

RF Cavity Design - an introduction -



Oxford – John Adams Institute

03 December 2014

Ciprian Plostinar

Overview

Part 1:

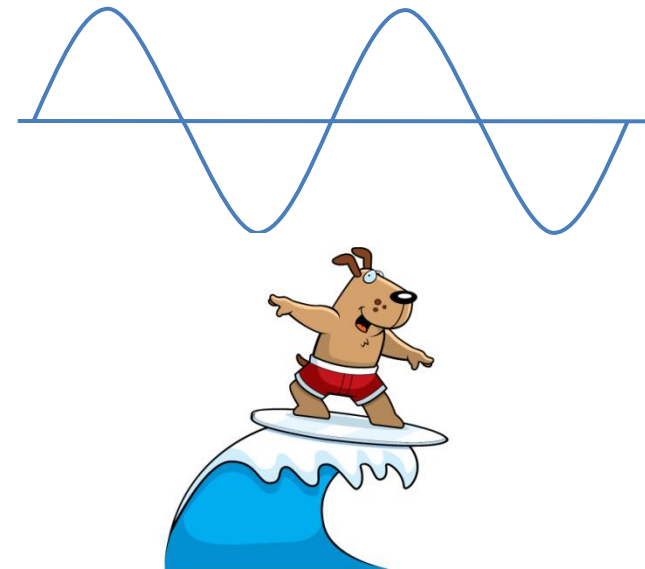
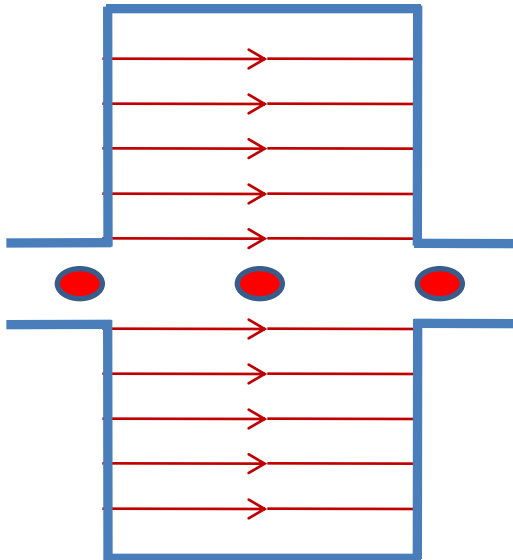
- RF Cavity Design
 - Design Criteria
 - Figures of Merit
- Introduction to Superfish (2D)
- Examples:
 - Pill-box type cavity
 - DTL type cavity
 - Elliptical cavity
 - A ferrite loaded cavity

Part 2:

- CST MicroWave Studio Demo (3D)
- Surprise Cavity Model
- A Simple Measurement

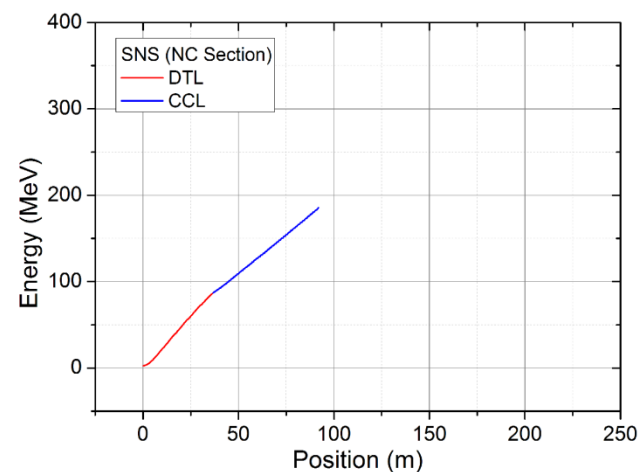
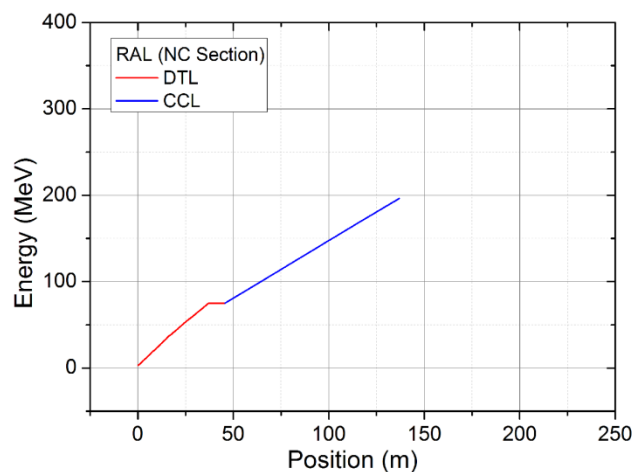
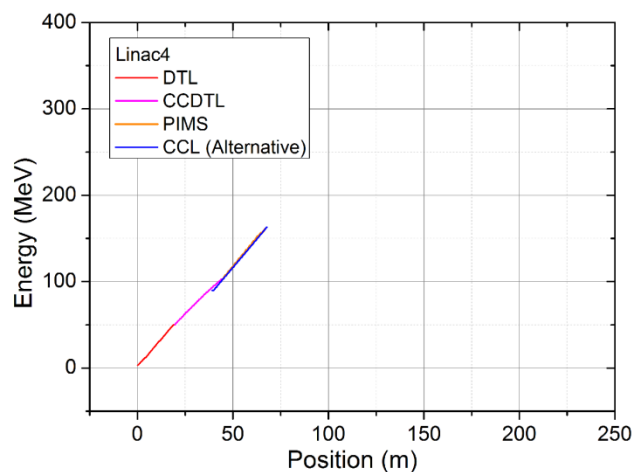
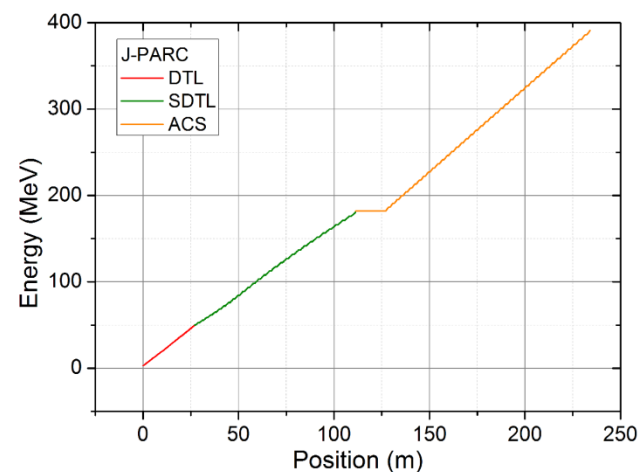
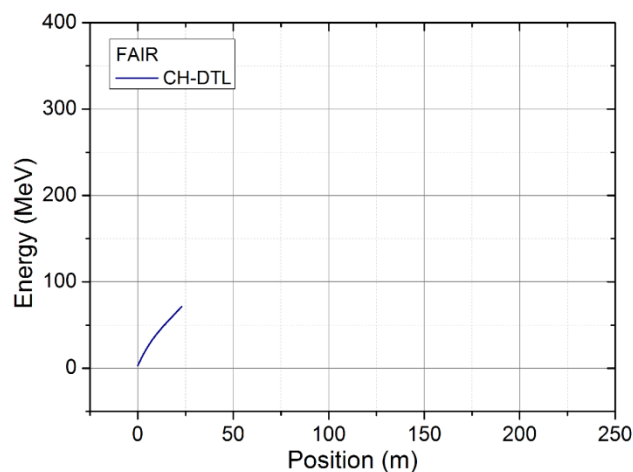
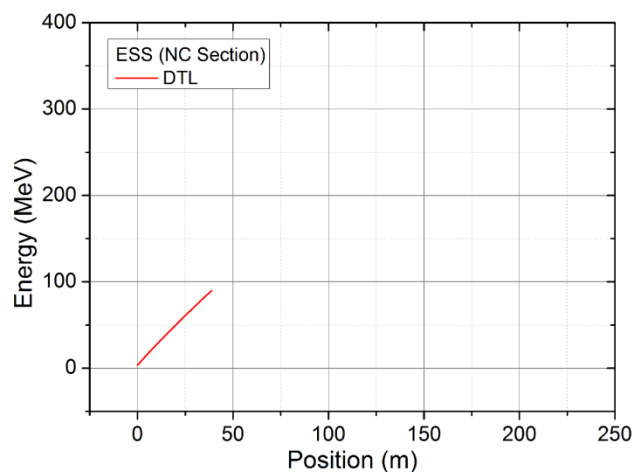
RF Cavity Design

