

FROM RESEARCH TO INDUSTRY



EXPERIMENTAL STUDY OF STABILITY AND TRANSIENTS IN A HORIZONTALLY HEATED BOILING HELIUM THERMOSYPHON

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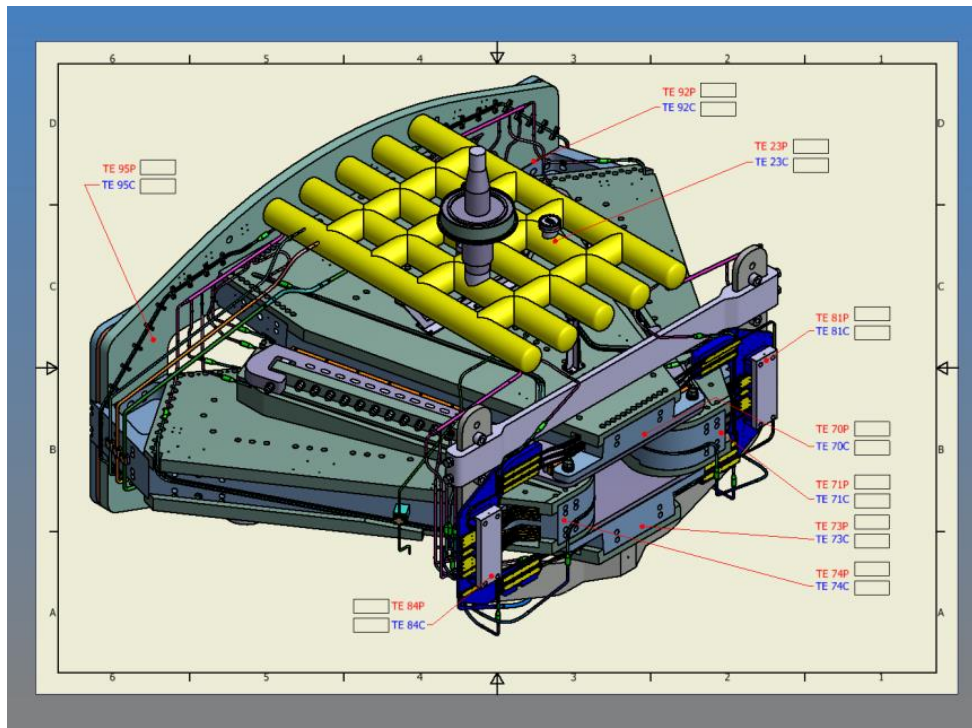
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Helium natural circulation loops are used for **cooling large superconducting magnets**.

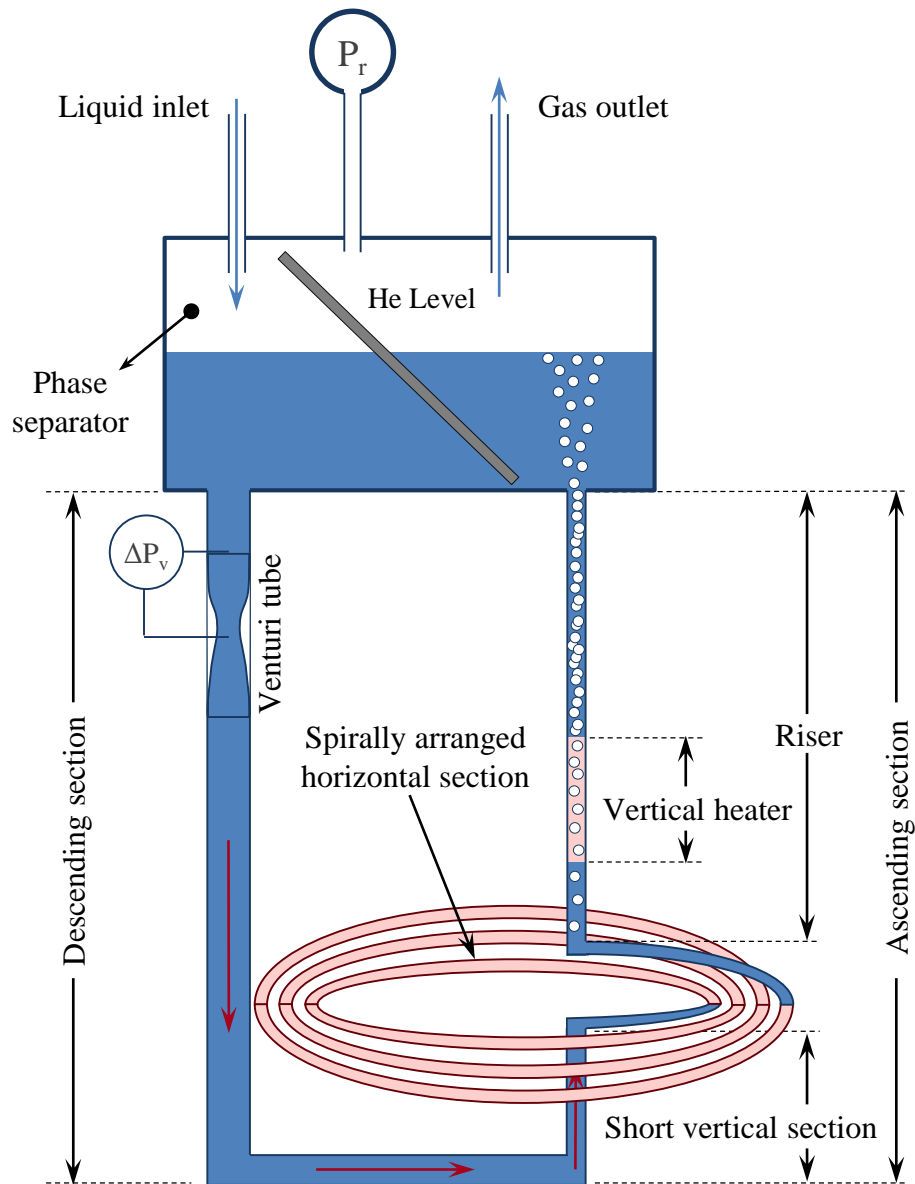
Within the R&D program for the R3B-GLAD spectrometer, horizontally heated loops started being studied at low power. Interesting dynamic behavior was observed.

