

# Nb<sub>3</sub>Sn Conductor Technology for the FCC

M.B. Field, H. Miao, M. Gerace, and J.A. Parrell

Oxford Superconducting Technology, Carteret, NJ 07008 USA



## Acknowledgements

- U.S. DOE - High Energy Physics (CDP work through LBNL)
- Lawrence Berkeley National Laboratory
- Fermi National Accelerator Laboratory
- Brookhaven National Laboratory
- European Organization for Nuclear Research (CERN)
- ASC - Florida State University / NHMFL
- Thank you for your continued support

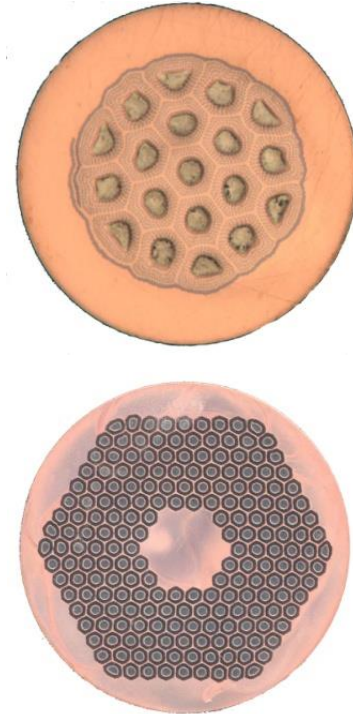
Property	Units	Values
Strand diameter	(mm)	0.5 mm to 1.0 mm
$J_c(4.2 \text{ K}, 16 \text{ T})$	(A/mm <sup>2</sup> )	$\geq 1500$
$\mu_0 M(1 \text{ T}, 4.2 \text{ K})$	(mT)	$\leq 150$
$\sigma(\mu_0 M)(1 \text{ T}, 4.2 \text{ K})$	(%)	$\leq 4.5$
$D_{\text{eff}}$	( $\mu\text{m}$ )	$\leq 20$
RRR		$\geq 150$
Unit Length	(km)	$\geq 5 \text{ km}$

“Targets for R&D on Nb<sub>3</sub>Sn conductor for High Energy Physics”,  
Ballarino and Bottura

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# $D_{\text{eff}} \leq 20\mu\text{m}$ in 0.5 - 1 mm diameter strands

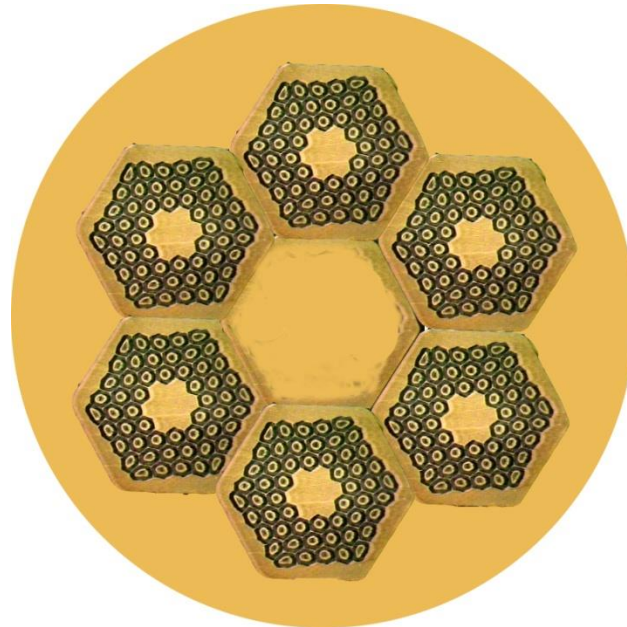
- Strand diameter – the issue is relationship to  $D_{\text{eff}}$ 
  - Single Barrier, “ITER” type strands,  $D_{\text{eff}} \sim 20\text{-}30\ \mu\text{m}$  at 0.82 mm (after HT, due to merging)
  - For distributed barrier strands (RRP®, PIT, tube)  $D_s$  is tough challenge with a single restack of appreciable weight (large aspect ratio)



	$D_s(\text{stack count})$ in $\mu\text{m}$						
wire dia.	169	217	271	331	397	469	547
1.0 mm	59	52	47	42	39	35	33
0.9 mm	53	47	42	38	35	32	30
0.85 mm	50	44	40	36	33	30	28
0.8 mm	47	42	37	34	31	28	26
0.7 mm	41	36	33	30	27	25	23
0.6 mm	35	31	28	25	23	21	20
0.5 mm	29	26	23	21	19	18	16

