The bubble wall velocity Cosmological phase transition front propagation

Ariel Mégevand

CONICET - University of Mar del Plata - Argentina

eLISA Cosmology Working Group Workshop - April 2015

◆□> ◆□> ◆三> ◆三> 三三 のへで

3

イロン イ団と イヨン イヨン

The free energy density (finite-temperature effective potential)

3

イロト イヨト イヨト イヨト

The free energy density (finite-temperature effective potential)

► The free energy density *F*(*T*) determines the equation of state: *p* = −*F*(*T*), *s* = *dp*/*dT*, *e* = *Ts* − *p*,...

The free energy density (finite-temperature effective potential)

- ► The free energy density *F*(*T*) determines the equation of state: *p* = −*F*(*T*), *s* = *dp*/*dT*, *e* = *Ts* − *p*,...
- ▶ In the presence of a background field  $\phi$ , the minimum of  $\mathcal{F}(\phi, T)$  gives the equilibrium expectation value  $\langle \phi \rangle$

イロン イロン イヨン イヨン 三日

The free energy density (finite-temperature effective potential)

- ► The free energy density *F*(*T*) determines the equation of state: *p* = −*F*(*T*), *s* = *dp*/*dT*, *e* = *Ts* − *p*,...
- In the presence of a background field φ, the minimum of F(φ, T) gives the equilibrium expectation value ⟨φ⟩

The electroweak theory  $\langle H \rangle = (0, \langle \phi \rangle / \sqrt{2})^T$ ,  $\phi$  real (Higgs)

・ロト ・ 日 ・ ・ 日 ・ ・ 日 ・ ・ 日

The free energy density (finite-temperature effective potential)

- ► The free energy density *F*(*T*) determines the equation of state: *p* = −*F*(*T*), *s* = *dp*/*dT*, *e* = *Ts* − *p*,...
- In the presence of a background field φ, the minimum of F(φ, T) gives the equilibrium expectation value ⟨φ⟩

The electroweak theory  $\langle H \rangle = (0, \langle \phi \rangle / \sqrt{2})^T$ ,  $\phi$  real (Higgs)  $\mathcal{F}(\phi, T) = V(\phi) + \Delta V(\phi, T)$ , where

(日) (雪) (ヨ) (ヨ) (ヨ)

The free energy density (finite-temperature effective potential)

- ► The free energy density *F*(*T*) determines the equation of state: *p* = −*F*(*T*), *s* = *dp*/*dT*, *e* = *Ts* − *p*,...
- In the presence of a background field φ, the minimum of F(φ, T) gives the equilibrium expectation value ⟨φ⟩

The electroweak theory  $\langle H \rangle = (0, \langle \phi \rangle / \sqrt{2})^T$ ,  $\phi$  real (Higgs)  $\mathcal{F}(\phi, T) = V(\phi) + \Delta V(\phi, T)$ , where

zero-T effective potential:  $V(\phi) = -m^{2}\phi^{2} + \lambda\phi^{4} \text{ (tree-level)}$   $+ \sum_{i} \frac{\pm g_{i}}{64\pi^{2}} \left[ m_{i}^{4}(\phi) \left( \log \left( \frac{m_{i}^{2}(\phi)}{m_{i}^{2}(v)} \right) - \frac{3}{2} \right) + 2m_{i}^{2}(\phi)m_{i}^{2}(v) \right]$   $(1\text{-loop, } m_{i}(\phi) = \text{Higgs-dependent particle masses})$ 

イロン イロン イヨン イヨン 三日

The free energy density (finite-temperature effective potential)

- ► The free energy density *F*(*T*) determines the equation of state: *p* = −*F*(*T*), *s* = *dp*/*dT*, *e* = *Ts* − *p*,...
- In the presence of a background field φ, the minimum of F(φ, T) gives the equilibrium expectation value ⟨φ⟩

The electroweak theory  $\langle H \rangle = (0, \langle \phi \rangle / \sqrt{2})^T$ ,  $\phi$  real (Higgs)  $\mathcal{F}(\phi, T) = V(\phi) + \Delta V(\phi, T)$ , where

zero-T effective potential:spontaneous symmetry<br/>breaking $V(\phi) = -m^2 \phi^2 + \lambda \phi^4$  (tree-level)breaking $+ \sum_i \frac{\pm g_i}{64\pi^2} \left[ m_i^4(\phi) \left( \log \left( \frac{m_i^2(\phi)}{m_i^2(v)} \right) - \frac{3}{2} \right) + 2m_i^2(\phi) m_i^2(v) \right]$ <br/>(1-loop,  $m_i(\phi) =$  Higgs-dependent particle masses) $\Delta V(\phi, T) = \sum_i (\pm g_i) \int \frac{d^3p}{(2\pi)^3} \log \left( 1 \mp e^{-\sqrt{p^2 + m_i(\phi)^2}/T} \right)$ <br/>finite-temperature correctionssymmetry restoration at high T

• At high T we have  $\langle \phi \rangle = 0$  while at T = 0 we have  $\langle \phi \rangle = v$ 

- At high T we have  $\langle \phi \rangle = 0$  while at T = 0 we have  $\langle \phi \rangle = v$
- At intermediate temperatures, the minimum of the free energy density *F*(φ, *T*) changes from φ = 0 to φ = v

- At high T we have  $\langle \phi \rangle = 0$  while at T = 0 we have  $\langle \phi \rangle = v$
- At intermediate temperatures, the minimum of the free energy density *F*(φ, *T*) changes from φ = 0 to φ = v
- For a first-order phase transition we have



 Two minima separated by a barrier (the absolute minimum is stable)

- 4 同 6 4 日 6 4 日 6

- At high T we have  $\langle \phi \rangle = 0$  while at T = 0 we have  $\langle \phi \rangle = v$
- At intermediate temperatures, the minimum of the free energy density *F*(φ, *T*) changes from φ = 0 to φ = v
- For a first-order phase transition we have



 Two minima separated by a barrier (the absolute minimum is stable)

(日) (周) (日) (日)

• High  $T: \phi = 0$ 

- At high T we have  $\langle \phi \rangle = 0$  while at T = 0 we have  $\langle \phi \rangle = v$
- At intermediate temperatures, the minimum of the free energy density *F*(φ, *T*) changes from φ = 0 to φ = ν
- For a first-order phase transition we have



 Two minima separated by a barrier (the absolute minimum is stable)

イロト イポト イヨト イヨト

- High  $T: \phi = 0$
- Low  $T: \phi = \phi_b(T)$

- At high T we have  $\langle \phi \rangle = 0$  while at T = 0 we have  $\langle \phi \rangle = v$
- At intermediate temperatures, the minimum of the free energy density *F*(φ, *T*) changes from φ = 0 to φ = ν
- For a first-order phase transition we have



- Two minima separated by a barrier (the absolute minimum is stable)
- High  $T: \phi = 0$
- Low  $T: \phi = \phi_b(T)$
- $T_c$  = critical temperature:  $\mathcal{F}(0, T_c) = \mathcal{F}(\phi_b, T_c)$