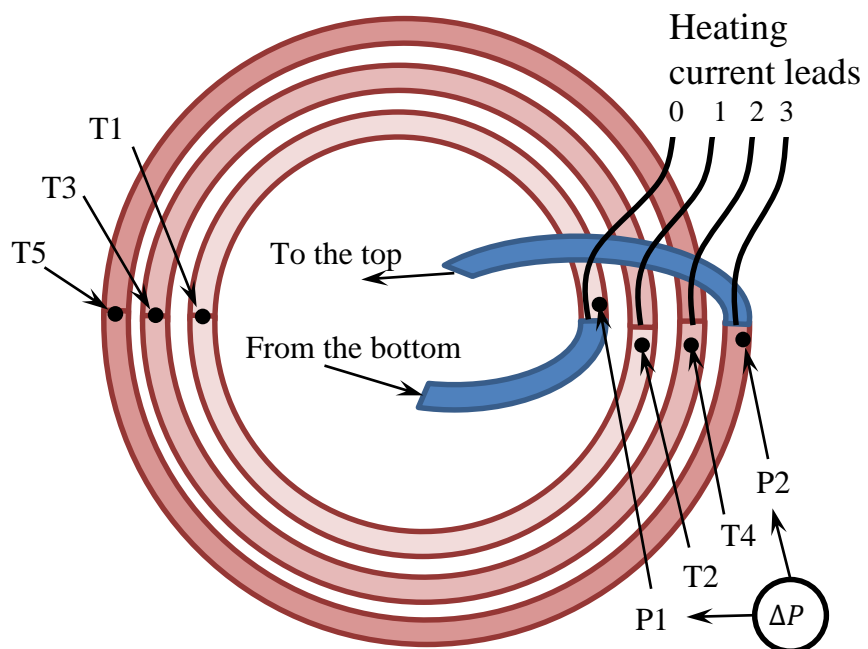


R3B-GLAD cooling system

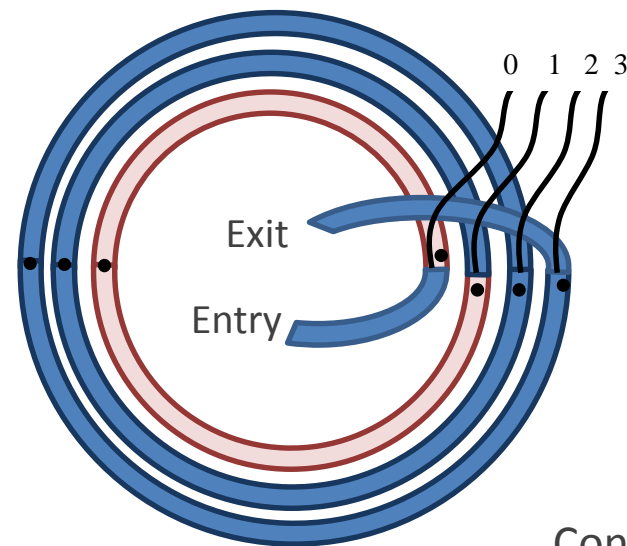
We now perform **experiments** on a big size helium natural circulation facility

- To **explore other existing thermalhydraulic regimes** during steady and transient power solicitation;
- To identify eventual **heat transfer deterioration** phenomena;
- To determine ways of **mitigating harmful effects**.