# $D_{\text{eff}} \leq 20\mu\text{m}$ in 0.5 - 1 mm diameter strands

- A “double restack” – restacking the restack – can access the smaller  $D_s$  at the desired wire size range
  - Need subelements tolerant to a high true strain (i.e. ductile)
  - Difficult to maintain high  $I_c$  value, as double restack adds copper to the cross section (i.e. dilutes superconductor fraction)

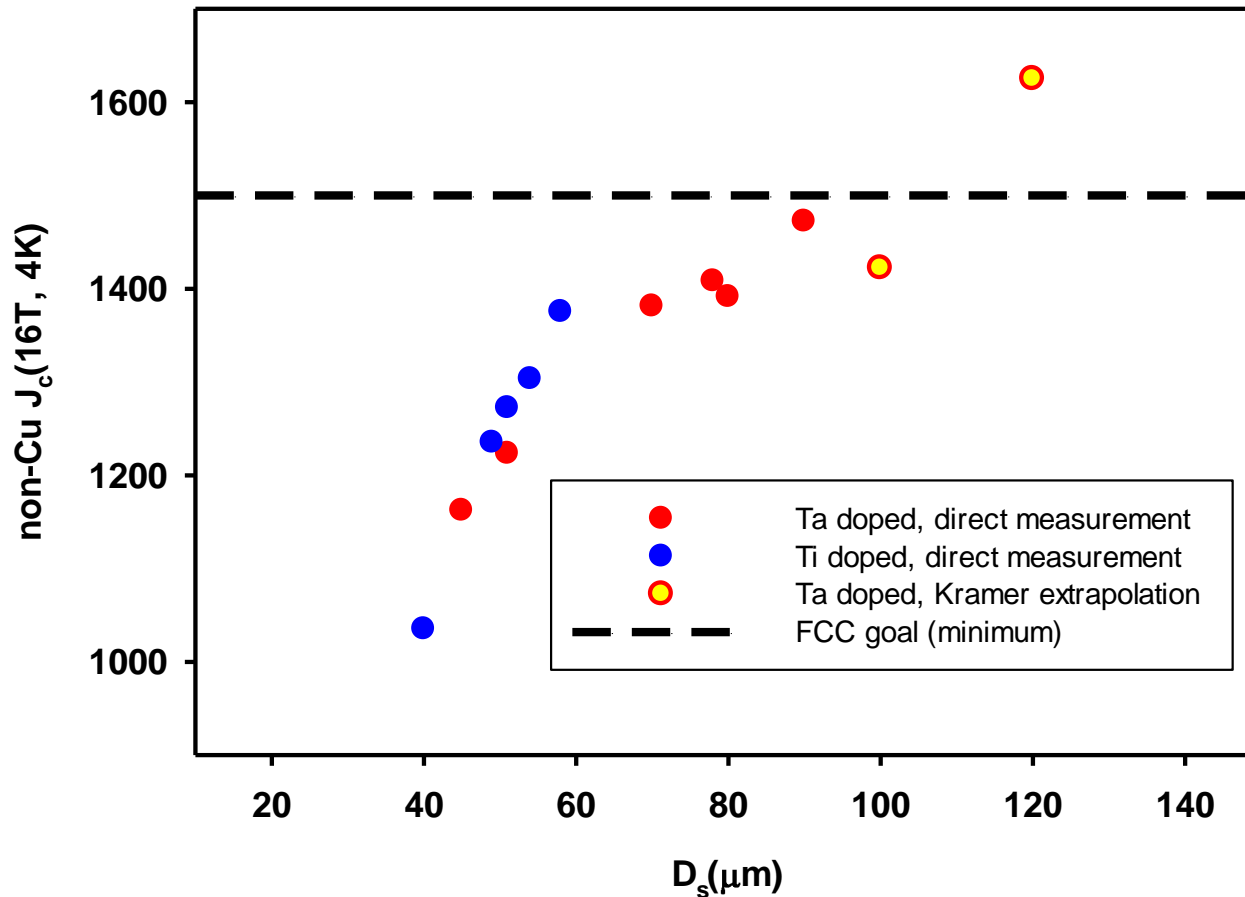


(illustration)  
7 stack X 61 stack  
 $D_s \sim 20 \mu\text{m}$  @ 0.8 mm

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# $J_c(4.2\text{ K}, 16\text{ T}) > 1500\text{ A/mm}^2$

