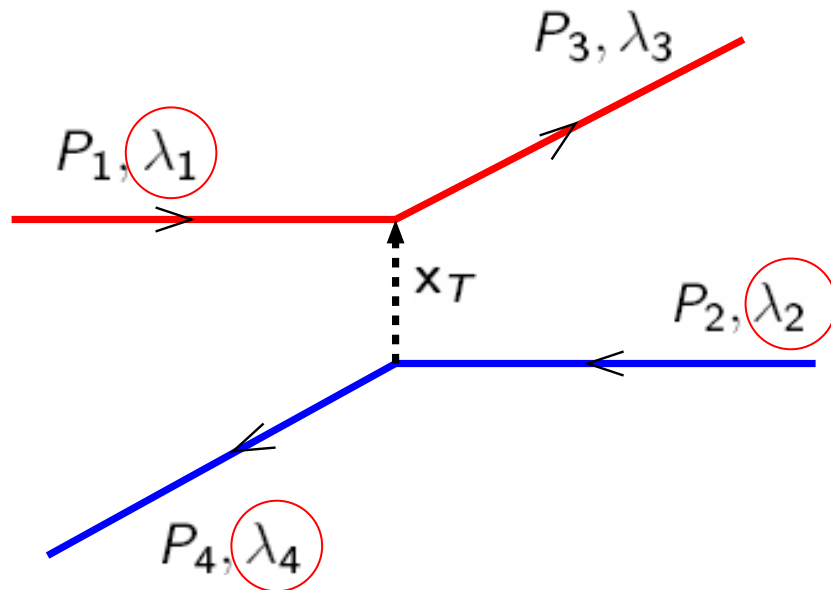


circularly polarized photon

$$qg \rightarrow q\gamma \quad (\bar{q}g \rightarrow \bar{q}\gamma)$$

A.Ipp, A.D.Piazza, J.Evers,
C.H.Keitel, arXiv:0710.5700

Collision configuration



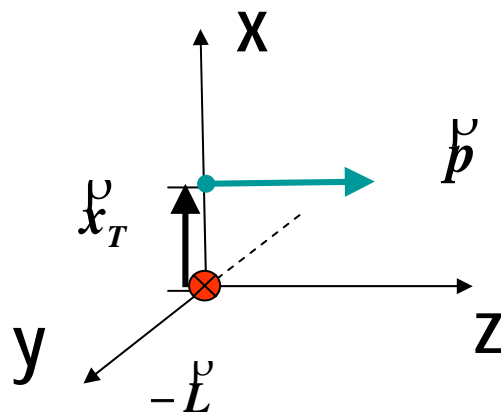
$$P_1 = (E_1, \mathbf{0}_T, p_{1z})$$

$$P_2 = (E_2, \mathbf{0}_T, p_{2z})$$

$$P_3 = (E_3, \mathbf{p}_T, p_{3z})$$

$$P_4 = (E_4, -\mathbf{p}_T, p_{4z})$$

$$\lambda_i = \begin{cases} +, \odot \\ -, \otimes \end{cases}$$



Spin inclusive process

$$\lambda_1, \lambda_2, \lambda_4$$



Summed


$$\lambda_3$$

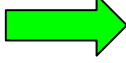


Kept

Calculation Formalism

cross section depends on polarization

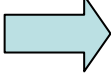
polarized cross section: 
$$\frac{d^2\sigma_\lambda}{d^2\mathbf{x}_T} = \frac{d^2\sigma}{d^2\mathbf{x}_T} + \lambda \frac{d^2\Delta\sigma}{d^2\mathbf{x}_T}$$

un-polarized cross section: 
$$\frac{d^2\sigma}{d^2\mathbf{x}_T} = \frac{1}{2} \left(\frac{d^2\sigma_+}{d^2\mathbf{x}_T} + \frac{d^2\sigma_-}{d^2\mathbf{x}_T} \right)$$

$$\frac{d^2\Delta\sigma}{d^2\mathbf{x}_T} = \frac{1}{2} \left(\frac{d^2\sigma_+}{d^2\mathbf{x}_T} - \frac{d^2\sigma_-}{d^2\mathbf{x}_T} \right)$$