- In most particle accelerators, the energy is delivered to the particle by means of a large variety of devices, normally known as **cavity resonators**.
- The ideal cavity: volume of perfect dielectric limited by infinitely conducting walls.
- Hollow cylindrical resonator excited by a radio transmitter -> standing wave -> accelerating fields (the pillbox cavity).



Why Cavity Design Is Important?

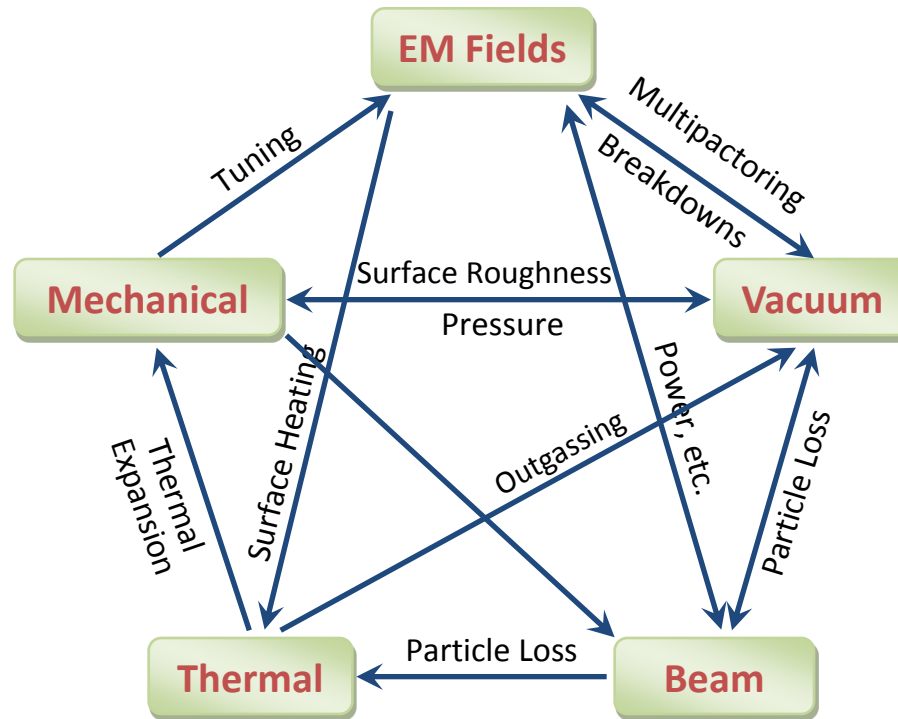
Acceleration Profile in Several Linacs



Design Criteria

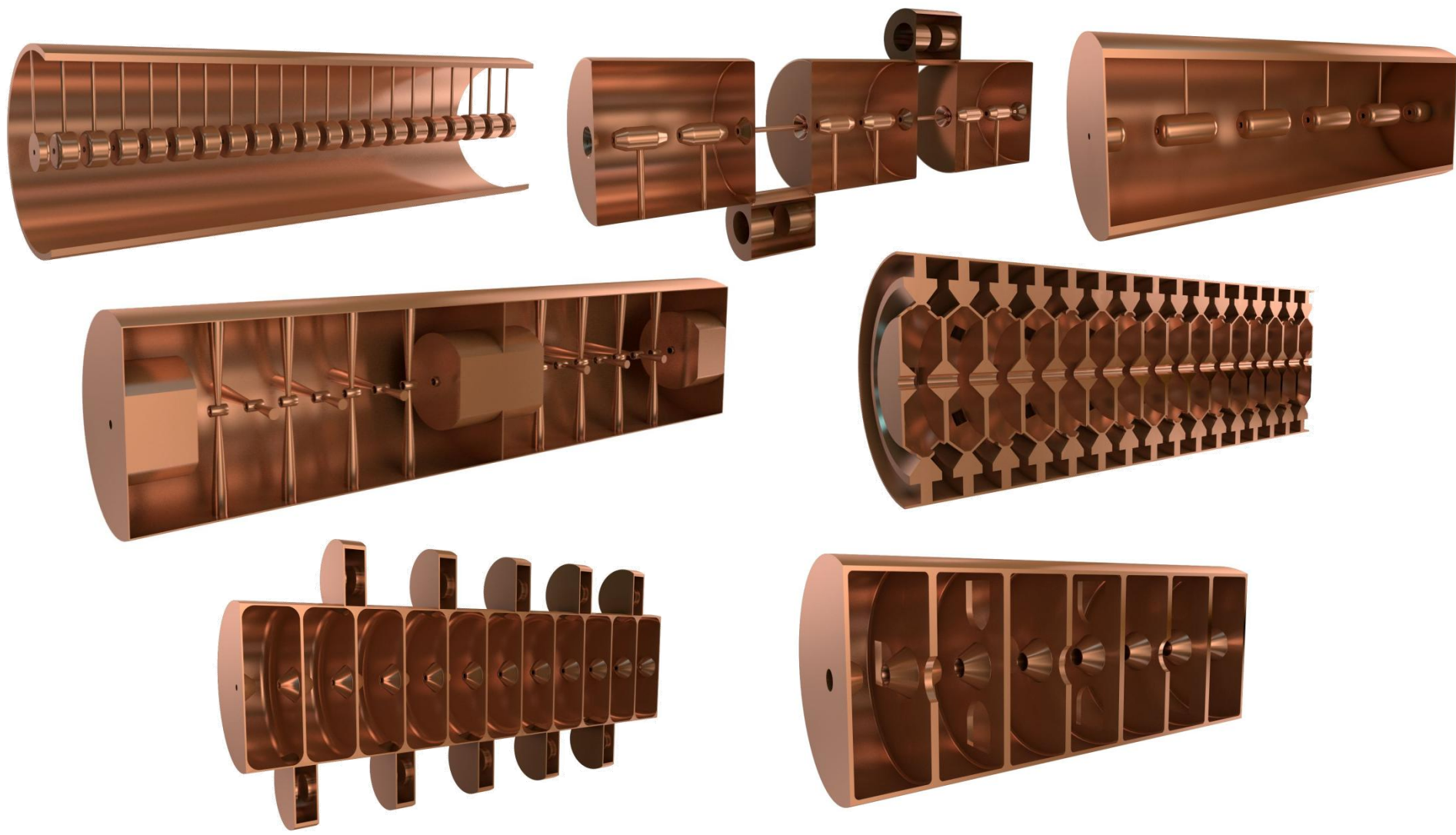
- Define the requirements (intended application), RF frequency, NC/SC, voltage, tuning, etc.
- General design criteria:
 - Power Efficiency & RF Properties
 - Beam Dynamics considerations (control of loss and emittance growth, etc.) – especially true for linacs
 - Technologies and precisions involved
 - Tuning procedures (frequency, field profile, stability against perturbations)
 - Sensitivity to RF errors (phase and amplitude)
 - Etc.

