

# Modelling AC ripples in HTS coated conductors by integral equations

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# This presentation consists of two parts

1. Calculation of AC current ripples by means of 2-D  $H$ -formulation

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## Modelling ac ripple currents in HTS coated conductors

Zhihan Xu and Francesco Grilli

2. Calculation of AC current ripples by means of 1-D integral equations
  - Superconductor modeled as 1-D line
  - 100-200 DOFs → Very fast computation
  - Comparison with  $H$ -formulation
  - Influence of  $n$ -value
  - Influence of  $J_c(B)$  dependence

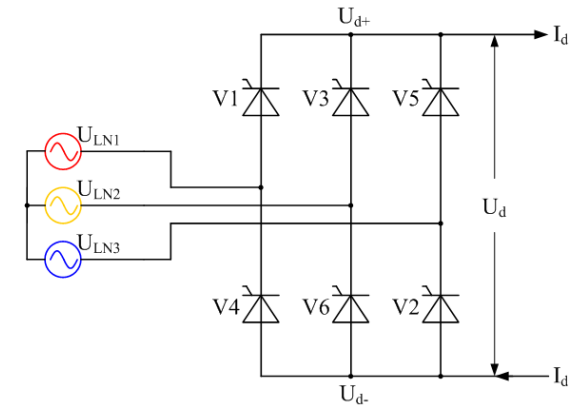
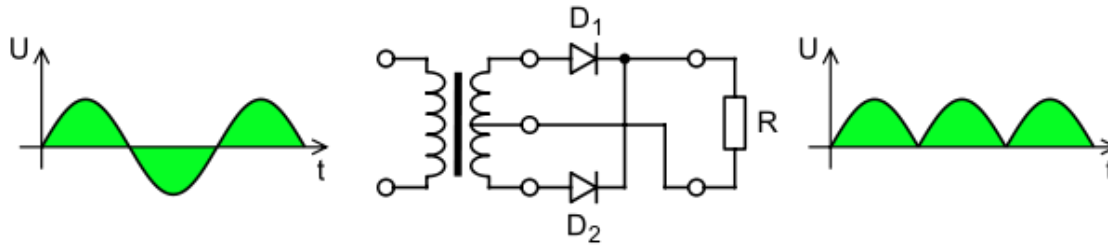
# HTS coated conductors for DC transmission

- Large green energy sources typically located far away from major consumption centres, up to several thousand km →
- Effective long-distance power transmission of GW level required →
- One potential solution: “lossless” HTS DC cables

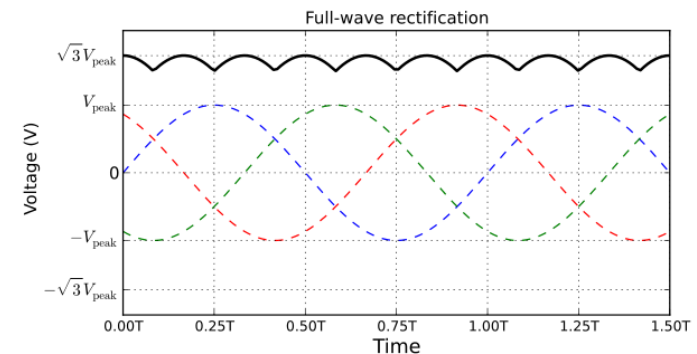
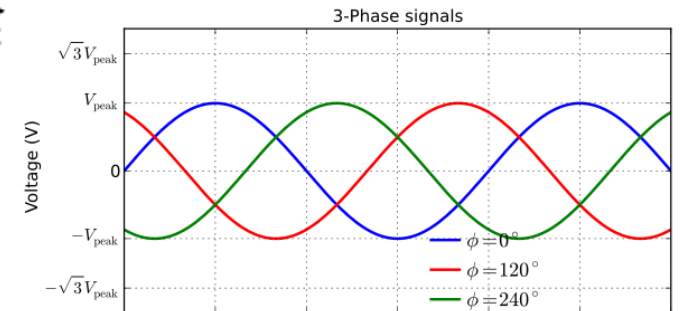
\* This is not a new idea, but rather one that has achieved a practical possibility only lately, owing to recent advances in superconducting materials, cryogenics and AC-DC conversion techniques.

# AC ripples in DC transmission cables

- Rectifiers: AC → DC + pulses/ripples
  - Single-phase, full-wave rectification
  - Three-phase, full-wave rectification



- **AC ripples → AC losses!**
- HTS DC cables are not completely lossless!



# Modelling AC ripples

## The problem

- Consider a 4-mm-wide YBCO tape subject to DC + AC ripples
- A typical applied current:  $I_{DC} = 0.8 * I_c$  plus  $I_{AC} = 10\% * I_{DC} * \sin(\omega t)$
- To estimate the losses caused by the ripples
- To understand the mechanisms behind

# Modelling AC ripples

## The method

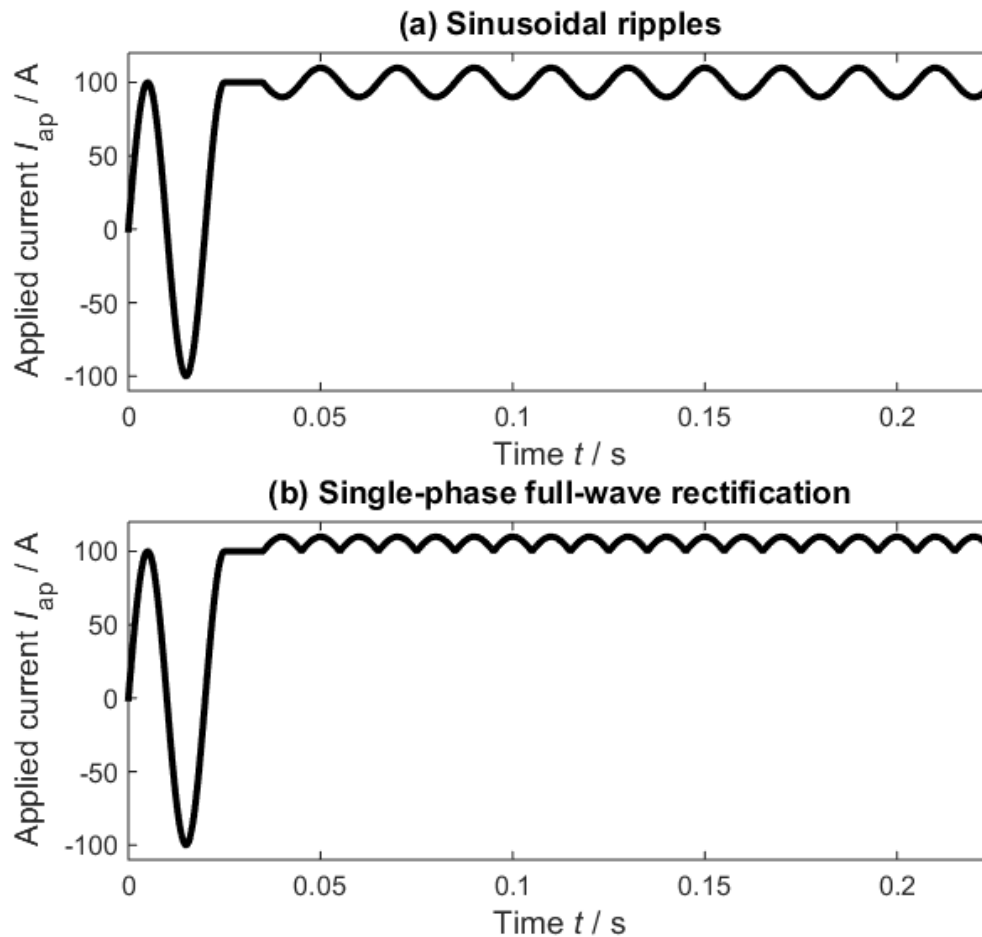
- 2-D finite-element analysis in COMSOL Multiphysics
- Maxwell's equations → H formulation
- E-J relation
  - The power law:  $n = 25$

