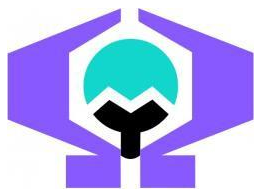


***Nb<sub>3</sub>Sn Internal – Tin Strands  
for FCC (Dream wire).  
Approaches to Optimization  
- Design, R&D,  
- Commercial Production***

**V. Pantsyrny**



## Chepetsky Mechanical Plant (Glazov) – Production of LTSC (NbTi and Nb<sub>3</sub>Sn) - 60 ton/year

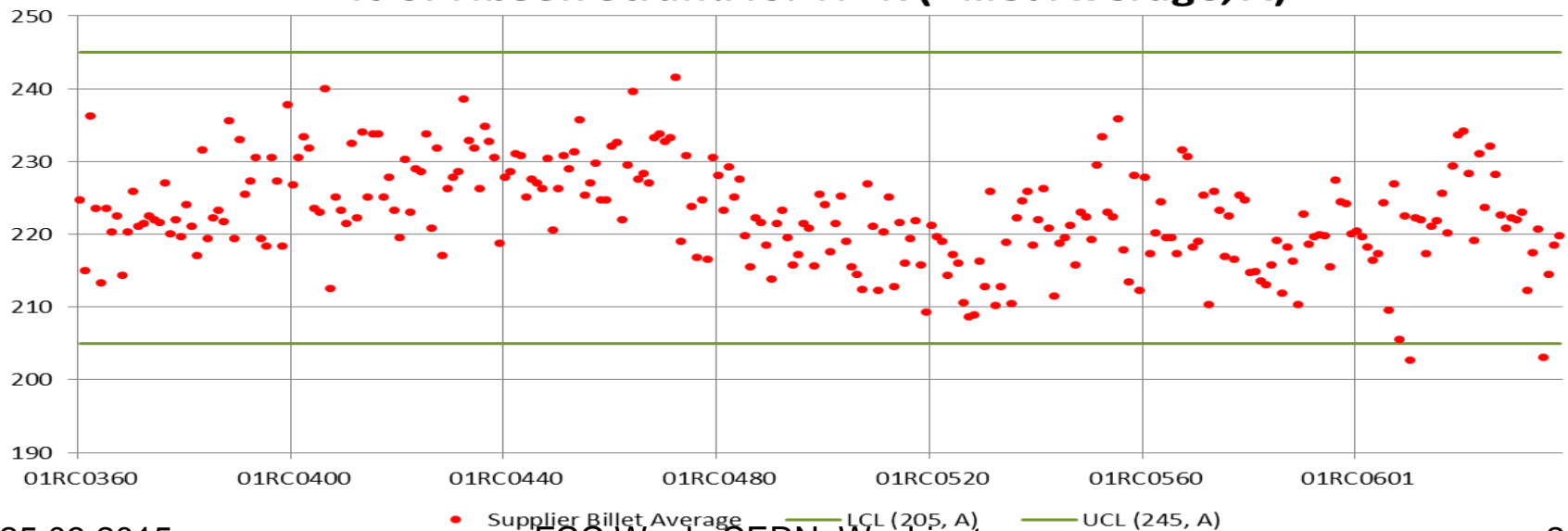
From - Melting of Nb, NbTi, Cu-Sn, Extrusion, Rolling, Drawing, Heat treatment  
To - Superconducting properties testing

### NbTi and Nb<sub>3</sub>Sn strands production status for ITER (2010-2014)

**127.6t of NbTi strand produced. Production has been completed.** Average yield is more than 90%. 798 billets have been produced:

**More than 90t of bronze Nb<sub>3</sub>Sn strand have been produced. Production has been completed;** Average yield is 88%, (**UCL =245A, LCL =205A**)

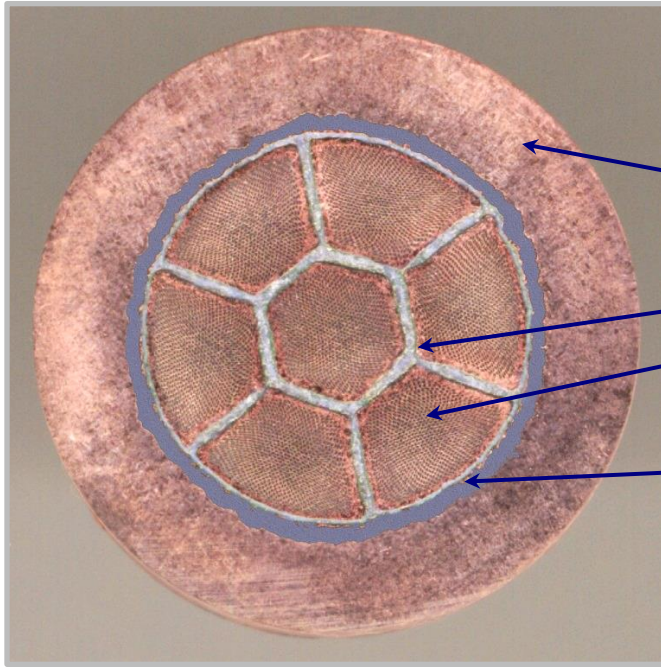
I<sub>c</sub> of Nb<sub>3</sub>Sn Strand for ITER (Billet Average, A)



25.03.2015

FCC Week, CERN, Washington.

**RF produced Internal Tin Nb<sub>3</sub>Sn strand for ITER  
tested in SULTAN facility in the scope of TF conductor (August 2007)**



**RFTF1 - showed Tcs = 6.25K  
ITER Requirements: Tcs > 5.7K**

**Cu stabilizer**

**Sn source**

**Filaments Nb / 2at.%Ti (421 in subelement)**

**Ta barrier**

**Initial billet size 43.5 mm**

**Specification requirements**

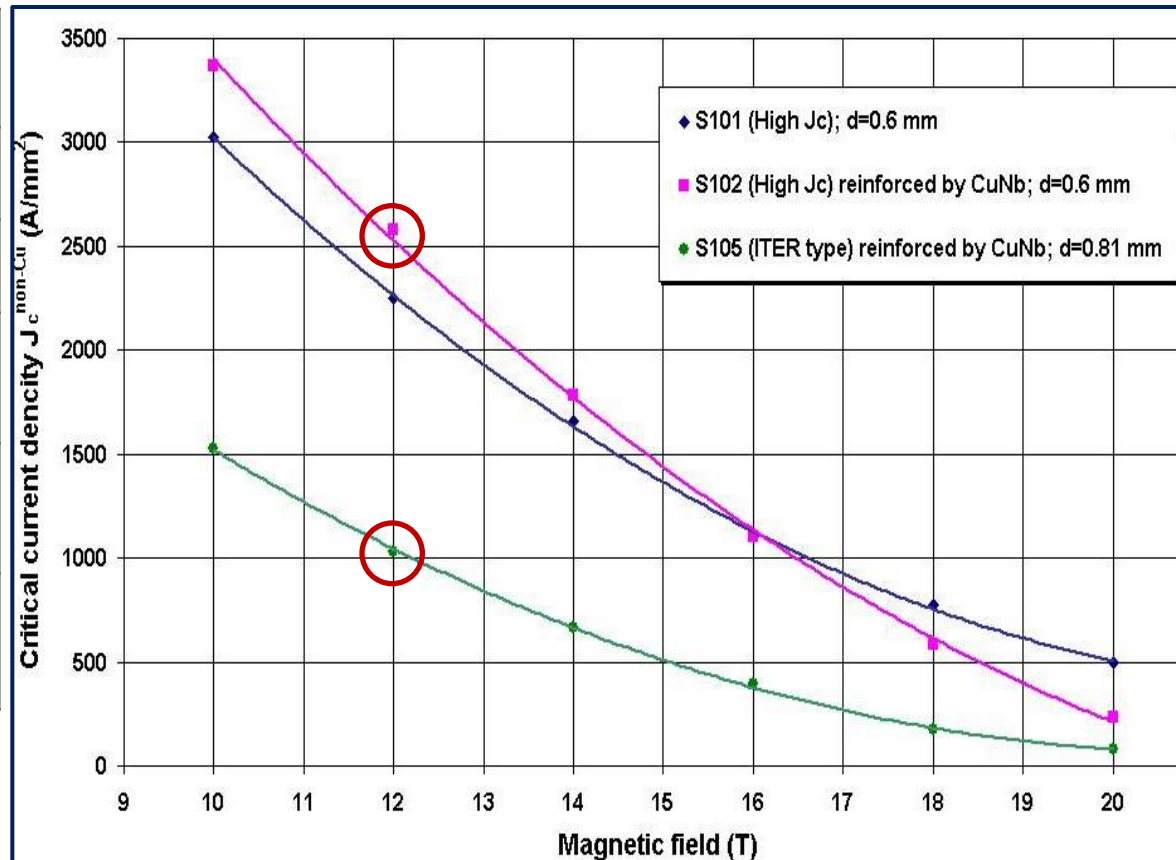
<b>Non-Cu Jc (at 12 T, 4.2K)</b>	<b>&gt; 800 A/mm<sup>2</sup></b>
<b>Non-Cu hysteresis losses on ± 3T field cycle at 4.2 K</b>	<b>&lt;1000 kJ/m<sup>3</sup></b>
<b>RRR after reaction heat treatment</b>	<b>&gt;100</b>