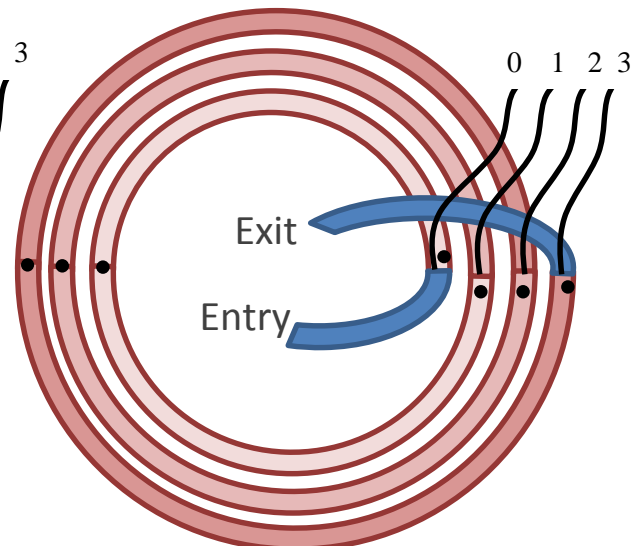




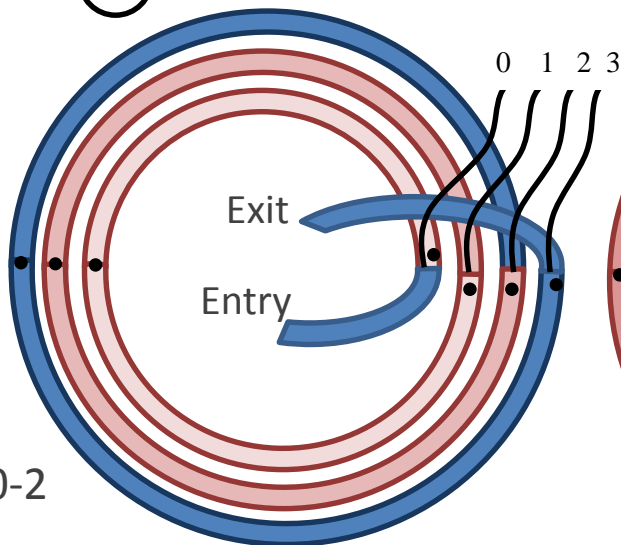
Configuration 0-1



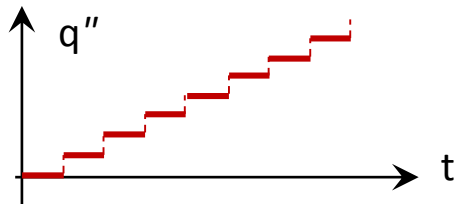
Configuration 0-3



Configuration 0-2



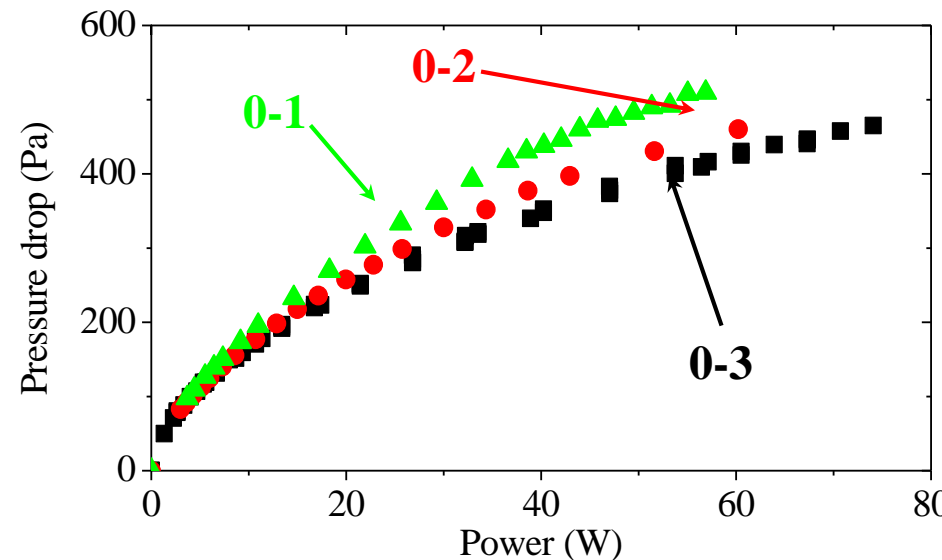
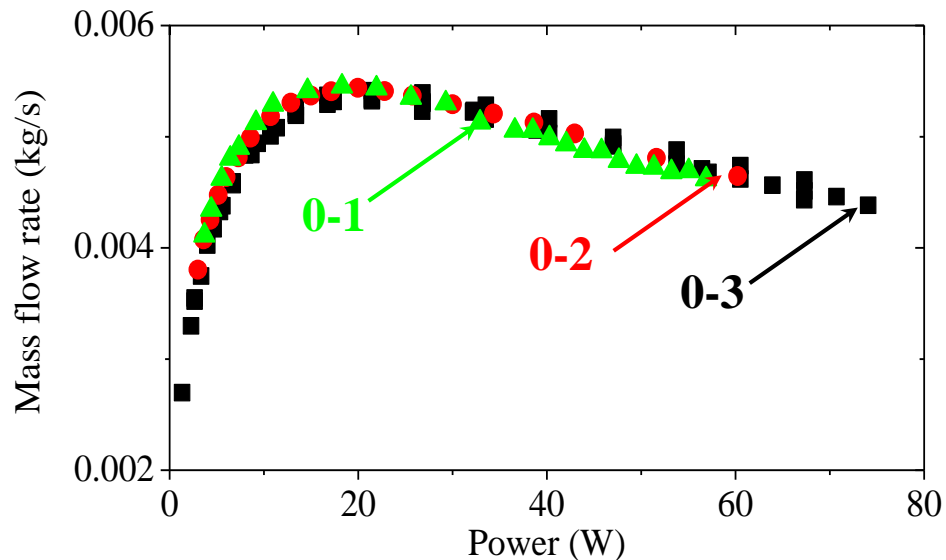
Power is increased gradually,
at steps (quasi-steady evolution)