$$E = E_c \left| \frac{J}{J_c} \right|^n$$

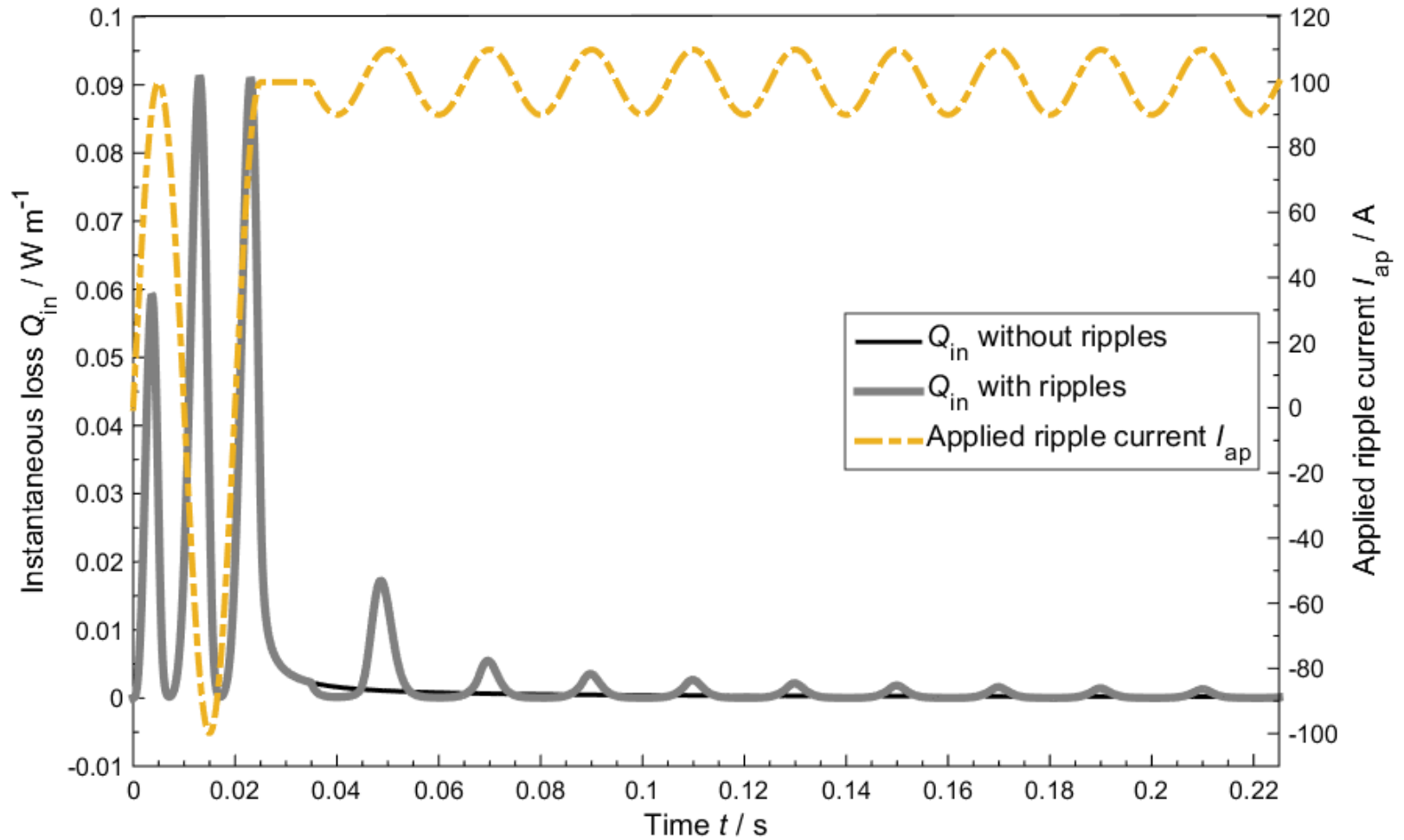
- $J_c$ -B relation
  - The constant- $J_c$  model:  $J_c = 3.125^{10} \text{ A m}^{-2} \rightarrow I_c = \mathbf{125 \text{ A}}$
  - The elliptical model:  $J_{c0} = 4 \cdot 10^{10} \text{ A m}^{-2}$ ,  $B_0 = 0.02 \text{ T}$ ,  $k=0.3$ ,  $b=0.6 \rightarrow I_c = \mathbf{125 \text{ A}}$

$$J_c = \frac{J_{c0}}{\left( 1 + \frac{\sqrt{k^2 B_{par}^2 + B_{perp}^2}}{B_0} \right)^b}$$