**Design parameters**

<b>Diameter of the strand, mm</b>	<b>0,82</b>
<b>Cu stabilizer fraction, vol.%</b>	<b>50</b>
<b>Barrier</b>	<b>Ta</b>
<b>Nb fraction (inside barrier), vol.%</b>	<b>33,7</b>
<b>Diameter of Nb filament, μm</b>	<b>5,7</b>
<b>Spacing between Nb filaments, μm</b>	<b>2,4</b>
<b>Non-Cu Jc (at 12 T, 4.2 K), A/mm<sup>2</sup></b>	<b>1000</b>

# Experimental data on ITER and HEP types Nb<sub>3</sub>Sn strand

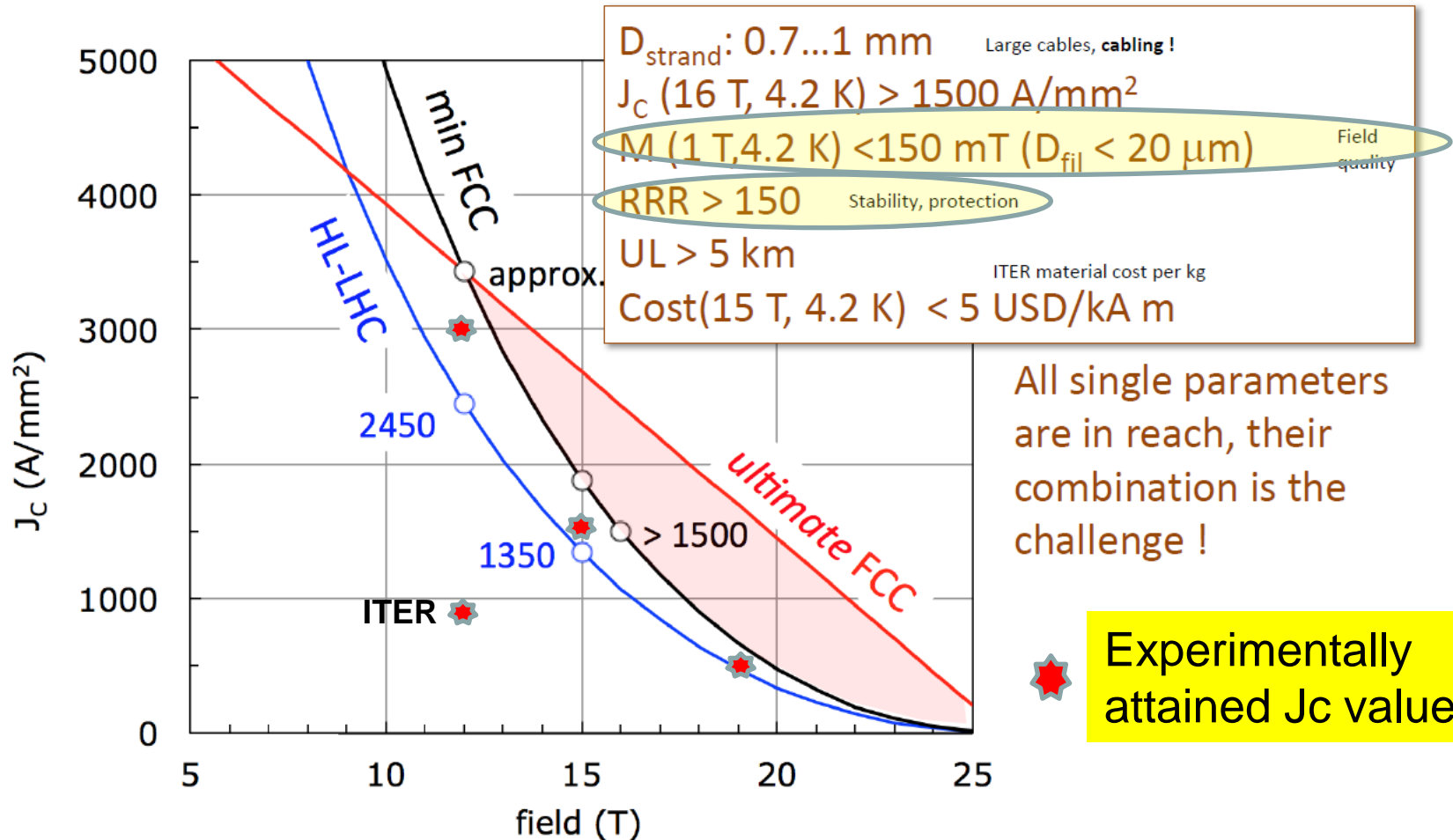
Strand diameter, mm	<b>0,6</b>
Number of filaments	<b>2947</b>
Cu stabilization, vol. %	<b>40</b>
Critical current density (12 T, 4,2 K), A/mm <sup>2</sup>	<b>2580</b>
Critical current density (15 T, 4,2 K), A/mm <sup>2</sup>	<b>1500</b>
Hysteresis losses (±3 T, 4,2 K), mJ/cm <sup>3</sup>	<b>~ 1200</b>



***Internal Tin (IT) Nb<sub>3</sub>Sn strands are very flexible in attaining of wide range of different J<sub>c</sub> levels (1000-3000 A/mm<sup>2</sup>).***

# The future challenges for internal tin strands

## FCC Nb<sub>3</sub>Sn performance targets



All single parameters are in reach, their combination is the challenge !

Experimentally attained  $J_c$  values

# OPTIMIZATION – to find a balance Quantity (amount of Nb<sub>3</sub>Sn) – Quality (pinning in Nb<sub>3</sub>Sn)

## Increase of Nb<sub>3</sub>Sn phase quantity

In bronze processed strands 15.0% of Sn in bronze matrix is available for transformation of Nb filaments to Nb<sub>3</sub>Sn phase.

**Attainable volume fraction of Nb<sub>3</sub>Sn phase is around 30% in the non-Cu area.**

For bronze processed strands non-Cu J<sub>c</sub> ~ **900 A/mm<sup>2</sup>**  
assumes J<sub>c</sub> in Nb<sub>3</sub>Sn phase ~ **3000 A/mm<sup>2</sup>**.