Stability limits

Configuration	NHHL (m)	Lower limit (W)	Upper limit (W)
0-3	0.360(10)	1.2(4)	78(3)
0-2	1.895(10)	2.8(4)	71(2)
0-1	3.315(10)	3.7(2)	60(1)

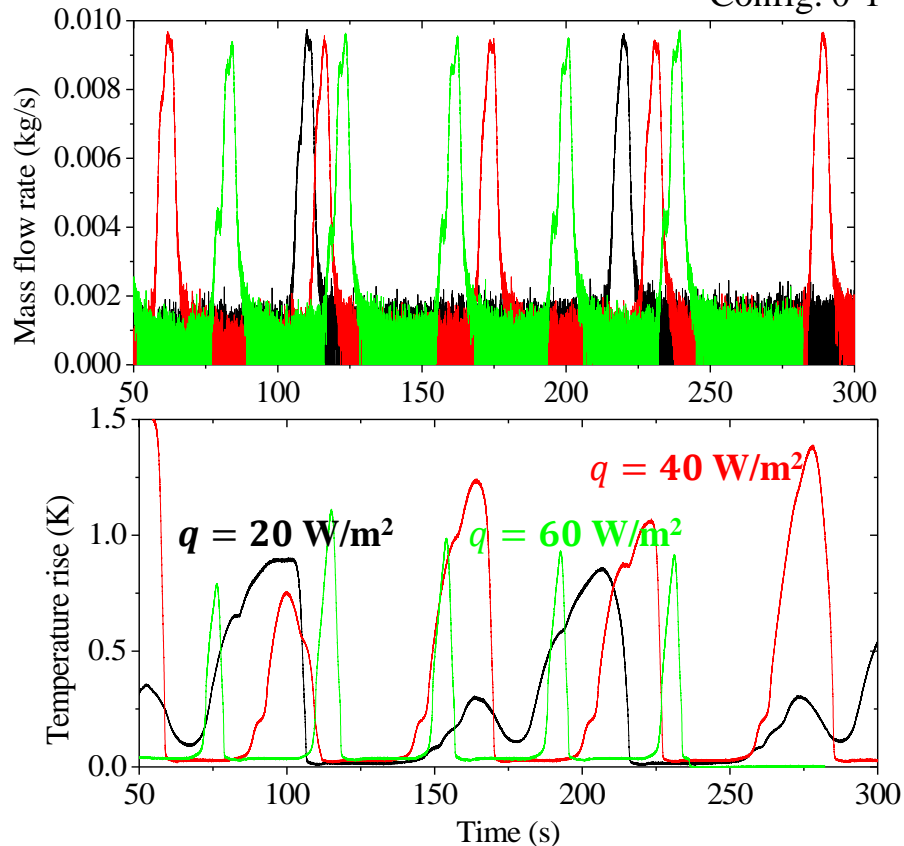
Stable behavior is only observed between lower and upper stability limits. The stability limits are affected by the heating geometry.



The unstable behavior at low power

- Exit quality strongly influential on density.
- Low mass flow rate \rightarrow long transit time.
- Important transport lag on riser density.