# Application of AC ripples (10%, 50 Hz)

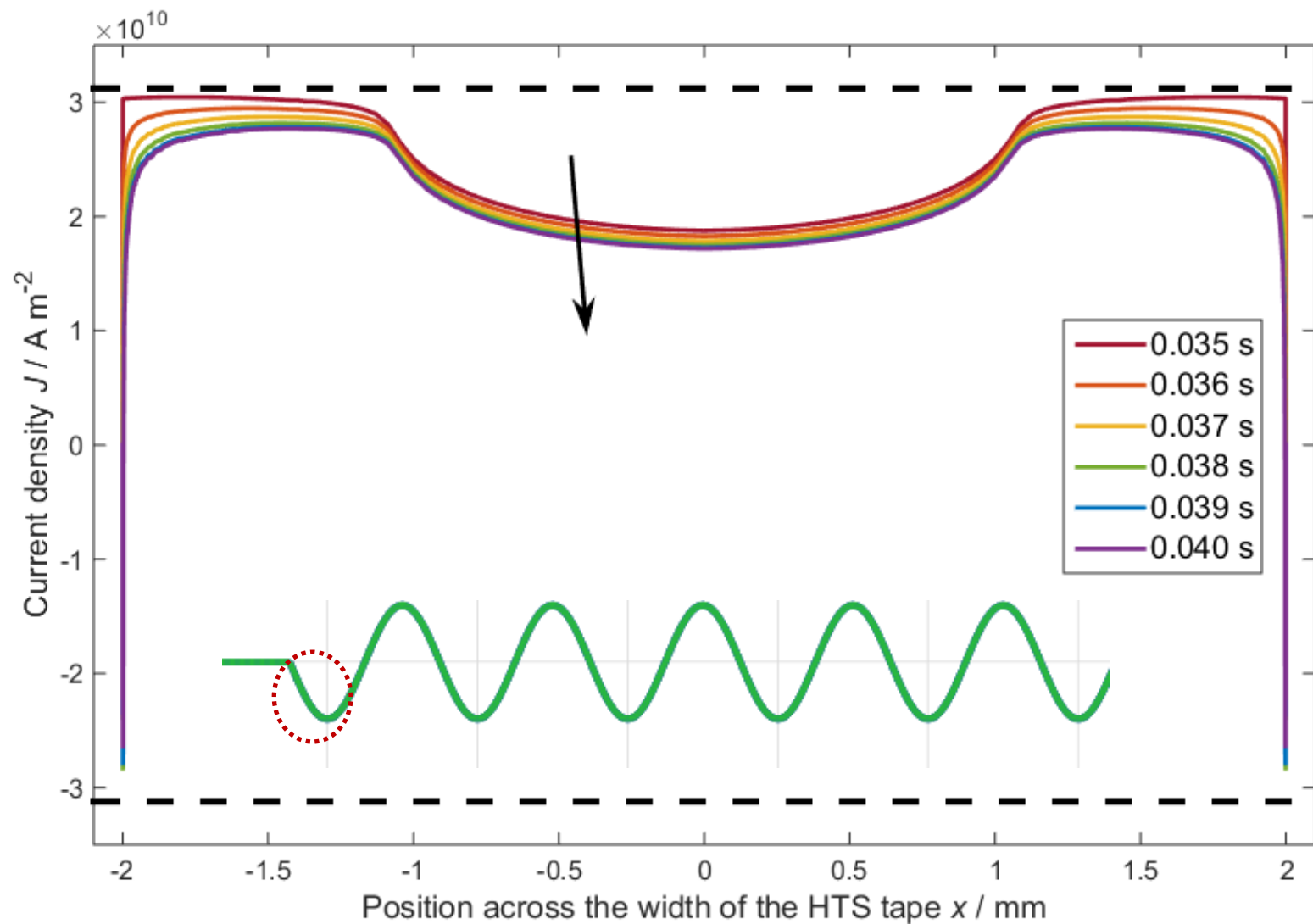


# Instantaneous dissipation

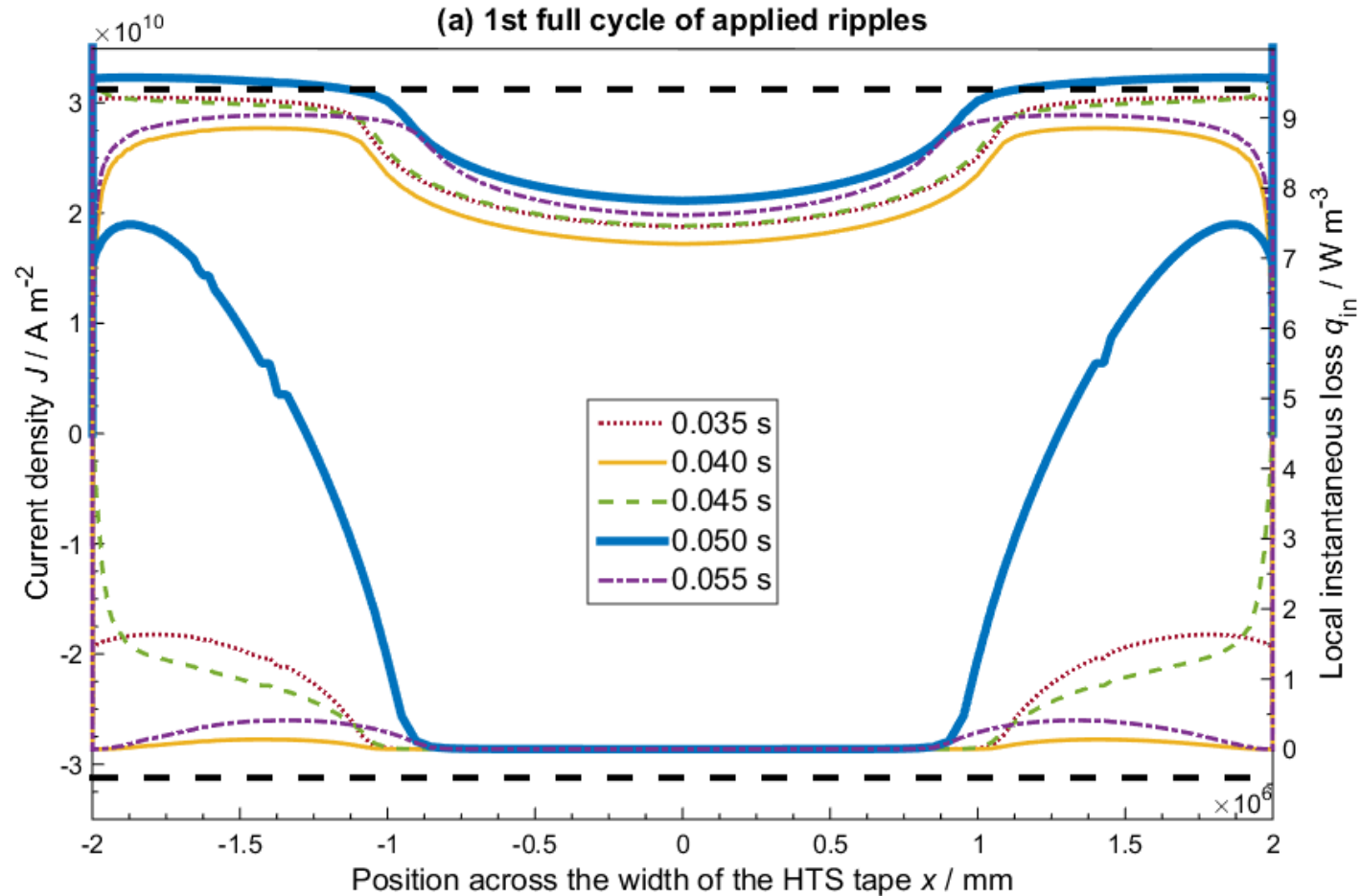
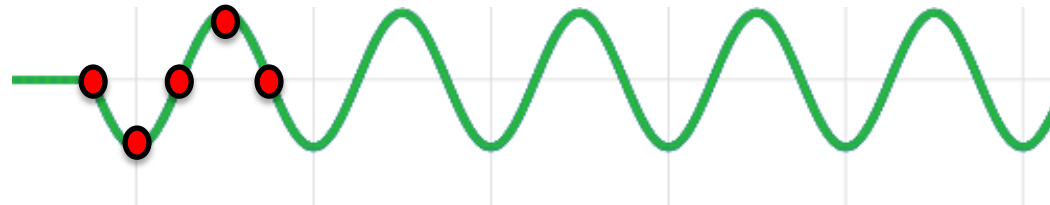