Total polarized and un-polarized cross section:
$$\sigma = \int_0^\infty dx \int_{-\infty}^\infty dy \frac{d^2\sigma}{d^2\mathbf{x}_T}$$

$$\Delta\sigma = \int_0^\infty dx \int_{-\infty}^\infty dy \frac{d^2\Delta\sigma}{d^2\mathbf{x}_T}$$


$$P_q = \frac{\Delta\sigma}{\sigma}$$

Ambiguity in conventional method

Differential cross section for

$$1(P_1\lambda_1) + 2(P_2\lambda_2) \longrightarrow 3(P_3\lambda_3) + 4(P_4\lambda_4)$$

$$d\sigma = \frac{1}{16|P_1 \cdot P_2|} \sum_{\lambda_1, \lambda_2, \lambda_4} |M(P_1\lambda_1, P_2\lambda_2, P_3\lambda_3, P_4\lambda_4)|^2 \\ \times (2\pi)^4 \delta^{(4)}(P_1 + P_2 - P_3 - P_4) \frac{d^3\mathbf{p}_3}{(2\pi)^3 2E_3} \frac{d^3\mathbf{p}_4}{(2\pi)^3 2E_4}$$

Integrate out $dp_{3z} d^3\mathbf{p}_4$

$$\Lambda^2(p_T) \equiv \left| E_3 p_{4z}^{(i)} - E_4 p_{3z}^{(i)} \right|$$

$$d\sigma = \frac{1}{64|P_1 \cdot P_2|} \sum_{i=1,2} \sum_{\lambda_1, \lambda_2, \lambda_4} |M(P_3\lambda_3, P_4\lambda_4)|^2 \frac{1}{\Lambda^2(p_T)} \frac{d^2\mathbf{p}_T}{(2\pi)^2}$$

Insert

$$\int d^2\mathbf{p}'_T \delta^{(2)}(\mathbf{p}'_T - \mathbf{p}_T) = \frac{1}{(2\pi)^2} \int d^2\mathbf{p}'_T d^2\mathbf{x}_T e^{i(\mathbf{p}'_T - \mathbf{p}_T) \cdot \mathbf{x}_T}$$

Ambiguity in conventional method

Differential cross section at fixed impact parameter

$$\frac{d^2\sigma}{d^2\mathbf{x}_T} = \frac{1}{64|P_1 \cdot P_2|} \int \frac{d^2\mathbf{p}_T}{(2\pi)^2} \frac{d^2\mathbf{p}'_T}{(2\pi)^2} e^{i(\mathbf{p}_T - \mathbf{p}'_T) \cdot \mathbf{x}_T} \times \sum_{i=1,2} \sum_{\lambda_1, \lambda_2, \lambda_4} \frac{M(P_3\lambda_3, P_4\lambda_4) M^*(P'_3\lambda_3, P'_4\lambda_4)}{\Lambda^2(p_T)}$$

We can replace $\frac{1}{\Lambda^2(p_T)} \rightarrow \frac{1}{\Lambda^{a_1}(p_T)} \frac{1}{\Lambda^{a_2}(p'_T)}$ with $a_1 + a_2 = 2$

$$\frac{d^2\sigma}{d^2\mathbf{x}_T} = \frac{1}{64|P_1 \cdot P_2|} \int \frac{d^2\mathbf{p}_T}{(2\pi)^2} \frac{d^2\mathbf{p}'_T}{(2\pi)^2} e^{i(\mathbf{p}_T - \mathbf{p}'_T) \cdot \mathbf{x}_T} \times \sum_{i=1,2} \sum_{\lambda_1, \lambda_2, \lambda_4} \frac{M(P_3\lambda_3, P_4\lambda_4) M^*(P'_3\lambda_3, P'_4\lambda_4)}{\Lambda^{a_1}(p_T) \Lambda^{a_2}(p'_T)}$$

