



Arc Vacuum Considerations and Beam Screen Design

Outline:

- Basic parameters of the synchrotron radiation for FCC-hh arcs
- Beam screen requirements and configuration
- LHC type beam screen
- Beam screen with absorber
- Roadmap
- Conclusion

The Synchrotron Radiation in the FCC-hh Arcs

Some Figures

FCC at nominal current and energy (0.5 A, 50 TeV), 16 T bending field:

- Critical energy: 4 keV,
- Photon flux: 10^{22} ph/s \rightarrow $1.4 \cdot 10^{17}$ ph/m/s
- Power: 2.2 MW \rightarrow $P' = 30$ W/m

By comparison, LHC at nominal current and energy (0.5 A, 7 TeV), 8.33 T bending field ($\rho=2804$ m):

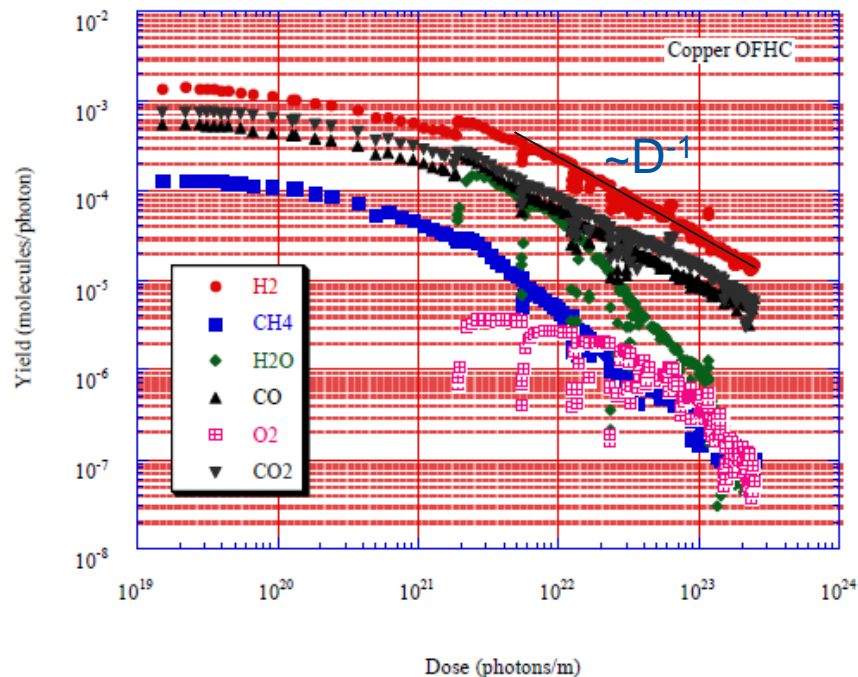
- Critical energy: 43.8 eV,
- Photon flux: $7.4 \cdot 10^{20}$ ph/s \rightarrow $4.2 \cdot 10^{16}$ ph/m/s
- Power: 3.3 kW \rightarrow 200 mW/m

Photodesorption is important for the vacuum quality in FCC-hh.

The Synchrotron Radiation in the FCC-hh Arcs

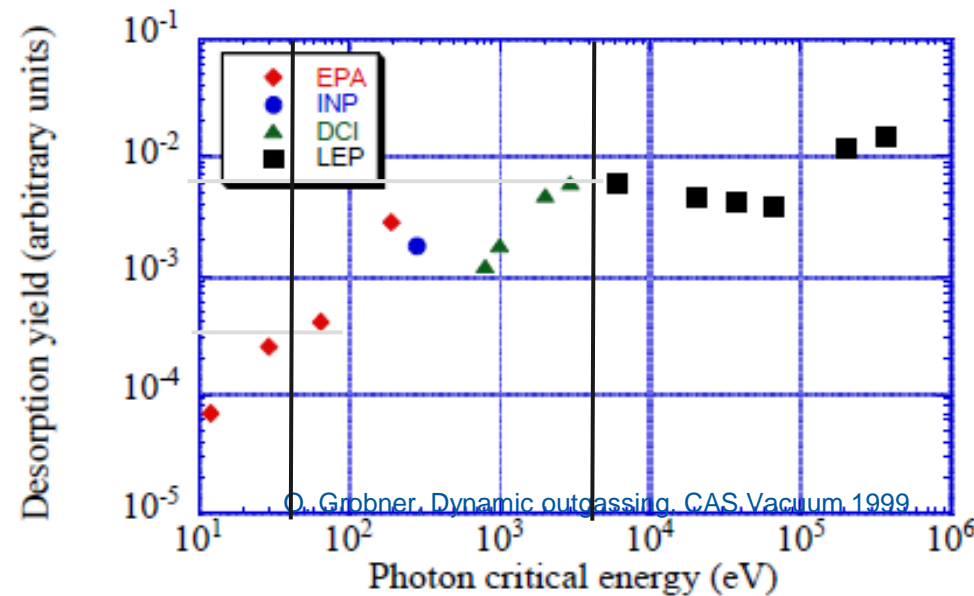
Photodesorption

Typical photodesorption yield of OFHC copper, after bake out, at room temperature, $\varepsilon_c=3.75$ keV



→ Photodesorption yield decreases as $\sim 1/D$, D being the photon dose.

Influence of the critical energy:



→ Factor ~ 17 between 4keV (FCC-hh) and 43 eV (LHC).

The Synchrotron Radiation in the FCC-hh Arcs Photodesorption

Influence of the temperature:

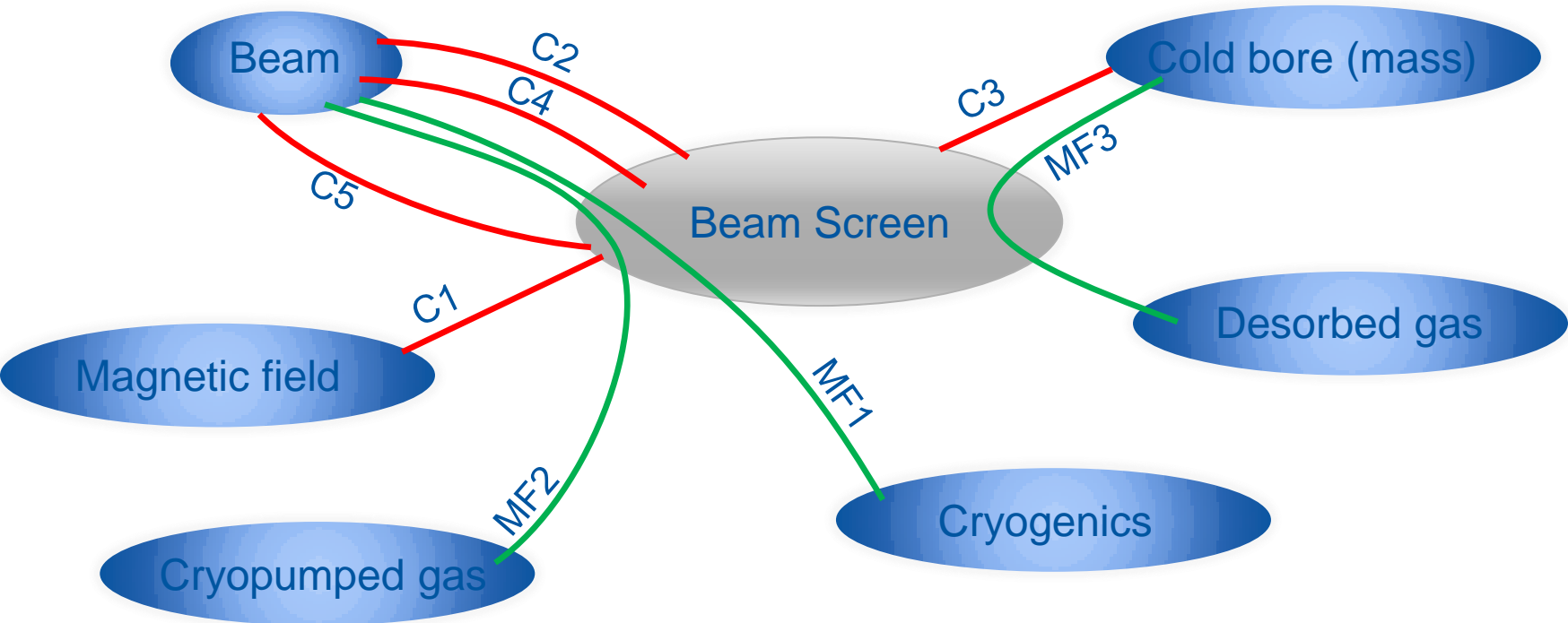
Photodesorption yields for OFE Copper, after $3 \cdot 10^{22}$ ph/m dose, $\epsilon_c=194$ eV

T[K]	H ₂	CH ₄	CO	CO ₂
5	$2 \cdot 10^{-4}$	-	-	-
78	$4 \cdot 10^{-4}$	$6 \cdot 10^{-6}$	$2 \cdot 10^{-5}$	-
114	$7 \cdot 10^{-4}$	$2 \cdot 10^{-5}$	$1 \cdot 10^{-4}$	$4 \cdot 10^{-5}$
300	$8 \cdot 10^{-4}$	$2 \cdot 10^{-5}$	$3 \cdot 10^{-4}$	$2 \cdot 10^{-4}$

V. Baglin et al., THP1B03, EPAC 2000, Vienna, Austria

→ Factor $\sim 1/2.5$ at 50 K w.r.t room temperature.