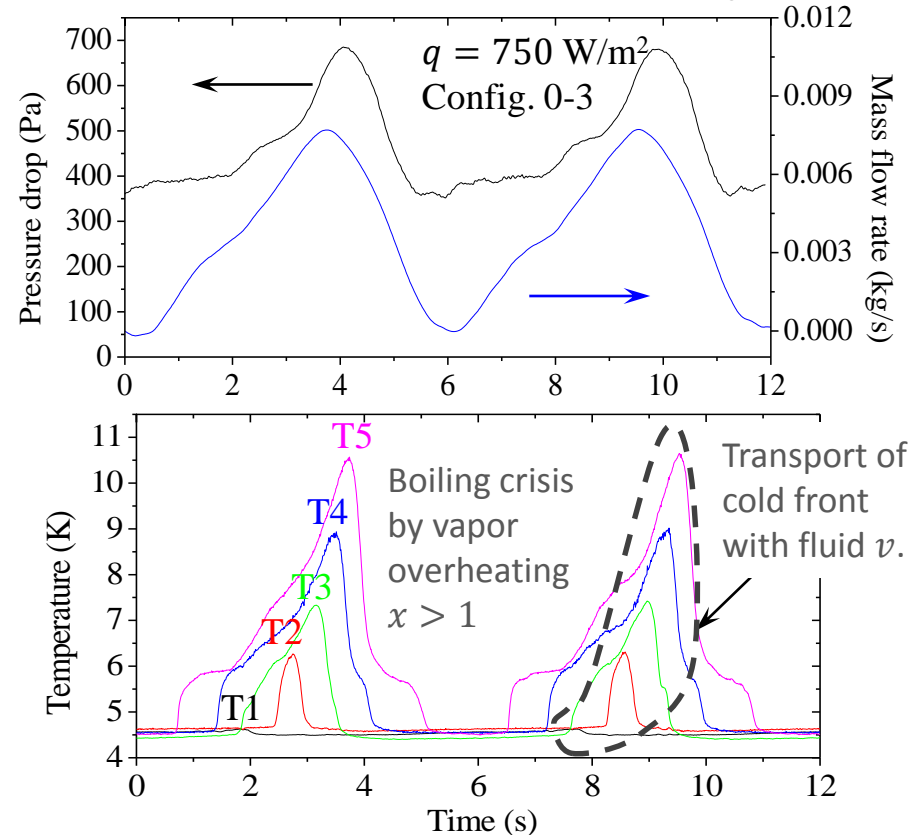
Config. 0-1



The unstable behavior at high power

- Equilibrium \dot{m} diminishes with q .
- *Friction*
- *Acceleration* } \rightarrow immediate response
- *Gravity (density)* \rightarrow transport lag

Config. 0-3

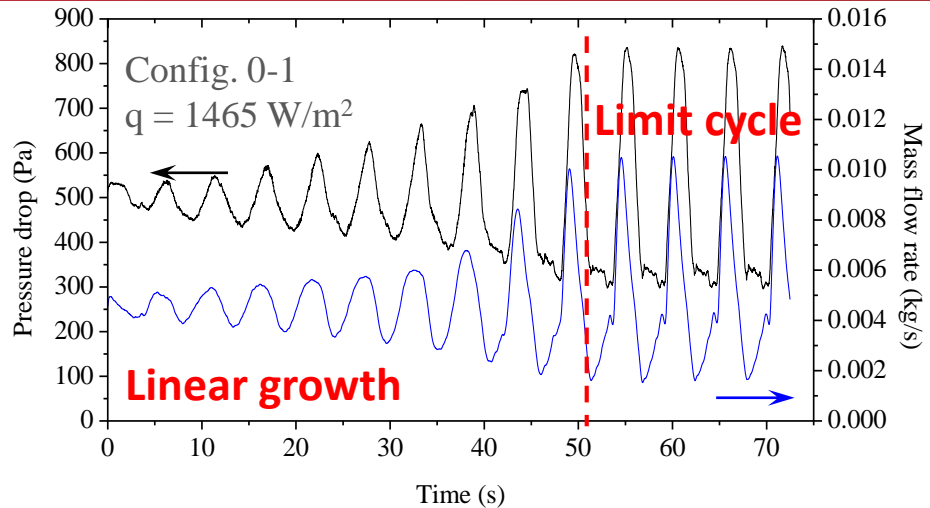


During the high power instability

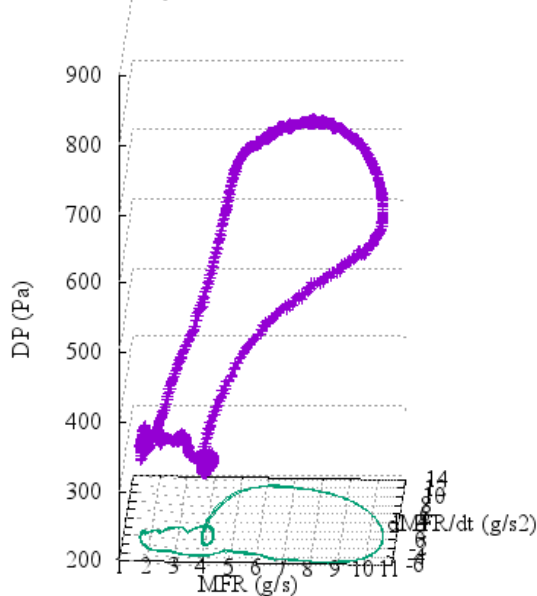
- initially linear (exp-sin)
- saturates to a periodic oscillation

The attractor is a **Limit Cycle**.