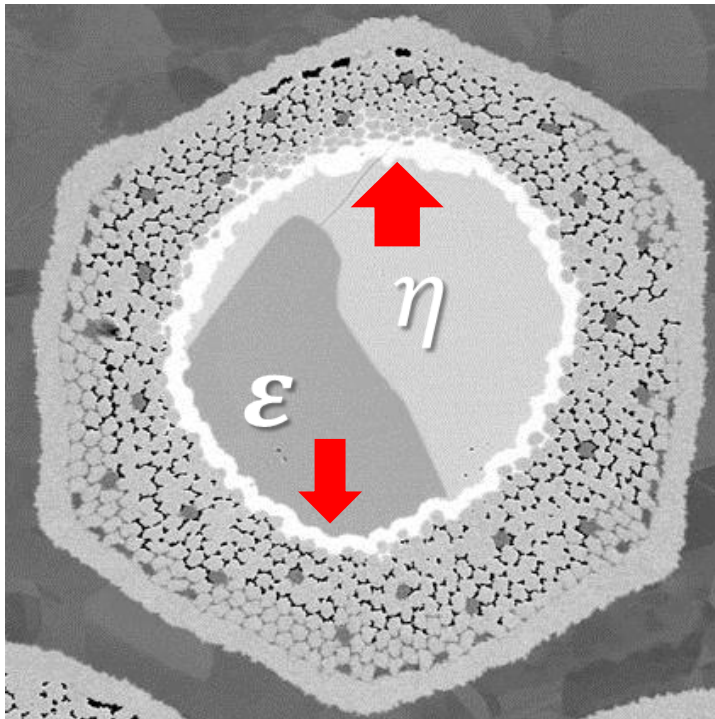
- The most critical parameter – need the  $J_c$  to get the field
  - present RRP® design is close – for  $D_s > 80\text{ }\mu\text{m}$



“best” 16 T  $J_c$  for various RRP across range of  $D_s$



- $J_c$  decreases significantly for  $D_s$  below  $\sim 50\text{ }\mu\text{m}$ 
  - Need better understanding of tin / bronze diffusion and the interaction with Nb-Sn-Cu ternary as  $D_s \downarrow$ 
    - Collaborations with Sanabria (FSU), Pong (LBL)