Differential cross section is not unique,

but total one is same

Improved method

Mixed representation

$$\begin{aligned} |p_{3z}, \lambda_3, \mathbf{x}_{3T}\rangle &= \int \frac{A_T d^2 \mathbf{p}_{3T}}{(2\pi)^2} e^{i\mathbf{p}_{3T} \cdot \mathbf{x}_{3T}} |\mathbf{p}_3, \lambda_3\rangle \\ |p_{4z}, \lambda_4, \mathbf{x}_{4T}\rangle &= \int \frac{A_T d^2 \mathbf{p}_{4T}}{(2\pi)^2} e^{i\mathbf{p}_{4T} \cdot \mathbf{x}_{4T}} |\mathbf{p}_4, \lambda_4\rangle \end{aligned}$$

Matrix element

$$\begin{aligned} S_{fi} &= \langle p_{3z}, \lambda_3, \mathbf{x}_{3T}; p_{4z}, \lambda_4, \mathbf{x}_{4T} | S | \mathbf{p}_1, \lambda_1, \mathbf{p}_2, \lambda_2 \rangle \\ &= \int \frac{A_T d^2 \mathbf{p}_{3T}}{(2\pi)^2} \frac{A_T d^2 \mathbf{p}_{4T}}{(2\pi)^2} \frac{1}{\sqrt{2E_1 V}} \frac{1}{\sqrt{2E_2 V}} \frac{1}{\sqrt{2E_3 V}} \frac{1}{\sqrt{2E_4 V}} \\ &\quad \times e^{-i\mathbf{p}_{3T} \cdot \mathbf{x}_{3T}} e^{-i\mathbf{p}_{4T} \cdot \mathbf{x}_{4T}} (2\pi)^4 \delta^{(4)}(P_1 + P_2 - P_3 - P_4) \\ &\quad \times M(P_3 \lambda_3, P_4 \lambda_4) \end{aligned}$$

Matrix element

8 delta-functions and 2 amplitudes

$$\begin{aligned}
 |S_{fi}|^2 &= \int \frac{A_T d^2 \mathbf{p}_{3T}}{(2\pi)^2} \frac{A_T d^2 \mathbf{p}_{4T}}{(2\pi)^2} \frac{A_T d^2 \mathbf{p}'_{3T}}{(2\pi)^2} \frac{A_T d^2 \mathbf{p}'_{4T}}{(2\pi)^2} \\
 &\times \frac{1}{V^4} \frac{1}{16 E_1 E_2 \sqrt{E_3 E_4 E'_3 E'_4}} \\
 &\times e^{-i(\mathbf{p}_{3T} - \mathbf{p}'_{3T}) \cdot \mathbf{x}_{3T}} e^{-i(\mathbf{p}_{4T} - \mathbf{p}'_{4T}) \cdot \mathbf{x}_{4T}} \\
 &\times (2\pi)^8 \delta^{(4)}(P_1 + P_2 - P_3 - P_4) \delta^{(4)}(P_1 + P_2 - P'_3 - P'_4) \\
 &\times M(P_3 \lambda_3, P_4 \lambda_4) M^*(P'_3 \lambda_3, P'_4 \lambda_4)
 \end{aligned}$$

Momentum configuration

$$\begin{array}{rcl}
 P_1 + P_2 & \rightarrow & P_3(E_3, \mathbf{p}_{3T}, p_{3z}) + P_4(E_4, \mathbf{p}_{4T}, p_{4z}) \\
 P_1 + P_2 & \rightarrow & P'_3(E_3, \mathbf{p}'_{3T}, p_{3z}) + P'_4(E_4, \mathbf{p}'_{4T}, p_{4z})
 \end{array}$$