**(In reality higher – due to non-uniformity of 3-4 μm in dia. Nb<sub>3</sub>Sn filaments)**

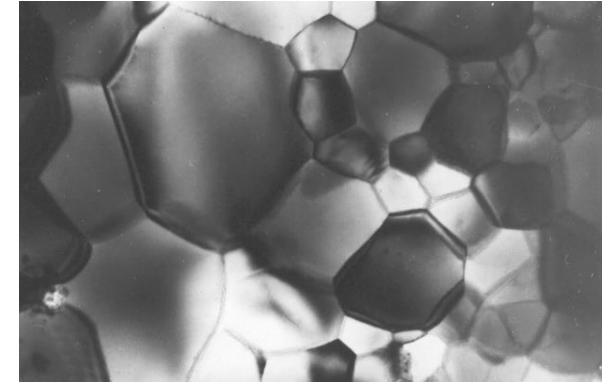
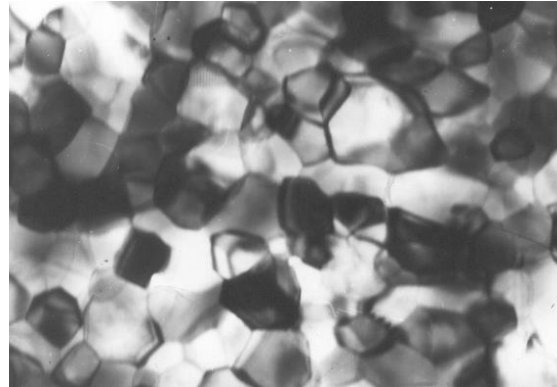
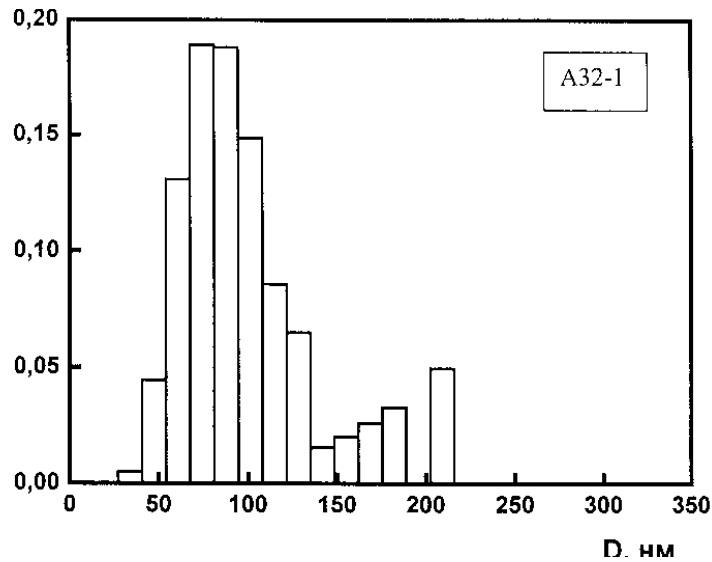
Unstabilized Nb<sub>3</sub>Sn strands parameters and properties (Sn content in bronze – 13 %)

No	Fil. number	Fil.space, μm	J <sub>c</sub> (12T), A/mm <sup>2</sup>	Wh ( ±3T) , mJ/cm <sup>3</sup>
1	44521	0.5	560	840
2	25531	0.9	480	650
4	7225	1.3	420	110

x 1.14
x 5.9

**The critical Fil.spacing - > 1 μm – STRONG LIMITATION on volume fraction of Nb<sub>3</sub>Sn phase in IT strands - R&D on strands design is required**

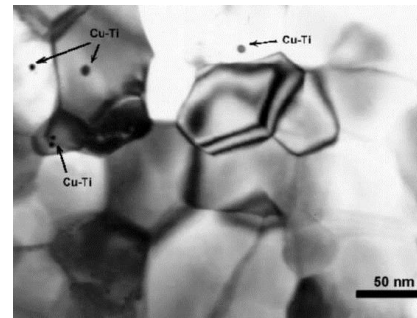
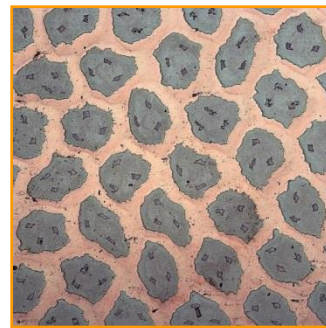
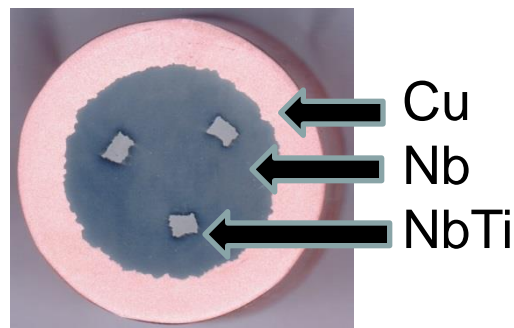
# Increase of Nb<sub>3</sub>Sn phase quality (pinning in Nb<sub>3</sub>Sn) by design and doping



**Distribution of the Nb<sub>3</sub>Sn grain size in ITER type bronze processed strands (heat treatment 575°C 150h + 650°C 200h)**

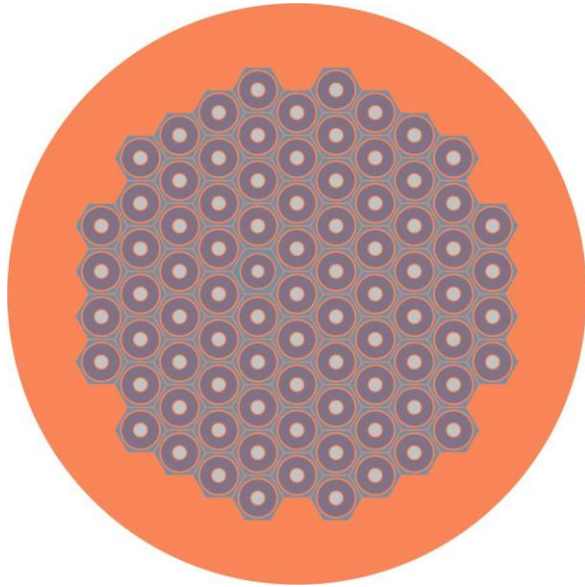
*The internal oxidation method (doping by Zr) can significantly refine the grain size and improve the high-field J<sub>c</sub> of Nb<sub>3</sub>Sn strands.*

*The Nb<sub>3</sub>Sn grain size could be reduced down to 20-50 nm, [XU X.;](#) [SUMPTION M.;](#) [Dr. PENG X.;](#) [Dr. COLLINGS, T.](#)*



Doping by distributed NbTi - Internal precipitations of Cu-Ti intermetallic particles

# Internal Tin Strands with tubular filaments

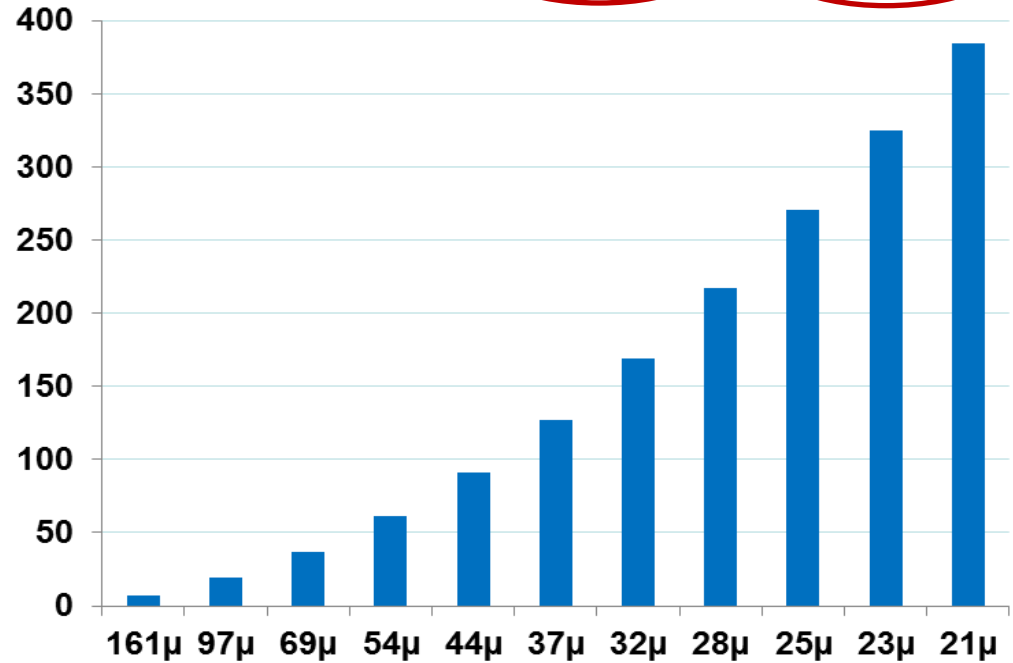


85 monoelements

Deff in the order of **50 mkm**

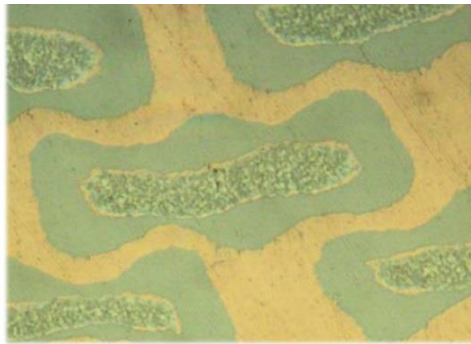
Target performance:

$J_c (12\text{ T}) > 3\text{ kA/mm}^2$  ;  $D_{\text{fil}} < 20\ \mu\text{m}$  ;  $\text{RRR} > 150$



Deff =20 mkm requires > 400 tubular filaments

**Thickness of Nb tubular filament should be less than 5  $\mu\text{m}$  and due to nonuniformity and deformation of the strands during cabling operation the  $\text{RRR} > 100$  could not be attained**

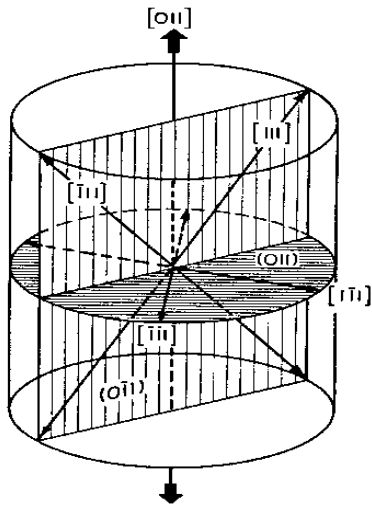
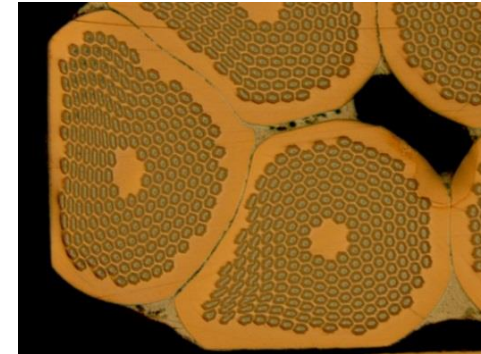
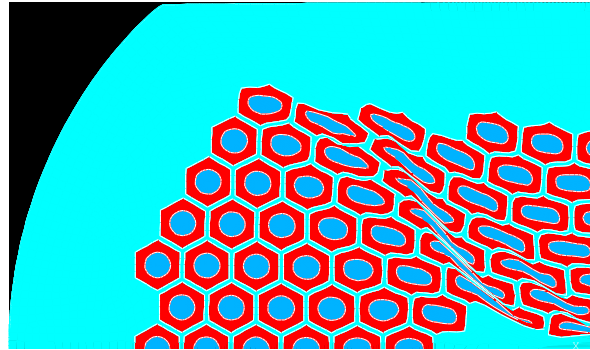




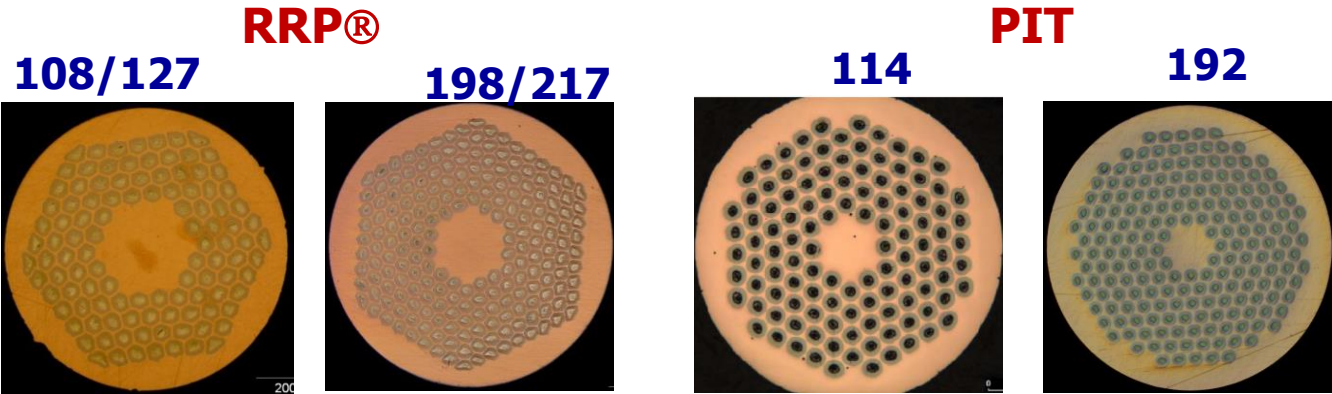
# Trials to attain the $D_{eff}$ equal to 20 $\mu\text{m}$ (Hi-Luminosity LHC $\text{Nb}_3\text{Sn}$ wire)

The texture of drawing with direction of  $z = [011]$  is developing in Nb filaments. In BCC Nb the dislocations slipping system  $[111](011)$  is prevailing, therefore less than 5 active slipping systems remain. The uniform deformation is substituted by the plane deformation.

Deformed results: Hexagonal models experience sub-element merging



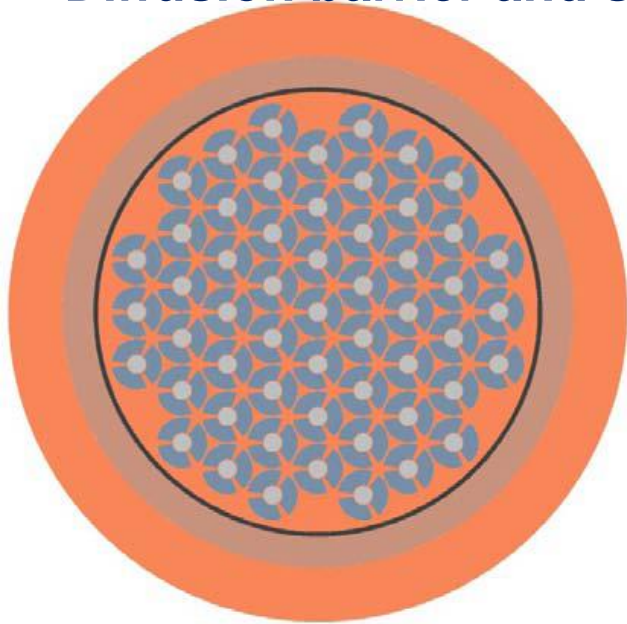
Smaller sub-element size



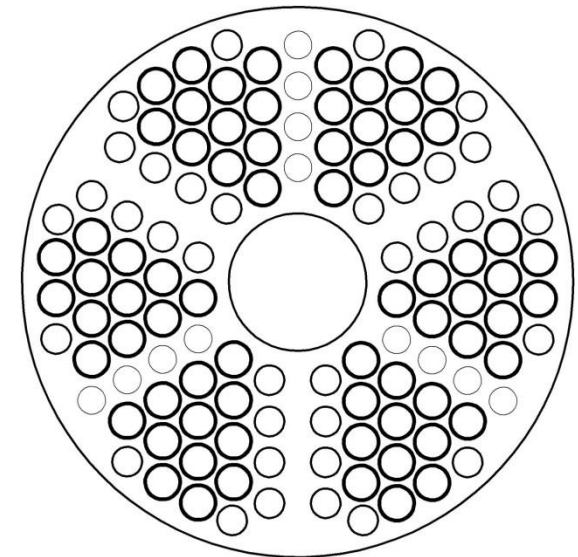
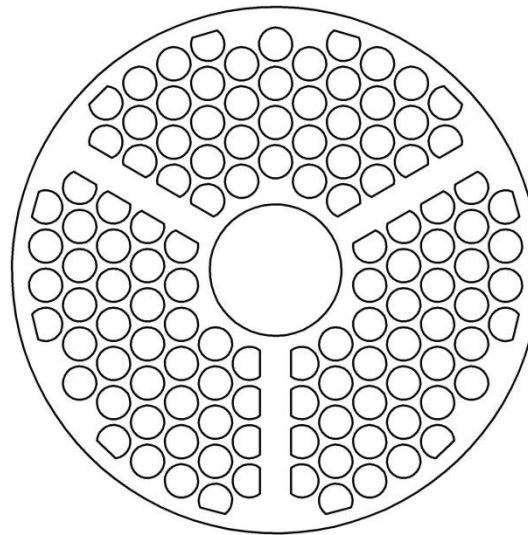
Still the amount of sub-elements have to be increased in a factor of 2