The “Magic Pentagon” of Cavity Design



- The pentagon shows the importance of each design and manufacturing choice
- Technologies are interdependent

Cavity Zoo

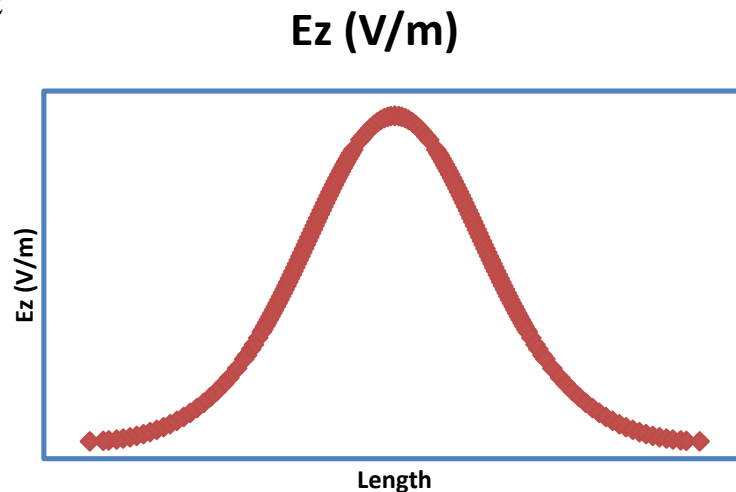
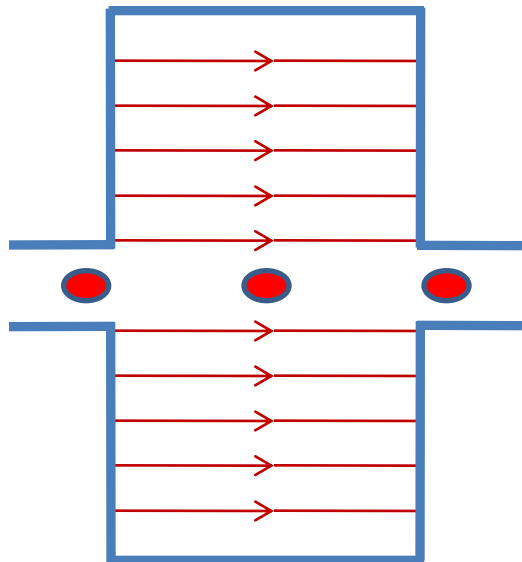


Figures of Merit

The Transit Time Factor, T

- While the particle crosses the cavity, the field is also varying -> less acceleration -> the particle sees only a **fraction** of the peak voltage -> T is a measure of the reduction in energy gain cause by the sinusoidal time variation of the field in the cavity.

$$T = \frac{\int_{-L/2}^{L/2} E(0, z) \cdot \cos \frac{2\pi z}{\beta \lambda} dz}{\int_{-L/2}^{L/2} E(0, z) dz}$$



Figures of Merit

The Quality Factor, Q

$$Q_0 = \frac{2\pi \cdot \text{stored energy}}{\text{energy consumed per period}} = \frac{2\pi W}{TP_0} = \omega \frac{U}{P_0}$$

- To first order, the Q-value will depend on the conductivity of the wall material only
- High Q -> narrower bandwidth -> higher amplitudes
- But, more difficult to tune, more sensitive to mechanical tolerances (even a slight temperature variation can shift the resonance)
- Q is dimensionless and gives only the ratios of energies, and not the real amount of power needed to maintain a certain resonant mode
- For resonant frequencies in the range 100 to 1000 MHz, typical values are 10,000 to 50,000 for normal conducting copper cavities; 10^8 to 10^{10} for superconducting cavities.

Figures of Merit

Shunt Impedance

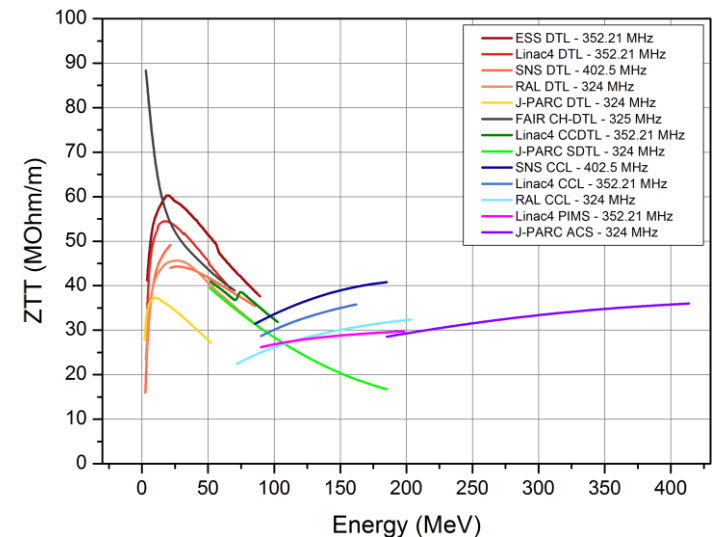
- A measure of the effectiveness of producing an axial voltage V_0 for a given power dissipated

$$r_s = \frac{V_0^2}{P_0}$$

- Effective Shunt Impedance per unit length

$$ZT^2 = \frac{r}{L} = \frac{(E_0 T)^2}{P_0 / L}$$

- Typical values of ZT^2 for normal conducting linacs is 30 to 50 $M\Omega/m$.
The shunt impedance is not relevant for superconducting cavities.



Figures of Merit

r/Q

- measures the efficiency of acceleration per unit of stored energy at a given frequency

$$\frac{r}{Q} = \frac{(V_0 T)^2}{\omega U}$$

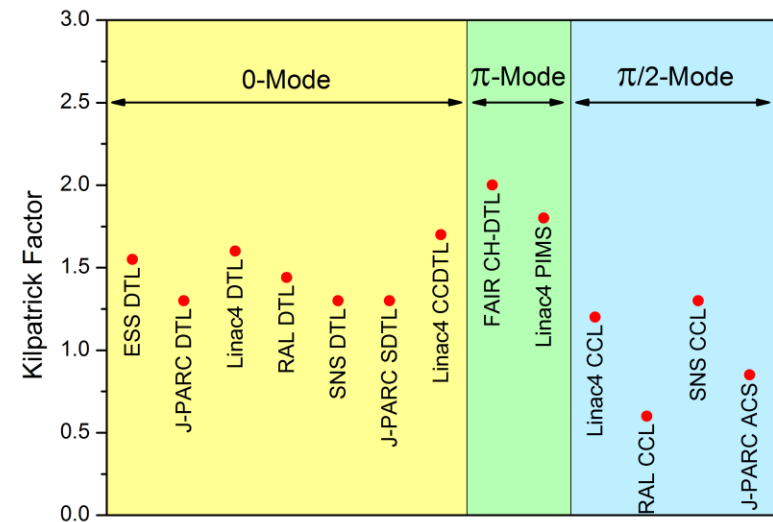
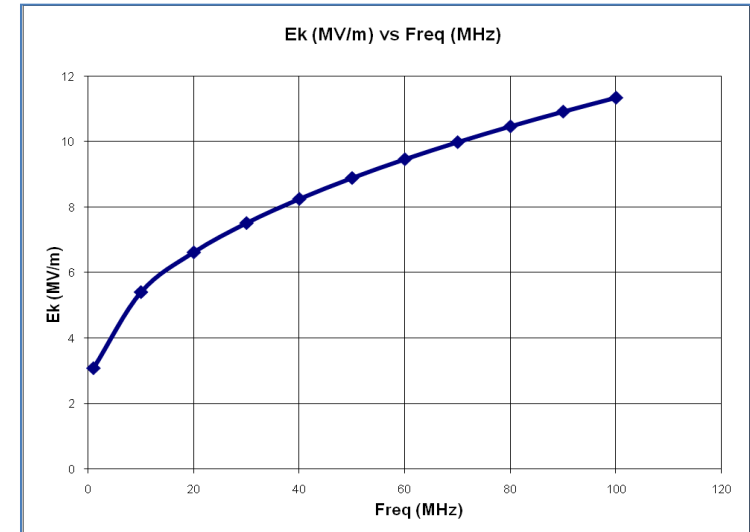
- It is a function only of the cavity geometry and is independent of the surface properties that determine the power losses.