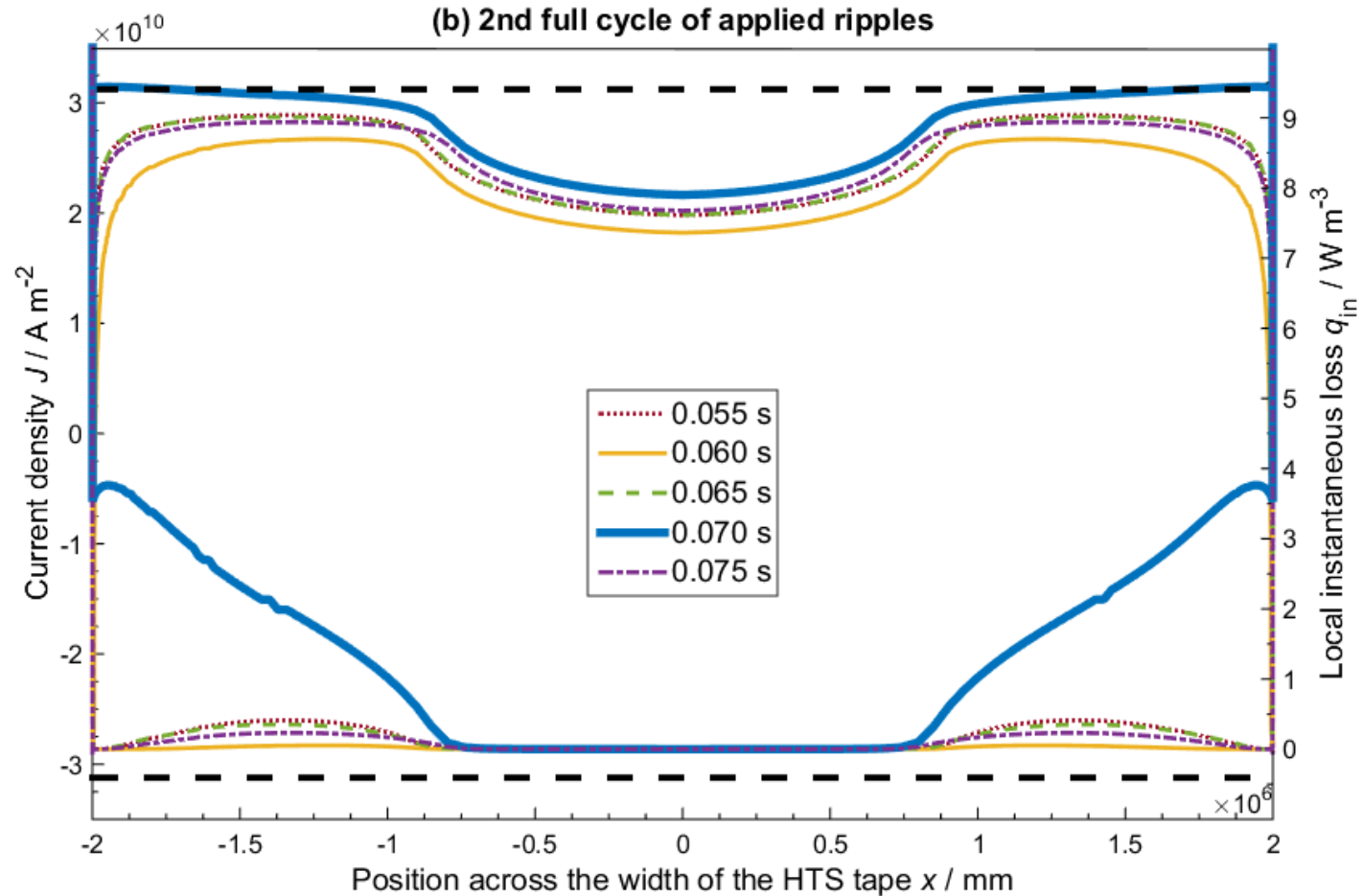
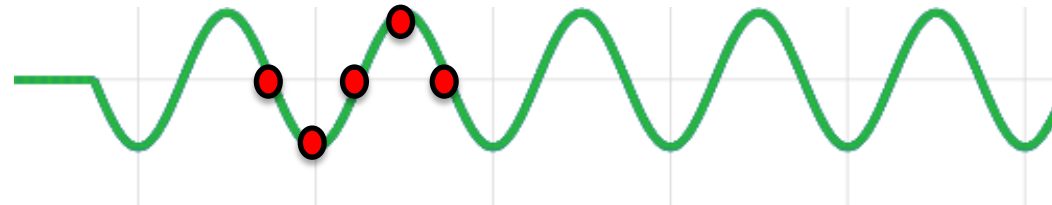
# Critical state ( $-J_c$ ) not reached at the valleys



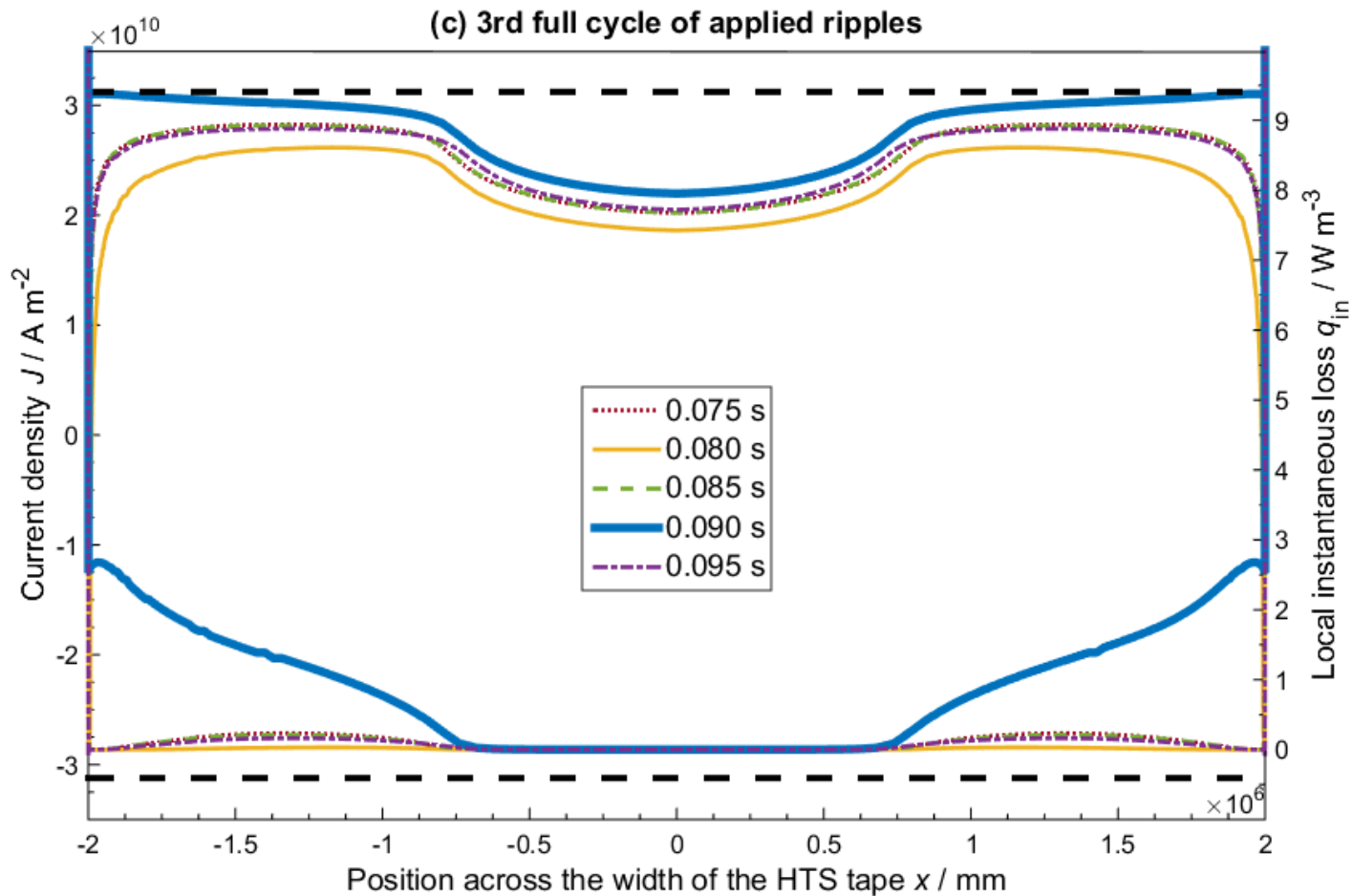
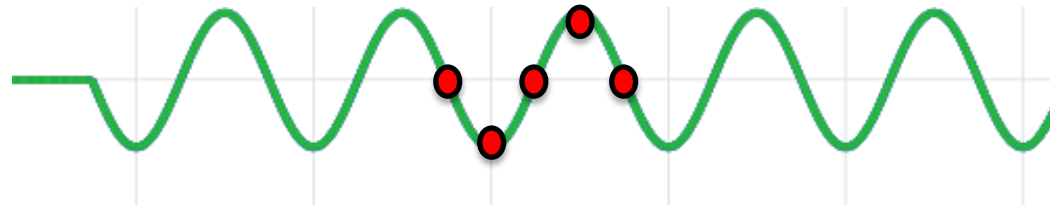
# Local power dissipation