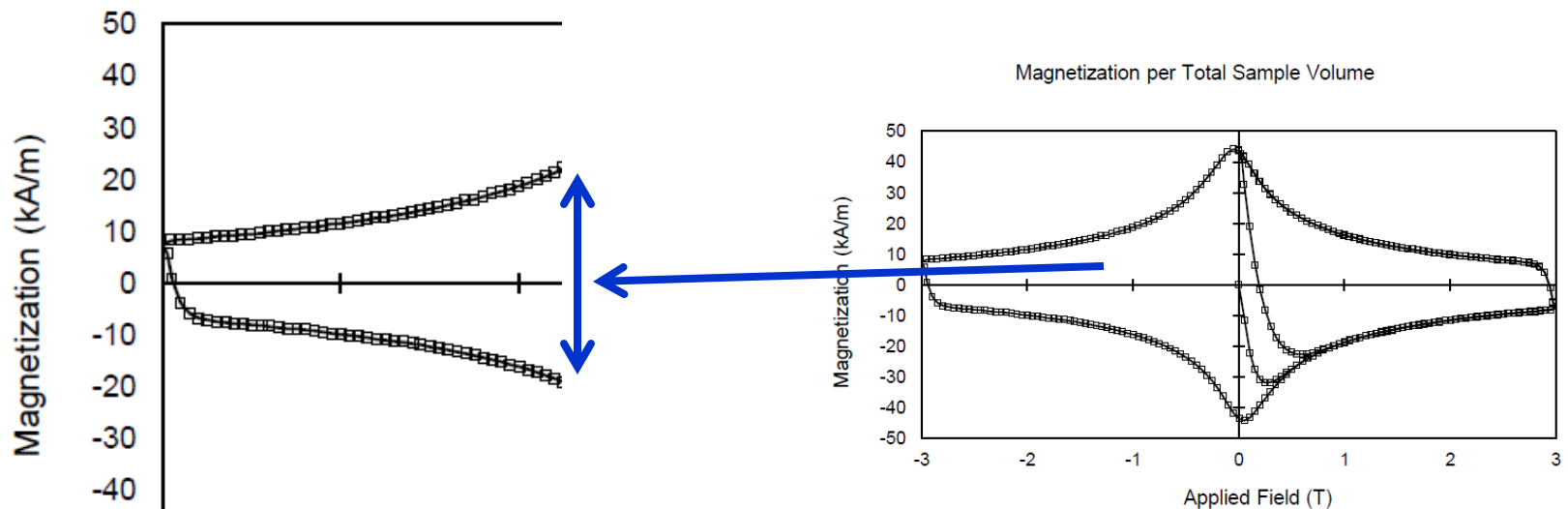


RRP reacted 210°C/48hr + 400°C/48hr,  
Courtesy of FSU (Peter Lee, Charlie  
Sanabria)

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$$\mu_0 M(1 \text{ T}, 4.2 \text{ K}) < 150 \text{ mT}, \sigma \leq 4.5\%$$

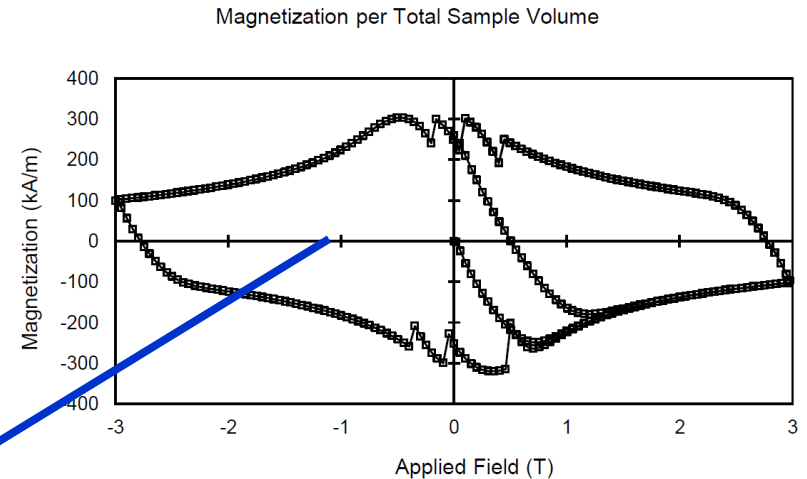
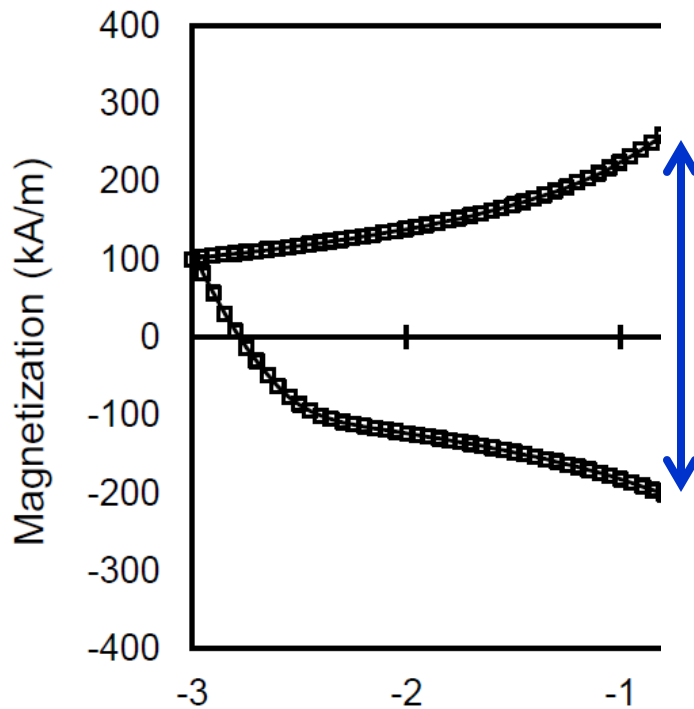
- $D_{\text{eff}}$  on order of  $20 \mu\text{m}$  is easier in single barrier strands, but layer  $J_c$  is the problem
  - Can layer  $J_c$  be increased by APC?
  - $\sigma$  is a challenge driven by  $J_c$  spread