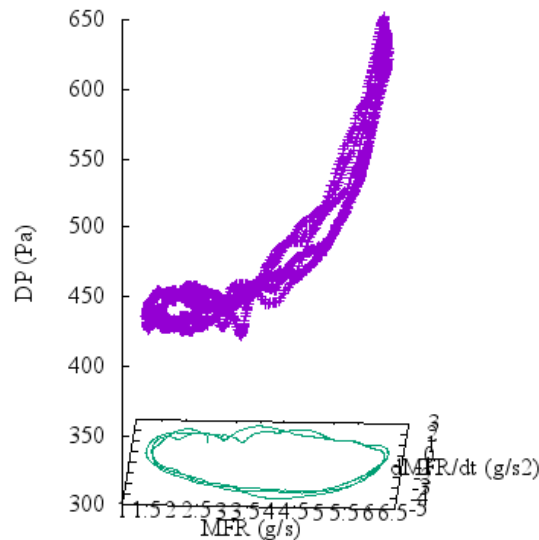
No quasi-periodicity, no chaos.



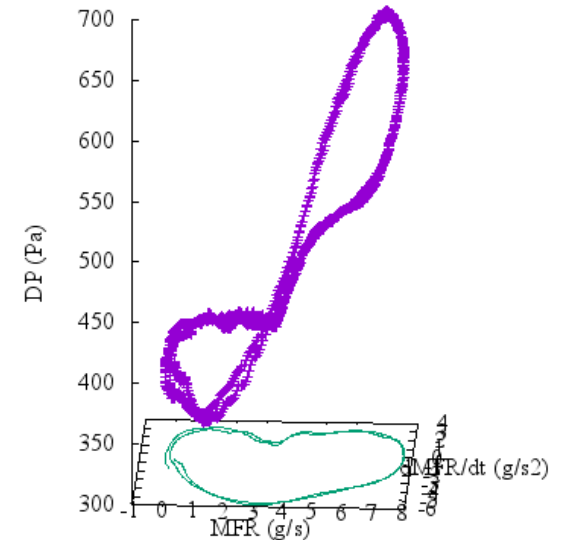
Config. 0-1; $q = 1465 \text{ W/m}^2$



Config. 0-3; $q = 625 \text{ W/m}^2$



Config. 0-3; $q = 750 \text{ W/m}^2$

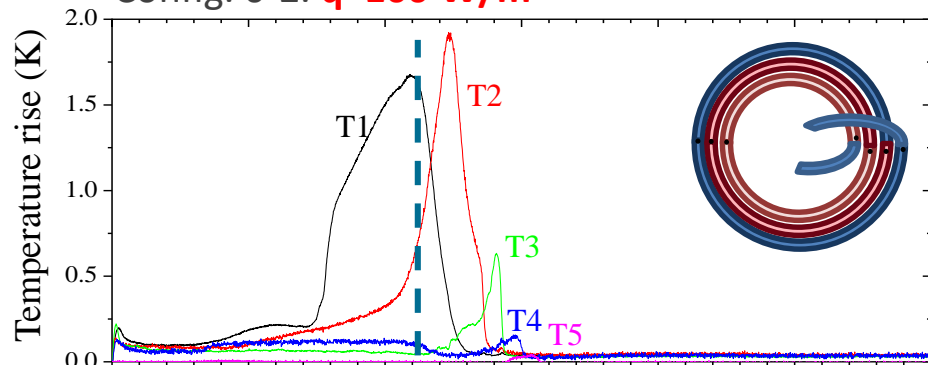


The system response to step heat load pulses was measured. In general, **2 stages** are observed:

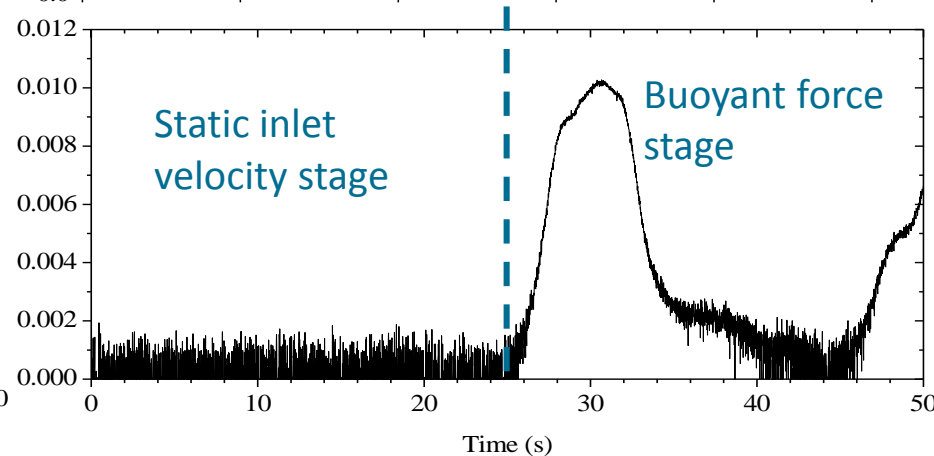
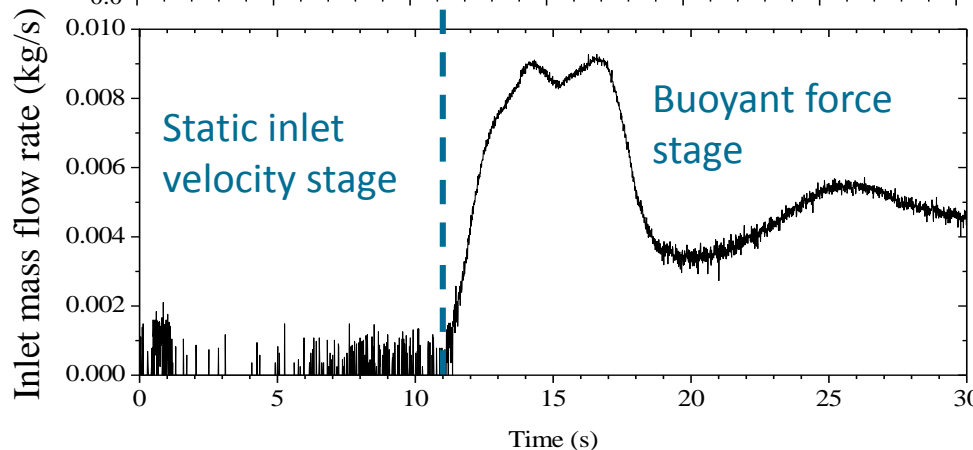
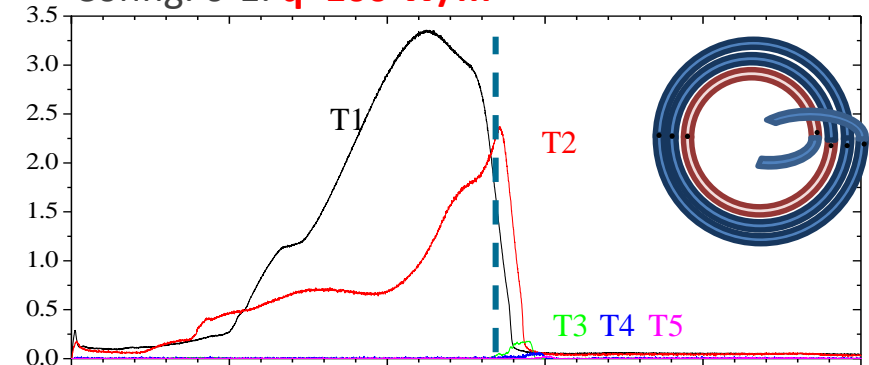
- **Static inlet velocity stage:** no buoyant force, two-phase expansion in the horizontal section, stratification.
- **Buoyant force stage:** vapor reaches the riser, positive inlet velocity, homogenization of flow.

At **low power** (boiling crisis is not expected at all) **high temperature** excursions can happen.