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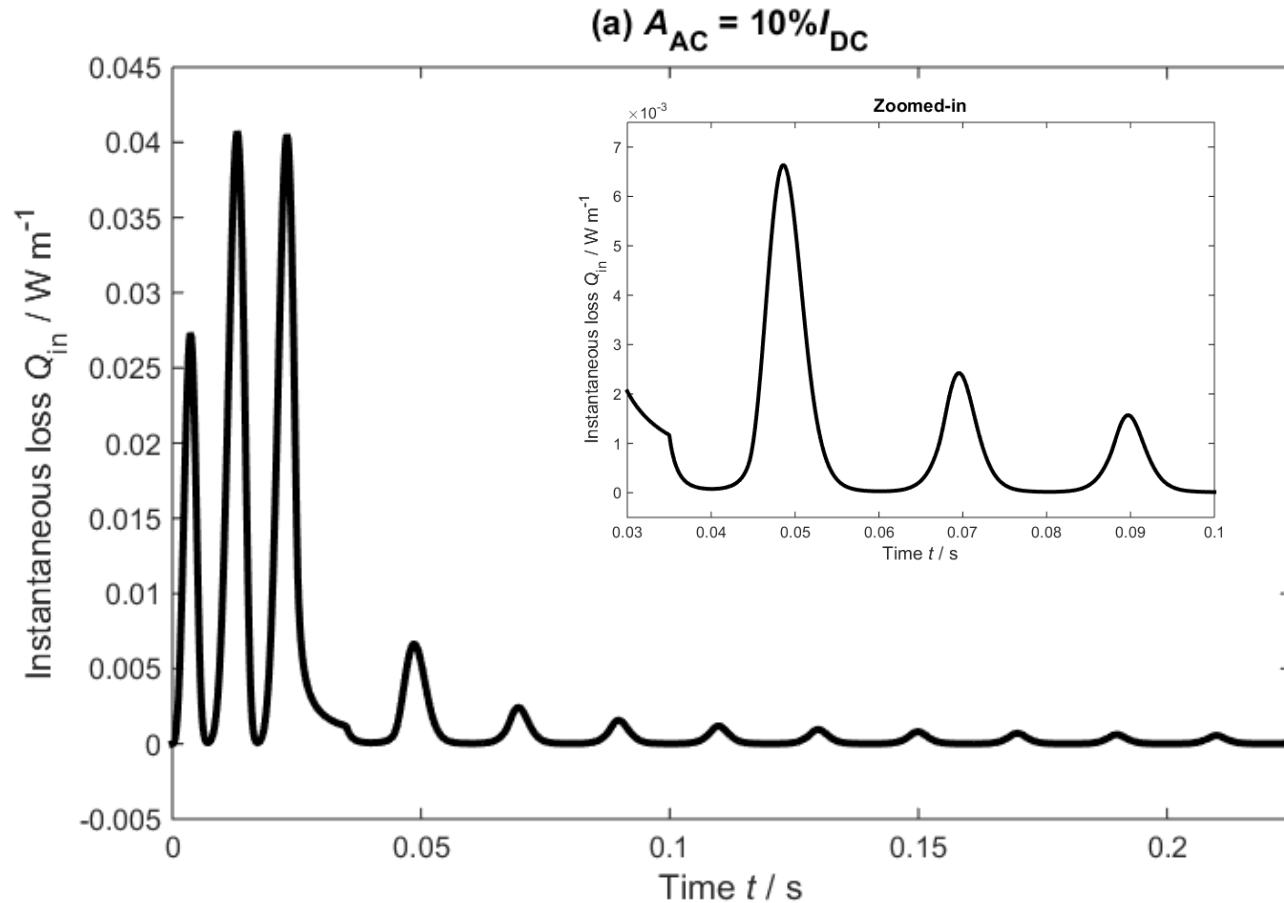


# Local power dissipation



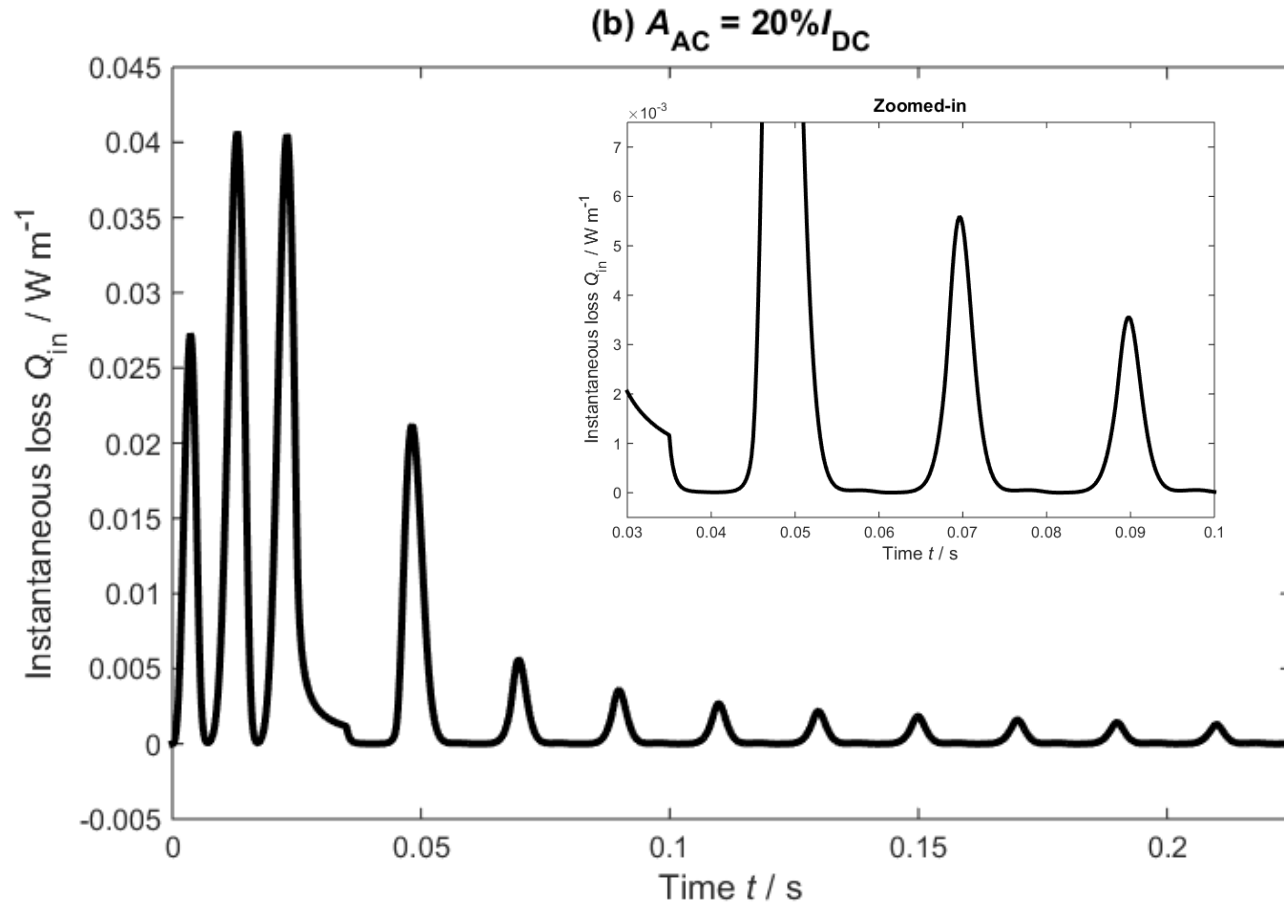
# How about larger ripples? Will $-J_c$ be reached?