\mathbf{p}_T $-\mathbf{p}_T$
 \mathbf{p}'_T $-\mathbf{p}'_T$

Differential cross section

Differential cross section at fixed impact parameter

$$d\sigma = \frac{d^2\mathbf{x}_T}{A_T} \frac{V}{4v_{rel}T} \sum_{\lambda_1, \lambda_2, \lambda_4} \int \frac{Ldp_{3z}}{2\pi} \frac{Ldp_{4z}}{2\pi} |S_{fi}|^2$$

$\mathbf{x}_T \equiv \mathbf{x}_{3T} - \mathbf{x}_{4T}$

Integrating out $d^2\mathbf{p}_{4T} dp_{3z} d^2\mathbf{p}'_{4T} dp_{4z}$ and using two z-component delta function are identical, and using $2\pi\delta^{(z)}(0) = L$

$$\begin{aligned} \frac{d^2\sigma}{d^2\mathbf{x}_T} &= \frac{1}{T} \frac{1}{64(2\pi)^3} \int d^2\mathbf{p}_T d^2\mathbf{p}'_T e^{-i(\mathbf{p}_T - \mathbf{p}'_T) \cdot \mathbf{x}_T} \delta(E_3 + E_4 - E'_3 - E'_4) \\ &\times \sum_{i=1,2} \sum_{\lambda_1, \lambda_2, \lambda_4} \frac{1}{|P_1 \cdot P_2| \sqrt{E_3 E_4 E'_3 E'_4}} \frac{E_3 E_4}{|E_3 p_{4z}^{(i)} - E_4 p_{3z}^{(i)}|} \\ &\times M(P_3 \lambda_3, P_4 \lambda_4) M^*(P'_3 \lambda_3, P'_4 \lambda_4) \end{aligned}$$

Treatment of last delta function

Using

$$2\pi\delta(E_3 + E_4 - E'_3 - E'_4) \approx \int_{-\tau/2}^{\tau/2} dt e^{i(E_3+E_4-E'_3-E'_4)t}$$

Interaction time

Differential cross section can be written

$$\begin{aligned} \frac{d^2\sigma}{d^2\mathbf{x}_T} &= \frac{1}{64(2\pi)^4 |P_1 \cdot P_2|} \int d^2\mathbf{p}_T d^2\mathbf{p}'_T \left\langle e^{-i(\mathbf{p}_T - \mathbf{p}'_T) \cdot \mathbf{x}_T} \right. \\ &\times \sum_{i=1,2} \sum_{\lambda_1, \lambda_2, \lambda_4} \frac{1}{\sqrt{E_3 E_4 E'_3 E'_4}} \frac{E_3 E_4}{\left| E_3 p_{4z}^{(i)} - E_4 p_{3z}^{(i)} \right|} \\ &\left. \times M(P_3 \lambda_3, P_4 \lambda_4) M^*(P'_3 \lambda_3, P'_4 \lambda_4) \right\rangle_t \end{aligned}$$

With time average $\langle \dots \rangle_t \equiv \frac{1}{\tau} \int_{-\tau/2}^{\tau/2} dt (\dots) e^{i(E_3+E_4-E'_3-E'_4)t}$

Interaction time expansion

Expansion if $|(E_3 + E_4 - E'_3 - E'_4)t| \ll 1$

$$e^{i(E_3 + E_4 - E'_3 - E'_4)t} \approx 1 + i(E_3 + E_4 - E'_3 - E'_4)t - \frac{1}{2}(E_3 + E_4 - E'_3 - E'_4)^2 t^2 + \dots$$