Beam Screen functions



MF1 : Intercept beam induced synchrotron power and transfer it to cryogenic cooling fluid

MF2 : Hide the cryopumped gas from beam induced photon impingement

MF3 : Provide sufficient pumping speed of desorbed gas toward the cold bore

C1: Withstand the Lorentz's forces during a quench

C2: Fulfil impedance requirements

C3: Minimise the heat loads to the cold bore

C4: Mitigate electron cloud

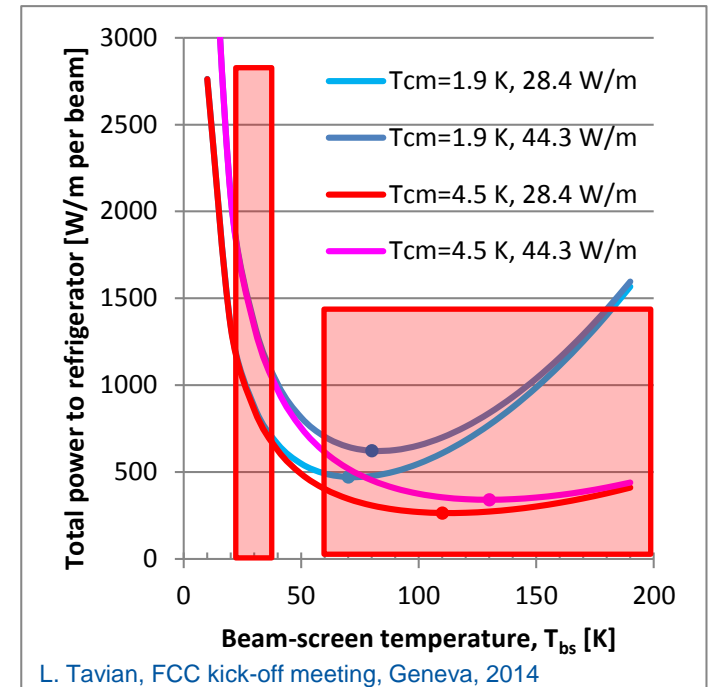
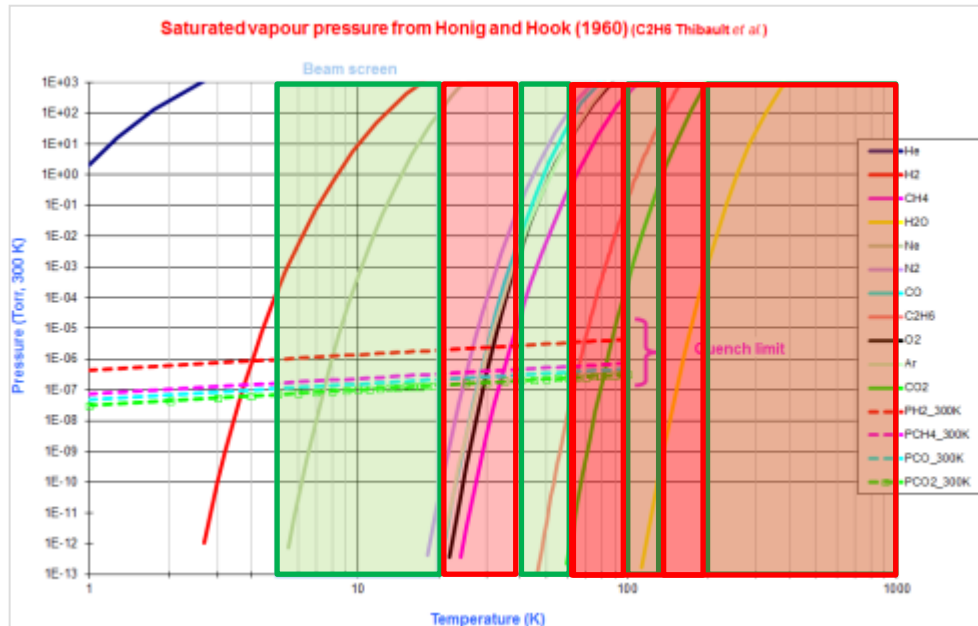
C5: Maximize the beam aperture

Beam Screen Boundary Conditions

Geometry:

- Coil inner diameter: 50 mm
- Helium radial gap: 1.5 mm (cooling of the coil and helium flow during quench)
- Cold bore thickness: 1.5 mm (stability under external pressure)

Temperature:



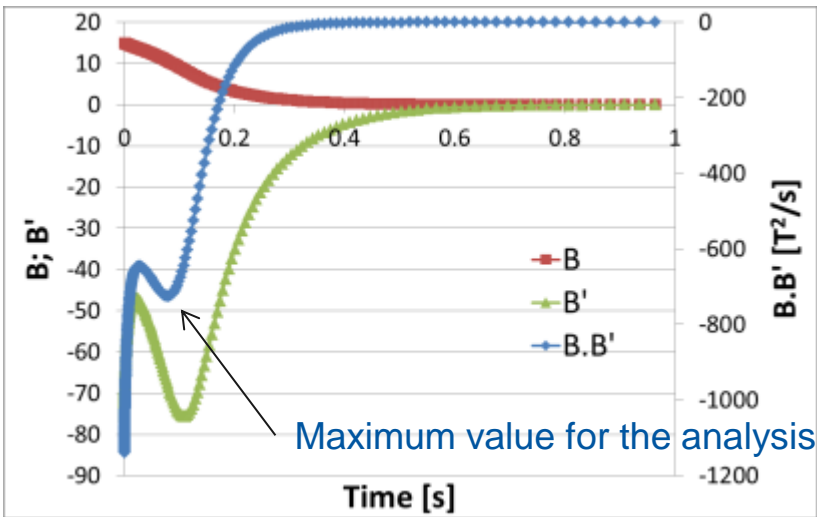
→ Beam screen temperature around 50 K.

Cold bore temperature is assumed to be **1.9 K**.

Beam Screen Boundary Conditions

Magnetic field:

- Magnetic field decay during a quench [E. Todesco]. $BB' \sim 725 \text{ T}^2 \cdot \text{s}^{-1}$



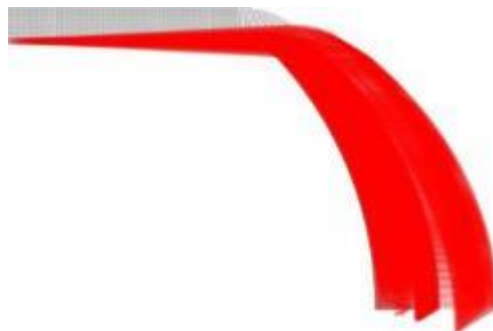
Lorentz forces during a quench are given by:

$$f = \frac{x B \dot{B}}{\rho}$$

Magnetic field

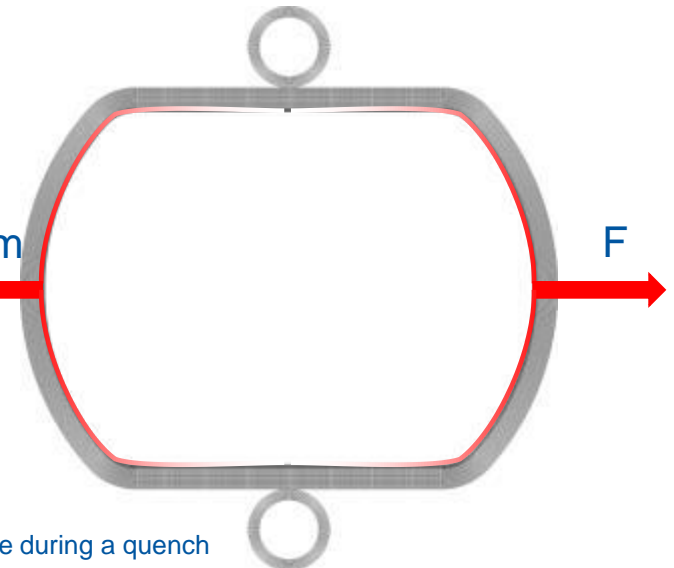
Specific force

Electrical resistivity



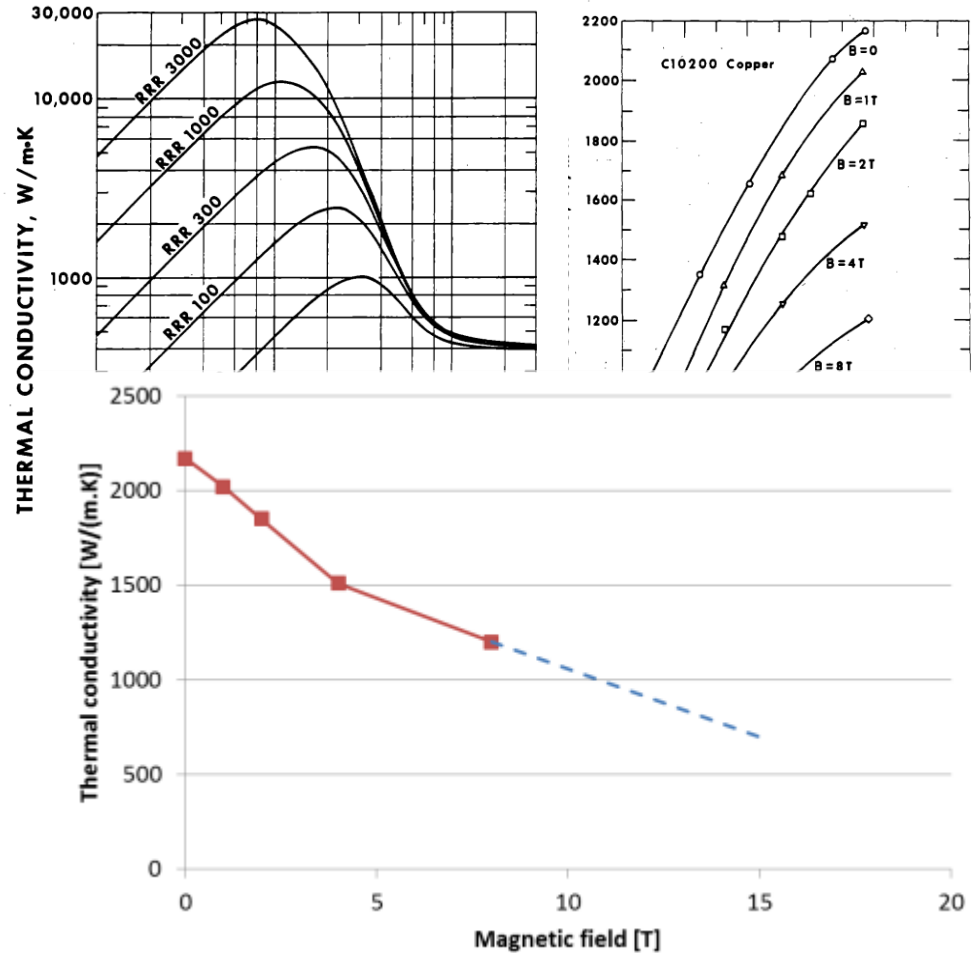
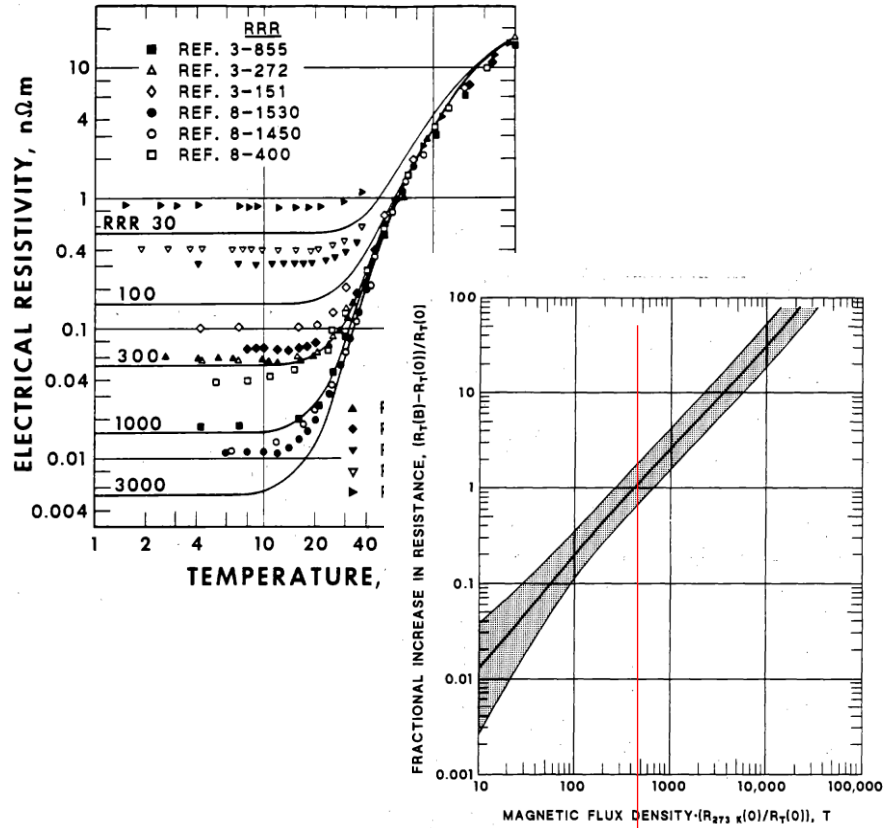
Nodal Lorentz force distribution and resulting force during a quench

$F \sim 140 \text{ N/mm}$
(* 7 LHC)



Some properties of copper

[N.J. Simon, E. S. Drexler, R.P. Reed, Properties of Copper and Copper Alloy at Cryogenic Temperatures, 1992]



→ Electrical resistivity at 50 K under 16 T : 1 $\text{n}\Omega\cdot\text{m}$

→ Thermal conductivity at 50 K under 16 T : 700 $\text{W}/(\text{m}\cdot\text{K})$

LHC-type Beam Screen

Configuration

Cooling tube:

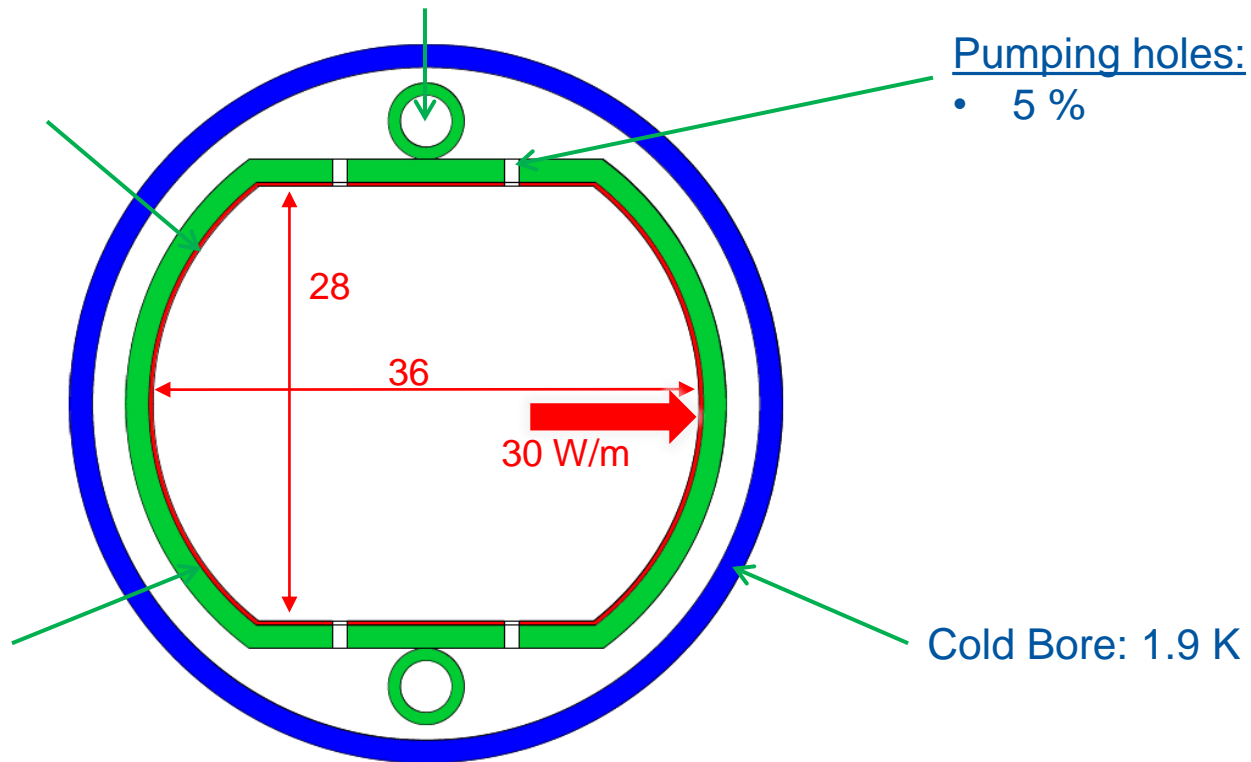
- Heat transfer coefficient: $150 \text{ W}/(\text{K}\cdot\text{m}^2)$
- Refrigerant temperature: 40 K

Copper layer:

- 0.3 mm ,
- $k \sim 700 \text{ W}/(\text{m}\cdot\text{K})$,
- $\sigma_y = 70 \text{ MPa}$

Pumping holes:

- 5%



Stainless steel:

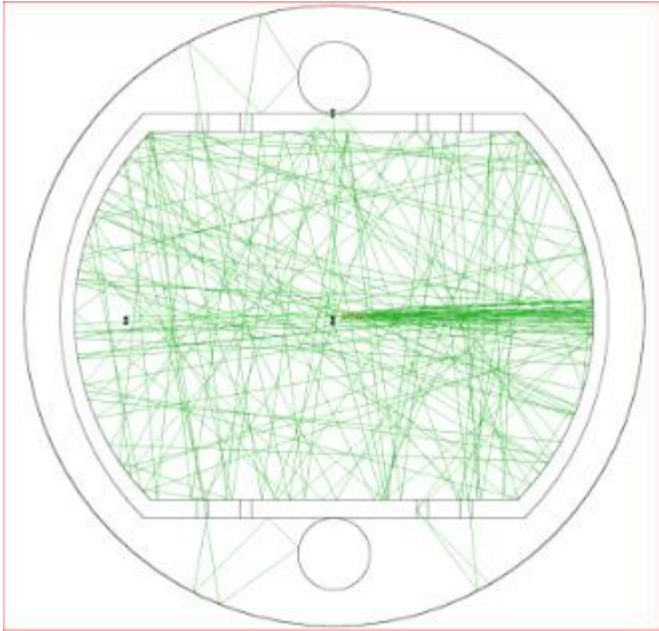
- 1.5 mm ,
- $k \sim 6 \text{ W}/(\text{m}\cdot\text{K})$,
- $\sigma_y = 1200 \text{ Mpa}$,
- $E: 240 \text{ GPa}$