< ロ > < 同 > < 回 > < 回 > < 回 > <

- At high T we have  $\langle \phi \rangle = 0$  while at T = 0 we have  $\langle \phi \rangle = v$
- At intermediate temperatures, the minimum of the free energy density *F*(φ, *T*) changes from φ = 0 to φ = v
- For a first-order phase transition we have



- Two minima separated by a barrier (the absolute minimum is stable)
- High  $T: \phi = 0$
- Low  $T: \phi = \phi_b(T)$

•  $T_c$  = critical temperature:  $\mathcal{F}(0, T_c) = \mathcal{F}(\phi_b, T_c)$ 

<ロト < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > <

► The two phases are characterized by two different EOS  $\mathcal{F}_u(T) = \mathcal{F}(0, T)$  and  $\mathcal{F}_b(T) = \mathcal{F}(\phi_b(T), T)$ unbroken-symmetry phase broken-symmetry phase

At a temperature  $T_n < T_c$  (supercooling) bubbles nucleate



イロト イポト イヨト イヨト

At a temperature  $T_n < T_c$  (supercooling) bubbles nucleate



At a temperature  $T_n < T_c$  (supercooling) bubbles nucleate



- 小田 ト イヨト

At a temperature  $T_n < T_c$  (supercooling) bubbles nucleate



A. Mégevand, Bubble wall velocity

(本部) (本語) (本語)

At a temperature  $T_n < T_c$  (supercooling) bubbles nucleate



・ロン ・四 ・ ・ ヨン ・ ヨン

At a temperature  $T_n < T_c$  (supercooling) bubbles nucleate



- $p_b(T_c) = p_u(T_c)$ , but  $p_b(T_n) > p_u(T_n)$
- ▶ also,  $e_b(T_c) < e_u(T_c)$ . Latent heat:  $L = e_u(T_c) e_b(T_c)$ .
- The latent heat reheats the plasma

・ロン ・四 ・ ・ ヨン ・ ヨン

At a temperature  $T_n < T_c$  (supercooling) bubbles nucleate



- $p_b(T_c) = p_u(T_c)$ , but  $p_b(T_n) > p_u(T_n)$
- ▶ also,  $e_b(T_c) < e_u(T_c)$ . Latent heat:  $L = e_u(T_c) e_b(T_c)$ .
- The latent heat reheats the plasma
- Configuration of the Higgs field  $(\phi \equiv \langle \hat{\phi} \rangle)$

・ロン ・四 ・ ・ ヨン ・ ヨン

At a temperature  $T_n < T_c$  (supercooling) bubbles nucleate



- $p_b(T_c) = p_u(T_c)$ , but  $p_b(T_n) > p_u(T_n)$
- ▶ also,  $e_b(T_c) < e_u(T_c)$ . Latent heat:  $L = e_u(T_c) e_b(T_c)$ .
- The latent heat reheats the plasma
- Configuration of the Higgs field  $(\phi \equiv \langle \hat{\phi} \rangle)$

• Bubbles expand (bubble walls move):  $\phi = \phi(\mathbf{x}, t)$ 

The field equation can be derived from the operator equation, with a suitable statistical average

・ロト ・ 四ト ・ ヨト ・ ヨト

- The field equation can be derived from the operator equation, with a suitable statistical average
- ► We have

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi, T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$
  
$$i = \text{particle species, } E_{i} = \sqrt{p^{2} + m_{i}^{2}(z, t)}$$

3

・ロト ・ 日 ト ・ ヨ ト ・ ヨ ト …

- The field equation can be derived from the operator equation, with a suitable statistical average
- We have

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi, T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$
  
*i* = particle species,  $E_{i} = \sqrt{p^{2} + m_{i}^{2}(z, t)}$   
 $\delta f_{i}$  = deviations from equilibrium particle distributions  $f_{0i}$ :  
 $f_{i} = f_{0i} + \delta f_{i}, \qquad f_{0i} = 1/(e^{E_{i}/T} \pm 1)$ 

3

イロト イヨト イヨト イヨト

- ► The field equation can be derived from the operator equation, with a suitable statistical average
- We have

1 δ

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi, T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$
  
*i* = particle species,  $E_{i} = \sqrt{p^{2} + m_{i}^{2}(z, t)}$   
 $\delta f_{i}$  = deviations from equilibrium particle distributions  $f_{0i}$ :  
 $f_{i} = f_{0i} + \delta f_{i}, \qquad f_{0i} = 1/(e^{E_{i}/T} \pm 1)$ 

The wall motion and latent heat release cause reheating and bulk motions of the fluid.

・ロン ・四 と ・ ヨン ・ ヨン

- The field equation can be derived from the operator equation. with a suitable statistical average
- We have

1 δ

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$
  
*i* = particle species,  $E_{i} = \sqrt{p^{2} + m_{i}^{2}(z,t)}$   
 $\delta f_{i}$  = deviations from equilibrium particle distributions  $f_{0i}$   
 $f_{i} = f_{0i} + \delta f_{i}, \quad f_{0i} = 1/(e^{E_{i}/T} \pm 1)$ 

The wall motion and latent heat release cause reheating and bulk motions of the fluid. We have e.g. T = T(x)

イロト イヨト イヨト イヨト

- The field equation can be derived from the operator equation, with a suitable statistical average
- We have

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$
  
*i* = particle species,  $E_{i} = \sqrt{p^{2} + m_{i}^{2}(z,t)}$   
 $\delta f_{i}$  = deviations from equilibrium particle distributions  $f_{0i}$   
 $f_{i} = f_{0i} + \delta f_{i}, \quad f_{0i} = 1/(e^{E_{i}/T} \pm 1)$ 

- The wall motion and latent heat release cause reheating and bulk motions of the fluid. We have e.g. T = T(x)
- So we must also consider the fluid equations

$$\partial_{\mu}\left(T^{\mu\nu}_{\mathrm{plasma}}+T^{\mu\nu}_{\phi}
ight)=0$$

f

イロト イヨト イヨト イヨト

► The equations for the fluid variables v(x, t), T(x, t) and the field φ(x, t) can be solved together (numerically)

・ロト ・ 日 ・ ・ ヨ ト ・ ヨ ト ・

- ► The equations for the fluid variables v(x, t), T(x, t) and the field φ(x, t) can be solved together (numerically)
- However, the width of the wall is much smaller than the length scale of fluid profiles

< ロ > < 同 > < 回 > < 回 > < 回 > <

- ► The equations for the fluid variables v(x, t), T(x, t) and the field φ(x, t) can be solved together (numerically)
- However, the width of the wall is much smaller than the length scale of fluid profiles
- The interface can be assumed to be infinitely thin

< ロ > < 同 > < 回 > < 回 > < 回 > <

- ► The equations for the fluid variables v(x, t), T(x, t) and the field φ(x, t) can be solved together (numerically)
- However, the width of the wall is much smaller than the length scale of fluid profiles
- The interface can be assumed to be infinitely thin
- On each side of the interface, we have  $\partial_{\mu}T^{\mu\nu} = 0$ , with  $T^{\mu\nu} = w u^{\mu}u^{\nu} - p g^{\mu\nu}$