- $0.7 \cdot I_c + 10\%$ , to be compared with ripples of 20% and 30%



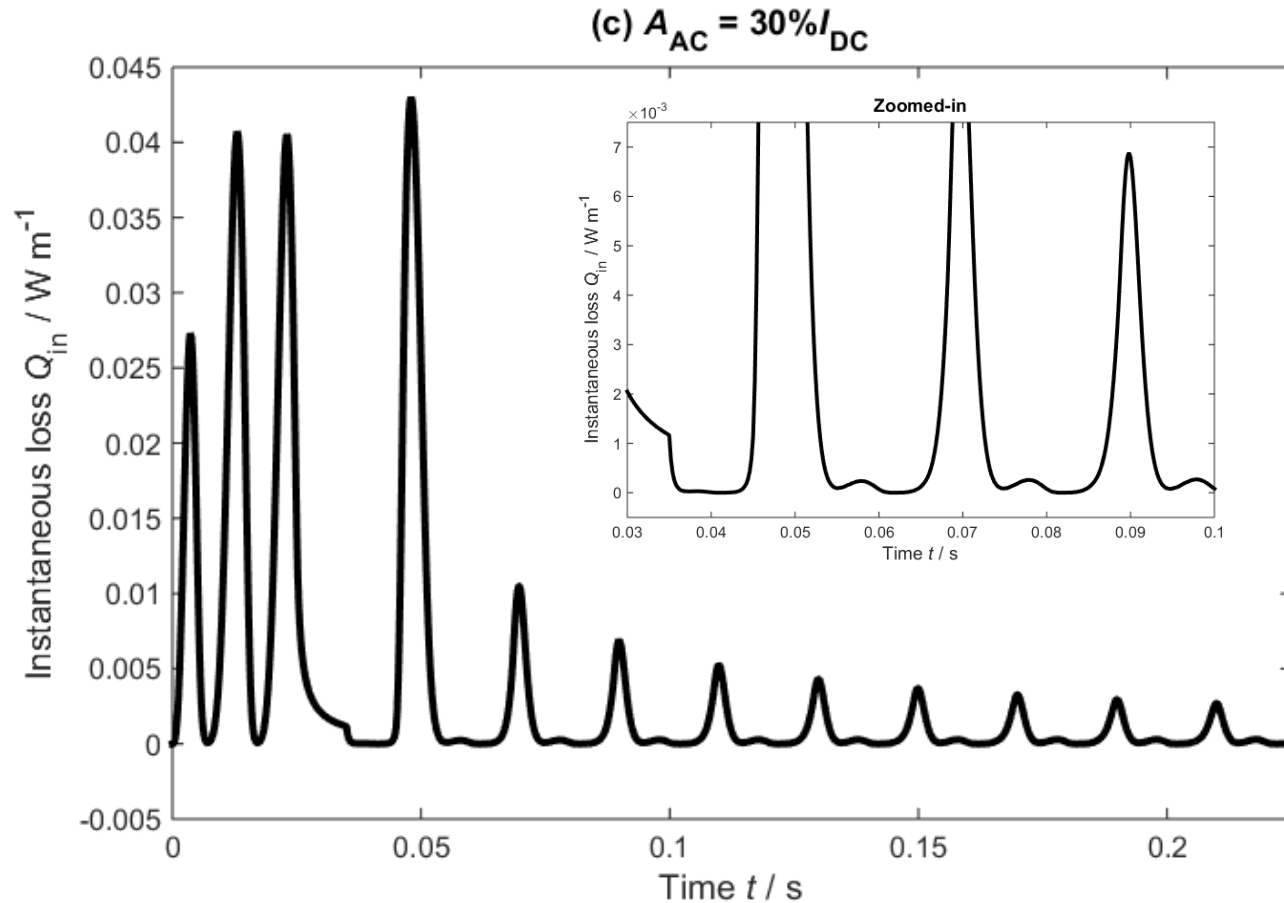
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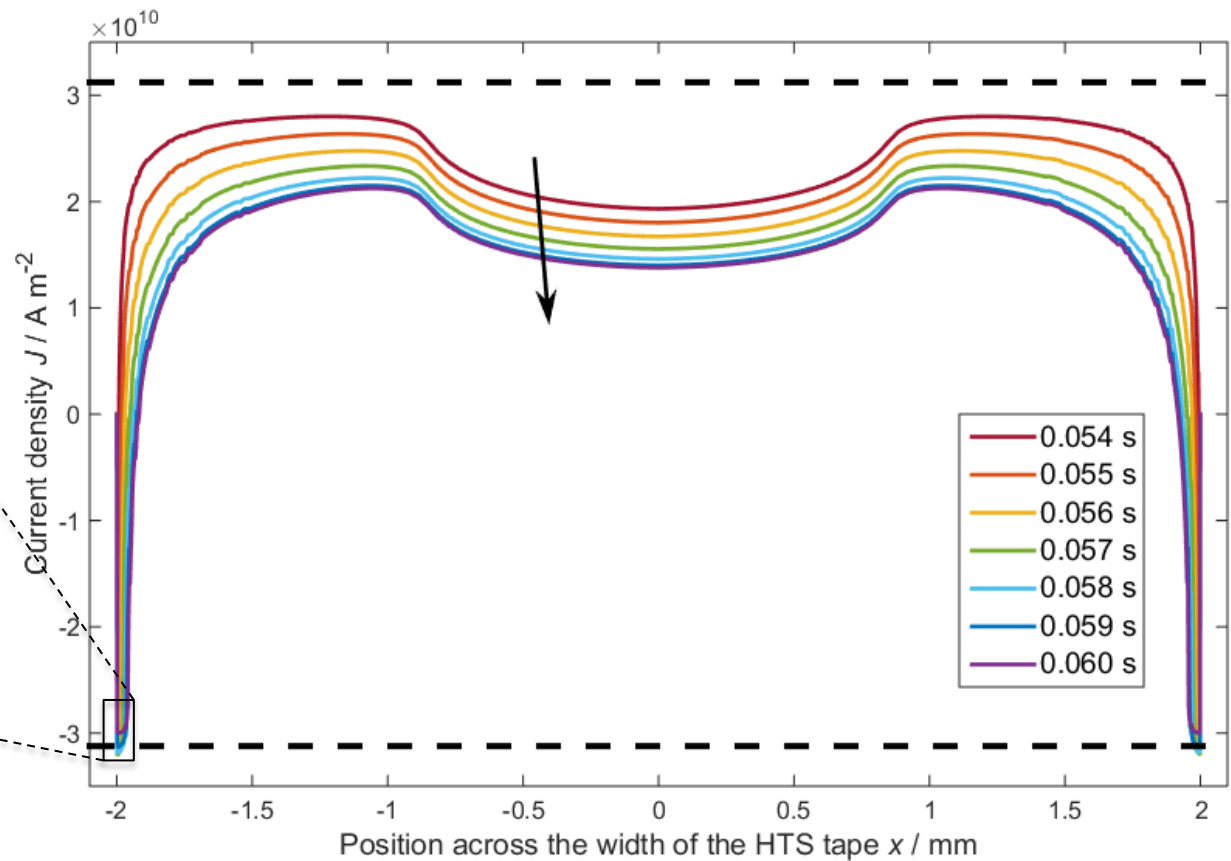
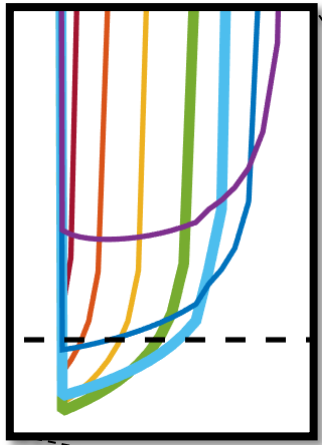
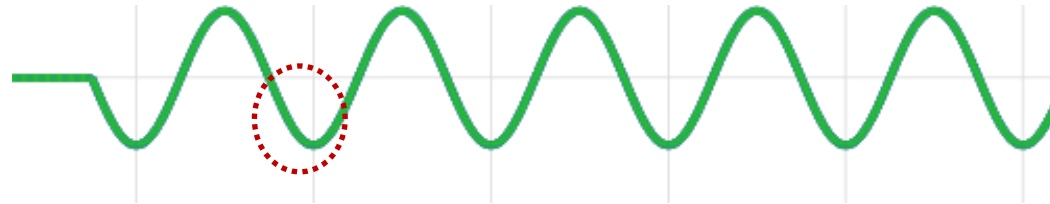


