

High-Gradient, Millimeter Wave Accelerating Structure

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Outline:

1. Problems of normal conducting millimeter wave structures
2. Helical accelerating structure with asynchronous transverse fields
3. Calculation methods: perturbation theory and HFSS simulations
4. Optimization in comparison with classical structures
5. Beam dynamics simulation by CST Microwave Studio
6. First results of low-power tests
7. Conclusion

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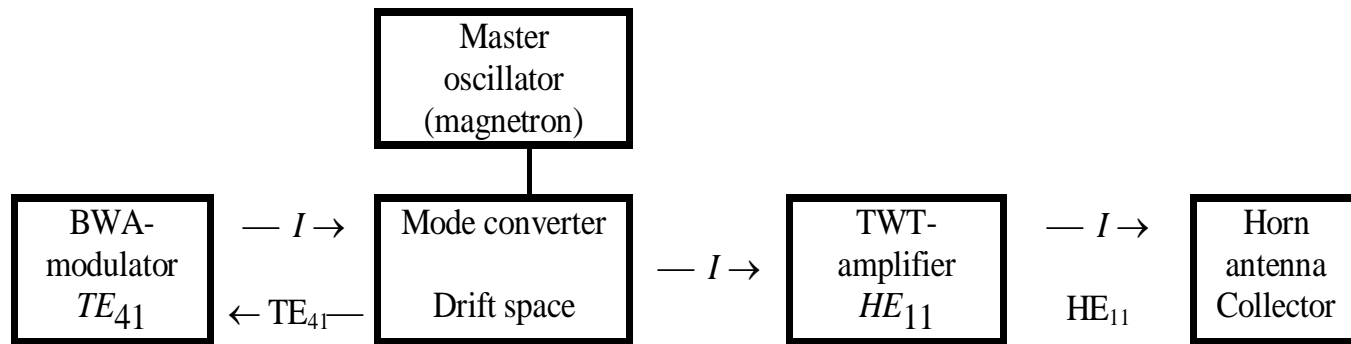
High-Gradient Mm-wave Accelerating Structure Based on Helical Waveguides

Recently Tantawi et al. (2014) showed **GV/m** level accelerating gradient in 116 GHz structure fed by short rf pulse produced by FACET's electron bunch. This experiments inspires to invent mm-wave accelerating structures having new properties:

1. Feeding by short, high repetition rate rf pulses ($\tau < 20 \text{ ns}$), in order to avoid breakdown and excessive pulse heating according to scaling laws:
$$E_s^p \tau = \text{const}, p = 5 - 6. \quad H_s^2 \sqrt{\tau} = \text{const}$$
2. Wide ($\geq 1 \text{ cm}$) channel in whole section without junctions for electron beam channeling and efficient pumping.
3. Because loss factor for excitation of wakefields is scaled as $\sim 1/a^2$ (a – structure's aperture), it is expected that beam emittance grows up with wavelength even faster (due to wakefields excited by geometry mistakes), one should preserve bunch emittances.
4. High coupling coefficient of cells to avoid strong sensitivity to spread of geometric parameters.
5. Smooth transverse beam focusing due to the ponderomotive (Miller's) force is also desirable.

Relativistic Cherenkov Electronics in Russia

There are GW level Cherenkov amplifiers with ~ 1 kHz repetition rate.
RF phase is controllable by low power stable RF source (proven in experiments).



Block diagram of GW level , 20 ns, X-band amplifier

Device	Wavelength cm	Power MW	Efficiency %	Gain dB	Voltage MV	Current kA
BWO+TWT ⁷	3.3	1100	20	47	0.8	6
TWT ⁸	0.8	100	10	44	0.5	2

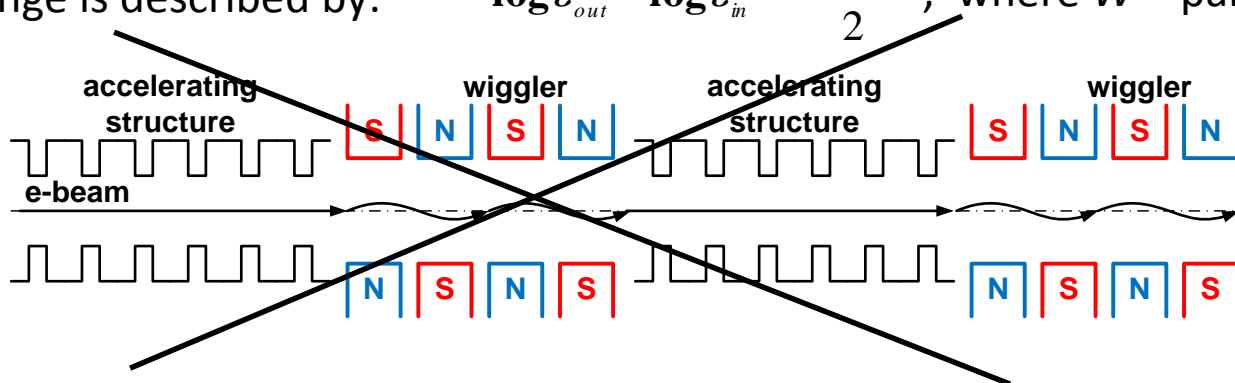


Short pulse superradiant BWO: 38 GHz, 1 GW, 3 ns, 100 Hz

Radiation beam cooling inside linear accelerator

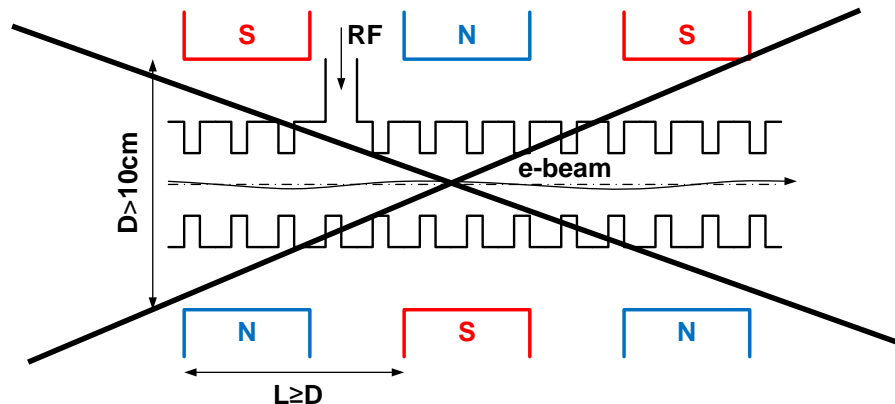
$P_\gamma [GeV/m] = 3.3 \cdot 10^{-13} \gamma^2 B^2 [T]$ - radiation cooling rate in a periodic DC-magnet field.

Emittance change is described by: $\log \varepsilon_{out} = \log \varepsilon_{in} - \frac{aB^2 W z}{2}$, where W – particle energy.



H.H. Braun et al. Potential of Non-standard Emittance Damping Schemes for Linear Colliders, 2004.

The accelerator with alternating accelerating sections and wigglers **reduces average gradient**.

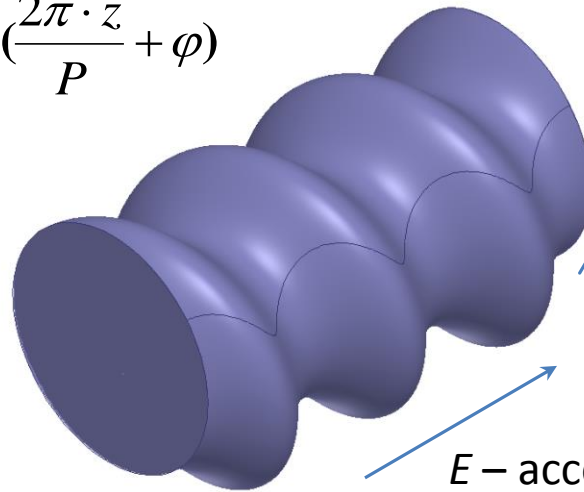


Such accelerating structure is **impractical**, because DC magnet system conflicts with feeding, focusing, and diagnostic systems. Inevitably large period does not allow to preserve small enough emittance, because an achievable emittance is proportional to squared wiggler period L .

Helical Accelerating Structure

Accelerating structure + RF undulator (+ lens)

$$r(z, \varphi) = R + a \cdot \sin\left(\frac{2\pi \cdot z}{P} + \varphi\right)$$



transverse field components
(far from Cherenkov synchronism)

E – accelerating field (synchronous with particles)

0 10 20 (mm)

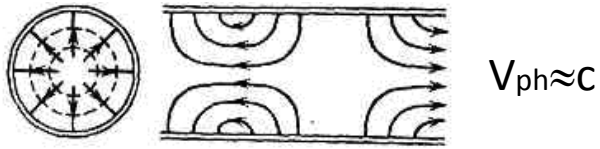


Copper magnet

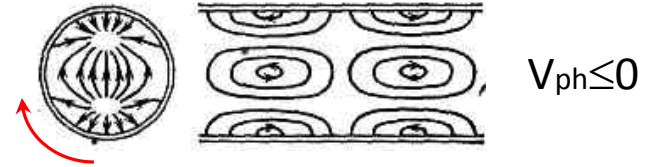
Appealing features:

1. Non-synchronous transverse field components might provide: 1) emittance control (beam cooling due to synchrotron radiation of particles); 2) near axis beam focusing
2. A new structure has smooth shape of constant circular cross-section (no expansions or narrowings) and big aperture (no small irises)
3. A new technology of the mass production seems possible which allows avoiding junctions inside long accelerating section