◆□▶ ◆圖▶ ◆臣▶ ◆臣▶ ○臣

- ► The equations for the fluid variables v(x, t), T(x, t) and the field φ(x, t) can be solved together (numerically)
- However, the width of the wall is much smaller than the length scale of fluid profiles
- The interface can be assumed to be infinitely thin
- On each side of the interface, we have  $\partial_{\mu}T^{\mu\nu} = 0$ , with  $T^{\mu\nu} = w u^{\mu}u^{\nu} - p g^{\mu\nu}$
- Matching conditions at the interface (integrating  $\partial_{\mu}T^{\mu\nu} = 0$ )  $\Delta(wv\gamma^2) = 0$ ,  $\Delta(wv^2\gamma^2 + p) = 0$

イロン 不良と 不良と 一度 …

- ► The equations for the fluid variables v(x, t), T(x, t) and the field φ(x, t) can be solved together (numerically)
- However, the width of the wall is much smaller than the length scale of fluid profiles
- The interface can be assumed to be infinitely thin
- On each side of the interface, we have  $\partial_{\mu}T^{\mu\nu} = 0$ , with  $T^{\mu\nu} = w u^{\mu}u^{\nu} - p g^{\mu\nu}$
- Matching conditions at the interface (integrating  $\partial_{\mu}T^{\mu\nu} = 0$ )  $\Delta(wv\gamma^2) = 0$ ,  $\Delta(wv^2\gamma^2 + p) = 0$
- ► The fluid equations depend on  $c_s^2 = dp/de$ ( $c_s$  = speed of sound; for radiation,  $c_s = \sqrt{1/3}$ )
# Steady state solutions (planar walls)



#### Weak deflagration:

- subsonic:  $v_w < c_s$
- preceded by a shock front

•  $T_u > T_n$ 

#### Jouguet deflagration

[Kurki-Suonio & Laine, 1995]

- supersonic:  $c_s < v_w < v_J$
- shock front and rarefaction wave

#### Weak detonation:

- supersonic:  $v_w > v_J(T_u) > c_s$
- followed by a rarefaction wave

(日)

$$\bullet \ T_u = T_n \ (T_b > T_u)$$

3

The equation for the wall is derived from the field equation

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$

э

・ロト ・ 日 ト ・ ヨ ト ・ ヨ ト …

The equation for the wall is derived from the field equation

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$

To transform into an equation for the bubble wall:

э

◆□ > ◆圖 > ◆臣 > ◆臣 > ○

The equation for the wall is derived from the field equation

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$

To transform into an equation for the bubble wall:

• Assume planar wall:  $\phi = \phi(z, t)$ 

イロン イロン イヨン イヨン 三日

The equation for the wall is derived from the field equation

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$

To transform into an equation for the bubble wall:

- Assume planar wall:  $\phi = \phi(z, t)$
- Assume steady state [In general, reached after a very short acceleration stage]

The equation for the wall is derived from the field equation

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$

To transform into an equation for the bubble wall:

- Assume planar wall:  $\phi = \phi(z, t)$
- Assume steady state [In general, reached after a very short acceleration stage]
- Go to the reference frame of the wall:  $\phi = \phi(z)$ ,  $\partial_{\mu}\partial^{\mu}\phi = \phi''(z)$

イロト イヨト イヨト イヨト ヨー のへの

The equation for the wall is derived from the field equation

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$

To transform into an equation for the bubble wall:

- Assume planar wall:  $\phi = \phi(z, t)$
- Assume steady state [In general, reached after a very short acceleration stage]
- ► Go to the reference frame of the wall:  $\phi = \phi(z)$ ,  $\partial_{\mu}\partial^{\mu}\phi = \phi''(z)$
- Multiply × φ'(z), integrate ∫ dz across the wall ⇒ the first term vanishes

$$\int_{b}^{u} dz \frac{d\phi}{dz} \frac{\partial \mathcal{F}(\phi, T)}{\partial \phi} + \sum_{i} \int_{b}^{u} dz \frac{dm_{i}^{2}}{dz} \int \frac{d^{3}p}{(2\pi)^{3} 2E_{i}} \delta f_{i} = 0$$

3

・ロト ・聞ト ・ヨト ・ヨト





(日) (周) (日) (日)



(日) (周) (日) (日)



•  $F_{\rm fr}$  depends on wall velocity through  $\delta f_i$ 

(日) (同) (三) (三)



- $F_{\rm dr}$  does not depend on the wall velocity
- $F_{\rm fr}$  depends on wall velocity through  $\delta f_i$
- For small velocities we have  $\delta f_i \propto v_w$  and  $F_{\rm fr} = -\eta_{NR} v_w$

・ロト ・聞ト ・ ヨト ・ ヨト



- $F_{\rm fr}$  depends on wall velocity through  $\delta f_i$
- For small velocities we have  $\delta f_i \propto v_w$  and  $F_{\rm fr} = -\eta_{NR} v_w$

Hence, in the non-relativistic limit we have  $p_b(T) - p_u(T) - \eta_{NR}v_w = 0$ 

イロン イヨン イヨン イヨン



• For small velocities we have  $\delta f_i \propto v_w$  and  $F_{\rm fr} = -\eta_{NR} v_w$ 

Hence, in the non-relativistic limit we have  $p_b(T) - p_u(T) - \eta_{NR} v_w = 0 \implies v_w = \Delta p / \eta_{NR}$ 

ヘロト 人間ト 人造ト 人造トー



- $F_{\rm fr}$  depends on wall velocity through  $\delta f_i$
- For small velocities we have  $\delta f_i \propto v_w$  and  $F_{\rm fr} = -\eta_{NR} v_w$

Hence, in the non-relativistic limit we have  $p_b(T) - p_u(T) - \eta_{NR} v_w = 0 \implies v_w = \Delta p / \eta_{NR}$ 

In the general case we have

• A non-linear friction force  $F_{\rm fr}(v_w)$ 

< ロ > < 同 > < 回 > < 回 > < 回 > <



- $F_{\rm dr}$  does not depend on the wall velocity
- $F_{\rm fr}$  depends on wall velocity through  $\delta f_i$
- For small velocities we have  $\delta f_i \propto v_w$  and  $F_{\rm fr} = -\eta_{NR} v_w$

Hence, in the non-relativistic limit we have  $p_b(T) - p_u(T) - \eta_{NR} v_w = 0 \implies v_w = \Delta p / \eta_{NR}$ 

In the general case we have

- A non-linear friction force  $F_{\rm fr}(v_w)$
- An inhomogeneous temperature, so  $F_{dr} = p_b(T_b) - p_u(T_u) + \int_b^u s(\phi, T) dT$

**BAR 4 BA** 

$$F_{\rm fr} = \sum_i \int_b^u dz \frac{dm_i^2}{dz} \int \frac{d^3p}{(2\pi)^3 2E_i} \delta f_i(z,p)$$

(日) (四) (三) (三) (三)

$$F_{\rm fr} = \sum_i \int_b^u dz \frac{dm_i^2}{dz} \int \frac{d^3p}{(2\pi)^3 2E_i} \delta f_i(z,p)$$