LHC-like BS solution

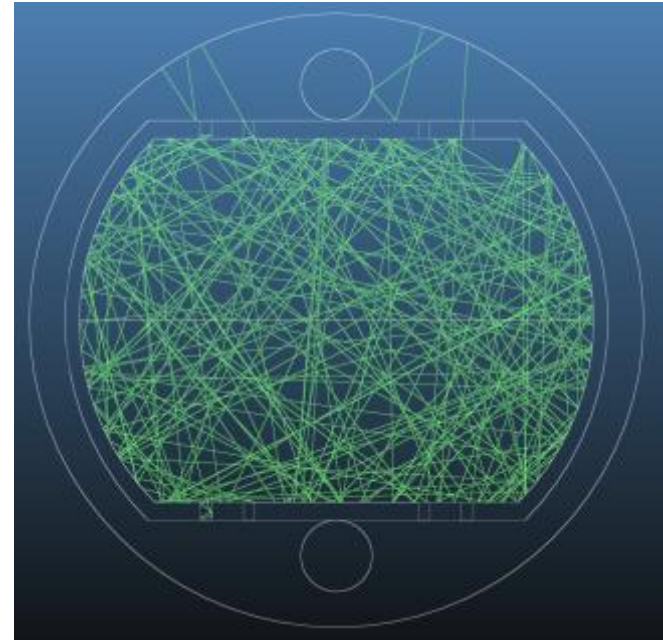
LHC-type Beam Screen

Vacuum study

1. Simulation of the flux and power distribution of the synchrotron light (Synrad+)



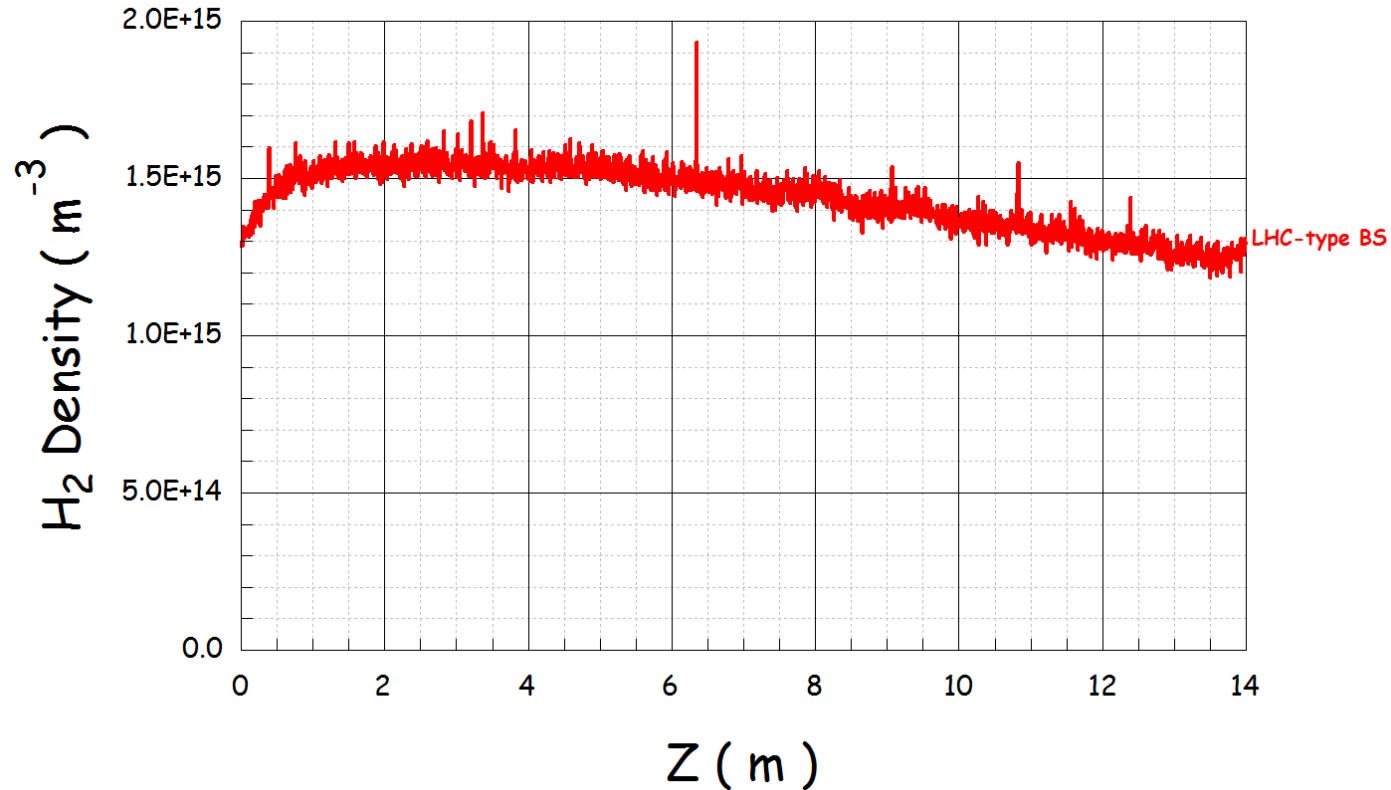
2. Simulation of the photon stimulated desorption and gas density (Molflow+)



All SR-induced gas load may interact with the beam.

LHC-type Beam Screen

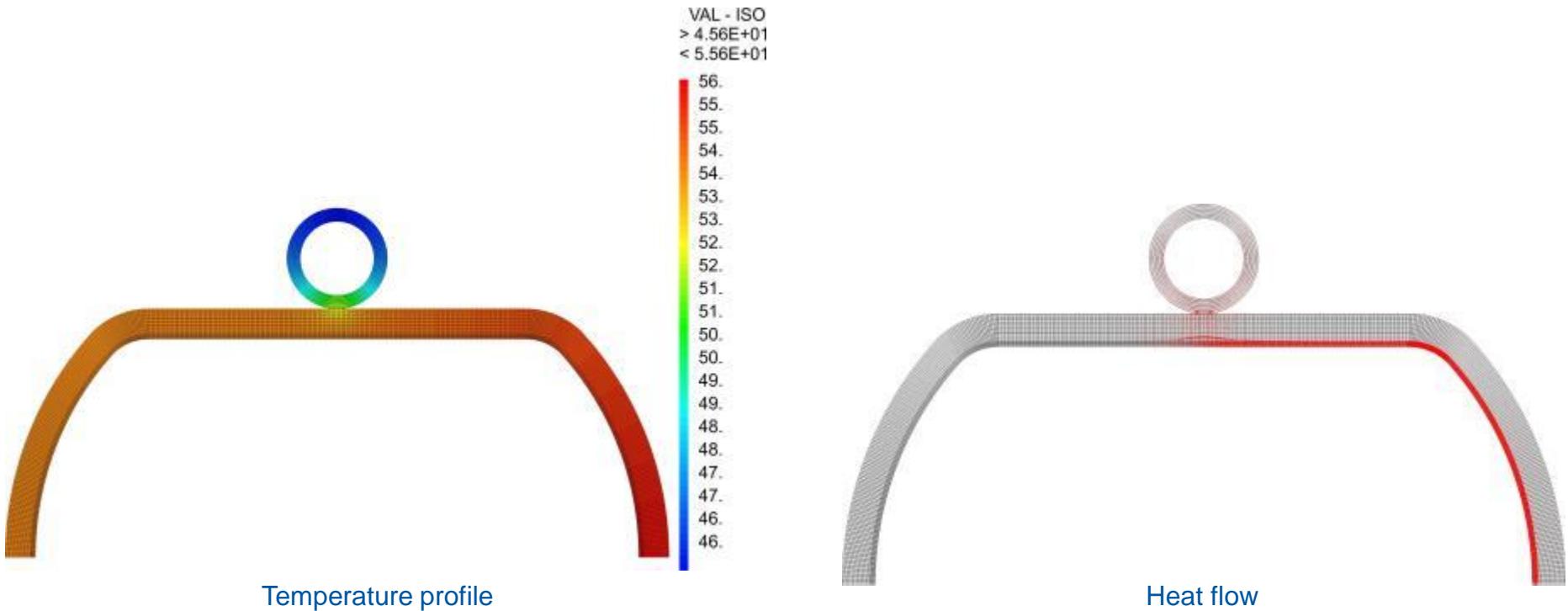
Vacuum study



A gas density, slightly higher than 10^{15} molecules/ m^3 , is expected after 1 day at nominal current and energy.

LHC-type Beam Screen

Thermal study

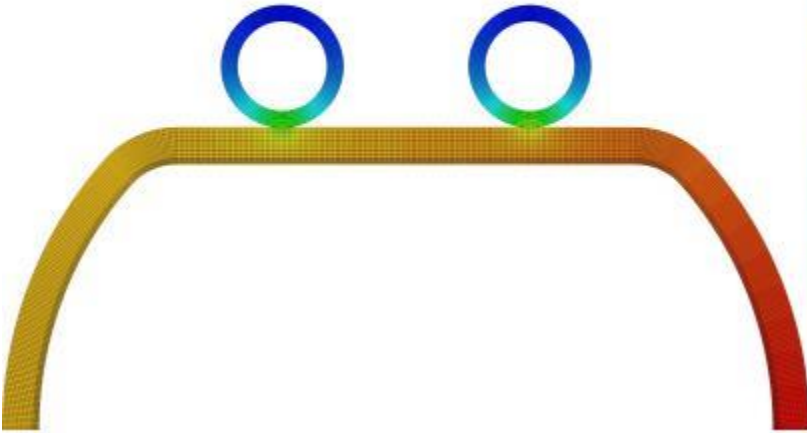
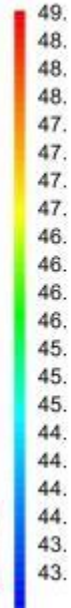


- Temperature difference between refrigerant and beam screen: ~ 16 K.
- Temperature gradient along the copper layer: ~ 2 K.
- Heat carried by the copper layer.