OST ITER Single Barrier @ 0.82 mm

$\mu_0 M(1 \text{ T}, 4.2 \text{ K}) < 150 \text{ mT}, \sigma \leq 4.5\%$

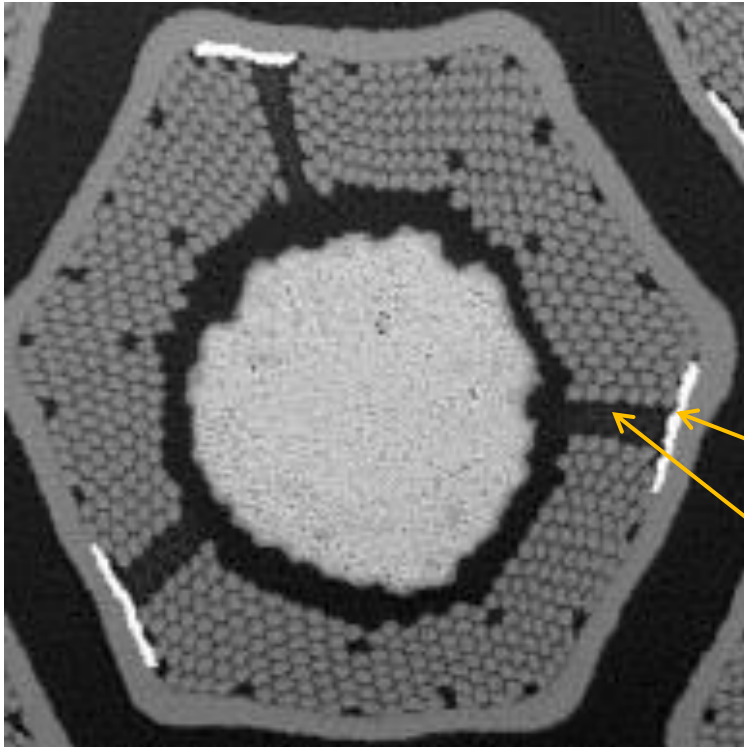
- Distributed barrier RRP® – 3-4x too high
  - Flux jumps also an issue



0.778 mm 127 stack,  
 $D_s \sim 50 \mu\text{m}$

$$\mu_0 M(1 \text{ T}, 4.2 \text{ K}) < 150 \text{ mT}, \sigma \leq 4.5\%$$

- What if  $D_s$  is large but  $D_{\text{eff}}$  is small?