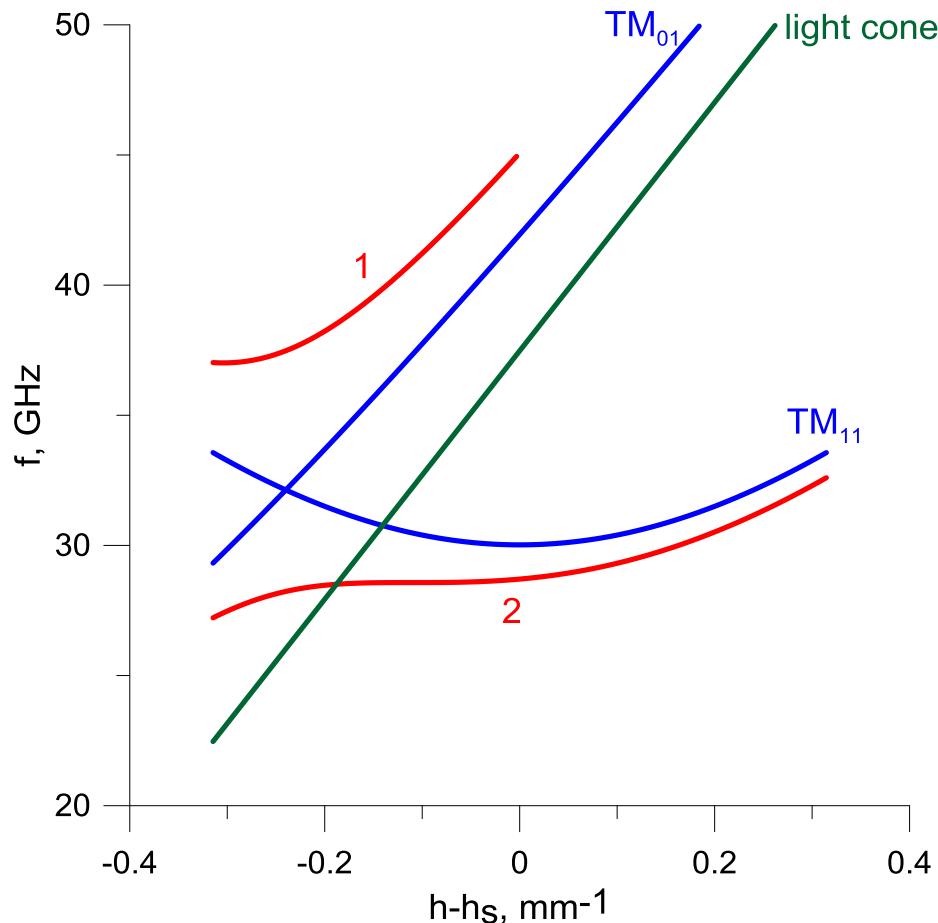
Partial waves: 1) travelling TM_{01} mode + 2) near to cut off rotating TM_{11} mode



TM_{01} : $E_z \neq 0$ at axis, $E_z \sim \exp(jhz - j\omega t)$



TM_{11} : $E_z = 0$ at axis, E_\perp and $H_\perp \neq 0$ at axis,
 $E_\perp, H_\perp \sim \exp(j(h - h_s)z - j\omega t)$, $h - h_s \rightarrow 0$



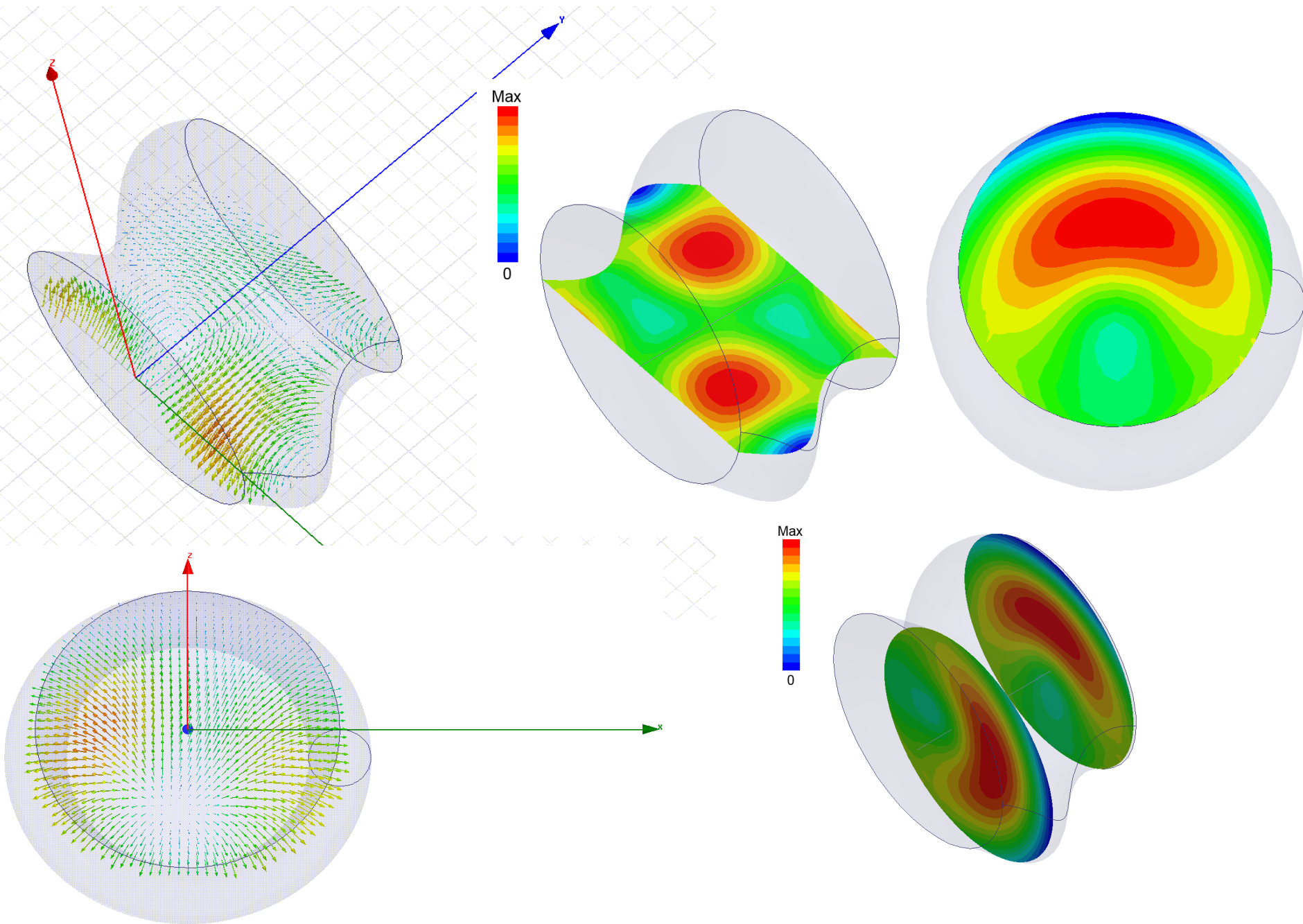
— Partial waves
 — Normal waves

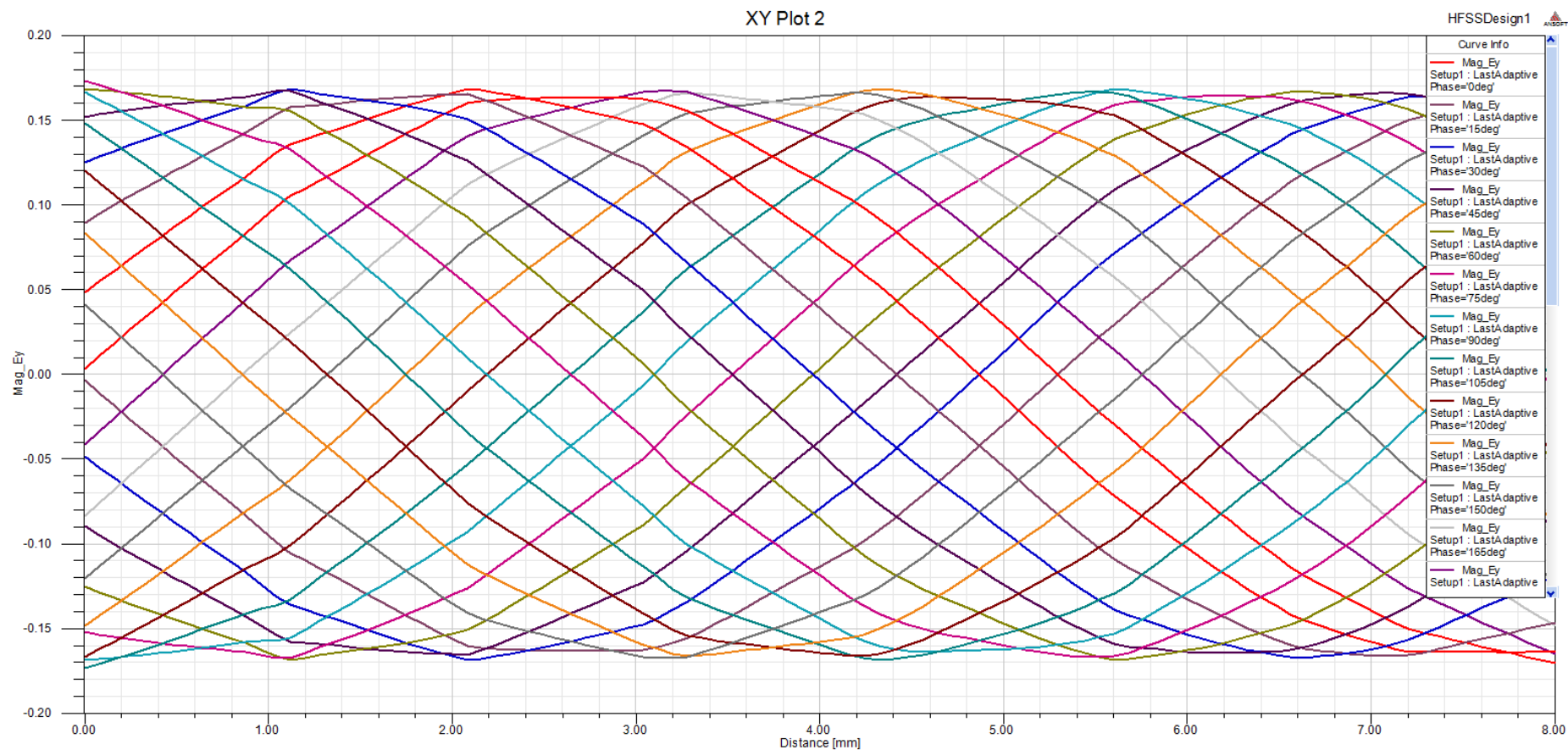
Slow normal wave 2 ($v_{gr} \times v_{ph} > 0$) consists of partial TM_{01} and TM_{11} waves.