# Optimization of Deff – subdividing the sub-elements on the groups of Nb filaments

Internal Tin Strands made with sub-elements surrounded by one Diffusion barrier and strengthened by nanostructured Cu-Nb material



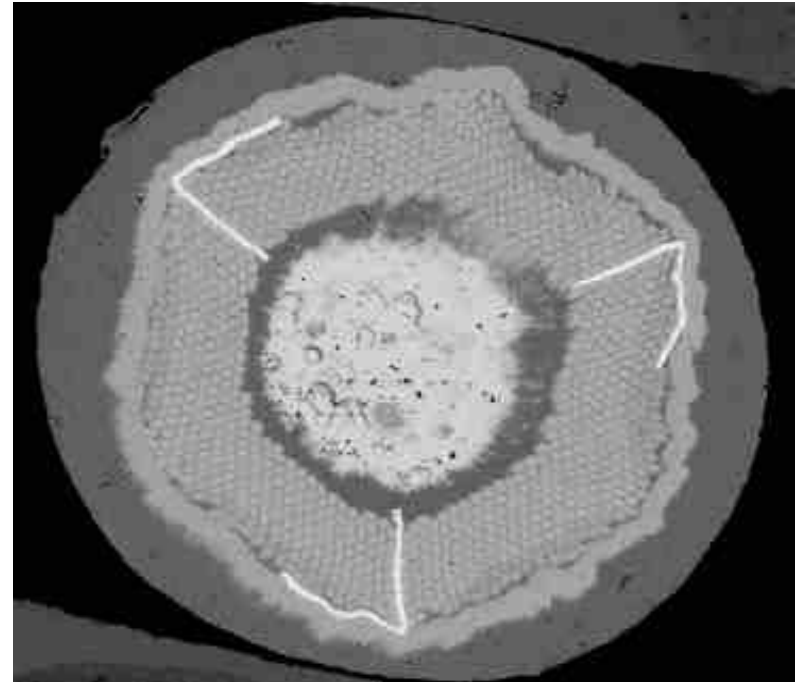
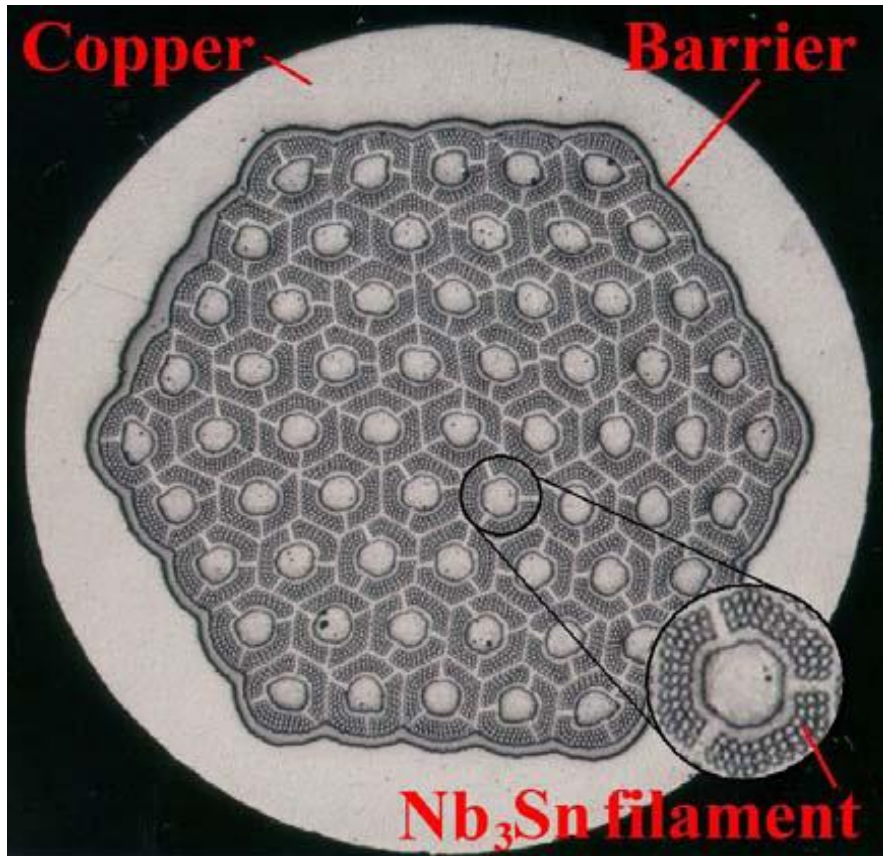
55 splitted sub-elements  
(equivalent to 330 effective filaments)



**The strands assembled with subelements, containing 3-6 groups of Nb filaments (20  $\mu\text{m}$  each), separated by the  $>1 \mu\text{m}$  spacings from each other could diminish the number of elements to be assembled in 6 times.**