Figures of Merit

The Kilpatrick limit

- High Field -> Electric breakdown
- Maximum achievable field is limited

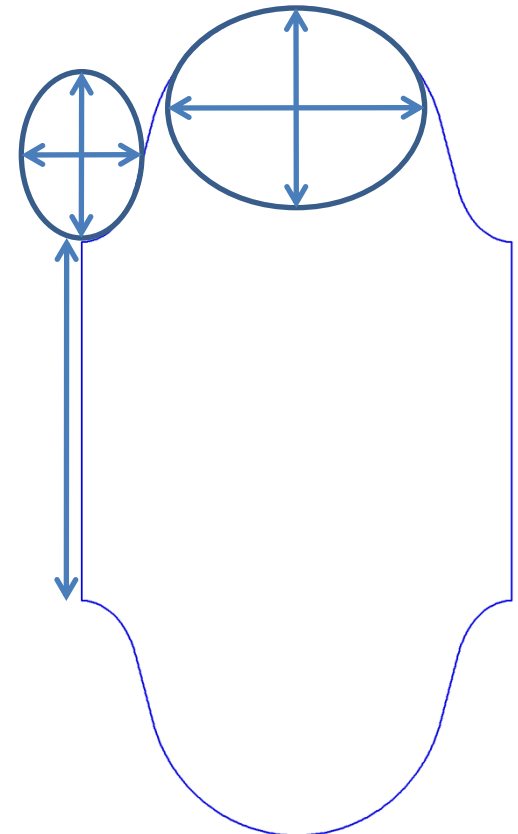
$$f = 1.64 E_k^2 e^{-8.5/E_k}$$



Figures of Merit

Superconducting Cavities (Slightly different story for):

- r/Q (characteristic impedance)
- G (Geometric Factor - the measure of energy loss in the metal wall for a given surface resistance)
- $E_{\text{peak}}/E_{\text{acc}}$ - field emissions limit (Eacc limit)
- $B_{\text{peak}}/E_{\text{acc}}$ – quench limit (sc breakdown)
- Higher Order Modes – manage and suppress HOM (e.g.: dipole modes can degrade the beam \rightarrow suppression scheme using HOM couplers)
- K_{cc} – Cell to cell coupling
- Multicell cavities: Field Flatness
- Optimise geometry to increase both r/Q and G resulting in less stored energy and less wall loss at a given gradient (low cryogenic losses)
- Optimise geometry to reduce $E_{\text{peak}}/E_{\text{acc}}$ and $B_{\text{peak}}/E_{\text{acc}}$
- Find optimum K_{cc} . (e.g.: a small aperture increases r/Q and G (!), but reduces K_{cc} . A small K_{cc} increases the sensitivity of the field profile to cell frequency errors.)



Introduction to Poisson Superfish

- You will need a laptop running Windows. If you have Linux/MacOS install VMWare/Wine.
- Please download and install Poisson Superfish. To do this go to the following address and follow the instructions:
http://laacg1.lanl.gov/laacg/services/download_sf.phtml
- Please download the example files to your computer from the JAI website.
- An extensive documentation can be found in the Superfish home directory (usually C:/LANL).
 - Have a look at the SFCODES.DOC file. Table VI-4 explains how the object geometry is defined in Superfish (page 157).
 - For a list of Superfish variables, see SFINTRO.doc, Table III-3 (page 76)
- For any questions, email Emmanuel (emmanuel.tsesmelis@cern.ch) or Ciprian (ciprian.plostinar@stfc.ac.uk). Good luck!

Introduction to Poisson Superfish

- Poisson and Superfish are the main solver programs in a collection of programs from LANL for calculating static magnetic and electric fields and radio-frequency electromagnetic fields in either 2-D Cartesian coordinates or axially symmetric cylindrical coordinates.
- Finite Element Method

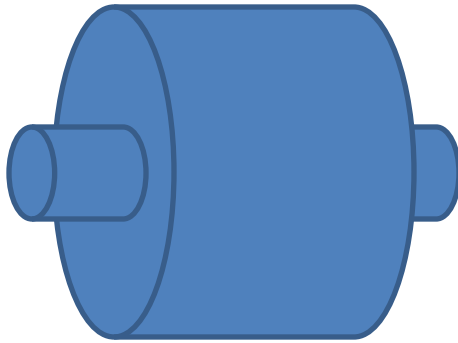
Solvers:

- **Automesh** – generates the mesh (always the first program to run)
- **Fish** – RF solver
- **Cfish** – version of Fish that uses complex variables for the rf fields, permittivity, and permeability.
- **Poisson** – magnetostatic and electrostatic field solver
- **Pandira** – another static field solver (can handle permanent magnets)
- **SFO, SF7** – postprocessing
- **Autofish** – combines Automesh, Fish and SFO
- **DTLfish, DTLCells, CCLfish, CCLcells, CDTfish, ELLfish, ELLCAV, MDTfish, RFQfish, SCCfish** – for tuning specific cavity types.
- **Kilpat, Force, WSFPlot**, etc.



A Pillbox Cavity

- The simplest RF cavity



For the accelerating mode (TM_{010}), the resonant wavelength is:

$$\lambda = \frac{\pi D}{x_1}$$

$$x_1 = 2.40483$$

x_1 - first root of the zero-th order Bessel function $J_0(x)$

- > Resonant frequency independent of the cell length
- > Example: a 40 MHz cavity (PS2) would have a diameter of ~ 5.7 m
- > In the picture, CERN 88 MHz