Leading order ~ 1 reproduces old result

$$\begin{aligned} \frac{d^2\sigma^{(0)}}{d^2\mathbf{x}_T} &= \frac{1}{64(2\pi)^4 |P_1 \cdot P_2|} \int d^2\mathbf{p}_T d^2\mathbf{p}'_T e^{-i(\mathbf{p}_T - \mathbf{p}'_T) \cdot \mathbf{x}_T} \\ &\times \sum_{i=1,2} \sum_{\lambda_1, \lambda_2, \lambda_4} \frac{1}{\Lambda^2(p_T)} M(P_3 \lambda_3, P_4 \lambda_4) M^*(P'_3 \lambda_3, P'_4 \lambda_4) \\ &= \frac{d^2\sigma_{upol}^{(0)}}{d^2\mathbf{x}_T} + \lambda_3 \frac{d^2\sigma_{pol}^{(0)}}{d^2\mathbf{x}_T} \end{aligned}$$

Leading order result

To leading order, the result is unique

$$\frac{1}{\Lambda^2(p_T)} \approx \frac{1}{\Lambda^{a_1}(p_T)} \frac{1}{\Lambda^{a_2}(p'_T)}$$

Here are polarized and unpolarized cross section

$$\frac{d^2\sigma_{upol}^{(0)}}{d^2\mathbf{x}_T} = \frac{\alpha_s^2}{9} A^2(x_T)$$

$$\frac{d^2\sigma_{pol}^{(0)}}{d^2\mathbf{x}_T} = \frac{\alpha_s^2}{9} \frac{2}{\sqrt{s}} \mathbf{n} \cdot (\mathbf{n}_1 \times \hat{\mathbf{x}}_T) A(x_T) \frac{dA(x_T)}{dx_T}$$

$$A(x_T) = \int d^2\mathbf{p}_T e^{\pm i\mathbf{p}_T \cdot \mathbf{x}_T} \frac{1}{p_T^2 + \mu_m^2} = 2\pi \int_0^{p_T^{cut}} dp_T \frac{p_T J_0(p_T x_T)}{p_T^2 + \mu_m^2}$$

Next-to-leading order

Next-to-leading order $\sim t^2$

$$\begin{aligned}
 \frac{d^2\sigma^{(1)}}{d^2\mathbf{x}_T} &= -\frac{\tau^2}{1536(2\pi)^4|P_1 \cdot P_2|} \int d^2\mathbf{p}_T d^2\mathbf{p}'_T e^{-i(\mathbf{p}_T - \mathbf{p}'_T) \cdot \mathbf{x}_T} \\
 &\times \sum_{i=1,2} \sum_{\lambda_1, \lambda_2, \lambda_4} \frac{(E_3 + E_4 - E'_3 - E'_4)^2}{\sqrt{E_3 E_4 E'_3 E'_4}} \frac{E_3 E_4}{\left| E_3 p_{4z}^{(i)} - E_4 p_{3z}^{(i)} \right|} \\
 &\times M(P_3 \lambda_3, P_4 \lambda_4) M^*(P'_3 \lambda_3, P'_4 \lambda_4) \\
 &= \frac{d^2\sigma_{upol}^{(1)}}{d^2\mathbf{x}_T} + \lambda_3 \frac{d^2\sigma_{pol}^{(1)}}{d^2\mathbf{x}_T}
 \end{aligned}$$