Hot Extruded Rod,  
US DOE CDP R&D  
Circa 2004

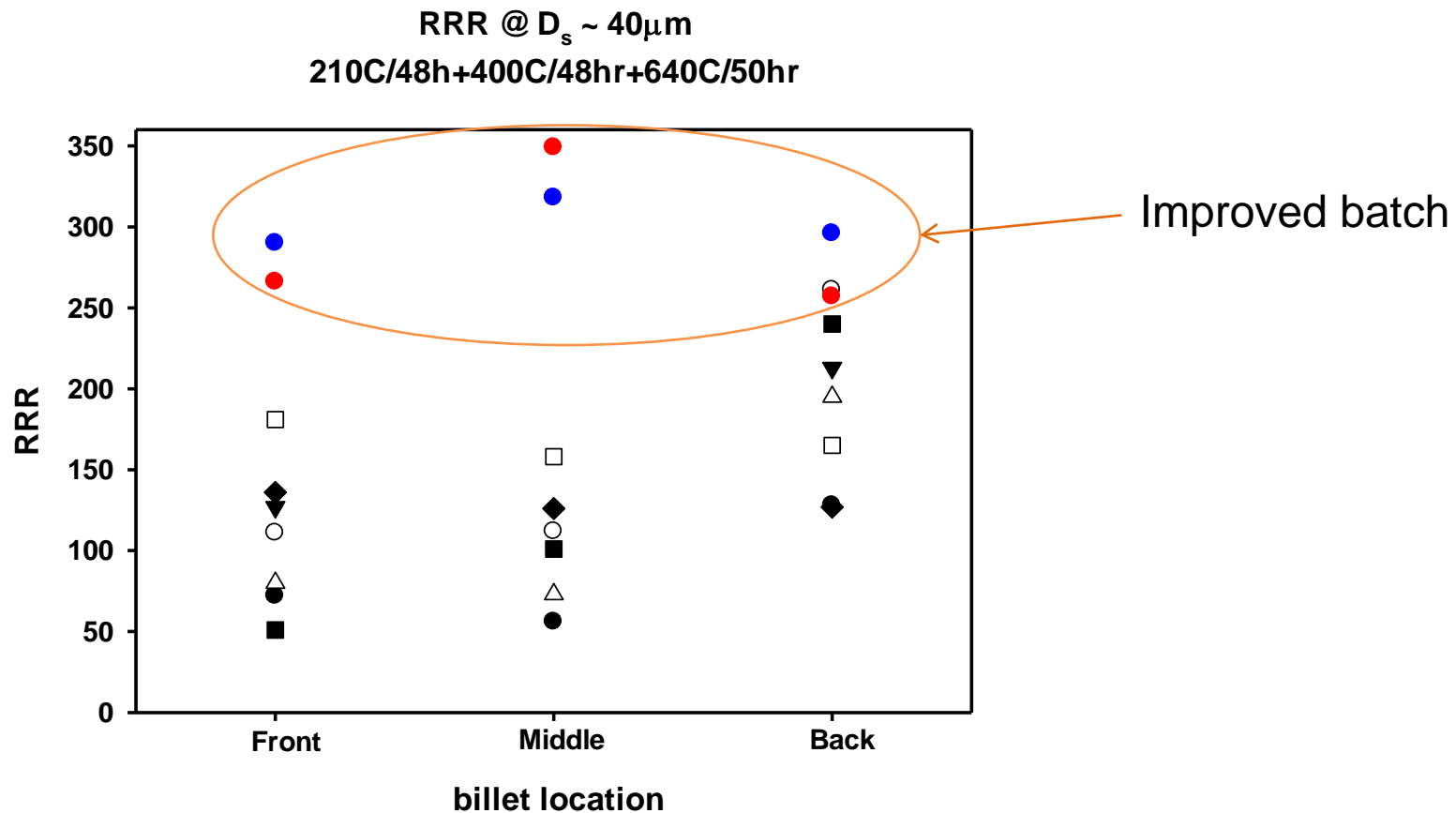
Ta

Nb-Ti

- Depress  $J_c$  in low fields - higher  $B_{c2}$
- $\sigma$  more challenging than single barrier –  $J_c$  spread wider

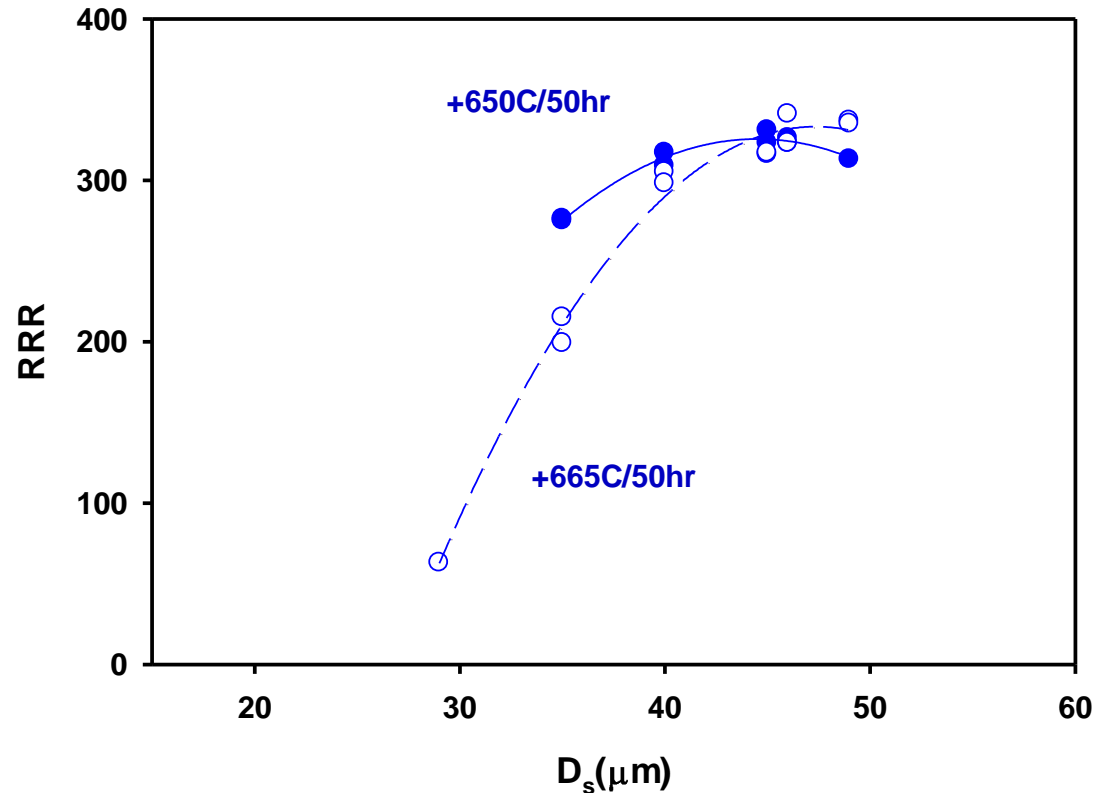
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- Improved RRR throughout billet by reducing sources of variation in design and in processing