# Similar approach for Internal tin strands design (subdividing of the sub-elements)

## Single and multiple diffusion barriers designs

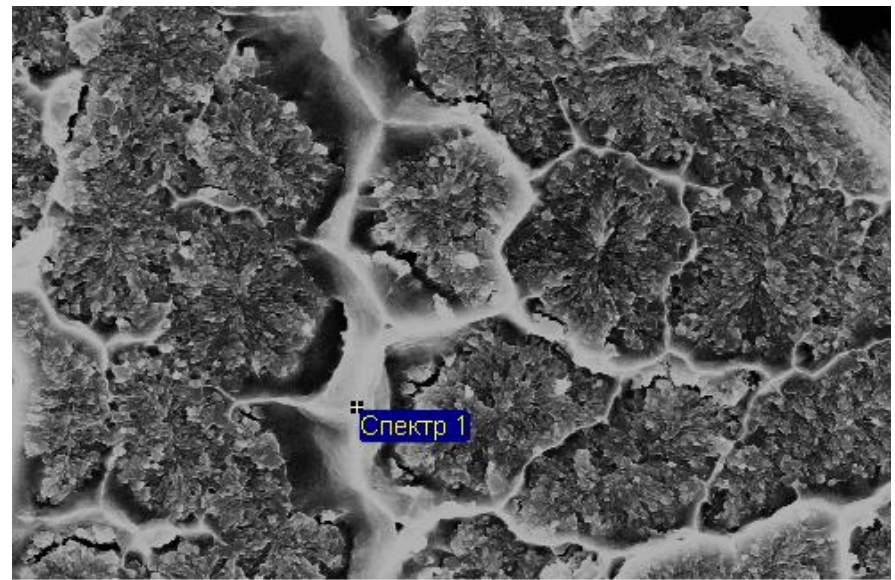
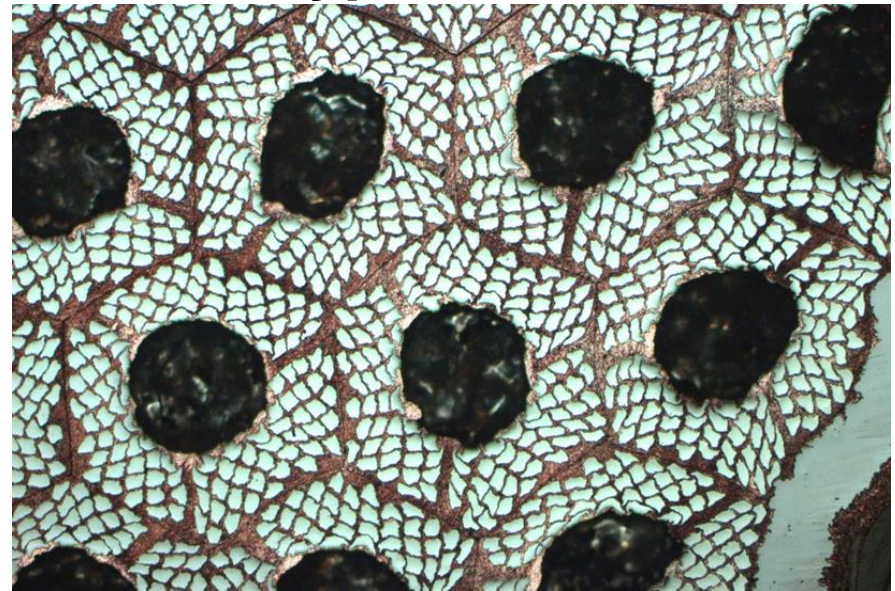
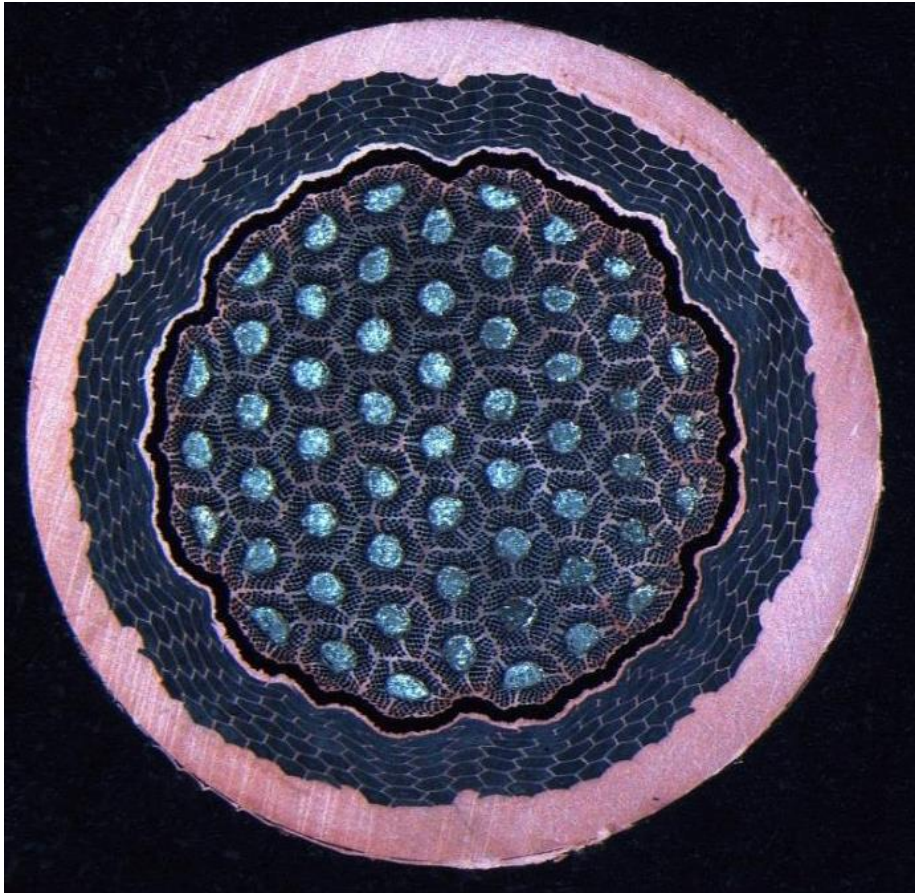


### OKAS, Supergenics

- three radial fins approach
- Ta 40 wt % Nb alloy to further subdivide Nb<sub>3</sub>Sn

# R&D and Design of the FCC –type strand

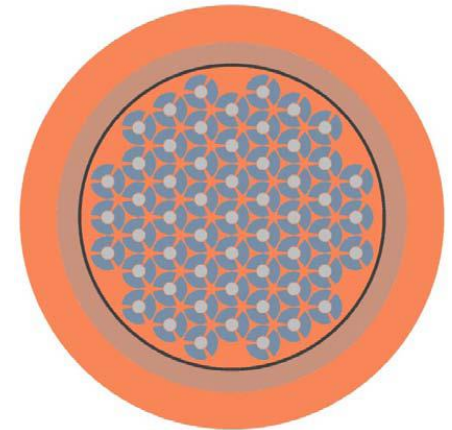
New design of Nb<sub>3</sub>Sn strand  
(55 sub-elements)  
with enhanced mechanical  
strength (Cu-Nb rods)



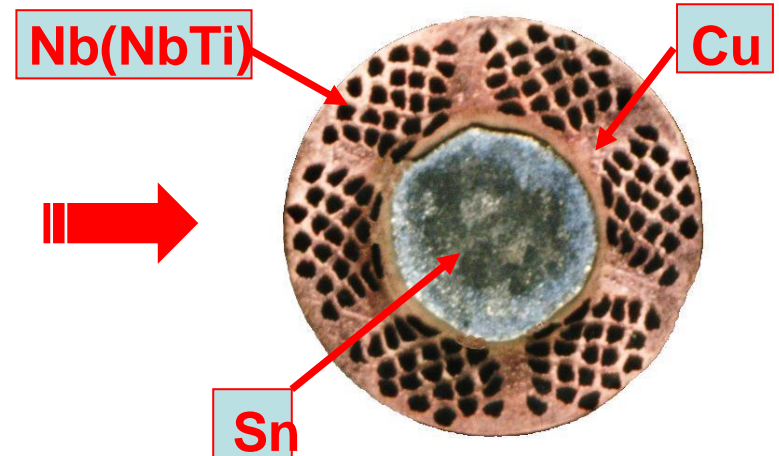
# Commercial production – Reduction of cost

## Cu-Nb subelements fabrication

The method of casting of Cu melt in Nb rods assemble for preparation of the Cu-Nb sub-elements billet has been developed



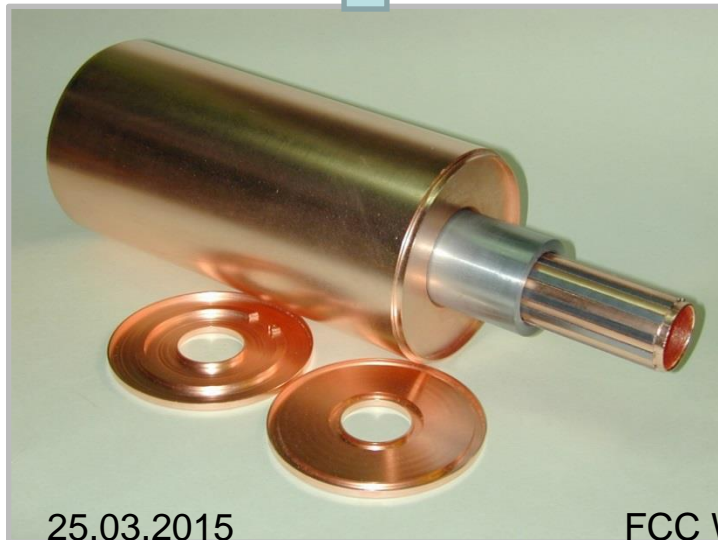
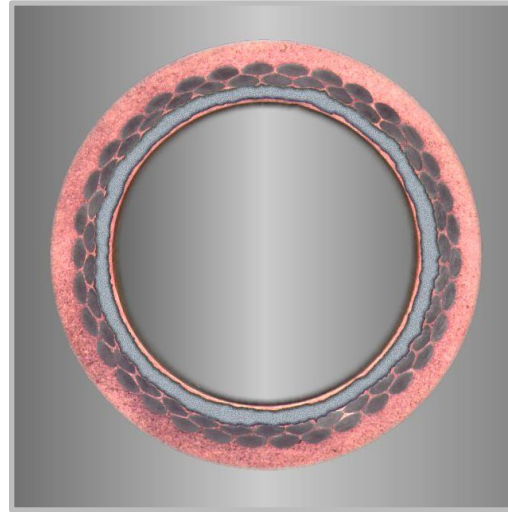
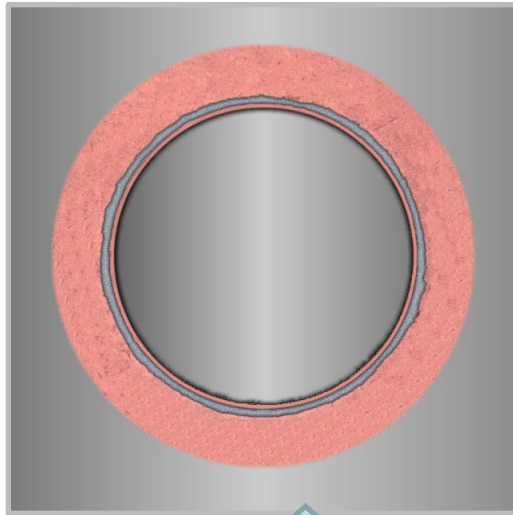
55 subelements