The wave 2 is the operating wave (might be in synchronism, it has low group velocity).

Dispersion curves: $R=6.09$ mm, $P=8$ mm, $a=1.25$ mm ($h_s = 2\pi / P$)

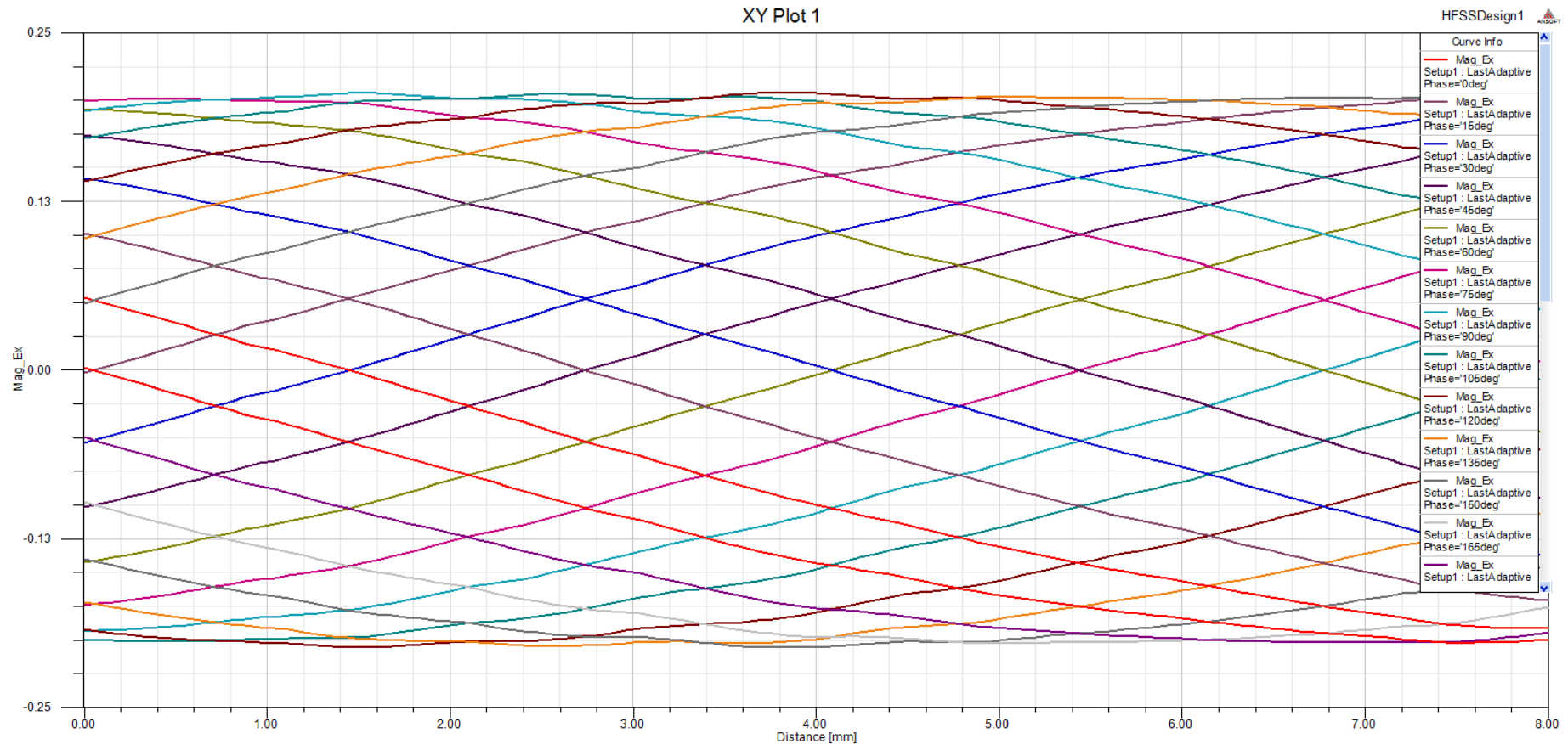
Electric field in helical accelerating structure. Calculation by HFSS





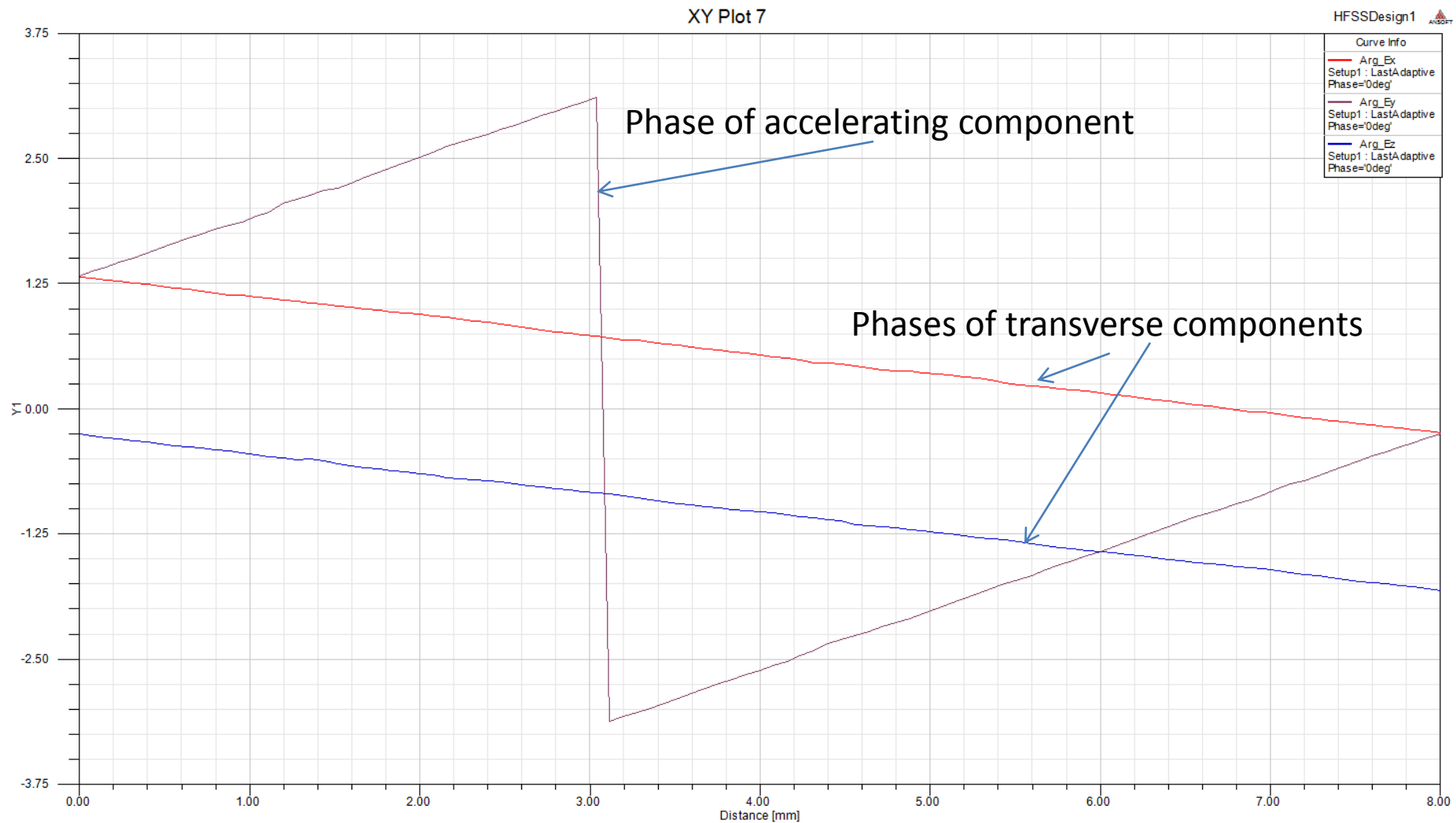
Accelerating field component vs longitudinal coordinate for different phases (with step 5°)

Accelerating component is uniform at beam line.



Transverse electric field components at beam line vs length for different phases

Transverse components are also uniform and have much longer spatial period in comparison with period of the accelerating component.



Phases of electric field components at beam line

Accelerating E-field and transverse E-fields have opposite phase velocities!
Phase velocity of the accelerating component actually equals the light velocity.