Config. 0-2. $q=100 \text{ W/m}^2$



Config. 0-1. $q=100 \text{ W/m}^2$

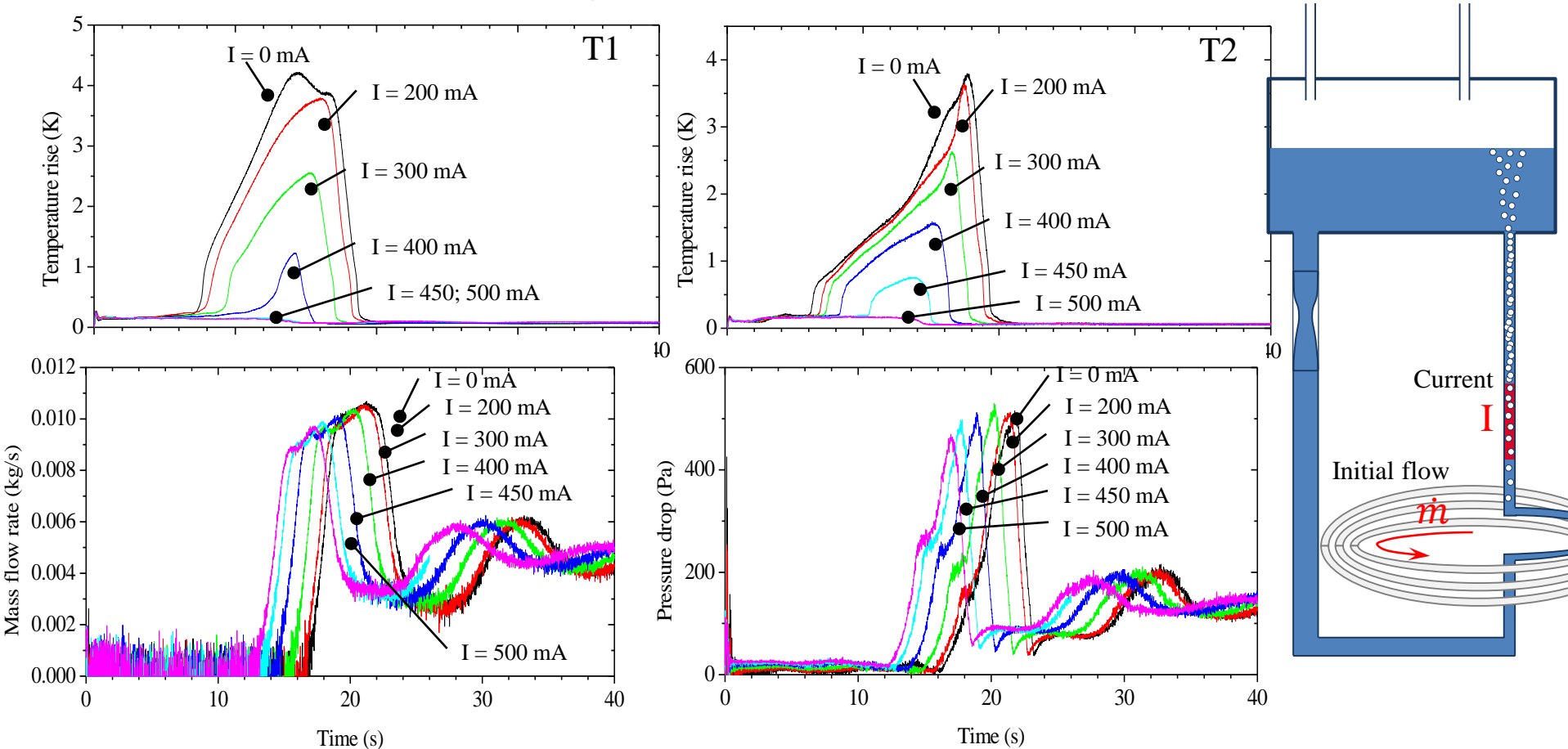


Applying of **power on the riser**.

Low power-high temperature **excursions** are **very sensitive to small mass flow rates** imposed externally.

$v_i \neq 0$ \rightarrow delays heat transfer deterioration
 \rightarrow advances the initiation of the buoyant force \rightarrow Mitigation of the excursion

Config. 0-1 $q = 150 \text{ W/m}^2$



Steady heat load

- **Horizontally heated helium natural circulation loops can be unstable** at sufficiently low or high driving power.
- The **stability power range** decrease as the **NHHL** downstream the heated section increases (transport lag destabilizes).
- The **unstable dynamics is attracted by limit cycles**.

Step-pulsed heat load

- **Transients** after a step-pulsed heat load **have two stages**:
 - static inlet MFR stage
 - buoyant stage
- **High temperature excursions** (a few K) **at very low heat flux** (even $<100 \text{ W/m}^2$) can take place during the first stage if initially the system is at rest, especially for long NHHL.
- **Initially established flow and short NHHL can inhibit** this transient feature, which gives us hints of how to protect devices from this undesired effect.

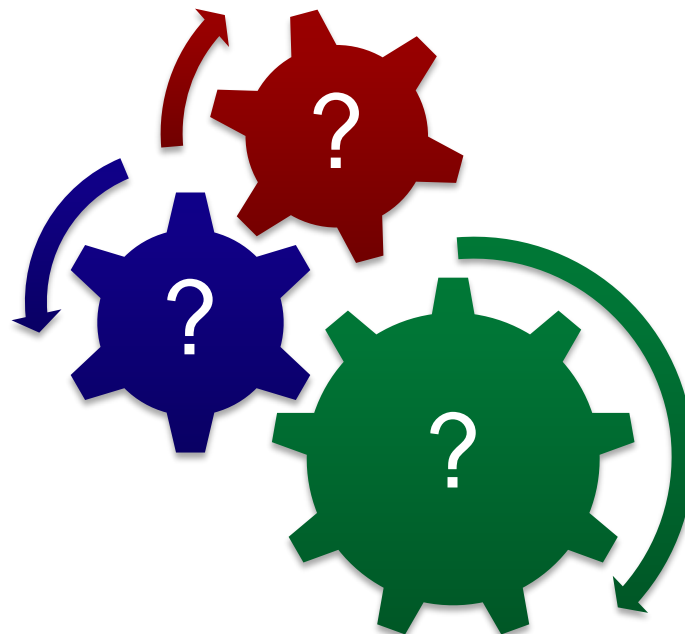
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Thank you for your attention!



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