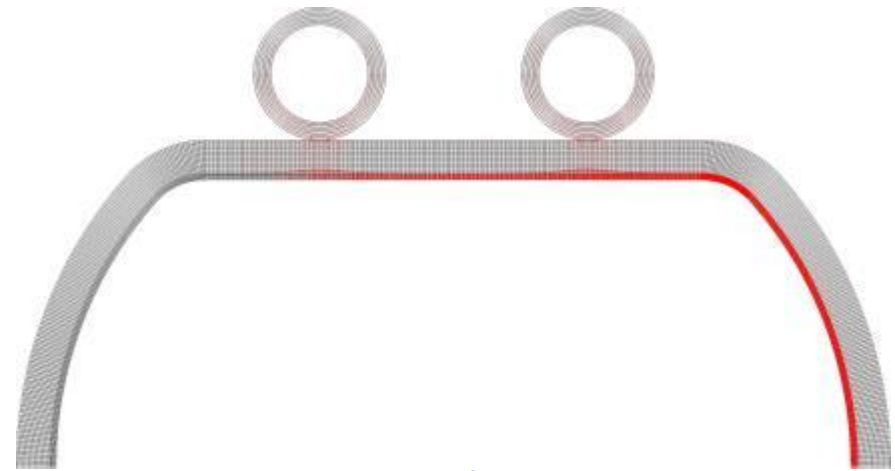
LHC-type Beam Screen

Thermal study

VAL - ISO
> 4.28E+01
< 4.87E+01



Temperature profile

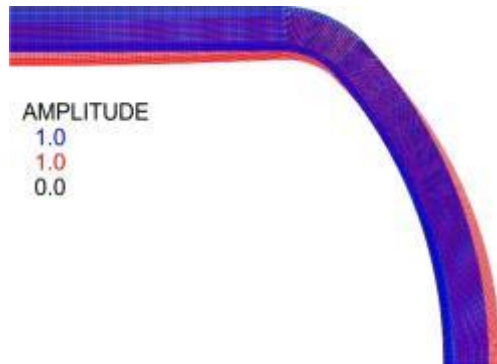


Heat flow

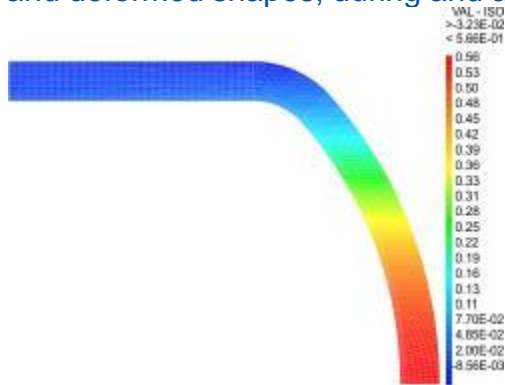
- Temperature difference between refrigerant and beam screen: ~ 9 K.
- Temperature gradient along the copper layer: ~ 1.6 K.
- Heat carried by the copper layer.

LHC-type Beam Screen

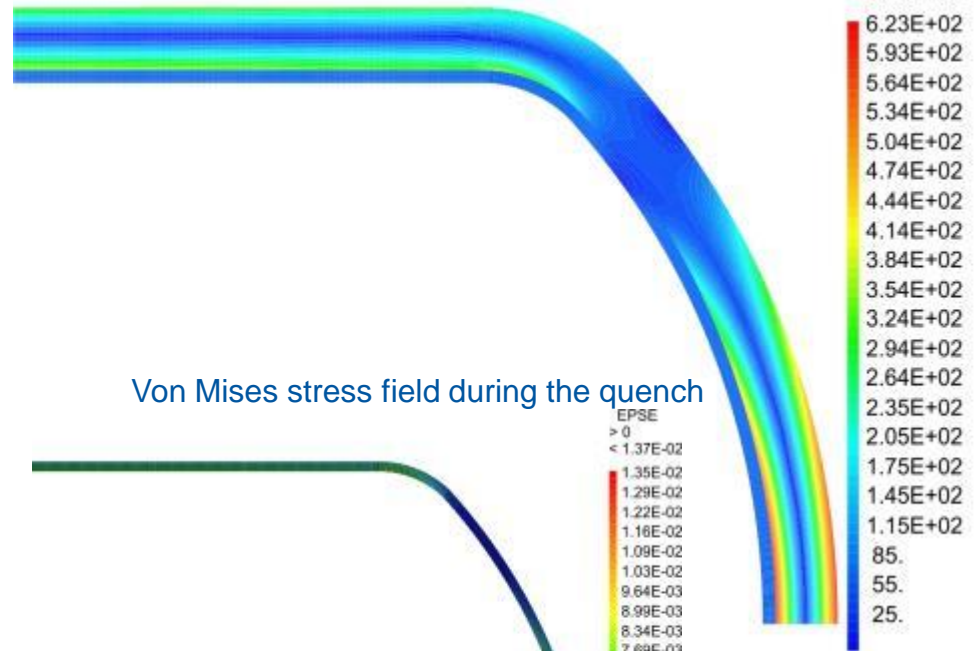
Mechanical study – Deformation, stress & strain fields



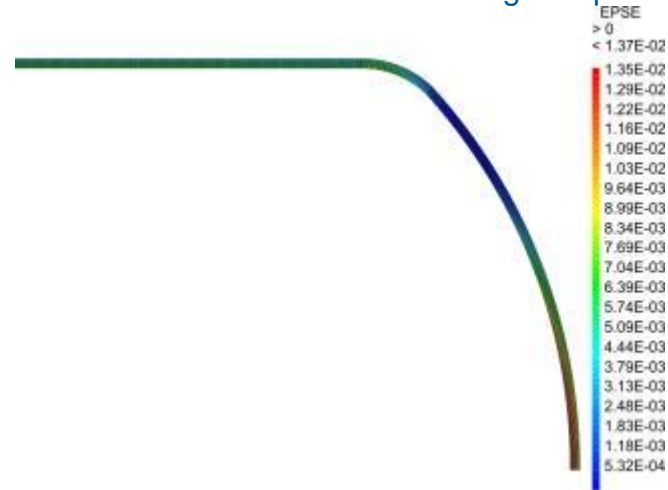
Initial and deformed shapes, during and after a quench



Horizontal displacement during the quench



Von Mises stress field during the quench

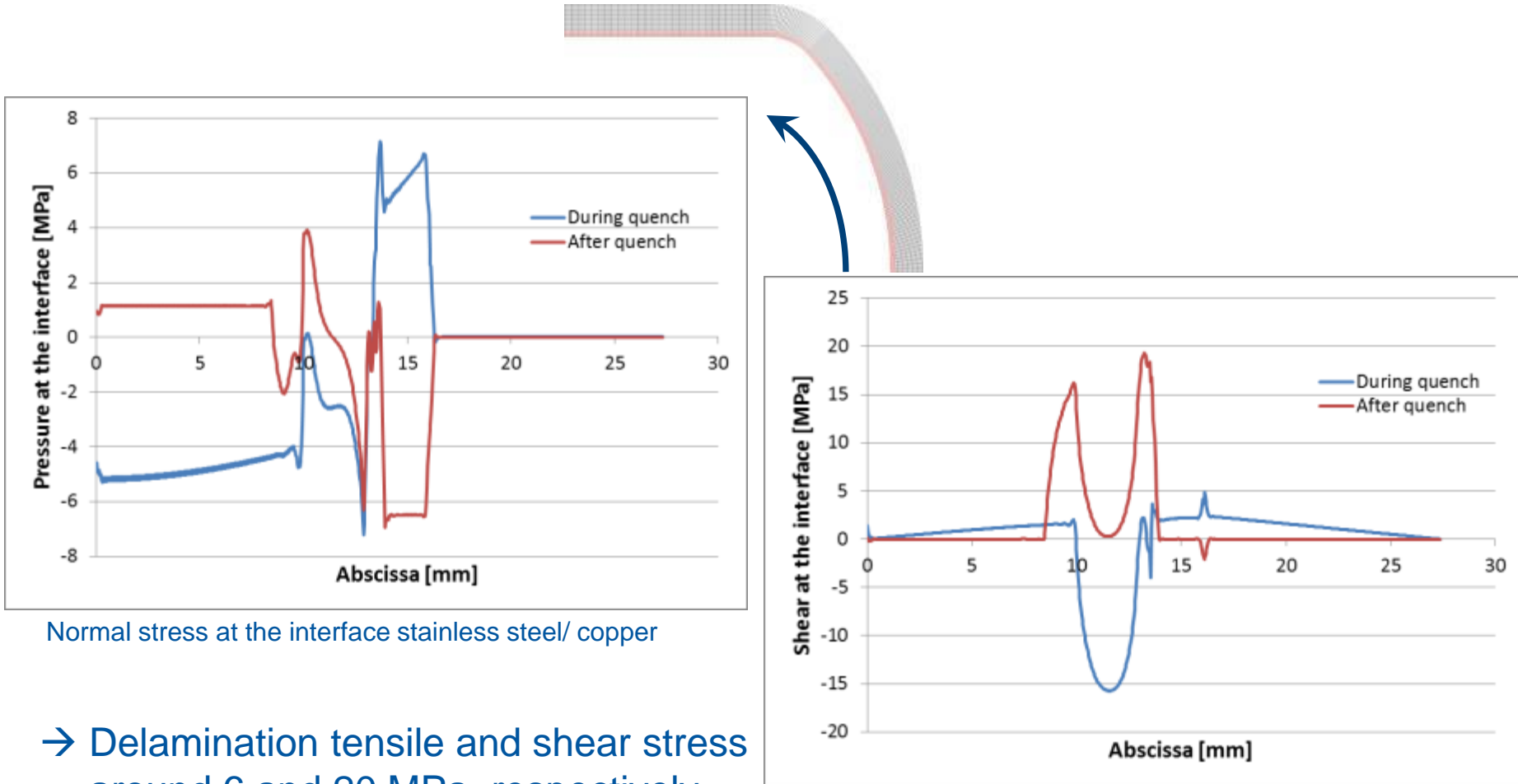


Plastic strain in the copper after the quench

- No significant overall plastic deformation of the beam screen
- Plastic deformation of the copper layer