Results of HFSS optimization

$R=6.09$ mm

$a=1.25$ mm

$P=8$ mm

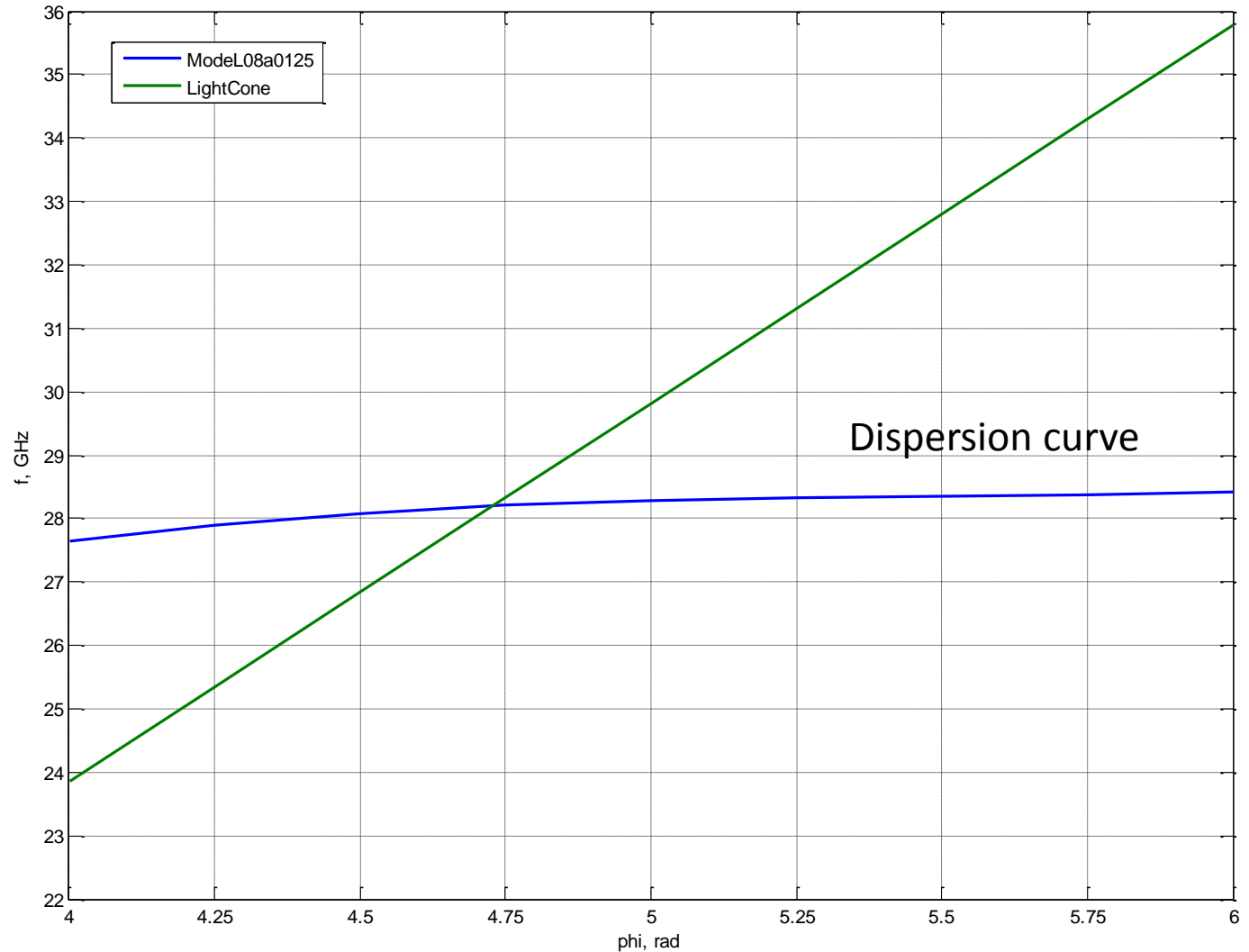
$hP=4.727$

$f=28.2$ GHz

$Q=10800$

$E_{acc}/E_{surf}=0.307$

$R_{sh}/L=18.9$ MOhm/m



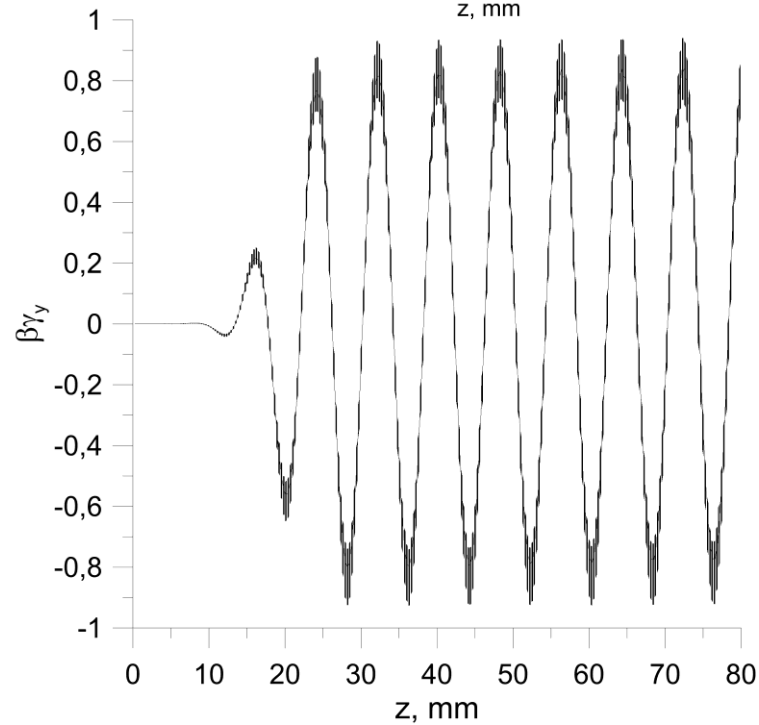
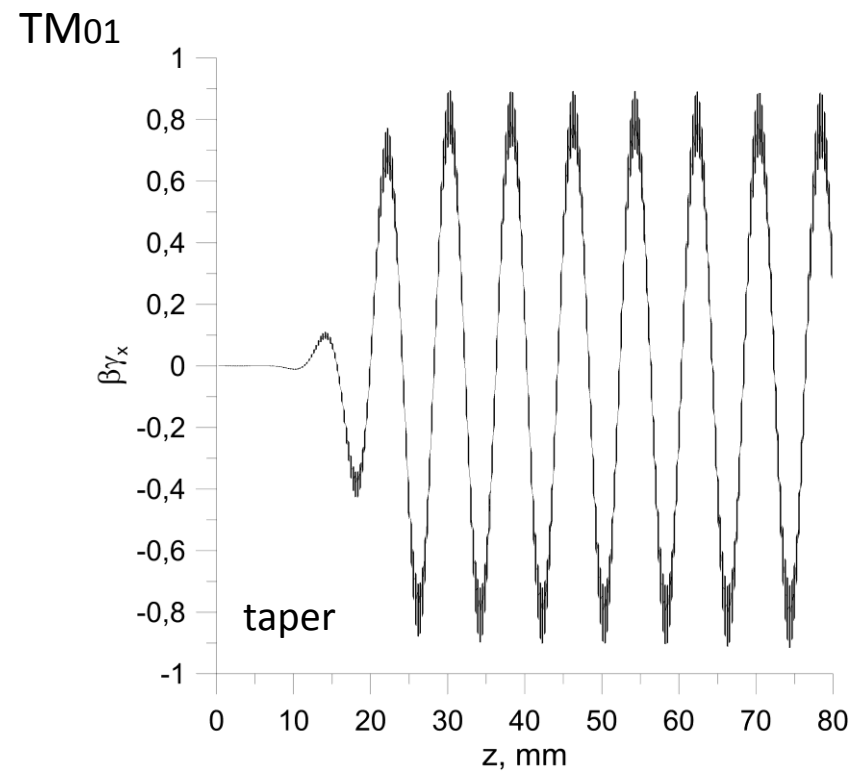
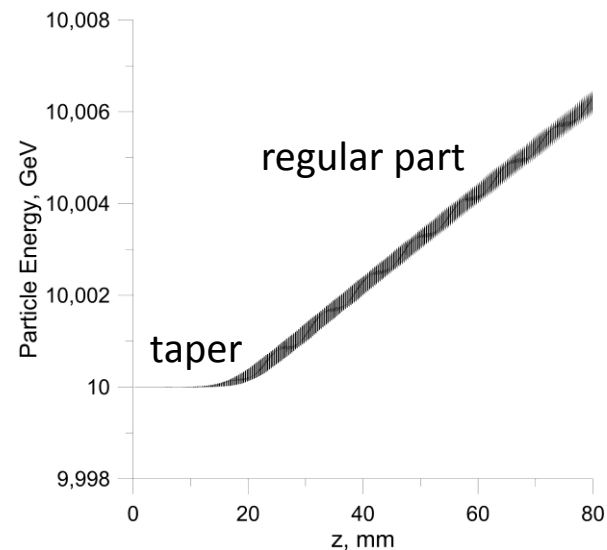
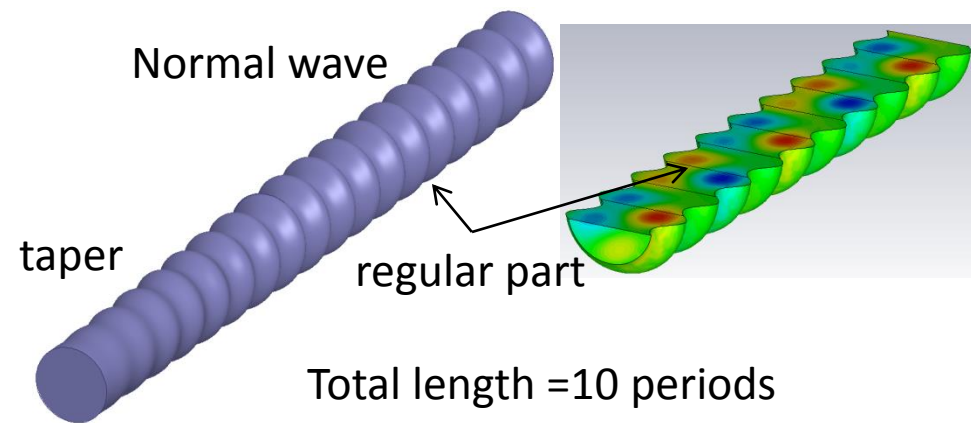
Example:

$f=30$ GHz structure, $G=E_{acc}=100$ MV/m, then $B=0.75$ T,

Beam energy $W=25$ GeV ($\gamma=49000$),

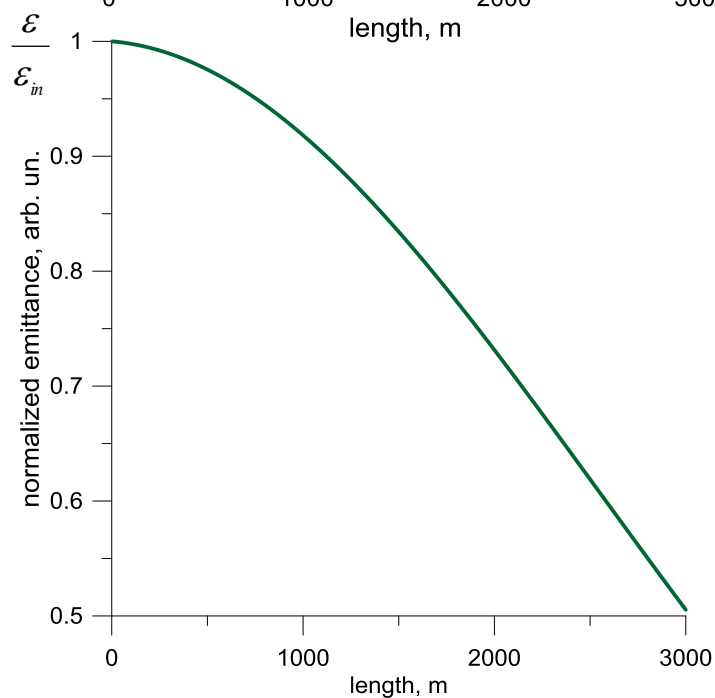
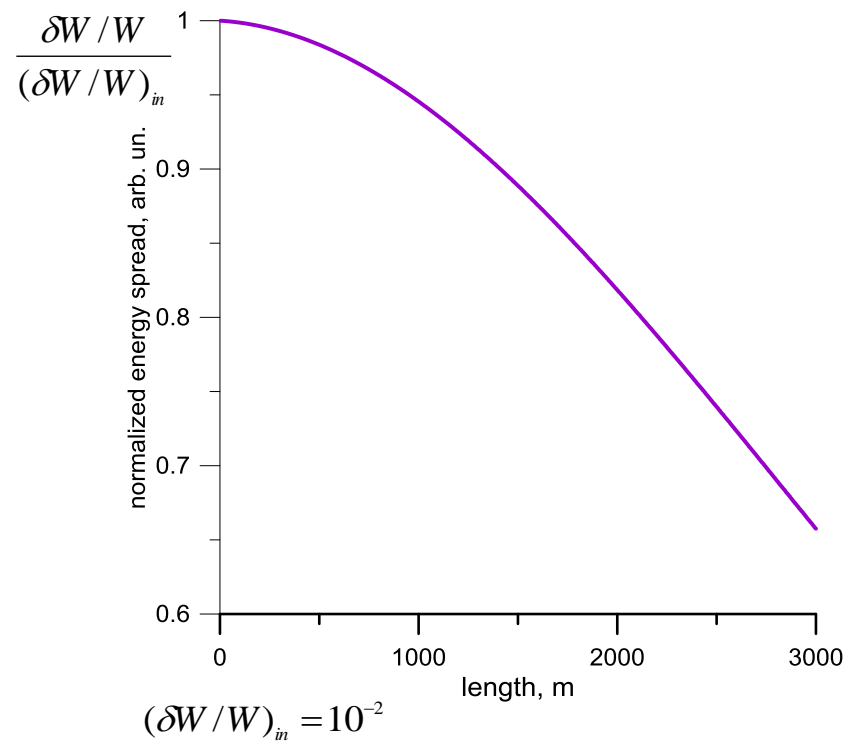
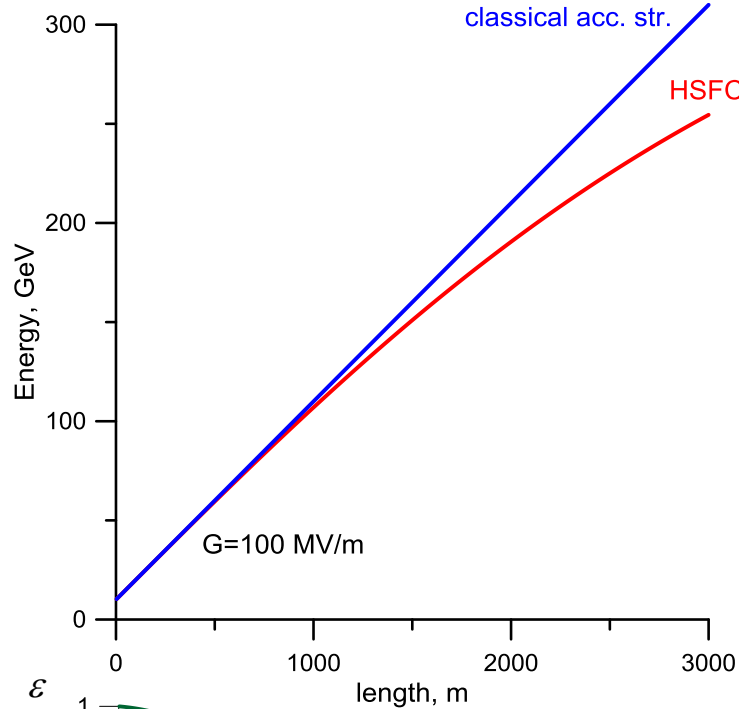
then necessary decay distance ≈ 2800 m.

Simulation of particle motion in 100 MV/m accelerating structure by CST Microwave Studio



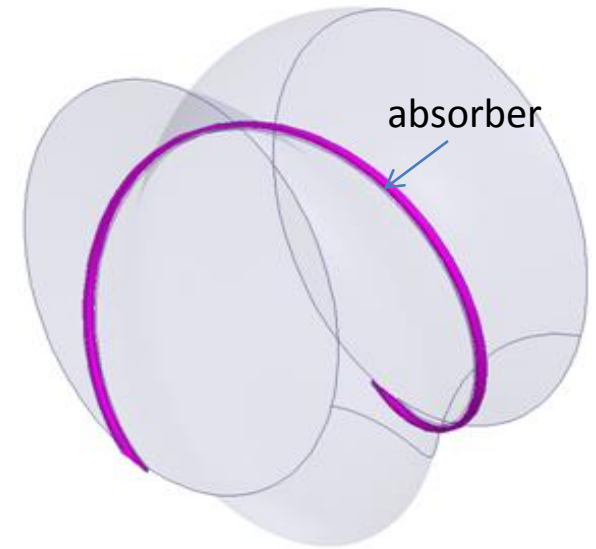
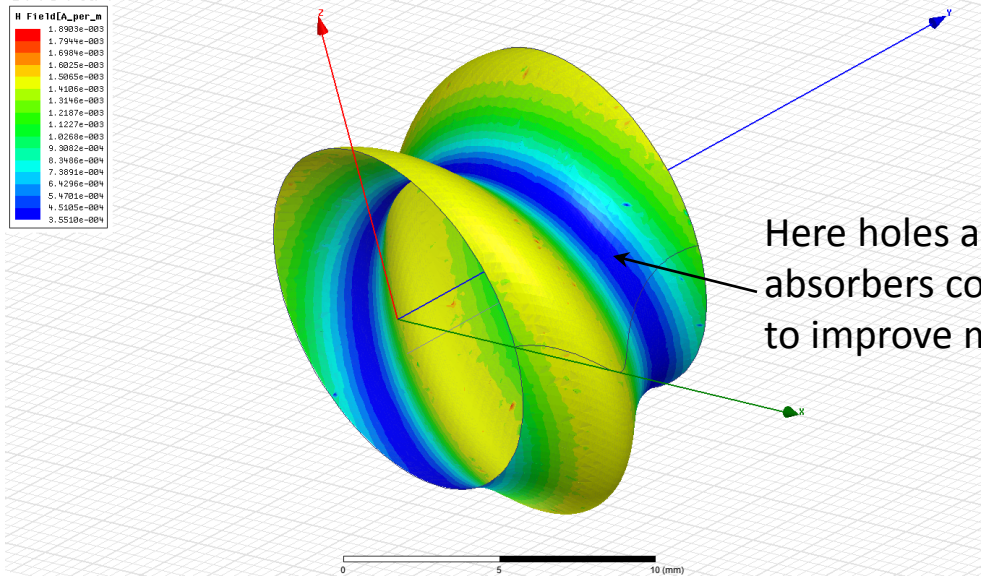
Transverse particle momentums