A Pillbox Cavity

Superfish input file

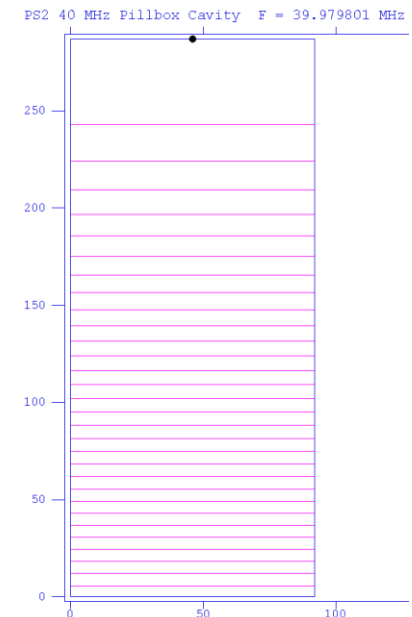
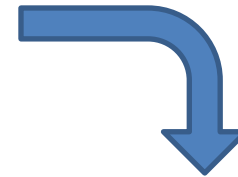
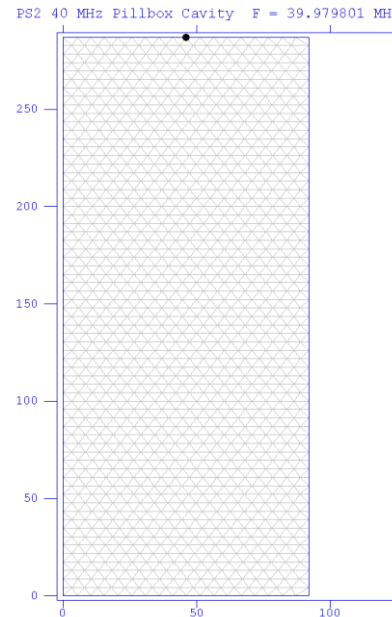
```

PS2 40 MHz Pillbox Cavity

PARTICLE H-,
$reg kprob=1,      ; Superfish problem
dx=5,              ; X mesh spacing
freq=40.,          ; Starting frequency in MHz
icylin=1

xdri=46.,ydri=287 $      ; Drive point location

$po x=0.0,y=0.0 $      ; Start of the boundary points
$po x=0.0,y=287 $
$po x=92,y=287 $
$po x=92,y=0.0 $
$po x=0.0,y=0.0 $
  
```



```

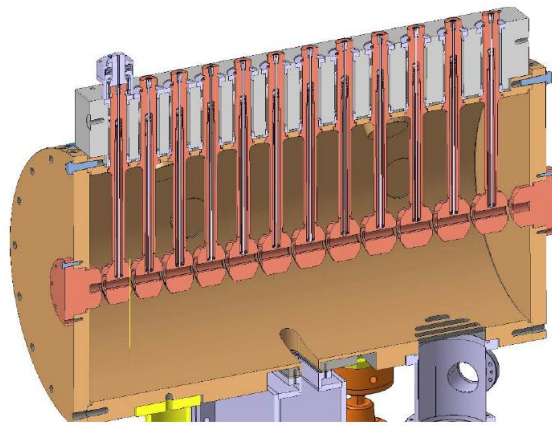
Lister - [c:\_Current Projects\Superfish Course Oxford\Example 1\PILLBOX.SFO]

All calculated values below refer to the mesh geometry only.
Field normalization (NORM = 0):  EZERO = 1.00000 MV/m
Frequency = 39.979801 MHz
Particle rest mass energy = 938.272029 MeV
Beta = 0.2453792 Kinetic energy = 29.590 MeV
Normalization factor for E0 = 1.000 MV/m = 5187.056
Transit-time factor = 0.0001158
Stored energy = 28.3520963 Joules
Using standard room-temperature copper.
Surface resistance = 1.64961 milliohm
Normal-conductor resistivity = 1.72410 microhm-cm
Operating temperature = 20.0000 C
Power dissipation = 25.9402 kW
Q = 274557. Shunt impedance = 35.466 Mohm/n
Rs*Q = 452.911 Ohm Z*T* = 0.000 Mohm/n
r/Q = 0.000 Ohm Wake loss parameter = 0.00000 U/pC
Average magnetic field on the outer wall = 1376.86 A/n, 156.361 mV/cm^2
Maximum H (at Z,R = 74.1111,287) = 1376.86 A/n, 156.361 mV/cm^2
Maximum E (at Z,R = 89.4444,287) = 1.00783E-04 MV/m, 1.22091E-05 K1lp.
Ratio of peak fields Bmax/Emax = 17167.7287 mT/(MV/m)
Peak-to-average ratio Emax/E0 = 0.0001

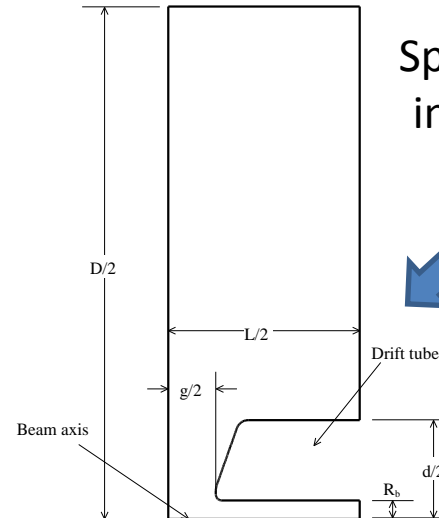
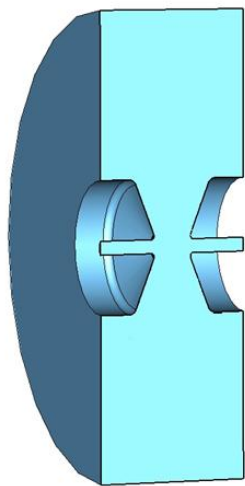
Wall segments:
Segment Zend Rend Enax Power P/A dF/dZ dF/dR
(cm) (cm) (MV/m) (kW) (mV/cm^2) (MHz/mm) (MHz/mm)
-----
1 0.0000 287.00 1.2258E-04 25.94 156.4 0.000 -1.3933E-02
2 92.000 287.00 1.2258E-04 25.94 156.4 0.000 -1.3933E-02
Total 25.94
  
```

A DTL-type Cavity

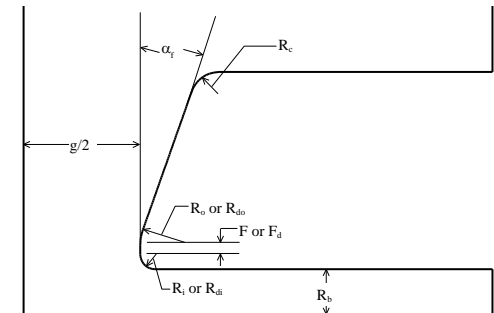
- Drift Tube Linac Cavity



← CERN Linac4 DTL prototype →



Special Superfish
input geometry



A DTL-type Cavity

Superfish input file

```

File Edit Options Help
Title
DTL-type cavity
Resonant Frequency = 324 MHz
ENDTitle

PARTICLE      H-
InitialEnergy  3      ; Energies used in program DTLCells

FILENAME_prefix DTL
SEQUENCE_number 1
FREQUENCY      324
BETA           0.079732
LENGTH        7.37748526582
DIAMETER       55.81982579555
G_OVER_Beta_lambda 0.2
GAP_Length     1.475497853164
E0 Normalization 2.5
E0T Normalization 1.65138369868
CORNER_radius  0.5
INNER_nose_radius 0.15
OUTER_nose_radius 0.3
FLAT_length    0.2
FACE_angle     10
DRIFT_TUBE_Diameter 18
GAP_Change     0.0
STEM_Diameter  3
STEM_Count     1
BORE_radius    1.4
PHASE_length   180
DELTA_Frequency 0.01
MESH_Size      2
INCREMENT      4
START          4

; Start codes for DTLfish:
; 1 No tuning
; 2 Adjust tank diameter
; 3 Adjust drift tube diameter (not recommended)
; 4 Adjust gap
; 5 Adjust face angle

EndFile
  