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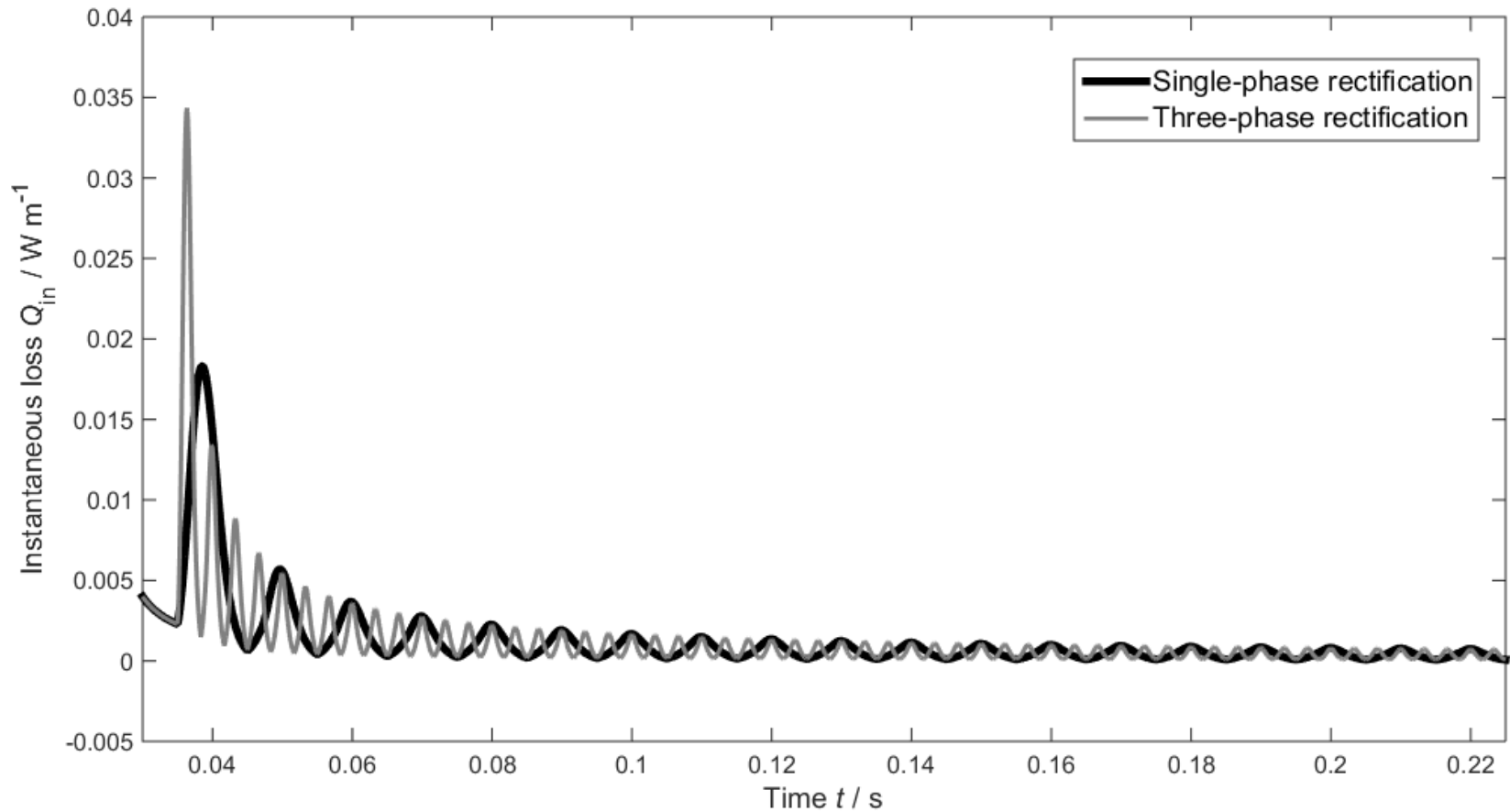
# $J(x)$ distribution for $0.7 \cdot I_c + 30\%$