- High RRR in small  $D_s$  distributed barrier strand still a challenge

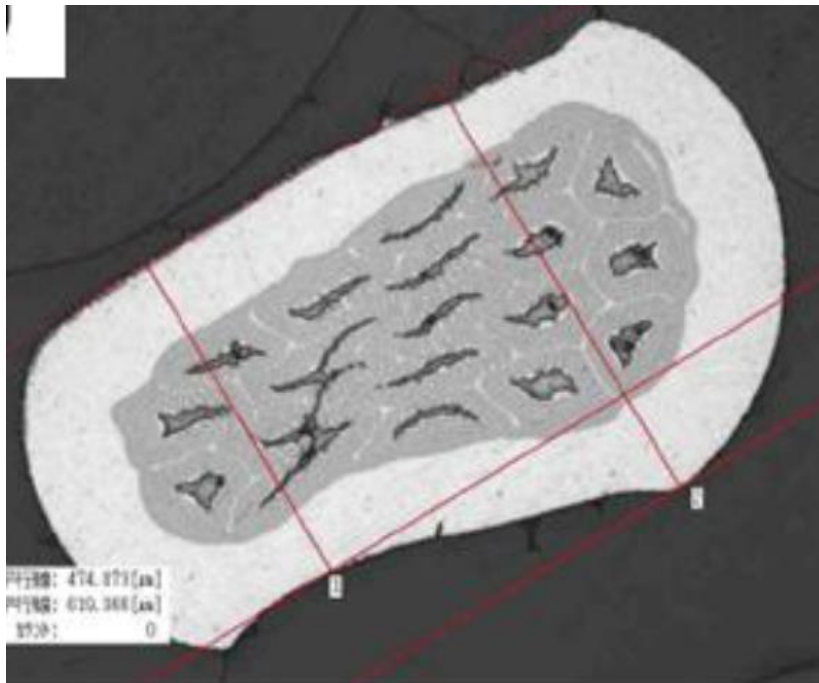
US DOE CDP R&D  
Barrier thickness studies  
169 stack, Nb:Sn 3.6:1



- Is RRR > 150 in round strand an absolute requirement? What about RRR after cabling? Ever possible to use RRR > 60?



- Single barrier (ITER style strands) – Ta barriers can remain intact during deformation better than the subelements inside



Extracted strand from CICC,  
“Challenges and Status of  
ITER conductor production”,  
Devred et al

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- Internal tin = (relatively) small billet volume
- Typical piece length depends on wire diameter?
  - 0.5 mm length 4x 1.0 mm length for same weight
- Need to consider total cost of cable (strand vs. cable yield)
  - As billets are relatively small, long lengths = limited yield
- ITER experience: 70 tons of production, averaged ~6km @ 0.82mm
  - However this was a more “simple” strand

# Nb<sub>3</sub>Sn for FCC – RRP<sup>®</sup> vs single barrier

Property	Units	Values	RRP <sup>®</sup>	Single bar.
Strand diameter	(mm)	0.5 mm to 1.0 mm	✓	✓
J <sub>c</sub> (4.2 K, 16 T)	(A/mm <sup>2</sup> )	≥ 1500	close	X
μ <sub>0</sub> M(1 T, 4.2 K)	(mT)	≤ 150	X	close?
σ(μ <sub>0</sub> M)(1 T, 4.2 K)	(%)	≤ 4.5	X	X
D <sub>eff</sub>	(μm)	≤ 20	X	✓
RRR		≥ 150	?	✓
Unit Length	(km)	≥ 5 km	?	?

- FCC Nb<sub>3</sub>Sn targets present new challenges
- Progress is being made in understanding how to preserve  $J_c$  and RRR as  $D_s$  is decreased
- New breakthrough needed: keep high layer  $J_c$  of RRP<sup>®</sup>, but with the filament spacing and layout of single barrier strand



Visual  
metaphor for  
future FCC  
strand!