```

Geometry file

```

File Edit Options Help
DTL-type cavity
Resonant frequency = 324 MHz
Adjusting gap, currently = 1.4754971, g/b1 = 0.2000000

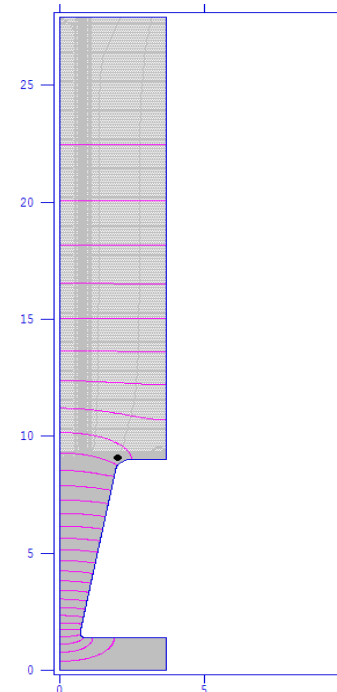
$REG KPROB=1      ; Superfish problem
H0I=1            ; Material air or empty space
FREQ=323.9997439729 ; Mode frequency, starting frequency in fish solve
FREQ0=324        ; Design frequency, used (with DPHI) to compute w
BETA=0.079732    ; Particle velocity, used to compute wave number
KNETH00=1        ; SFO will use BETA to compute wave number
DPHI=180         ; Phase length of the half cavity, used (with FREQ)
NCSUP=1,NBSLO=0,NBSRT=1,NBSLF=1 ; Boundary conditions
LINES=1          ; Fix internal points on line regions
ICVLIH=1         ; X>2,Y>0, cylindrical coordinates
NBOH=0           ; Normalize to EZERO
EZERO=2500000    ; Accelerating field
DIL=1            ; Cavity is drift-tube linac
RMSS=3           ; Best mesh value or indicator
EPS0=1.0E-6      ; Mesh optimization convergence parameter
IRIYPE=0         ; RS method: Normal conductor formula
XDR1=1.098814697996 ; Drive point X coordinate
YDR1=0.09621635729 ; Drive point Y coordinate
DSLOPE=1        ; Allow convergence in 1 iteration

; X line-region physical locations:
XREG=0.557748526582,0.677748526582,0.947748526582,1.067748526582,
; X line-region logical locations:
XREG=1,0.11,25,24,
KMAX=62          ; Column number for X = XMAX
; V line-region physical locations:
VREG=0.0282842712475,1.357573593129,3.698196086483,9.084852813742,
9.367695526217,
; V line-region logical locations:
VREG=1,3.51,219,418,415,
LMAX=580 &      ; Row number for V = VMAX

; Start of boundary points
EPD X=0.0,Y=0.0 & ; 1
EPD X=0.0,Y=27.98991289778 & ; 2
EPD X=3.68874263291,Y=27.98991289778 & ; 3
EPD X=3.68874263291,Y=9 & ; 4
EPD X=2.431048968741,Y=9 & ; 5
EPD NT=2,X=2.431048968741,Y=0.5, ; 6
X=0.4924838765861,Y=0.086824888835 & ; 7
EPD X=0.7423282086783,Y=1.8320944533 & ; 8
EPD NT=2,X=1.837748526582,Y=1.75, ; 9
X=0.3,Y=0.0 & ; 10
EPD X=0.737748526582,Y=1.55 & ; 11
EPD NT=2,X=0.887748526582,Y=1.55, ; 12
X=0.0,Y=-8.15 & ; 13
EPD X=3.68874263291,Y=1.4 & ; 14
EPD X=3.68874263291,Y=0.0 & ; 15
EPD X=0.0,Y=0.0 & ; 16
  
```

Solution

DTL-type cavity F = 323.99974 MHz

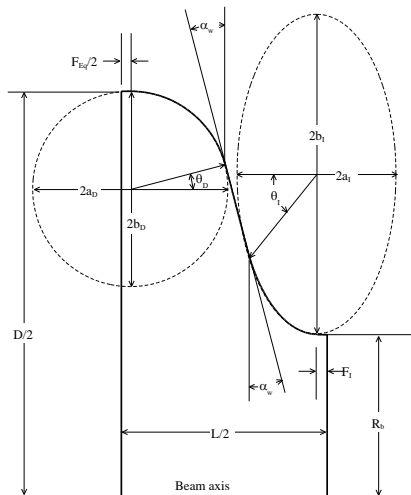


An Elliptical Cavity

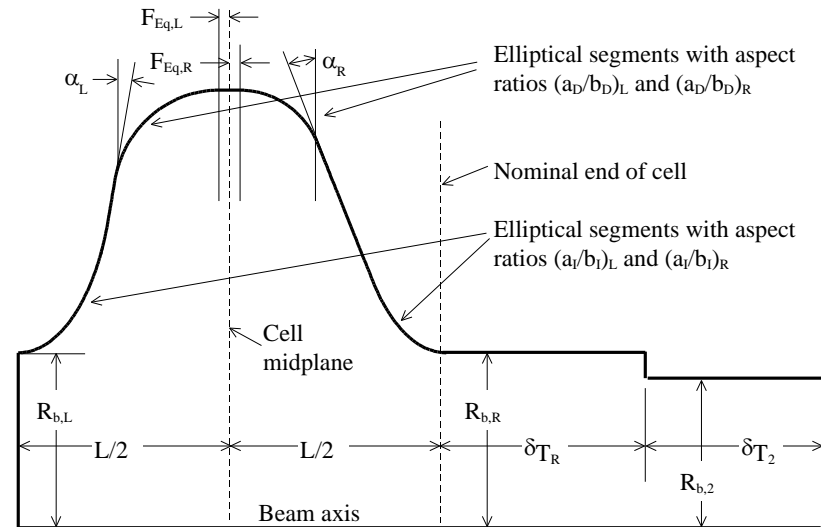
- Often used in superconducting applications



INFN & CEA 704 MHz elliptical SC cavities



Special Superfish input geometry



An Elliptical Cavity

Superfish input file

```

Elliptical Cavity - Notepad
File Edit Format View Help
Title
Tuning elliptical cavity NF muon linac
Design beta = 1
Resonant frequency = 201.49 MHz, Bore radius = 23.00 cm
ENDTitle
REST_mass 105.658369
SUPERCONDUCTOR 2 9.2 1.0E-08
NUMBEROFCELLS 10 ; used by the ELLCAV code
FULL_CAVITY
FILENAME_PREFIX elliptical
SEQUENCE_NUMBER 1
FREQUENCY 201.249
BETA 1
LENGTH 74.48296836258
DIAMETER 137.098152098
EO_Normalization 14.81357443775
EOT_Normalization 10
DOVE_B 20
LEFT_DOVE_B 18.16662400282
RIGHT_DOVE_B 1
DOVE_A/B 1
LEFT_DOVE_A/B 1
RIGHT_DOVE_A/B 1
WALL_ANGLE 20
LEFT_WALL_ANGLE 20
RIGHT_WALL_ANGLE 20
EQUATOR_FLAT 0.0
LEFT_EQUATOR_FLAT 0.0
RIGHT_EQUATOR_FLAT 0.0
IRIS_FLAT 0.0
LEFT_IRIS_FLAT 0.0
RIGHT_IRIS_FLAT 0.0
RIGHT_BEAM_TUBE 60
IRIS_A/B 0.7
LEFT_IRIS_A/B 0.7
RIGHT_IRIS_A/B 0.7
BETASTART 0.0
BETASTOP 0.0
BETASTEP 0.0
BETATABLE 0.0
BORE_RADIUS 23
LEFT_BORE_RADIUS 23
RIGHT_BORE_RADIUS 0.0
SECOND_BEAM_TUBE 0.0
SECOND_TUBE_RADIUS 0.0
DELTA_FREQUENCY 0.01
MESH_SIZE 1
INCREMENT 2
START 1
; Start codes for ELLfish:
; 1 No tuning
; 2 Adjust diameter
; 3 Adjust dome ellipse size
; 4 Adjust wall slope
; 5 Adjust wall slope with fixed iris ellipse size
; (Right side only in full cavities for 3, 4, and 5.)
EndFile