Moore & Prokopec, 1995 (SM)

$$F_{\rm fr} = \sum_i \int_b^u dz \frac{dm_i^2}{dz} \int \frac{d^3p}{(2\pi)^3 2E_i} \delta f_i(z,p)$$

Moore & Prokopec, 1995 (SM)

► Boltzmann equations for  $f_i = f_{0i} + \delta f_i$ , small wall velocity  $\Rightarrow$  small  $\delta f_i$ 

・ロト ・ 日 ・ ・ ヨ ト ・ ヨ ト ・

$$F_{\rm fr} = \sum_{i} \int_{b}^{u} dz \frac{dm_i^2}{dz} \int \frac{d^3p}{(2\pi)^3 2E_i} \delta f_i(z,p)$$

Moore & Prokopec, 1995 (SM)

- ► Boltzmann equations for  $f_i = f_{0i} + \delta f_i$ , small wall velocity  $\Rightarrow$  small  $\delta f_i$ 
  - Valid for  $p \gg L_w^{-1}$  ( $L_w$  = wall width)

イロト 不得 トイヨト イヨト

$$F_{\rm fr} = \sum_{i} \int_{b}^{u} dz \frac{dm_i^2}{dz} \int \frac{d^3p}{(2\pi)^3 2E_i} \delta f_i(z,p)$$

Moore & Prokopec, 1995 (SM)

- ► Boltzmann equations for  $f_i = f_{0i} + \delta f_i$ , small wall velocity  $\Rightarrow$  small  $\delta f_i$ 
  - Valid for  $p \gg L_w^{-1}$  ( $L_w$  = wall width)
  - Good approximation for p ~ T (thermal particles)
     Does not take into account infrared boson excitations

<ロ> (四) (四) (三) (三) (三) (三)

$$F_{\rm fr} = \sum_{i} \int_{b}^{u} dz \frac{dm_i^2}{dz} \int \frac{d^3p}{(2\pi)^3 2E_i} \delta f_i(z,p)$$

Moore & Prokopec, 1995 (SM)

- ► Boltzmann equations for  $f_i = f_{0i} + \delta f_i$ , small wall velocity  $\Rightarrow$  small  $\delta f_i$ 
  - Valid for  $p \gg L_w^{-1}$  ( $L_w$  = wall width)
  - Good approximation for p ~ T (thermal particles)
     Does not take into account infrared boson excitations
  - System of integro-differential equations, depends on all the particle interactions, several approximations needed

< ロ > < 回 > < 回 > < 回 > < 回 > <

$$F_{\rm fr} = \sum_{i} \int_{b}^{u} dz \frac{dm_i^2}{dz} \int \frac{d^3p}{(2\pi)^3 2E_i} \delta f_i(z,p)$$

Moore & Prokopec, 1995 (SM)

- ► Boltzmann equations for  $f_i = f_{0i} + \delta f_i$ , small wall velocity  $\Rightarrow$  small  $\delta f_i$ 
  - Valid for  $p \gg L_w^{-1}$  ( $L_w$  = wall width)
  - Good approximation for p ~ T (thermal particles)
     Does not take into account infrared boson excitations
  - System of integro-differential equations, depends on all the particle interactions, several approximations needed
- Results (SM,  $0 < m_H < 90$ GeV):  $v_w \approx 0.4$

イロト 不得下 イヨト イヨト 二日

This is the usual approach. However...

3

< ロ > < 圖 > < 画 > < 画 > <

This is the usual approach. However...

Moore, 2000 (SM)

Considered infrared bosons

▲日 ▶ ▲圖 ▶ ▲ 国 ▶ ▲ 国 ▶ →

#### This is the usual approach. However...

Moore, 2000 (SM)

Considered infrared bosons

Classical treatment, overdamped evolution

・ロト ・ 日 ・ ・ ヨ ト ・ ヨ ト ・

#### This is the usual approach. However...

Moore, 2000 (SM)

Considered infrared bosons

Classical treatment, overdamped evolution

Results for the SM:

•  $v_w \simeq 0.1$  for  $m_H \simeq 45 {
m GeV}$ ,  $v_w \simeq 0.01$  for  $m_H \simeq 80 {
m GeV}$ 

< ロ > < 同 > < 回 > < 回 > < 回 > <

#### This is the usual approach. However...

Moore, 2000 (SM)

Considered infrared bosons

Classical treatment, overdamped evolution

Results for the SM:

•  $v_w \simeq 0.1$  for  $m_H \simeq 45 {
m GeV}$ ,  $v_w \simeq 0.01$  for  $m_H \simeq 80 {
m GeV}$ 

 $v_w$  quite smaller than the Boltzmann result ( $v_w \approx 0.4$ )

イロト 不得 トイヨト イヨト

#### This is the usual approach. However...

Moore, 2000 (SM)

Considered infrared bosons

Classical treatment, overdamped evolution

Results for the SM:

•  $v_w \simeq 0.1$  for  $m_H \simeq 45 {
m GeV}$ ,  $v_w \simeq 0.01$  for  $m_H \simeq 80 {
m GeV}$ 

 $v_w$  quite smaller than the Boltzmann result ( $v_w \approx 0.4$ ) For the SM, this infrared boson contribution gives a larger friction than the thermal particles contribution

イロト 不得 トイヨト イヨト 二日

Parametric dependence (analytic approximations) To lowest order in  $v_w$  we have  $F_{\rm fr} = -\eta_{NR}v_w$ with  $\eta_{NR} = \eta_{\rm th} + \eta_{\rm ir}$ 

イロン イロン イヨン イヨン 三日

Parametric dependence (analytic approximations) To lowest order in  $v_w$  we have  $F_{\rm fr} = -\eta_{NR}v_w$ with  $\eta_{NR} = \eta_{\rm th} + \eta_{\rm ir}$ 

- thermal particles:  $\eta_{
  m th} \sim \sum_i (g_i h_i^4 / \bar{\Gamma}) (\phi_b^2 \sigma)$ 
  - $h_i$  = coupling of particles with Higgs
  - $\bar{\Gamma}$  = effective interaction rate  $\sim 10^{-2} T$
- infrared bosons:  $\overline{\eta_{\mathrm{ir}}} \sim \sum_i (g_i m_D^2 / L_w) \log(m_i L_w)$

[See, e.g., A.M. & A.Sánchez, NPB 825, 151 (2010)]

イロン イロン イヨン イヨン 三日

 Away from the NR limit, the friction has been hardly calculated (more on this in a moment)

3

イロト イヨト イヨト イヨト

- Away from the NR limit, the friction has been hardly calculated (more on this in a moment)
- ► To obtain a description for 0 < v<sub>w</sub> < 1 it is convenient to replace the last term of the field equation</p>

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$

with a simpler dissipative term.