Parameters of cooling in 100 MV/m structure

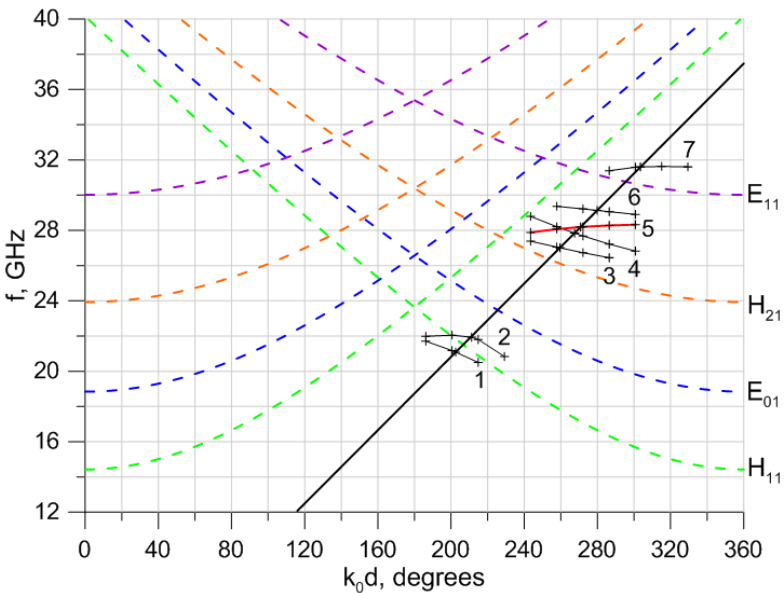


$$\epsilon_{in} = 1.4 \text{ mrad} \times \text{mm}$$

Mode selection properties



Surface magnetic field



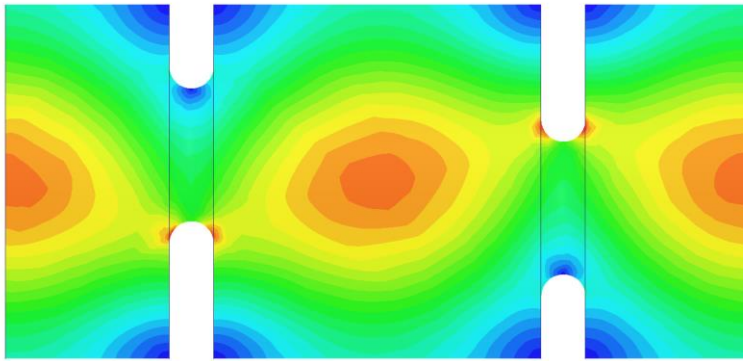
No absorber

Absorber

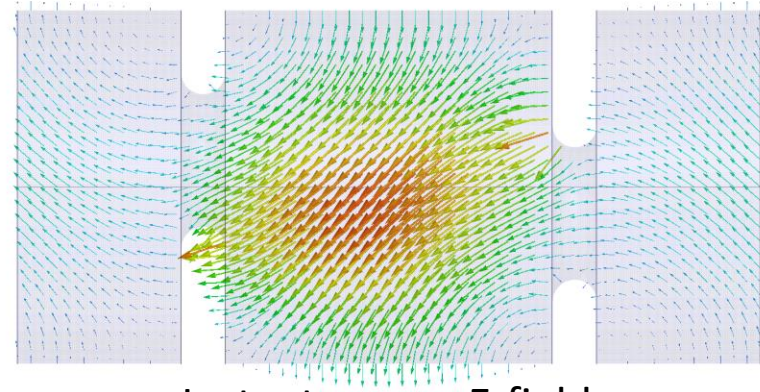
Mode	Rotation	Phase, rad	Frequency, GHz	Q-factor	Frequency, GHz	Q-factor
H ₁₁	ccw	3.5346	21.0869	9255	21.0862	2607
H ₁₁	cw	3.687	21.9336	8832	21.9368	3464
H ₂₁	ccw	4.53	27.0125	7141	26.9984	1650
H ₂₁	cw	4.67	27.8435	7869	27.8277	2623
E ₁₁	ccw	4.727	28.193	10824	28.193	8168
E ₁₁	cw	4.885	29.1356	9940	29.1345	6391
H ₀₁	-	5.2975	31.6039	14856	31.5939	3004

High shunt impedance in bi-periodic accelerating structure

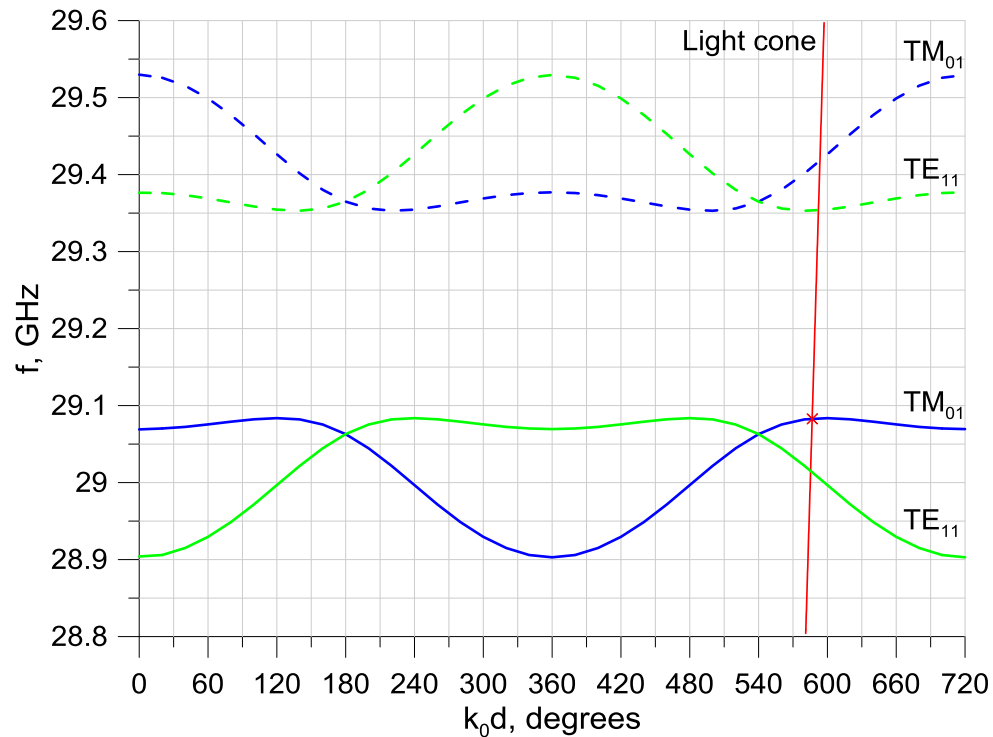
The first period is shaped by irises which are shifted transversally with twice bigger period.



Average E-field



Instantaneous E-field

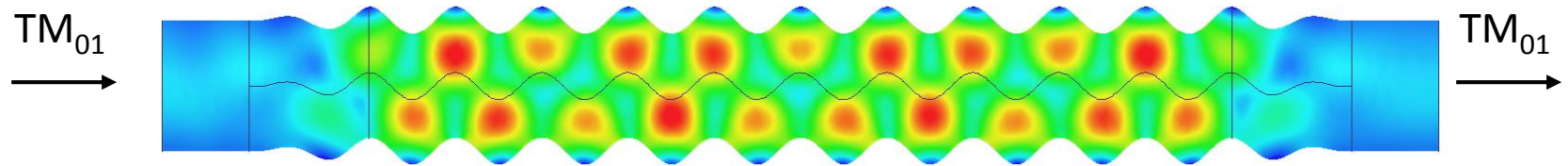


At 30 GHz shunt impedance exceeds 90 MOhm/m.

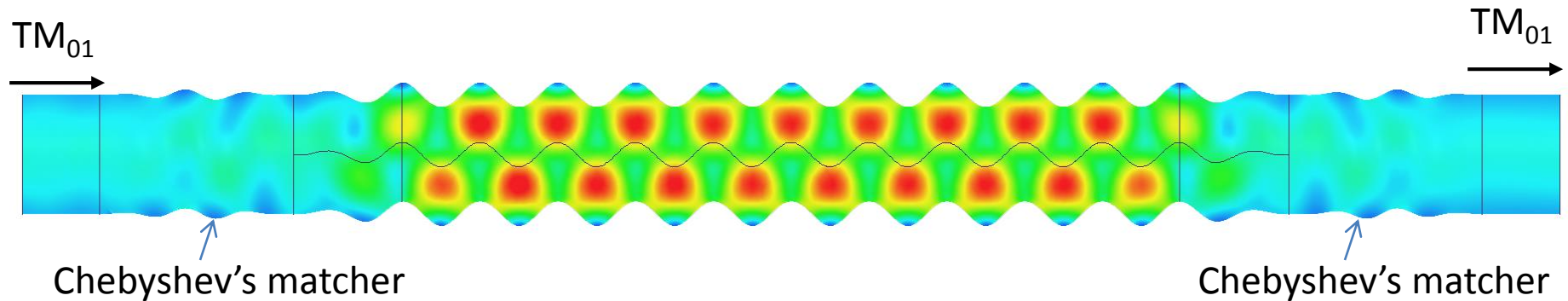
But some advantages of the primary idea are lost in this design.

Couplers for Helical Accelerating Structure

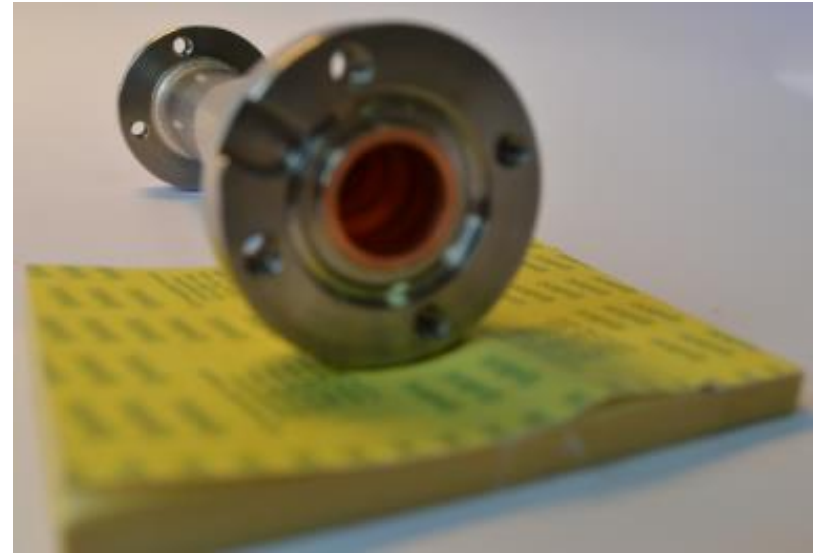
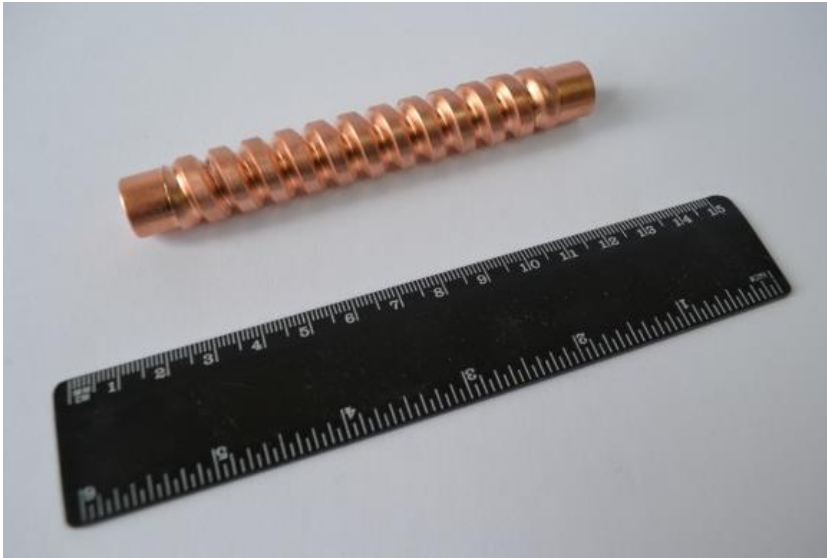
1) Reflections of the left and right ends compensate each other. In this case the length of the whole structure is fixed.