```

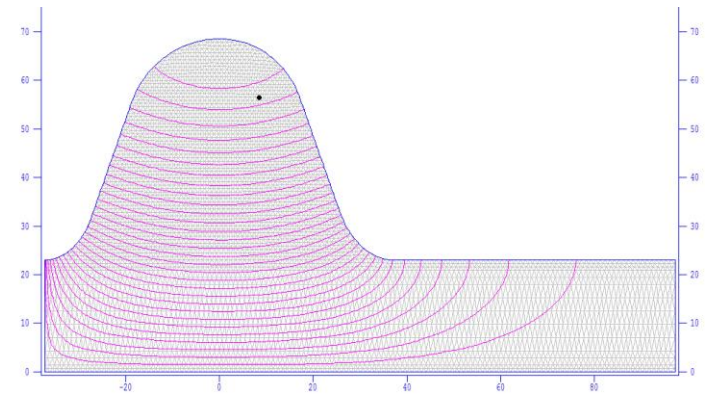
Geometry file

```

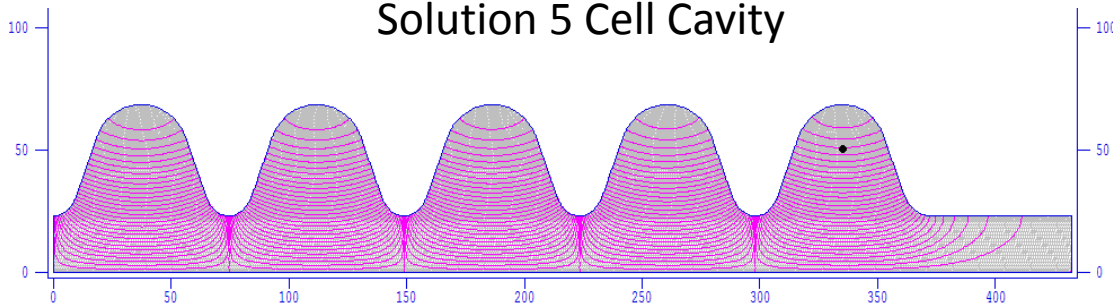
Elliptical Cavity - Notepad
File Edit Options View
Tuning elliptical cavity NF muon linac
Design beta = 1
Resonant frequency = 201.49 MHz, Bore radius = 23.00 cm
No tuning on this cavity.
$REQ $PROB=1 ; Superfish problem
$MT=1 ; Material air or empty space
$REQ=201.2491888163 ; Mode frequency, starting frequency in
$REQ=201.249 ; Design frequency, used (with DP1) to
$BETA=1 ; Particle velocity, used to compute w
$RHS=0 ; SFB will use BETA to compute wave num
$DP1=180 ; Phase length of the cavity, used (with
$MSUP=1,$MSLO=0,$MSRT=0,$MSLF=0 ; Boundary conditions
$LINE=1 ; Fix internal points on line regions
$CYL=1 ; X>Z,Y>0, cylindrical coordinates
$NORM=1 ; Normalize to EZEROT
$EZEROT=1.E+07 ; Accelerating field times t
$SCON=1 ; Superconducting elliptical cavity
$RMSS=105.658369 ; Rest mass value or indicator
$EPS=1.E-06 ; Mesh optimization convergence parameter
$IRTYPE=1 ; $S method: Superconductor formula
$TEMP=2 ; Superconductor temperature, degrees K
$TC=0.2 ; Critical resistance
$XDR1=0.531253899282 ; Drive point X coordinate
$YDR1=0.58146824014 ; Drive point Y coordinate
$DSLOPE=1 ; Allow convergence in 1 iteration
$DX=1 ; Mesh spacing in X direction
; V line-region physical locations:
$VREQ=1.414213562373,4.242640687119,18.85825253169,20.87867965644,
; V line-region logical locations:
$LINE=1,3,5,10,12, ; Row number for V = VMAX
$LMX=0.0 ;
; Start of boundary points
$EPD X=0.0,Y=0.0,Z=0.0 ; 1
$EPD X=-37.24148418129,Y=0.0,Z=0.0 ; 2
$EPD X=-37.24148418129,Y=23.0,Z=0.0 ; 3
$EPD MT=2,X0=-37.24148418129,Y0=30.66951733241, ; 4
R=10.96866213269,ROURB=0.7,
X=9.731759780735,Y=-7.228789358454,Z=0.0
$EPD X=-18.79385241572,Y=55.38749436551,Z=0.0 ; 5
$EPD MT=2,X0=0.0,Y0=48.547891499, ; 6
R=20,ROURB=1,
X=0.0,Y=20,Z=0.0
$EPD MT=2,X0=0.0,Y0=58.38866789618, ; 7
R=18.16662400282,ROURB=1,
X=17.87184252804,Y=6.213351345188,Z=0.0
$EPD X=05.43276923568,Y=53.86792864119,Z=0.0 ; 8
$EPD MT=2,X0=37.24148418129,Y0=41.69888937394, ; 9
R=13.88386256176,ROURB=0.7,
X=8.8,Y=-18.69888937394,Z=0.0
$EPD X=97.24148418129,Y=23.0,Z=0.0 ; 10
$EPD X=97.24148418129,Y=0.0,Z=0.0 ; 11
$EPD X=0.0,Y=0.0,Z=0.0 ; 12

```

Solution 1 Cell

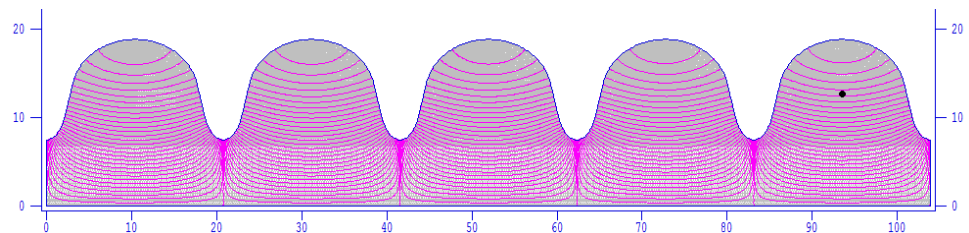
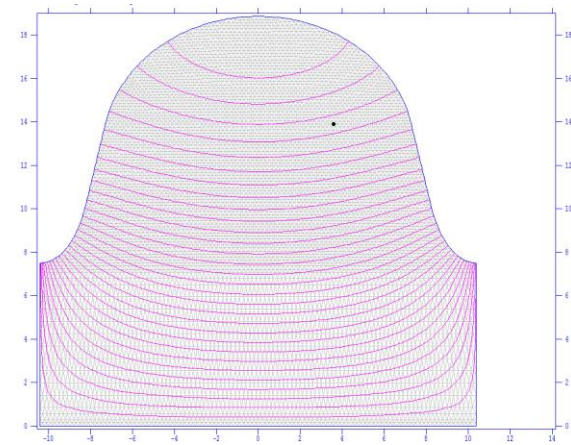
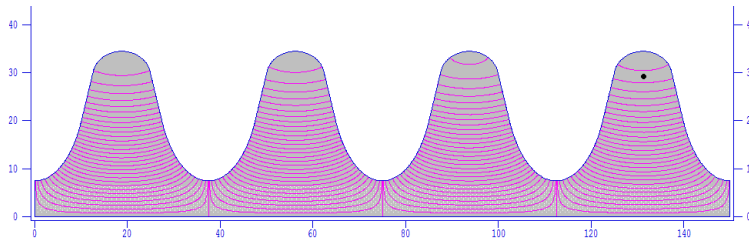
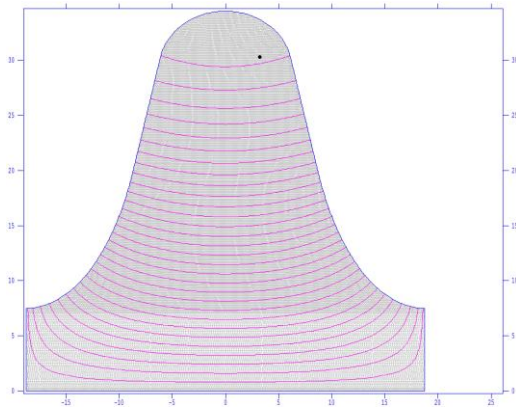