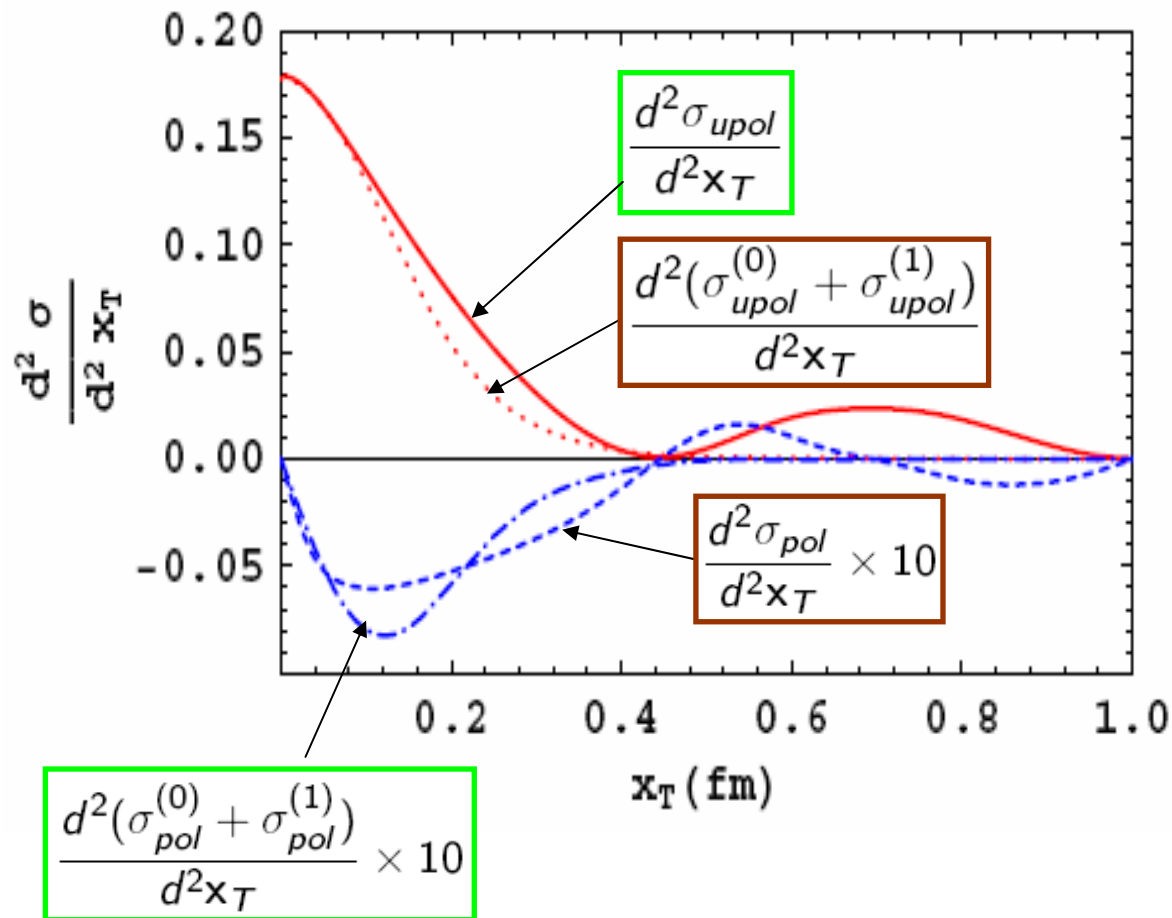
Next-to-leading order

Here are polarized and unpolarized cross section

$$\begin{aligned}\frac{d^2\sigma_{upol}^{(1)}}{d^2\mathbf{x}_T} &= -\frac{\tau^2\alpha_s^2}{27s}(A_0A_1 - A_2^2) \\ \frac{d^2\sigma_{pol}^{(1)}}{d^2\mathbf{x}_T} &= -\frac{\tau^2\alpha_s^2}{27s^{3/2}}\mathbf{n}\cdot(\mathbf{n}_1\times\hat{\mathbf{x}}_T)\frac{d}{dx_T}(A_0A_1 - A_2^2) \\ A_i(x_T) &\equiv \int_0^{p_T^{cut}} dp_T \frac{p_T^{n_i}}{p_T^2 + \mu_m^2} J_0(p_T x_T), \quad \text{for } i = 0, 1, 2\end{aligned}$$

Numerical result

Exact result and result with expansion



Conclusions

- A general approach to the differential cross section with impact parameters: well-defined and free of ambiguity existing in the conventional approach.
- The method is making use of the fact that the final state energy is not fixed at fixed impact parameter
- An expansion is proposed in terms of $\Delta E = E_f - E_i \sim 1/\tau$ the leading order result reproduces result from conventional method
- Applicable to many other parton-parton scatterings in non-central nuclear and proton-proton collisions