Diameter of Filaments bundle – ( $D_{eff}$ ) equal to approximately  $0.3 \times D$  subelement

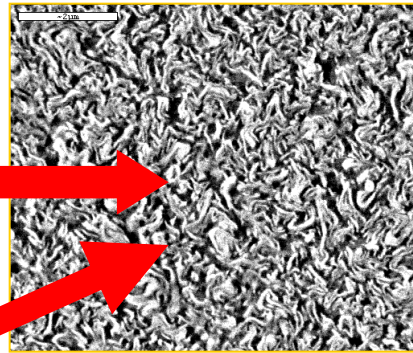
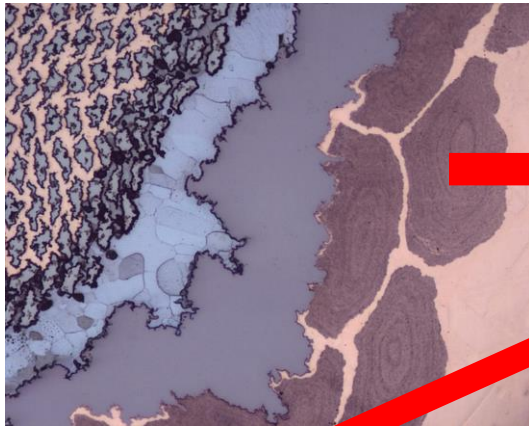
# Commercial production – Reduction of cost

Diffusion barriers with Cu stabilization and Cu-Nb strengthening

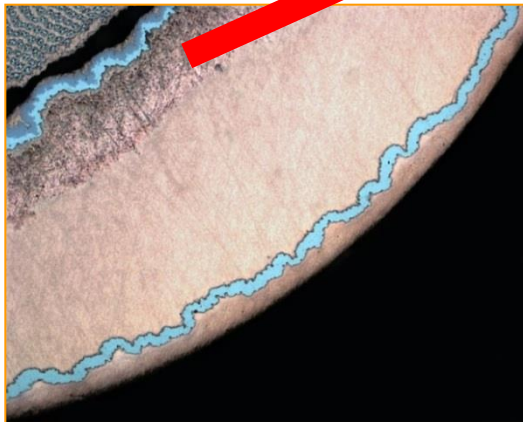


**The technology of composite (Cu-CuNb-Ta-Cu) tubes with necessary diameters (25-50 mm) and lengths (up to 5 m) is developed**

# Mitigation of deformation induced degradation of Jc and RRR by introduction of Cu-Nb strengthening elements

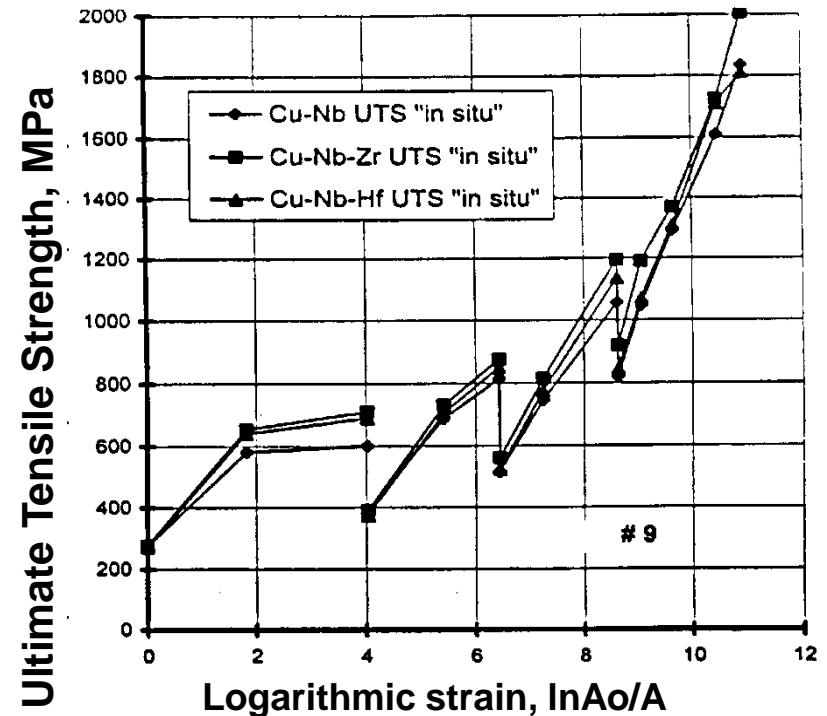


Cross section of Cu-Nb

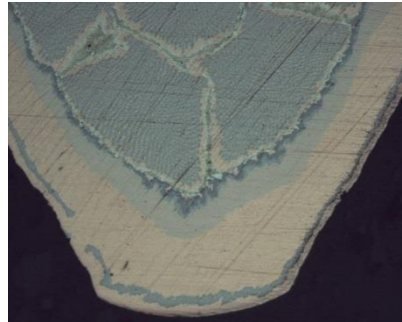
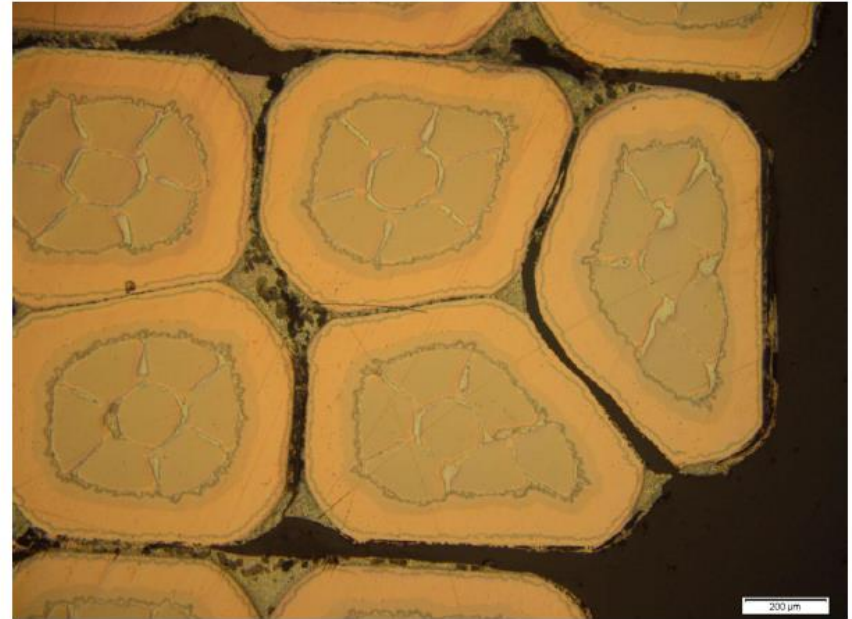
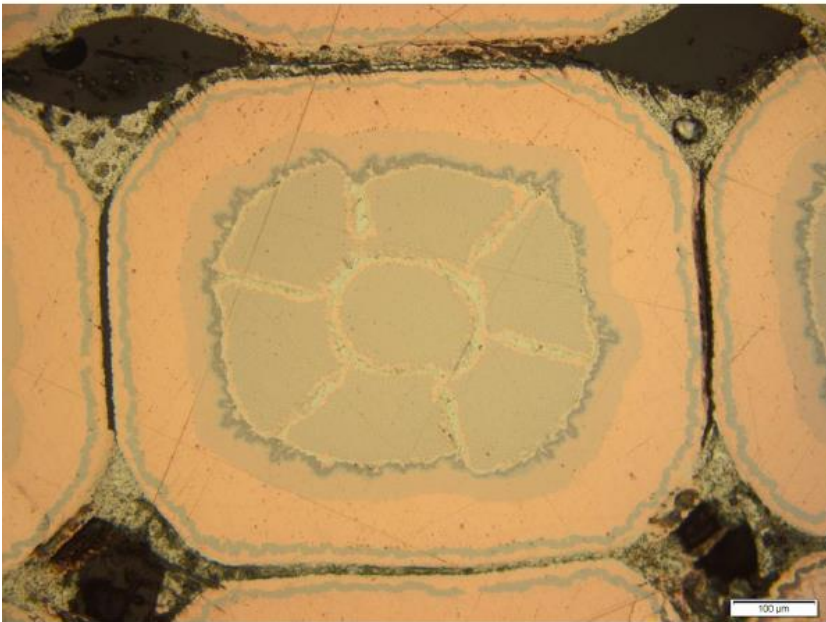
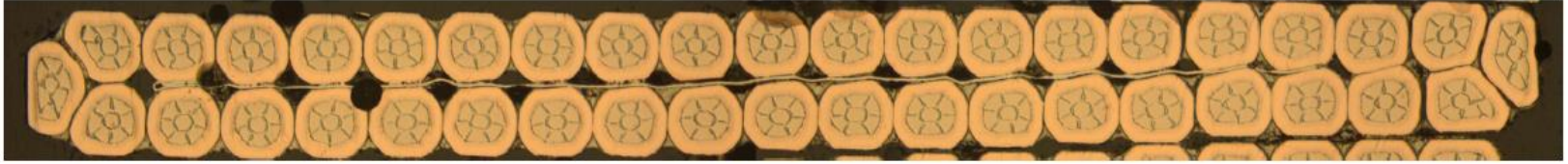