Solution 5 Cell Cavity



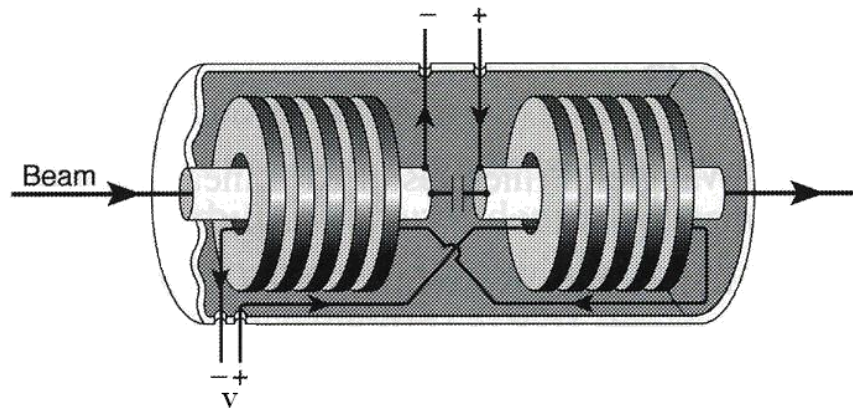
An Elliptical Cavity

- Example 1: 400 MHz
 - Like the LHC 400 MHz RF
 - 4-cell cavity, 4 cavities/Cryomodule
- Example2: 721.4 MHz
 - SPL-like cavities
 - 5-cell cavity



Ferrite Loaded Cavities

- Used when variable resonance is needed
- The torus of the ferrite encircles the beam path
- Ferrite properties are important (limit the cavity capabilities)
- Bias current \rightarrow Variable magnetic field \rightarrow Variable magnetic permeability of the ferrite \rightarrow Frequency change
- The structure can be thought of as a resonant transformer in which the beam constitutes a one-turn secondary winding.
- Frequencies domain: 100 kHz and 60 MHz
- Typical gap voltage of up tens of kV
- Different requirements (large frequency ranges, rapid swings, space, etc) \rightarrow various designs.



Ferrite Loaded Cavities

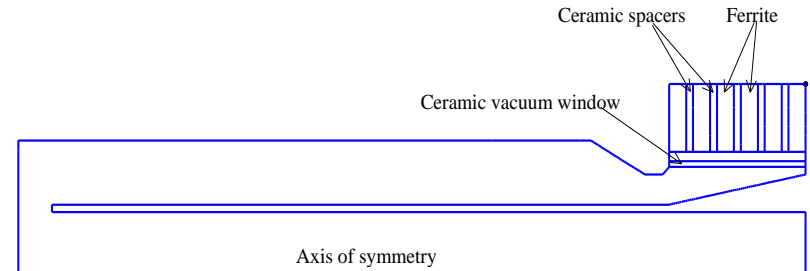
Six ferrite blocks: Epsilon = 14.5, μ = 1.5

Five ceramic-spacers: Epsilon = 10.0, μ = 1.0

Ceramic vacuum window: Epsilon = 9.0, μ = 1.0

Cavity length: 116 cm

Number of gaps: 1



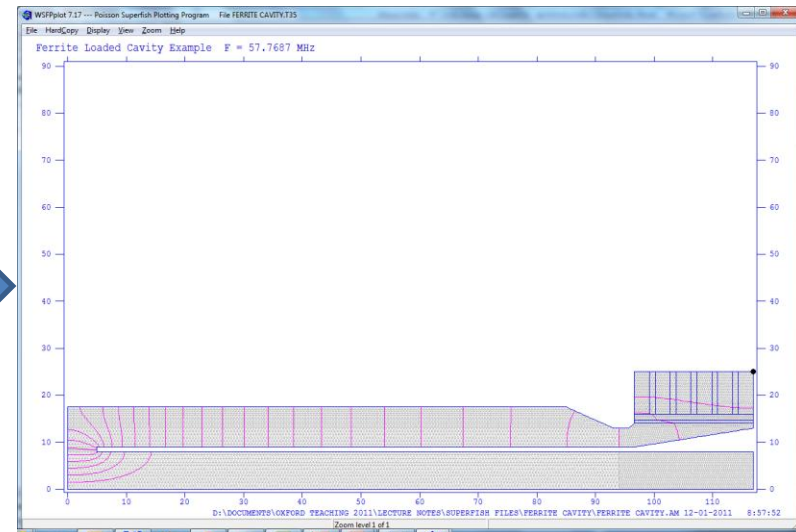
```

Lister - [D:\Documents\Oxford Teaching 2011\Lecture Notes\Superfish Files\Ferrite Cavity\Ferrite Cavity.am]
File Edit Options Encoding Help
Ferrite Loaded Cavity Example
Six ferrite blocks: Material 2, Epsilon = 14.5, Mu = 1.5
Five ceramic-spacers: Material 4, Epsilon = 10.0, Mu = 1.0
Ceramic vacuum window: Material 3, Epsilon = 9.0, Mu = 1.0
Initialize one large ferrite block, then superimpose ceramic spacers
[Originally appeared in 1987 Reference Manual 6.12.2]

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; Unauthorized commercial use is prohibited.

Greg kprob=1,      ! Superfish problem
icilin=1,          ! Cylindrical symmetry
Freq=57.76775,    ! Starting frequency
dslope=-1,        ! Allow convergence after one iteration
xreg1=94.0,        ! X line region
kreg1=188,         ! Logical coordinate for XREG1
yreg1=8,yreg2=9,   ! Y line regions
yreg3=13,yreg4=17.5 ! Logical coordinates for YREGS
lreg1=12,lreg2=15, ! Logical coordinates for YREGS
lreg3=21,lreg4=31, ! Logical coordinates for YREGS
kmax=240,lmax=43 & ! Maximum X and Y logical coordinates

&po x=0.0,y=0.0 &
&po x=116.88,y=0.0 &
&po x=116.88,y=0.0 &
&po x=5.0,y=0.0 &
&po x=5.0,y=9.0 &
&po x=96.64,y=9.0 &
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&po x=93.0,y=13.0 &
&po x=85.0,y=17.5 &
&po x=0.0,y=17.5 &
&en v=0.0 u=0.0 &
  
```



Now, use your imagination!