LHC-type Beam Screen

Mechanical study – Interface copper/stainless steel



→ Delamination tensile and shear stress around 6 and 20 MPa, respectively

Beam Screen with absorber

Configuration

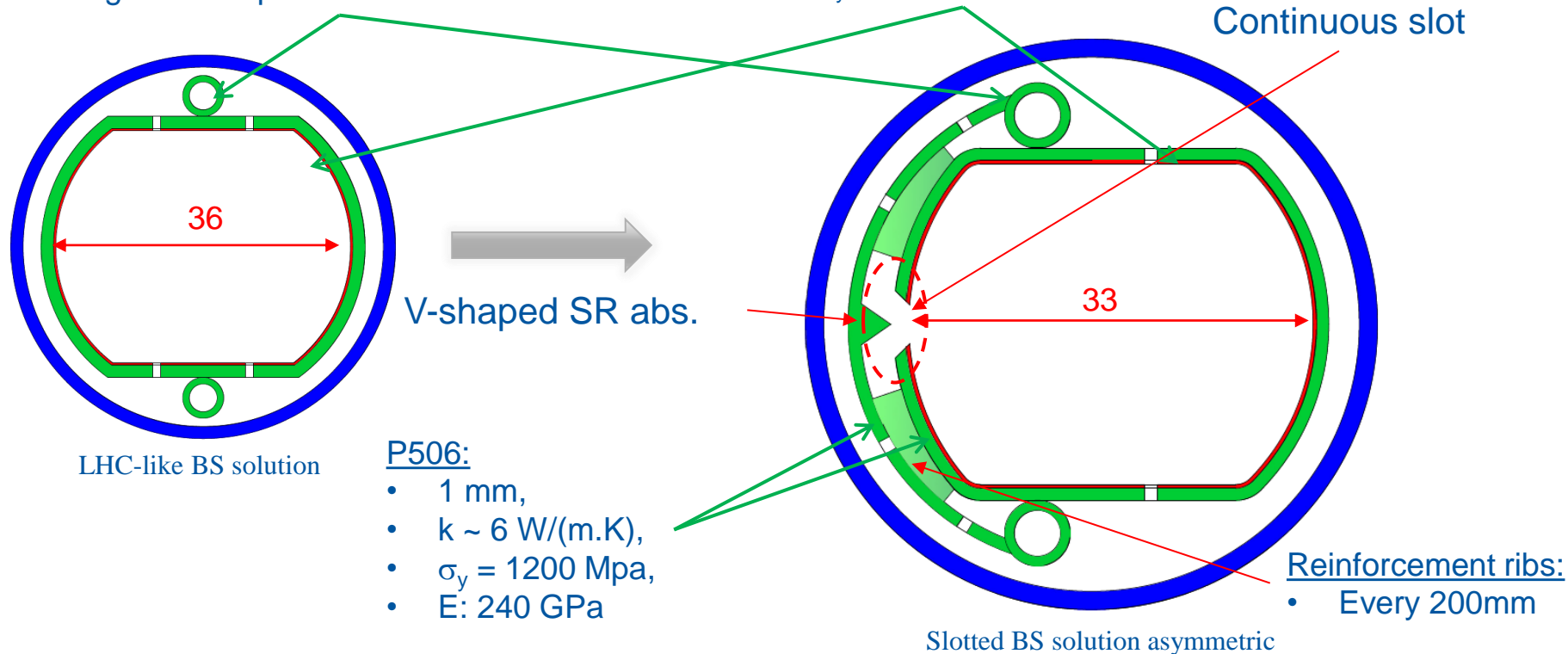
A combined BS, made up of a LHC-like BS with a continuous slot and an “external” SR power absorber is proposed.

Cooling tube:

- Heat transfer coefficient: $150 \text{ W}/(\text{K}\cdot\text{m}^2)$
- Refrigerant temperature: 40 K

Copper layer:

- 0.3mm,
- $k \sim 700 \text{ W}/(\text{m}\cdot\text{K})$,
- $\sigma_y = 70 \text{ MPa}$



LHC-like BS solution

V-shaped SR abs.

P506:

- 1 mm,
- $k \sim 6 \text{ W}/(\text{m}\cdot\text{K})$,
- $\sigma_y = 1200 \text{ Mpa}$,
- $E: 240 \text{ GPa}$

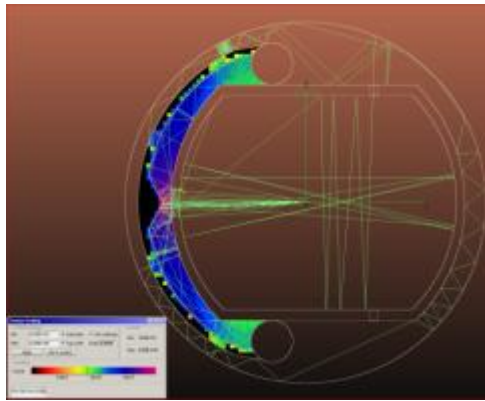
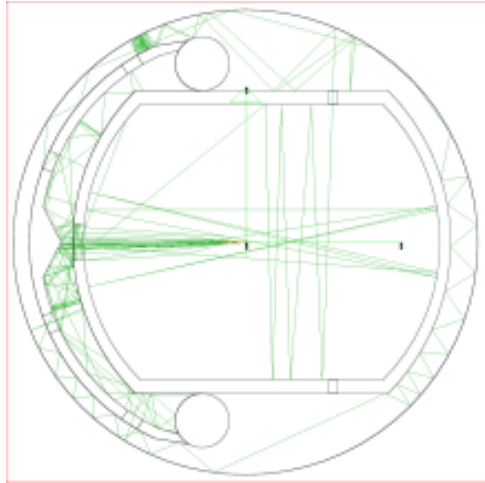
Slotted BS solution asymmetric

Reinforcement ribs:

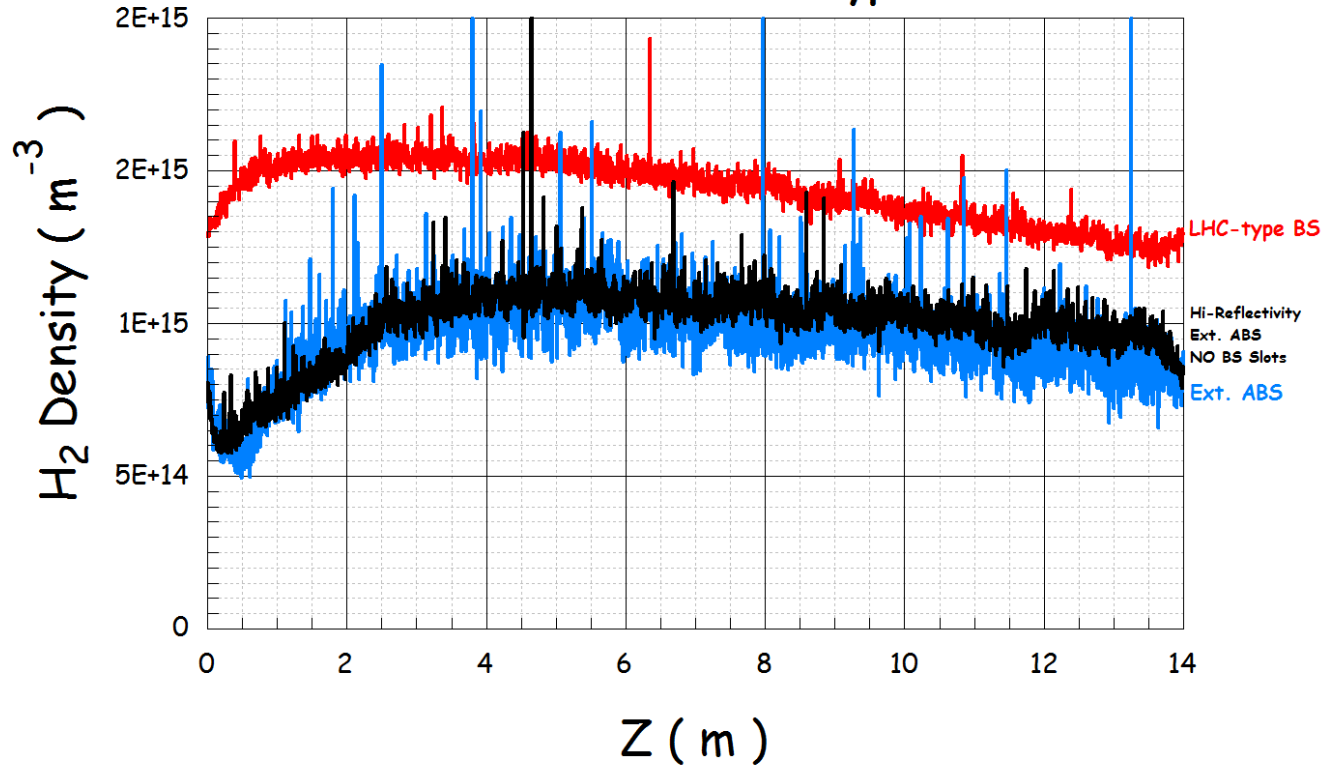
- Every 200mm

Beam Screen with absorber

Vacuum study



FCC-hh: Comparison of Pressure Profiles vs Beam-Screen Type



Monte Carlo simulations of photon distribution

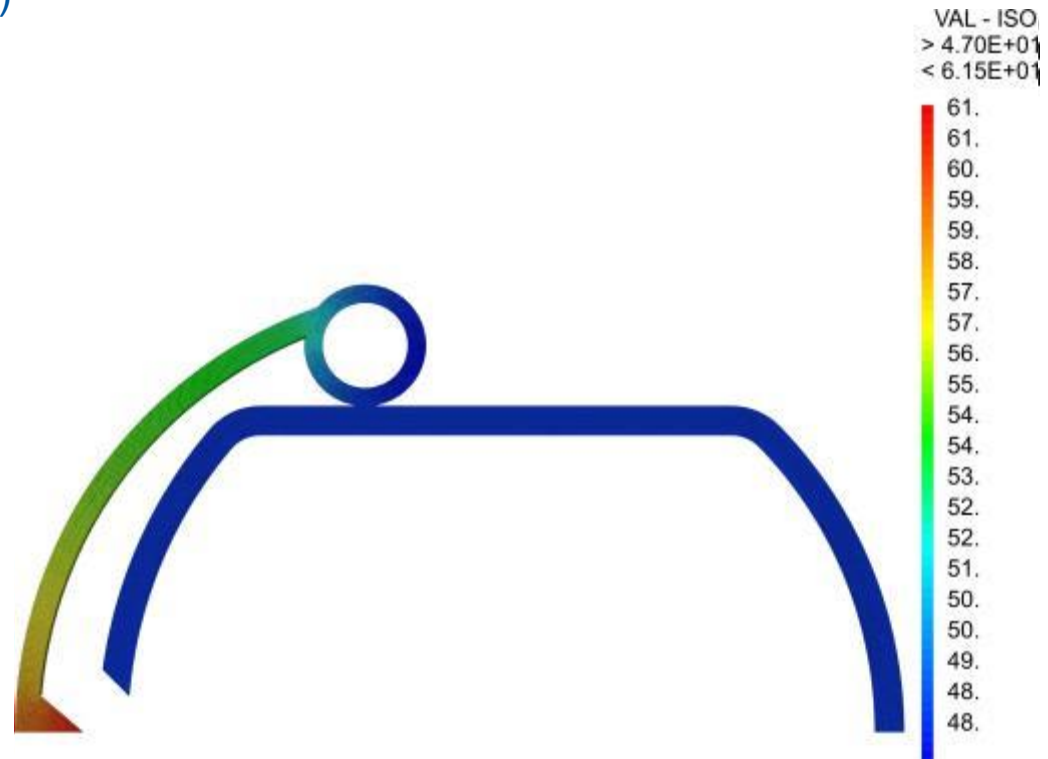
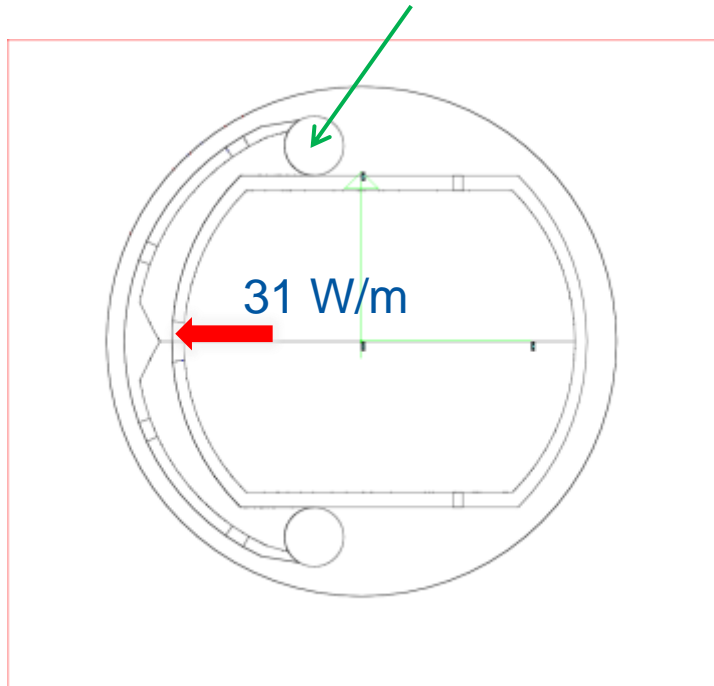
A gas density of around 10^{15} molecules/m³ is expected after 1 day at nominal current and energy.

Beam Screen with absorber

Thermal study

Cooling tube:

- Heat transfer coefficient: $150 \text{ W}/(\text{K}\cdot\text{m}^2)$
- Refrigerant temperature: 40 K

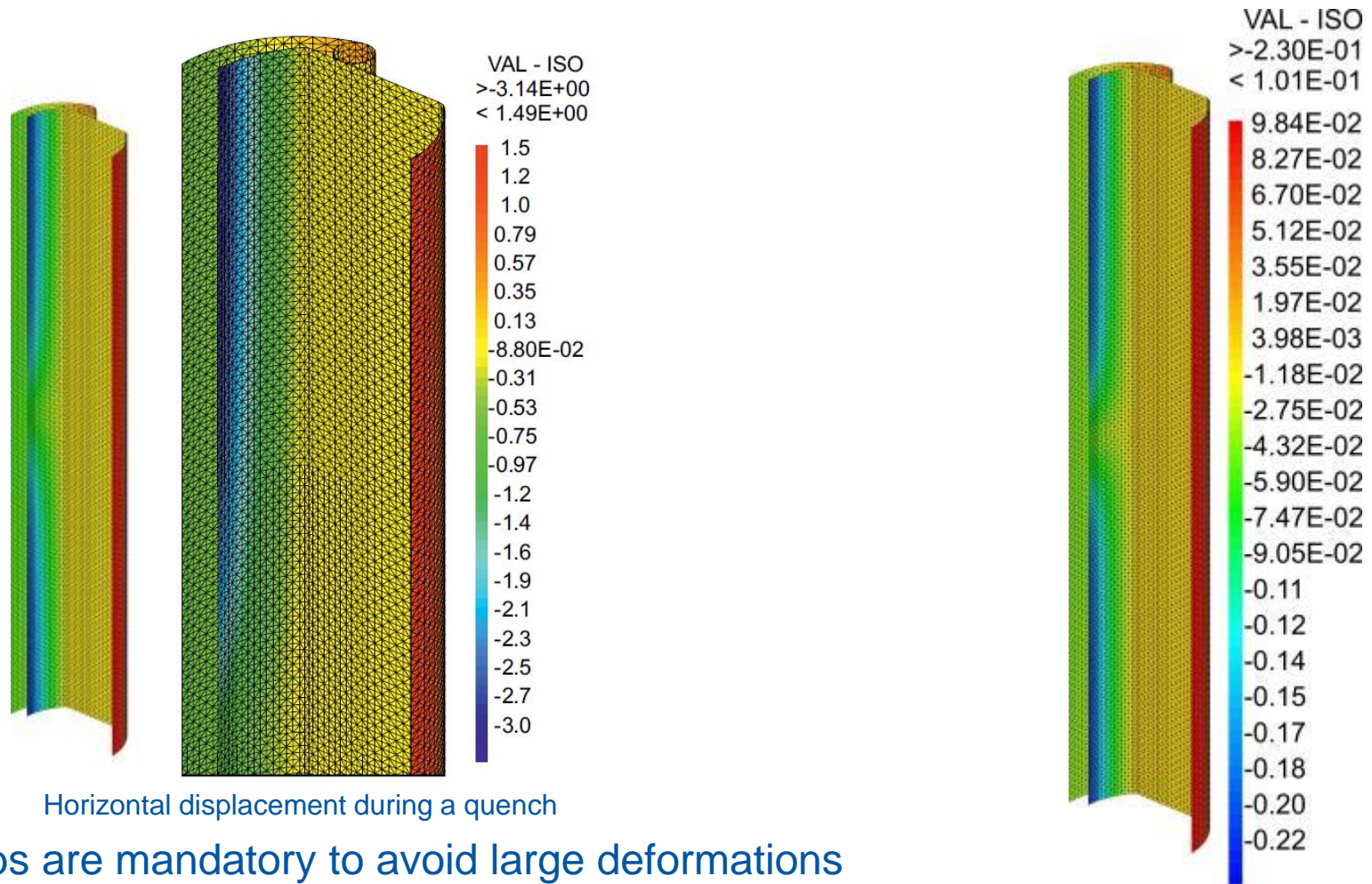


Temperature profile with 0.1 mm copper layer on the absorber

Heat carried by the low thermal conductivity absorber \rightarrow high temperature : $\sim 100 \text{ K}$
Thermal conductive layer required.

Beam Screen with absorber

Mechanical study - Displacements



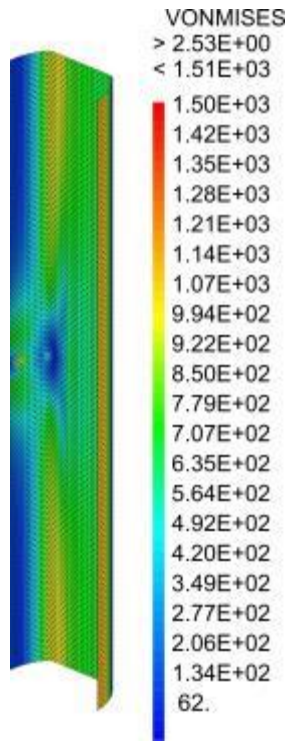
Horizontal displacement during a quench

Residual horizontal displacement after a quench

- Ribs are mandatory to avoid large deformations
- Residual deformation after the quench

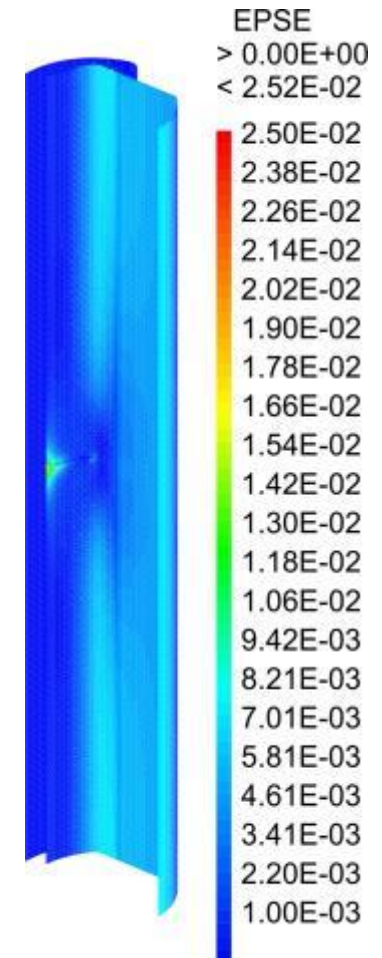
Beam Screen with absorber

Mechanical study – stress, strain fields



Von Mises stress field in the beam screen wall

- High stress level in the beam screen
- Plastic deformation of the copper layer
- ⇒ Increase the thickness and/or higher strength material (titanium alloy)