2) Each end is matched by its own Chebyshev's matcher (short section of the smaller corrugation rotated by proper angle relative to main corrugation). In this case the length of the structure can be arbitrary.



First low-power tests

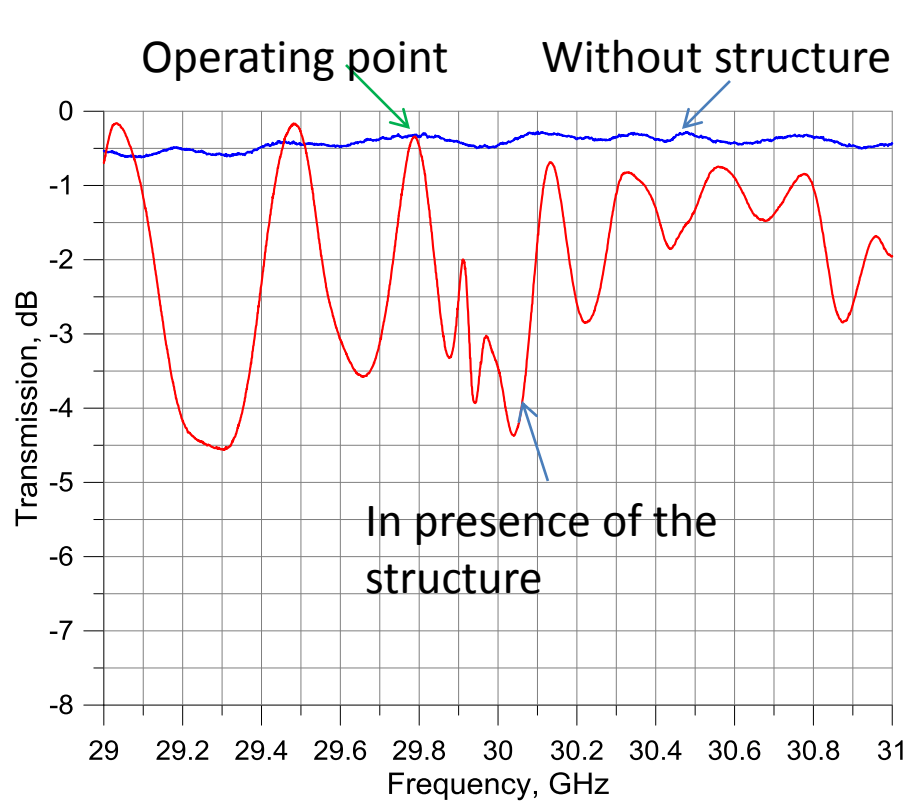
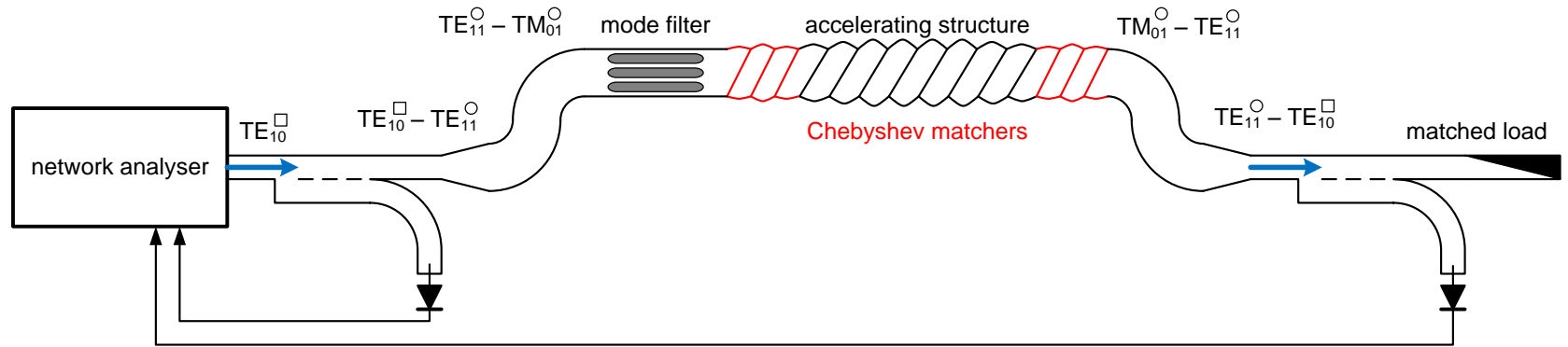