・ロン ・四 と ・ ヨン ・ ヨン … ヨ

- Away from the NR limit, the friction has been hardly calculated (more on this in a moment)
- To obtain a description for 0 < v<sub>w</sub> < 1 it is convenient to replace the last term of the field equation

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int\frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$

with a simpler dissipative term. For instance

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial \mathcal{F}(\phi, T)}{\partial \phi} + \tilde{\eta}(\phi) u^{\mu} \partial_{\mu}\phi = 0$$
  
 $u^{\mu} = (\gamma, \gamma \mathbf{v})$  fluid four-velocity

- Away from the NR limit, the friction has been hardly calculated (more on this in a moment)
- To obtain a description for 0 < v<sub>w</sub> < 1 it is convenient to replace the last term of the field equation

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi, T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int \frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$

with a simpler dissipative term. For instance

$$\partial_{\mu}\partial^{\mu}\phi+rac{\partial\mathcal{F}(\phi,T)}{\partial\phi}+\widetilde{\eta}(\phi)\,u^{\mu}\,\partial_{\mu}\phi=0$$

 $u^{\mu}=(\gamma,\gamma\mathbf{v})$  fluid four-velocity

To convert the field equation into a wall equation, assume φ = φ(z) in the rest frame of the wall, multiply ×∂<sub>z</sub>φ, integrate ∫ dz. We obtain

$$\int_{b}^{u} \frac{\partial \mathcal{F}}{\partial \phi} \frac{d\phi}{dz} dz + \int_{b}^{u} \tilde{\eta} \gamma v \left[\frac{d\phi}{dz}\right]^{2} dz = 0$$

イロン 不聞 とうき とうせい ほ
A phenomenological approach to the friction

- Away from the NR limit, the friction has been hardly calculated (more on this in a moment)
- To obtain a description for 0 < v<sub>w</sub> < 1 it is convenient to replace the last term of the field equation

$$\partial_{\mu}\partial^{\mu}\phi + \frac{\partial\mathcal{F}(\phi, T)}{\partial\phi} + \sum_{i}\frac{dm_{i}^{2}}{d\phi}\int \frac{d^{3}p}{(2\pi)^{3}2E_{i}}\delta f_{i} = 0$$

with a simpler dissipative term. For instance

$$\partial_{\mu}\partial^{\mu}\phi + rac{\partial\mathcal{F}(\phi,T)}{\partial\phi} + \tilde{\eta}(\phi) u^{\mu} \partial_{\mu}\phi = 0$$

 $u^{\mu} = (\gamma, \gamma \mathbf{v})$  fluid four-velocity

To convert the field equation into a wall equation, assume φ = φ(z) in the rest frame of the wall, multiply ×∂<sub>z</sub>φ, integrate ∫ dz. We obtain

$$\int_{b}^{u} \frac{\partial \mathcal{F}}{\partial \phi} \frac{d\phi}{dz} dz + \int_{b}^{u} \tilde{\eta} \gamma v \left[\frac{d\phi}{dz}\right]^{2} dz = 0$$
  
Here,  $\gamma v$  comes from  $u^{z}$   $(v \equiv v_{z} \sim -v_{w})_{z}$ 

A. Mégevand, Bubble wall velocity

• Thus, we have a friction force of the form  $F_{
m fr} \sim \gamma v$ 

◆□▶ ◆□▶ ◆臣▶ ◆臣▶ □臣 = のへ⊙

▶ Thus, we have a friction force of the form  $F_{\rm fr} \sim \gamma v$ 

▶ In the NR limit we have  $F_{\rm fr} = -\eta v_{\rm w}$  ( $\eta =$  free parameter)

◆□▶ ◆□▶ ◆三▶ ◆三▶ ○三 のへ⊙

- ▶ Thus, we have a friction force of the form  $F_{\rm fr} \sim \gamma v$ 
  - In the NR limit we have  $F_{\rm fr} = -\eta v_w$  ( $\eta =$  free parameter)
  - Setting  $\eta = \eta_{NR}$  (from microphysics calculations),  $F_{\rm fr}$  matches the correct NR limit

(日) (四) (三) (三) (三)

- ► Thus, we have a friction force of the form  $F_{\rm fr} \sim \gamma v$ 
  - ▶ In the NR limit we have  $F_{\rm fr} = -\eta v_w$  ( $\eta =$  free parameter)
  - Setting η = η<sub>NR</sub> (from microphysics calculations), F<sub>fr</sub> matches the correct NR limit
- With suitable approximations for the profiles inside the wall, e.g.,  $\langle \gamma v \rangle = (\gamma_b v_b + \gamma_u v_u)/2$ ,

・ロト ・ 日 ・ ・ 日 ・ ・ 日 ・ ・ 日

- ► Thus, we have a friction force of the form  $F_{\rm fr} \sim \gamma v$ 
  - ▶ In the NR limit we have  $F_{\rm fr} = -\eta v_w$  ( $\eta =$  free parameter)
  - Setting η = η<sub>NR</sub> (from microphysics calculations), F<sub>fr</sub> matches the correct NR limit
- With suitable approximations for the profiles inside the wall, e.g.,  $\langle \gamma v \rangle = (\gamma_b v_b + \gamma_u v_u)/2$ ,
- ▶ and using the bag EOS,  $p_{u,b} = a_{u,b}T^4/3 \epsilon_{u,b}$ , we have

・ロト ・ 日 ・ ・ 日 ・ ・ 日 ・ ・ 日

- Thus, we have a friction force of the form  $F_{
  m fr} \sim \gamma v$ 
  - ▶ In the NR limit we have  $F_{\rm fr} = -\eta v_w$  ( $\eta =$  free parameter)
  - Setting η = η<sub>NR</sub> (from microphysics calculations), F<sub>fr</sub> matches the correct NR limit
- With suitable approximations for the profiles inside the wall, e.g.,  $\langle \gamma v \rangle = (\gamma_b v_b + \gamma_u v_u)/2$ ,
- ▶ and using the bag EOS,  $p_{u,b} = a_{u,b}T^4/3 \epsilon_{u,b}$ , we have

$$\frac{L}{4}\left(1-\frac{T_u^2 T_b^2}{T_c^4}\right) = \eta \frac{\gamma_b v_b + \gamma_u v_u}{2}$$

- ► Thus, we have a friction force of the form  $F_{\rm fr} \sim \gamma v$ 
  - ▶ In the NR limit we have  $F_{\rm fr} = -\eta v_w$  ( $\eta =$  free parameter)
  - Setting η = η<sub>NR</sub> (from microphysics calculations), F<sub>fr</sub> matches the correct NR limit
- With suitable approximations for the profiles inside the wall, e.g.,  $\langle \gamma v \rangle = (\gamma_b v_b + \gamma_u v_u)/2$ ,
- ▶ and using the bag EOS,  $p_{u,b} = a_{u,b}T^4/3 \epsilon_{u,b}$ , we have

$$\frac{L}{4}\left(1-\frac{T_u^2 T_b^2}{T_c^4}\right) = \eta \frac{\gamma_b v_b + \gamma_u v_u}{2}$$

- With these approximations, v<sub>w</sub> depends only on:
  - the friction coefficient η,
  - the latent heat L,
  - the amount of supercooling  $T_n/T_c$

# Wall velocity as a function of the friction Solutions



Agree with numerical computations Kurki-Suonio & Laine, 1995-1996, *static case* 

- 小田 ト - 日 ト - 日 ト

Wall velocity as a function of the friction **Stable** solutions (A.M., A. Membiela, 2014)



Also in agreement with Kurki-Suonio & Laine, 1995-1996, *dynamic calculation* 

Wall velocity as a function of the friction Realized in the phase transition



(according to the dynamic calculation of Kurki-Suonio & Laine, 1995-1996)

(人間) トイヨト イヨト

# Application to physical models (electroweak PT)



< 回 > < 回 > < 回 >

# Application to physical models (electroweak PT)



< ∃⇒

So far I have considered a friction of the form  ${\it F_{\rm fr}}\sim v\gamma$ 

イロン イロン イヨン イヨン 三日

So far I have considered a friction of the form  $F_{\rm fr} \sim v \gamma$  However...