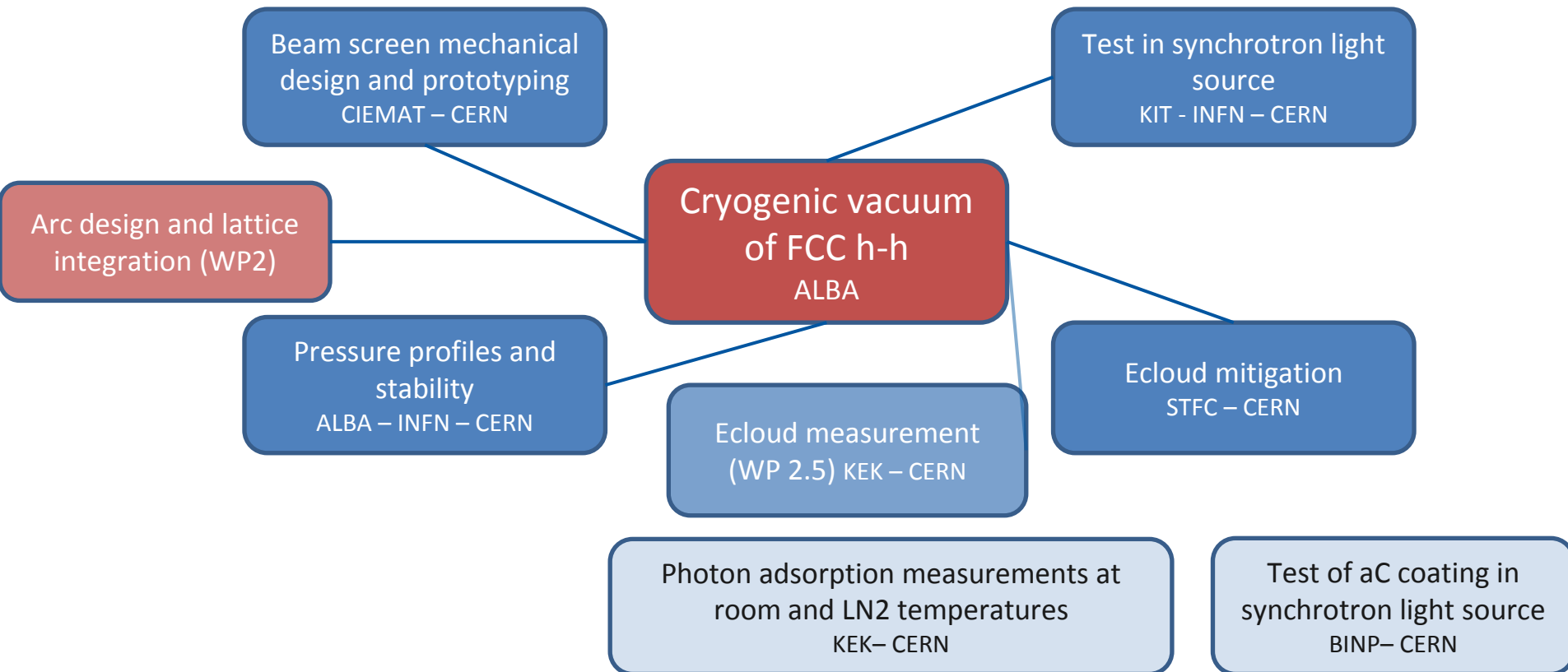


Plastic strain field in the copper after a quench

Roadmap

The technical design concept for the FCC-hh beam-pipe is covered by the cryogenic beam vacuum system work package (WP4) of the European Circular Energy-Frontier Collider Study (EuroCirCol).

Several participants are involved:



Roadmap

Deliverables:

- | | |
|---|--------|
| 1. Analysis of vacuum stability at cryogenic temperature | Oct-16 |
| 2. Preliminary beam screen and beam pipe engineering design | May-17 |
| 3. Measurements of vacuum chamber at light source | Sep-17 |
| 4. Analysis of beam-induced vacuum effects | Nov-17 |
| 5. Preliminary cryogenic-beam-vacuum system design | Sep-18 |

Milestones:

- | | |
|---|---------|
| 1. WP group established and hiring complete | May-15 |
| 2. Beam screen model heat load and photo-electrons density analysis | Dec-15 |
| 3. Measurement setup at light source operational | Mar-16 |
| 4. Proposal of coatings to mitigate electron-cloud effects | Jun- 16 |
| 5. Report on recommended follow-up R&D | Dec-18 |

Conclusions

Preliminary concepts of the FCC-hh beam screen are under study. Vacuum, thermal and mechanical aspects have to be integrated.

The design of the FCC-hh cryogenic vacuum system is very challenging:

- From a technical point of view:
 - Dynamic vacuum
 - Heat transfer of the synchrotron radiation power
 - Mechanical stability, in particular during a quench
 - Material properties at cryogenic temperature under high magnetic field
- From an organizational point of view:
 - Several collaborators
 - Different expertise
 - New setups

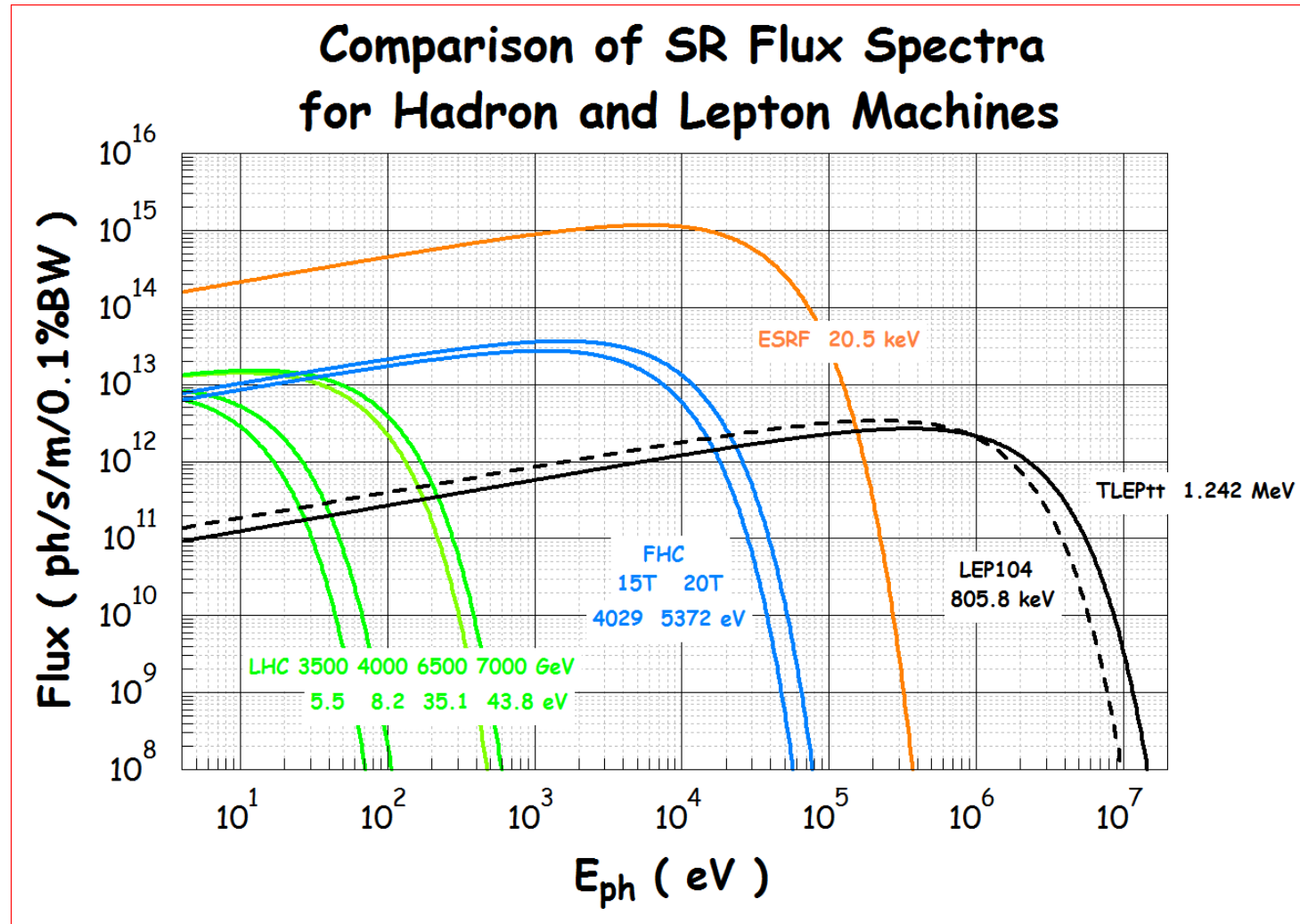
Both are very exciting.

Thanks for your attention



The Synchrotron Radiation in the FCC-hh Arcs

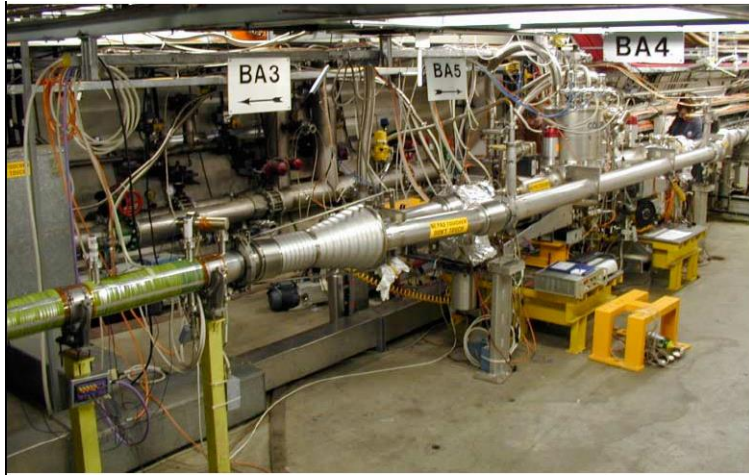
SR spectra



Electron cloud mitigation: anti-multipacting coating or surface treatment

Coating:

- Amorphous carbon coating
- Operating temperature at 40-60 K
- Tests ongoing in ColdEx (SPS beam)



~2.2 m, ID 67 beam screen
Internally coated with amorphous carbon



Surface treatment:

- Laser induced surface texture []
- Operating temperature at 40-60 K