Photographs of the copper prototype and the equipped structure

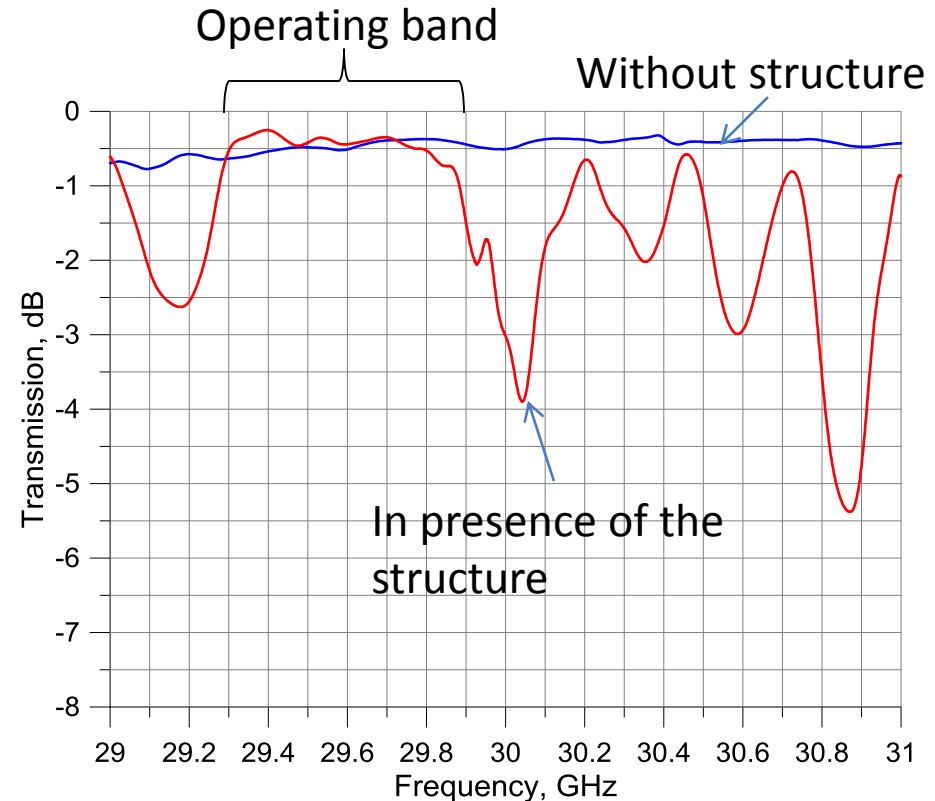


Experimental setup

Measurements of efficiency using transmission scheme

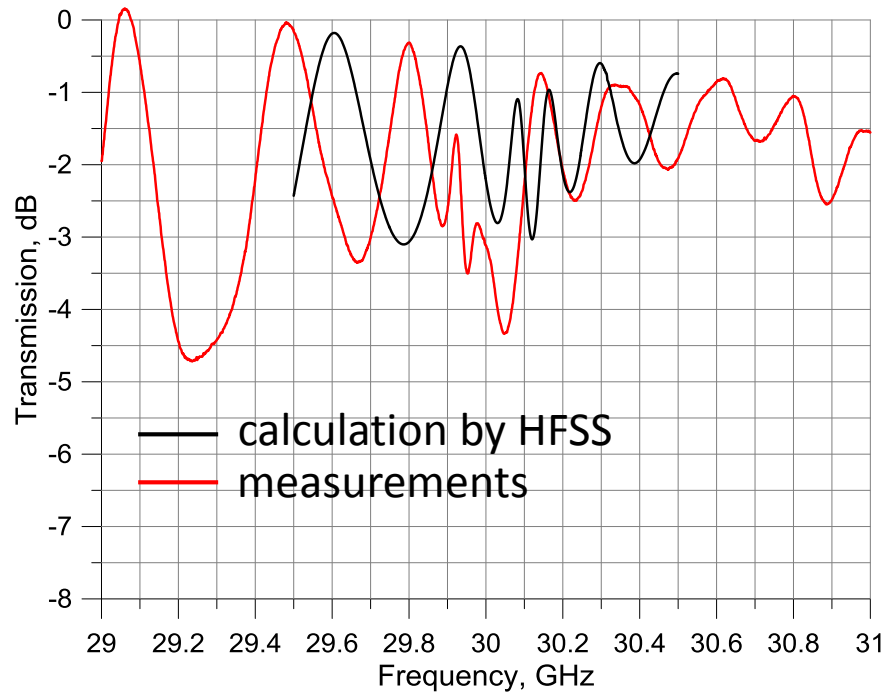


Transmitted power through the structure **without** Chebyshev's matchers

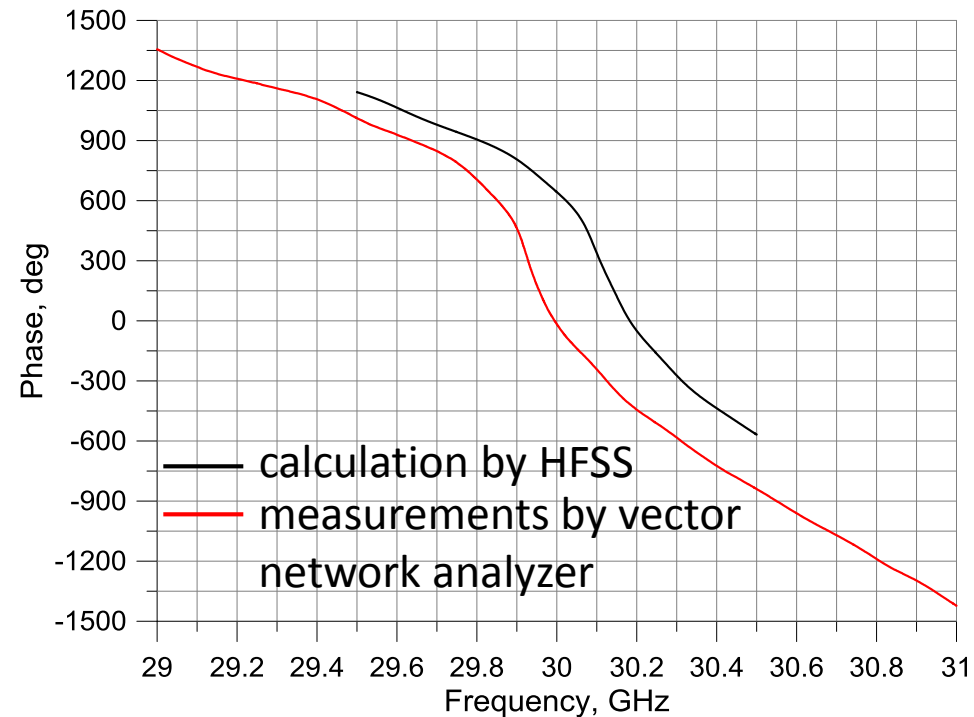


Transmitted power through the structure **with** Chebyshev's matchers

Measurements of frequency shift and dispersion of the structure



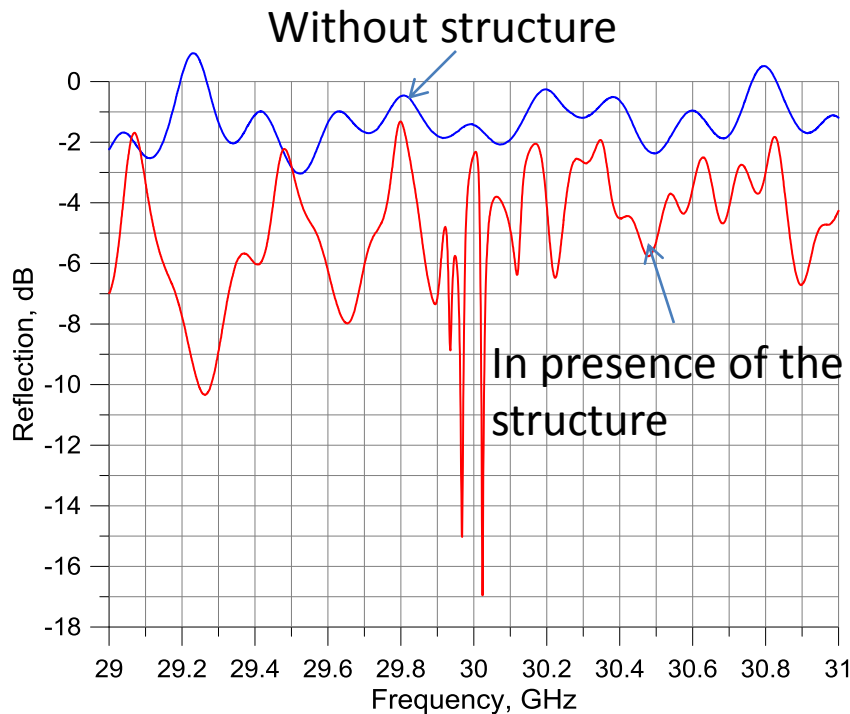
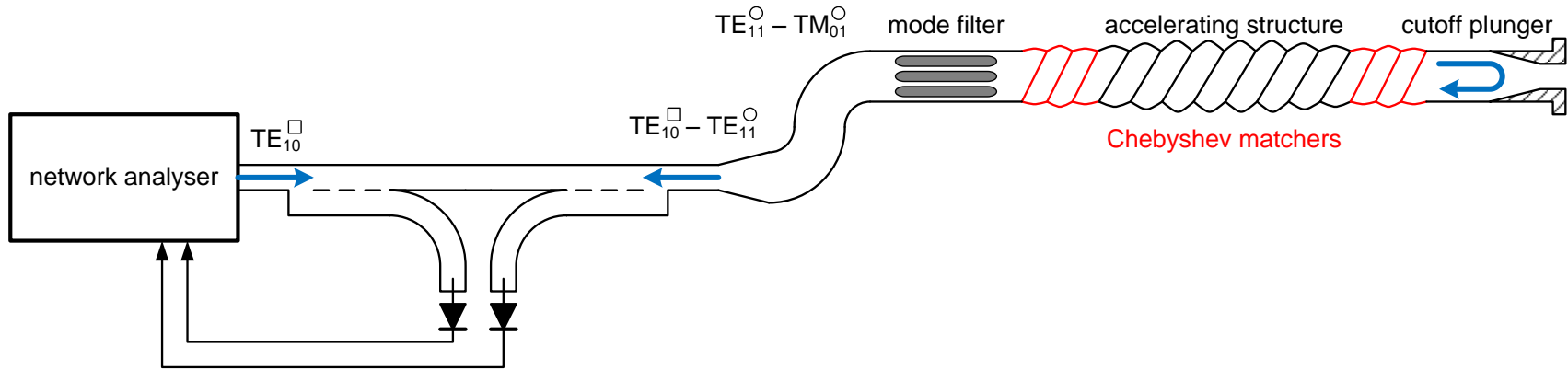
Transmitted power for the structure
without matchers



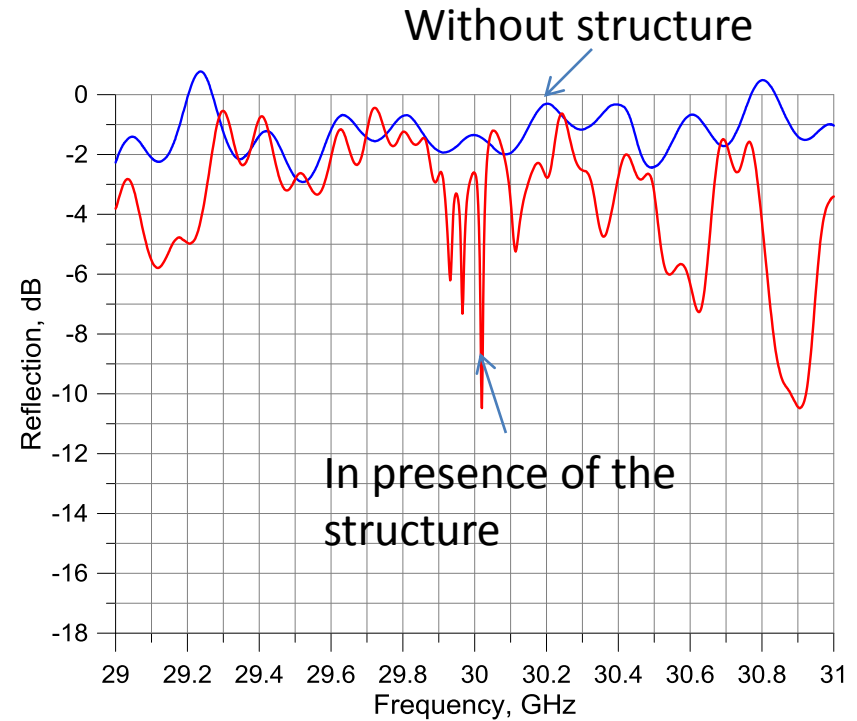
Dispersion of the helical structure without
Chebyshev's matchers

We have observed 150 MHz shift between calculation and measurements.
The reason is technological mistake for the average radius of the helical waveguide.

Measurements of efficiency using reflection scheme



Reflected power through the structure **without** Chebyshev's matchers



Reflected power through the structure **with** Chebyshev's matchers

Conclusion

1. $TM_{01} - TM_{11}$ helical accelerating structure has several appealing properties. In particular, non-synchronous electric and magnetic field components are used, in order to preserve low beam emittance and small energy spread. The structure allows high accelerating gradient due to nanosecond filling time.
2. Shunt impedance is slightly less than in a conventional accelerating structure.
3. In order to increase shunt impedance, one might use the design based on irises with periodic off-axis shift.
4. The carried out first low-power tests show promising results.
5. High-power experiment with the use of multi-megawatt 30 GHz FEM to feed the structure is coming.