Two designs of nanostructured Cu-Nb elements – tube and rods.

The logarithmic deformation ( $\ln A_0/A$ ) of the wire should be around 7 for rods and up to 8.5 for Cu-Nb tube.



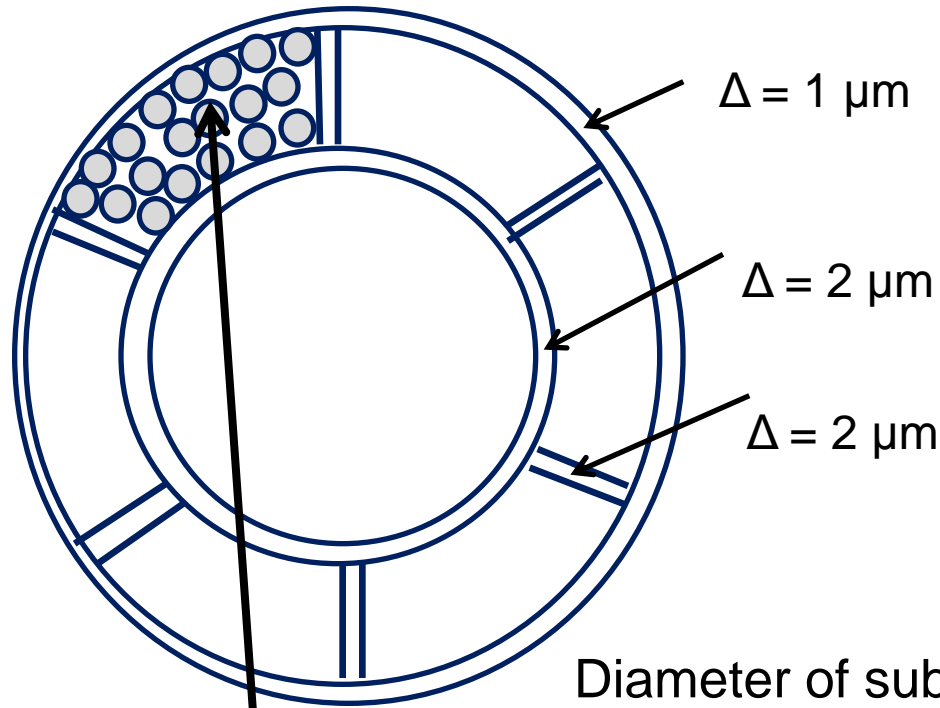
# The Rutherford cable made from strengthened $\text{Nb}_3\text{Sn}$ strands



The replacement of the part of stabilizing Cu by nanostructured Cu-Nb tubular strengthening element leads to better geometry, better uniformity and survivability of Ta diffusion barrier and prevent the diffusion of Sn in case of leakage.

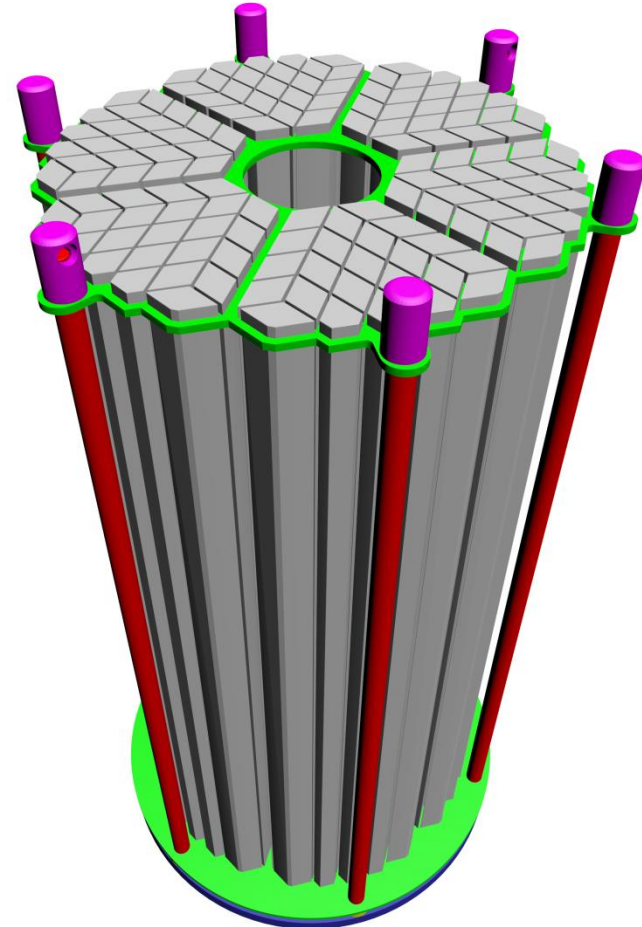


# Preliminary design of the sub-element for “Dream” IT Nb<sub>3</sub>Sn strand for FCC (Number of sub-elements 55-81)



**Local volume fraction  
of Nb ~ 70%**

Diameter of sub-element  
50-60 $\mu\text{m}$   
Extensive bridging inside  
the sub-element



<b><math>J_c = 3000 \text{ A/mm}^2</math></b>	<b><math>J_c (\text{Nb}_3\text{Sn}) \sim 5000 \text{ A/mm}^2</math></b>
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## SUMMARY

Advanced Nb<sub>3</sub>Sn IT strands with enhanced mechanical properties and high critical current density that meet the HL-LHC specifications could be produced on the base of existing technologies in RF in cooperation of Research centers (Bochvar Institute, Nanoelectro) and industrial plant (JSC ChMP).

Dream Nb<sub>3</sub>Sn IT strands for FCC magnet system require R&D on design and technology in order to meet challenging not yet attained complex of properties (Jc + D eff + RRR + cost + Unit length + mechanical properties).

Combination of several local doping (tin source, copper matrix, filament materials) altogether with optimized arrangements of filaments groups in sub-elements and the introduction of nanostructured strengthening Cu-Nb elements in stabilized copper could lead to attaining of the FCC requirements in Nb<sub>3</sub>Sn IT strands and have to be experimentally verified.