Study of RF Breakdown in Normal Conducting Waveguides and Single Cell Structures

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Outline

Waveguides

Different geometries
Different materials

Single Cell Structures

Motivation

• **Predict** breakdown limits for practical structures of *different shapes, materials, circuits*

To do this, we need to understand the physics of rf breakdown.

Difficulties

• Full scale structures are long, complex, expensive and difficult to simulate

Solution

- *High gradient waveguides* with gradients, power and pulse energy close to that of practical structures
- Single Cell Traveling Wave and Standing Wave Structures

If we cannot understand small structures we will not be able to understand full scale structures

Operating conditions for X-band traveling wave accelerating structures and high power waveguides

•RF power ~100 MW

- •Area of high electric field $\sim 10 \text{ cm}^2$
- •Pulse width $\sim 1 \mu s$
- •Energy absorbed in the breakdown $\sim 10 \text{ J}$
- •Distance between metal surfaces ~1 cm

Geometries



Low magnetic field waveguide, height 10 mm High magnetic field waveguide, height 1.3 mm

The peak electric field surface area equal that of the low magnetic field waveguide
For a given input power both waveguide have the same peak electric field — 80 MV/m at 100 MW of rf power
Ratio between magnetic field in the middle of wide wall (maximum surface electric field) between both guides = 21

Field Distribution

Electric field



Magnetic field



Low magnetic field waveguide





High magnetic field waveguide

Breakdown threshold measurements for waveguides with different geometries



Comparison of *Power*sqrt(pulse widths)* for 3 accelerating structures and 2 copper waveguides "destruction limit"



Materials in low magnetic field waveguide

- Copper
- Stainless steel
- Gold
- Molybdenum

We like to thank Lisa Laurent and NLCTA team for their help with molybdenum waveguide experiment.

Molybdenum waveguide installed at NLCTA



Processing of molybdenum waveguide



Peak power vs. measurement number (one measurement every 2 sec)

Input pulse shape

Low magnetic field waveguides with different surface materials



Breakdown threshold measurements for low-magnetic-field waveguides with different materials

Peak power vs. pulse width during processing of molybdenum waveguide

Comparison of Power*sqrt(Pulse Width) for low-magnetic-field waveguides made of different metal



Pulse width [ns]

Peak Power*sqrt(Pulse Width) vs. pulse widthBreakdown Power*sqrt(Pulse Width) vs. pulseduring processing for molybdenum
waveguidewidth for copper, gold and stainless steel

Waveguide Summary

•Macroscopic geometry is a very important parameter in breakdown phenomena. High magnetic field waveguide has a lower breakdown threshold than low-magnetic-field waveguide. The electric field gap is much smaller (1.3mm vs. 10mm) in the high magnetic field waveguide. This gap dependence contradicts a DC model of the breakdown, where breakdown threshold usually decreases with increased gap.

Breakdown properties are strongly dependant on surface material. The stainless steel waveguide we tested had a higher breakdown threshold than copper. Gold had a lower threshold than copper.
For molybdenum waveguide, direct comparison was possible only to gold waveguide. This comparison shows the superiority of the molybdenum waveguide. If we project molybdenum results using dependence P*sqrt(pulse width) to longer pulse width, we consider molybdenum superior to copper and possibly close to the performance of the stainless steel waveguide.

More tests

• Stainless still high magnetic field waveguide and chromium-plated low magnetic field waveguide were made at SLAC and available for the test

Single Cell Structures

Work on single cell traveling wave and standing wave structures is done in collaboration with Yasuo Higashi and Toshiyasu Higo from KEK

Single Cell Structures

Traveling Wave

- Fields are the same as in first cell of NLC structure T53VG3
- High electric and magnetic fields are *only in this cell* (not in couplers)
- **Reusable couplers** mode launchers that transform the TE_{10} mode of rectangular waveguide into the "accelerating" circular TM_{01} mode

Standing Wave

- Fields in the middle cell of the SW structure are similar to fields of a large-aperture SW structure SW20a565
- Fields in the middle cell twice as high as in other two cells
- Breakdowns in one cell => *easy diagnostic*
- Small geometry => *easy simulation* with 3D particle and electromagnetic codes

TM₀₁ Mode Launcher



Cutaway view of the mode launcher





Surface electric fields in T splitter, E_{max} = 30 MV/m for 100 MW



Surface electric fields in the mode launcher E_{max} = 49 MV/m for 100 MW

Single Cell Traveling Wave Structures

Single Cell Traveling Wave Structure





Cold Test With Single Cell Traveling Wave Structure



On axis field profile for three single cell TW structures

High Power Test

High power test of single cell structures is done at Klystron Test Lab with great help of Chris Pearson, John Eichner, Lisa Laurent, Arnold Vlieks, Chuck Yoneda, John Glenn, John Van Pelt.









Single Cell Standing Wave Structures

Single Cell Standing Wave Structure HFSS Calculation



Bead-Pull Measurements



On axis field profile for single cell SW structures

Single Cell Traveling Wave and Standing Wave Structures



Molybdenum Structures



Input cell of SW structure

Molybdenum Structures



Molybdenum SW structure

Molybdenum TW structure

Molybdenum-Copper Structures



Molybdenum-copper SW structure cells

Molybdenum-copper TW structure cells

Molybdenum-Copper Structures



Input of single cell SW structure

Interface of molybdenum and copper after etching

Status of Single Cell Structure Tests

- We started high power conditioning of SLACmade single cell traveling wave structure. At present setup klystron is capable of delivering of 50 MW and 1.5 μ s rf.
- We expect shipment of single cell standing wave structures from KEK this month (Y. Higashi).