◆□▶ ◆圖▶ ◆臣▶ ◆臣▶ ○臣

So far I have considered a friction of the form  ${\it F}_{\rm fr} \sim v \gamma$  However...

Bödeker & Moore, 2009: the UR regime

Assume the wall has reached an ultra-relativistic velocity, with  $\gamma = 1/\sqrt{1-\nu^2} \gg 1$ 

イロト 不得下 イヨト イヨト 二日

So far I have considered a friction of the form  ${\it F}_{\rm fr} \sim {\it v}\gamma$  However...

Bödeker & Moore, 2009: the UR regime

Assume the wall has reached an ultra-relativistic velocity, with  $\gamma=1/\sqrt{1-\textit{v}^2}\gg 1$ 

Allows several assumptions which simplify the problem

イロン イロン イヨン イヨン 三日

So far I have considered a friction of the form  ${\it F}_{\rm fr} \sim {\it v}\gamma$  However...

Bödeker & Moore, 2009: the UR regime

Assume the wall has reached an ultra-relativistic velocity, with  $\gamma = 1/\sqrt{1-\nu^2} \gg 1$ 

- Allows several assumptions which simplify the problem
- The calculation is simpler than the NR case:

 $\begin{aligned} F_{\text{net}} &= \\ V(\phi_u) - V(\phi_b) - \sum_i [m_i^2(\phi_b) - m_i^2(\phi_u)] \int \frac{d^3 p}{(2\pi)^3 2 E_{iu}} f_{iu}^{\text{eq}}(p, T_n) \end{aligned}$ 

イロン イロン イヨン イヨン 三日

So far I have considered a friction of the form  $F_{\rm fr} \sim v \gamma$  However...

Bödeker & Moore, 2009: the UR regime

Assume the wall has reached an ultra-relativistic velocity, with  $\gamma=1/\sqrt{1-\textit{v}^2}\gg 1$ 

- Allows several assumptions which simplify the problem
- The calculation is simpler than the NR case:

$$\begin{aligned} F_{\rm net} &= \\ V(\phi_u) - V(\phi_b) - \sum_i [m_i^2(\phi_b) - m_i^2(\phi_u)] \int \frac{d^3 p}{(2\pi)^3 2 E_{iu}} f_{iu}^{\rm eq}(p, T_n) \end{aligned}$$

• The total force  $F_{net}(T_n)$  does not depend on the wall velocity

So far I have considered a friction of the form  $F_{\rm fr} \sim v \gamma$  However...

Bödeker & Moore, 2009: the UR regime

Assume the wall has reached an ultra-relativistic velocity, with  $\gamma = 1/\sqrt{1-\nu^2} \gg 1$ 

- Allows several assumptions which simplify the problem
- The calculation is simpler than the NR case:

$$\begin{aligned} F_{\text{net}} &= \\ V(\phi_u) - V(\phi_b) - \sum_i [m_i^2(\phi_b) - m_i^2(\phi_u)] \int \frac{d^3 p}{(2\pi)^3 2 E_{iu}} f_{iu}^{\text{eq}}(p, T_n) \end{aligned}$$

- The total force  $F_{net}(T_n)$  does not depend on the wall velocity
- $\blacktriangleright$  It means that in the limit  $\nu\gamma \rightarrow \infty$  the friction saturates

イロト 不得下 イヨト イヨト 二日

So far I have considered a friction of the form  $F_{\rm fr} \sim v \gamma$  However...

#### Bödeker & Moore, 2009: the UR regime

Assume the wall has reached an ultra-relativistic velocity, with  $\gamma=1/\sqrt{1-\textit{v}^2}\gg 1$ 

- Allows several assumptions which simplify the problem
- The calculation is simpler than the NR case:

$$F_{\text{net}} = V(\phi_u) - V(\phi_b) - \sum_i [m_i^2(\phi_b) - m_i^2(\phi_u)] \int \frac{d^3p}{(2\pi)^3 2E_{iu}} f_{iu}^{\text{eq}}(p, T_n)$$

- The total force  $F_{net}(T_n)$  does not depend on the wall velocity
- $\blacktriangleright$  It means that in the limit  $\nu\gamma \rightarrow \infty$  the friction saturates
- ► No stationary state: if F<sub>net</sub>(T<sub>n</sub>) > 0 we have an accelerated wall (runaway)

イロン イロン イヨン イヨン 三日

▶ Even if we obtain  $F_{\rm net} > 0$ , the wall has to reach  $\gamma \gg 1$  for the treatment to be valid

◆□▶ ◆□▶ ◆臣▶ ◆臣▶ 三臣 - のへ⊙

- ▶ Even if we obtain  $F_{\rm net} > 0$ , the wall has to reach  $\gamma \gg 1$  for the treatment to be valid
- Intermediate cases (between NR and UR) were hardly investigated

- ▶ Even if we obtain  $F_{\rm net} > 0$ , the wall has to reach  $\gamma \gg 1$  for the treatment to be valid
- Intermediate cases (between NR and UR) were hardly investigated

Konstandin, Nardini, Rues, 2014

Extended the treatment of Moore and Prokopec (1995) out of the NR regime, still considering small deviations  $\delta f_i$ 

< ロ > < 圖 > < 画 > < 画 > <

- ▶ Even if we obtain  $F_{\rm net} > 0$ , the wall has to reach  $\gamma \gg 1$  for the treatment to be valid
- Intermediate cases (between NR and UR) were hardly investigated

Konstandin, Nardini, Rues, 2014

Extended the treatment of Moore and Prokopec (1995) out of the NR regime, still considering small deviations  $\delta f_i$ 

The result does not match the UR regime

< ロ > < 圖 > < 画 > < 画 > <

- ▶ Even if we obtain  $F_{\rm net} > 0$ , the wall has to reach  $\gamma \gg 1$  for the treatment to be valid
- Intermediate cases (between NR and UR) were hardly investigated

Konstandin, Nardini, Rues, 2014

Extended the treatment of Moore and Prokopec (1995) out of the NR regime, still considering small deviations  $\delta f_i$ 

The result does not match the UR regime

Alternative: Consider a phenomenological model

- ▶ Even if we obtain  $F_{\rm net} > 0$ , the wall has to reach  $\gamma \gg 1$  for the treatment to be valid
- Intermediate cases (between NR and UR) were hardly investigated

Konstandin, Nardini, Rues, 2014

Extended the treatment of Moore and Prokopec (1995) out of the NR regime, still considering small deviations  $\delta f_i$ 

The result does not match the UR regime

Alternative: Consider a phenomenological model

The term η̃(φ) u<sup>μ</sup>∂<sub>μ</sub>φ is too simplistic, since F<sub>fr</sub> ∼ vγ does not saturate in the UR limit

イロン 不聞 とうき とうせい ほ

Espinosa, Konstandin, No, Servant, 2010

Considered the modification

$$ilde \eta(\phi)\,u^\mu\partial_\mu\phi o { ilde \eta(\phi)\,u^\mu\partial_\mu\phi\over \sqrt{1+(u^\mu\lambda_\mu)^2}}$$

Espinosa, Konstandin, No, Servant, 2010

Considered the modification

$$ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi o rac{ ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi}{\sqrt{1+(u^\mu \lambda_\mu)^2}}$$

with  $\lambda_{\mu} = (0, 0, 0, 1)$  in the wall frame

イロト イロト イヨト イヨト 二日

Espinosa, Konstandin, No, Servant, 2010

Considered the modification

$$ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi o rac{ ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi}{\sqrt{1+(u^\mu \lambda_\mu)^2}}$$

with  $\lambda_{\mu}=(0,0,0,1)$  in the wall frame

► With this  $\lambda_{\mu}$  we have, in the wall frame,  $\frac{\gamma v}{\sqrt{1+(\gamma v)^2}} = v!!!$ 

◆□▶ ◆□▶ ◆臣▶ ◆臣▶ 三臣 - のへの

Espinosa, Konstandin, No, Servant, 2010

Considered the modification

$$ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi o rac{ ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi}{\sqrt{1+(u^\mu \lambda_\mu)^2}}$$

with  $\lambda_{\mu} = (0, 0, 0, 1)$  in the wall frame

- ▶ With this  $\lambda_{\mu}$  we have, in the wall frame,  $\frac{\gamma v}{\sqrt{1+(\gamma v)^2}} = v!!!$
- This changes the behavior from  $F_{\rm fr}^{\rm old} \sim \eta \, \mathbf{v} \gamma$  to  $F_{\rm fr}^{\rm new} \sim \eta \, \mathbf{v}$  $\Rightarrow$  the friction saturates

イロト イヨト イヨト イヨト ヨー のへの

Espinosa, Konstandin, No, Servant, 2010

Considered the modification

$$ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi o rac{ ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi}{\sqrt{1+(u^\mu \lambda_\mu)^2}}$$

with  $\lambda_{\mu} = (0, 0, 0, 1)$  in the wall frame

- ▶ With this  $\lambda_{\mu}$  we have, in the wall frame,  $\frac{\gamma v}{\sqrt{1+(\gamma v)^2}} = v!!!$
- ► This changes the behavior from  $F_{\rm fr}^{\rm old} \sim \eta \, v \gamma$  to  $F_{\rm fr}^{\rm new} \sim \eta \, v$ ⇒ the friction saturates
- However, a single free parameter  $\eta$  cannot match quantitatively the two limits: we have  $F_{\rm fr}|_{NR} = -\eta v_w$  and  $F_{\rm fr}|_{UR} = -\eta$

イロト イヨト イヨト イヨト ヨー のへの

Espinosa, Konstandin, No, Servant, 2010

Considered the modification

$$ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi o rac{ ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi}{\sqrt{1+(u^\mu \lambda_\mu)^2}}$$

with  $\lambda_{\mu} = (0, 0, 0, 1)$  in the wall frame

- ▶ With this  $\lambda_{\mu}$  we have, in the wall frame,  $\frac{\gamma v}{\sqrt{1+(\gamma v)^2}} = v!!!$
- ► This changes the behavior from  $F_{\rm fr}^{\rm old} \sim \eta \, v \gamma$  to  $F_{\rm fr}^{\rm new} \sim \eta \, v$ ⇒ the friction saturates
- However, a single free parameter  $\eta$  cannot match quantitatively the two limits: we have  $F_{\rm fr}|_{NR} = -\eta v_w$  and  $F_{\rm fr}|_{UR} = -\eta$
- We need a model with two free parameters

イロン 不良と 不良と 一度 …

Espinosa, Konstandin, No, Servant, 2010

Considered the modification

$$ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi o rac{ ilde{\eta}(\phi) \, u^\mu \partial_\mu \phi}{\sqrt{1 + (u^\mu \lambda_\mu)^2}}$$

with  $\lambda_{\mu} = (0, 0, 0, 1)$  in the wall frame

- ▶ With this  $\lambda_{\mu}$  we have, in the wall frame,  $\frac{\gamma v}{\sqrt{1+(\gamma v)^2}} = v!!!$
- ► This changes the behavior from  $F_{\rm fr}^{\rm old} \sim \eta \, v \gamma$  to  $F_{\rm fr}^{\rm new} \sim \eta \, v$ ⇒ the friction saturates
- However, a single free parameter  $\eta$  cannot match quantitatively the two limits: we have  $F_{\text{frr}}|_{NR} = -\eta v_{w}$  and  $F_{\text{frr}}|_{UR} = -\eta$
- We need a model with two free parameters

Notice that the vector  $\partial_{\mu}\phi$  is  $(0, 0, 0, \partial_{z}\phi)$  in the wall frame

A friction which interpolates between the NR and UR limits

Consider instead the term [A.M., 2013]

$$rac{ ilde\eta\,\partial_\mu\phi\,u^\mu}{\sqrt{1+( ilde\lambda\,\partial_\mu\phi\,u^\mu)^2}}$$

イロン イロン イヨン イヨン 三日

A friction which interpolates between the NR and UR limits

Consider instead the term [A.M., 2013]

$$rac{ ilde\eta\,\partial_\mu\phi\,u^\mu}{\sqrt{1+( ilde\lambda\,\partial_\mu\phi\,u^\mu)^2}}$$

In the wall frame and after the usual manipulations, we have a friction force of the form

$$F_{
m fr} \sim rac{\eta \ \gamma m{v}}{\sqrt{1+\lambda^2 \ (\gamma m{v})^2}}$$

・ロン ・ 日 ・ ・ 日 ・ ・ 日 ・ ・
Consider instead the term [A.M., 2013]

$$rac{ ilde\eta\,\partial_\mu\phi\,u^\mu}{\sqrt{1+( ilde\lambda\,\partial_\mu\phi\,u^\mu)^2}}$$

In the wall frame and after the usual manipulations, we have a friction force of the form

$$F_{
m fr} \sim rac{\eta \ \gamma m{v}}{\sqrt{1+\lambda^2 \ (\gamma m{v})^2}}$$

• gives  $F_{
m fr} \sim \eta v$  for small v, and  $F_{
m fr} \sim \eta / \lambda$  for v 
ightarrow 1

イロト イロト イヨト イヨト 二日

Consider instead the term [A.M., 2013]

$$rac{ ilde\eta\,\partial_\mu\phi\,u^\mu}{\sqrt{1+( ilde\lambda\,\partial_\mu\phi\,u^\mu)^2}}$$

In the wall frame and after the usual manipulations, we have a friction force of the form

$$F_{
m fr} \sim rac{\eta \ \gamma v}{\sqrt{1+\lambda^2 \ (\gamma v)^2}}$$

- gives  $F_{
  m fr} \sim \eta v$  for small v, and  $F_{
  m fr} \sim \eta / \lambda$  for v 
  ightarrow 1
- We may choose  $\eta = \eta_{NR}$

イロン イロン イヨン イヨン 三日

Consider instead the term [A.M., 2013]

$$rac{ ilde\eta\,\partial_\mu\phi\,u^\mu}{\sqrt{1+( ilde\lambda\,\partial_\mu\phi\,u^\mu)^2}}$$

In the wall frame and after the usual manipulations, we have a friction force of the form

$$F_{
m fr} \sim rac{\eta \ \gamma m{v}}{\sqrt{1+\lambda^2 \ (\gamma m{v})^2}}$$

- gives  $F_{
  m fr} \sim \eta v$  for small v, and  $F_{
  m fr} \sim \eta / \lambda$  for v 
  ightarrow 1
- We may choose  $\eta = \eta_{NR}$  and  $\eta/\lambda = F_{\rm fr}|_{UR}$

イロン イロン イヨン イヨン 三日

Consider instead the term [A.M., 2013]

$$rac{ ilde\eta\,\partial_\mu\phi\,u^\mu}{\sqrt{1+( ilde\lambda\,\partial_\mu\phi\,u^\mu)^2}}$$

In the wall frame and after the usual manipulations, we have a friction force of the form

$$F_{
m fr} \sim rac{\eta \ \gamma m{v}}{\sqrt{1+\lambda^2 \ (\gamma m{v})^2}}$$

- gives  $F_{
  m fr} \sim \eta v$  for small v, and  $F_{
  m fr} \sim \eta / \lambda$  for v 
  ightarrow 1
- We may choose  $\eta = \eta_{NR}$  and  $\eta/\lambda = F_{\rm fr}|_{UR}$

#### UR friction force

• In the UR limit we have a net force  $F_{net}(T_n)$ 

<ロト < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < 回 > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > <

Consider instead the term [A.M., 2013]

$$rac{ ilde\eta\,\partial_\mu\phi\,u^\mu}{\sqrt{1+( ilde\lambda\,\partial_\mu\phi\,u^\mu)^2}}$$

In the wall frame and after the usual manipulations, we have a friction force of the form

$${m F_{
m fr}} \sim rac{\eta \ \gamma m v}{\sqrt{1+\lambda^2} \ (\gamma m v)^2}$$

- gives  $F_{
  m fr} \sim \eta v$  for small v, and  $F_{
  m fr} \sim \eta / \lambda$  for v 
  ightarrow 1
- We may choose  $\eta = \eta_{NR}$  and  $\eta/\lambda = F_{\rm fr}|_{UR}$

#### UR friction force

- In the UR limit we have a net force  $F_{net}(T_n)$
- The friction part must be identified [A.M., 2013]

Consider instead the term [A.M., 2013]

$$rac{ ilde\eta\,\partial_\mu\phi\,u^\mu}{\sqrt{1+( ilde\lambda\,\partial_\mu\phi\,u^\mu)^2}}$$

In the wall frame and after the usual manipulations, we have a friction force of the form

$$F_{
m fr} \sim rac{\eta \ \gamma m{v}}{\sqrt{1+\lambda^2 \ (\gamma m{v})^2}}$$

- gives  $F_{
  m fr} \sim \eta v$  for small v, and  $F_{
  m fr} \sim \eta/\lambda$  for v 
  ightarrow 1
- We may choose  $\eta = \eta_{NR}$  and  $\eta/\lambda = F_{\rm fr}|_{UR}$

#### UR friction force

- In the UR limit we have a net force  $F_{net}(T_n)$
- The friction part must be identified [A.M., 2013]
- To lowest order in  $m(\phi)/T$ , we have

 $F_{\mathrm{fr}} = \sum_{\mathrm{bos}} (g_i T/12\pi) \left[ m_i^3(\phi_b) - m_i^3(\phi_u) \right] \sim \sum g_i h_i^3 \phi_b^3 T$ 



# Old phenomenological model: $\lambda = 0$

- The second sec





э

A (10) × (10) × (10) ×



▶ For a finite value of  $\eta$  we have  $v_w \rightarrow 1$  (runaway)

< 回 > < 回 > < 回 >



• For a finite value of  $\eta$  we have  $v_w \rightarrow 1$  (runaway)

• This happens for  $F_{dr}(T_u, T_b) = \eta/\lambda$  (i.e., for  $v_w = 1$ )

- 4 同 6 4 日 6 4 日 6



• For a finite value of  $\eta$  we have  $v_w \rightarrow 1$  (runaway)

► This happens for  $F_{dr}(T_u, T_b) = \eta/\lambda$  (i.e., for  $v_w = 1$ ) with  $F_{dr} \simeq p_b(T_b) - p_u(T_u) - \langle s \rangle (T_b - T_u)$ 

ヘロト 人間ト 人造ト 人造トー



- For a finite value of  $\eta$  we have  $v_w \rightarrow 1$  (runaway)
- ► This happens for  $F_{dr}(T_u, T_b) = \eta/\lambda$  (i.e., for  $v_w = 1$ ) with  $F_{dr} \simeq p_b(T_b) - p_u(T_u) - \langle s \rangle (T_b - T_u)$
- The runaway wall solution is possible if  $F_{dr}(T_n, T_n) = \eta/\lambda$

・ロト ・個ト ・ヨト ・ヨト



• For a finite value of  $\eta$  we have  $v_w \rightarrow 1$  (runaway)

- ► This happens for  $F_{dr}(T_u, T_b) = \eta/\lambda$  (i.e., for  $v_w = 1$ ) with  $F_{dr} \simeq p_b(T_b) - p_u(T_u) - \langle s \rangle (T_b - T_u)$
- The runaway wall solution is possible if  $F_{dr}(T_n, T_n) = \eta/\lambda$ i.e.,  $F_{dr} = p_b(T_n) - p_u(T_n)$

・ロト ・個ト ・ヨト ・ヨト



- For a finite value of  $\eta$  we have  $v_w \rightarrow 1$  (runaway)
- ► This happens for  $F_{dr}(T_u, T_b) = \eta/\lambda$  (i.e., for  $v_w = 1$ ) with  $F_{dr} \simeq p_b(T_b) - p_u(T_u) - \langle s \rangle (T_b - T_u)$
- The runaway wall solution is possible if  $F_{dr}(T_n, T_n) = \eta/\lambda$ i.e.,  $F_{dr} = p_b(T_n) - p_u(T_n)$
- As a consequence, stationary and runaway solutions coexist



< 🗇 🕨



< 🗇 🕨



э

・ 同 ト ・ ヨ ト ・ ヨ ト



#### Outlook

Apply to GW generation in the electroweak phase transition

< 回 > < 回 > < 回 > < 回 > < 回 > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ >



#### Outlook

Apply to GW generation in the electroweak phase transition Extra slides Weak deflagrations are unstable for  $v_w < v_{crit}$  (good for GWs)

- 小田 ト - 日 ト - 日 ト