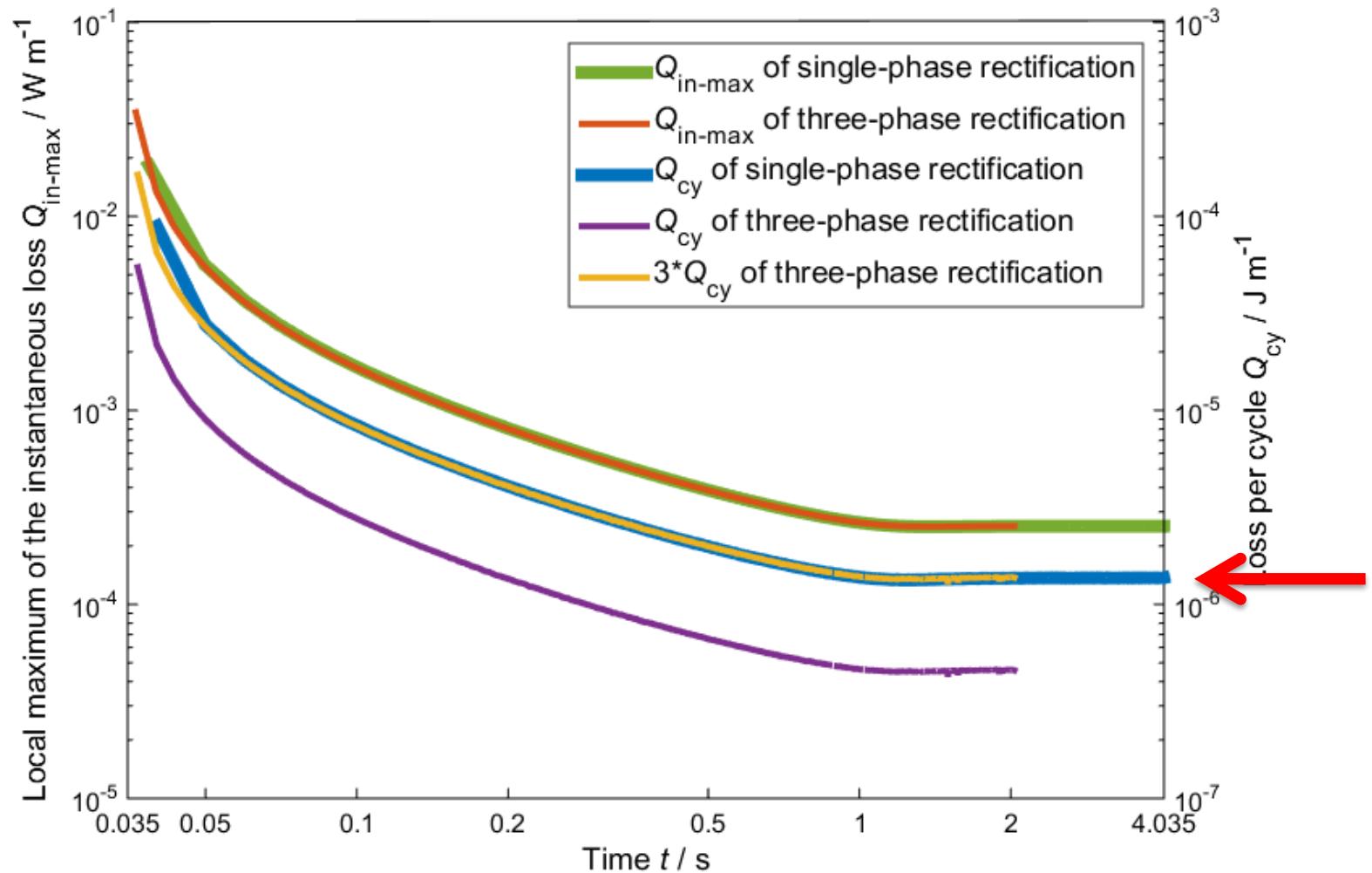


# Single-phase, full-wave rectification (10%, 100 Hz)

Amplitude of instantaneous dissipation not influenced by frequency of ripples



# Three-phase, full-wave rectification (10%, 300 Hz)



## What does this mean for a kA-range DC cable (20 tapes)?

$$P = 1.5 \times 10^{-4} \text{ W m}^{-1} \times 20 = 3 \times 10^{-3} \text{ W m}^{-1}$$

Radiation heat loss is typically  $1 \text{ W m}^{-1}$

Loss caused by AC ripples not a concern

# Integral equations

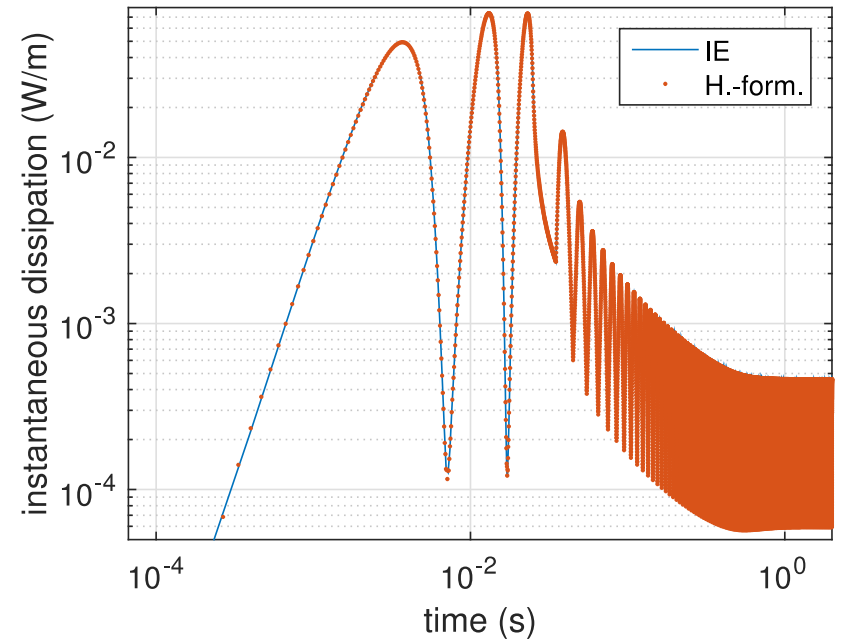
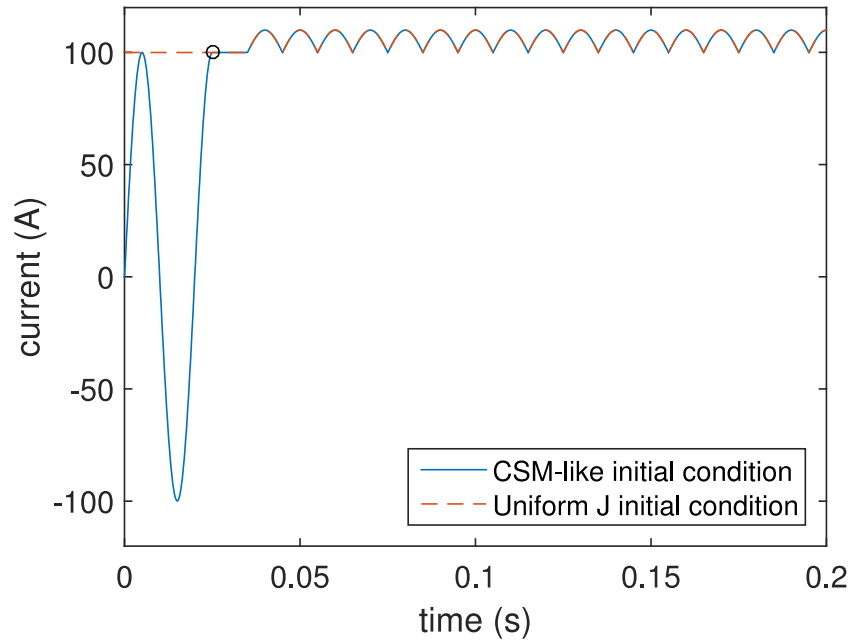
# Integral equations

- Superconductor modeled as 1-D line
- Finite elements, 100-200 DOFs → Very fast computation
- In the following:
  - Comparison with H-formulation
  - Influence of  $n$ -value
  - Influence of  $J_c(B)$  dependence

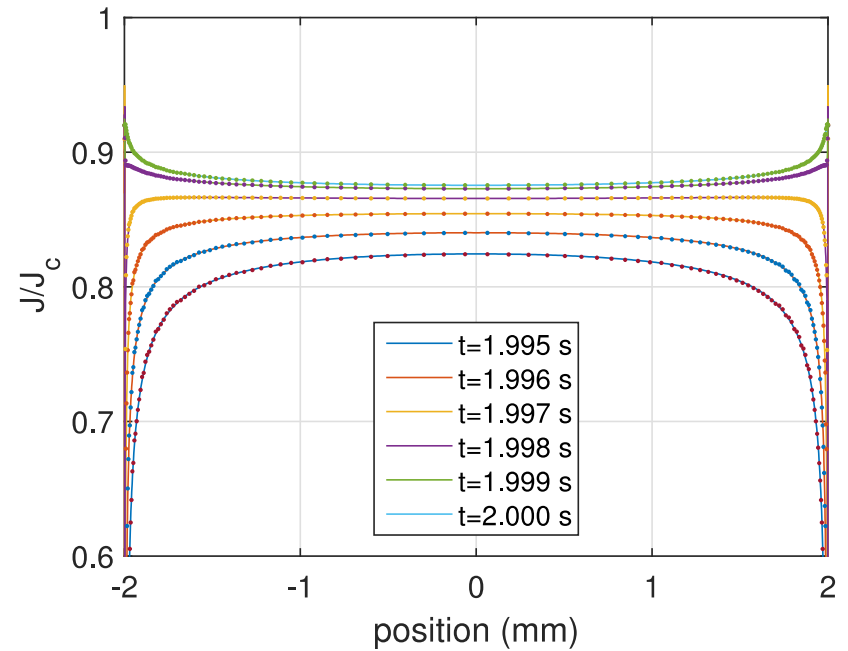
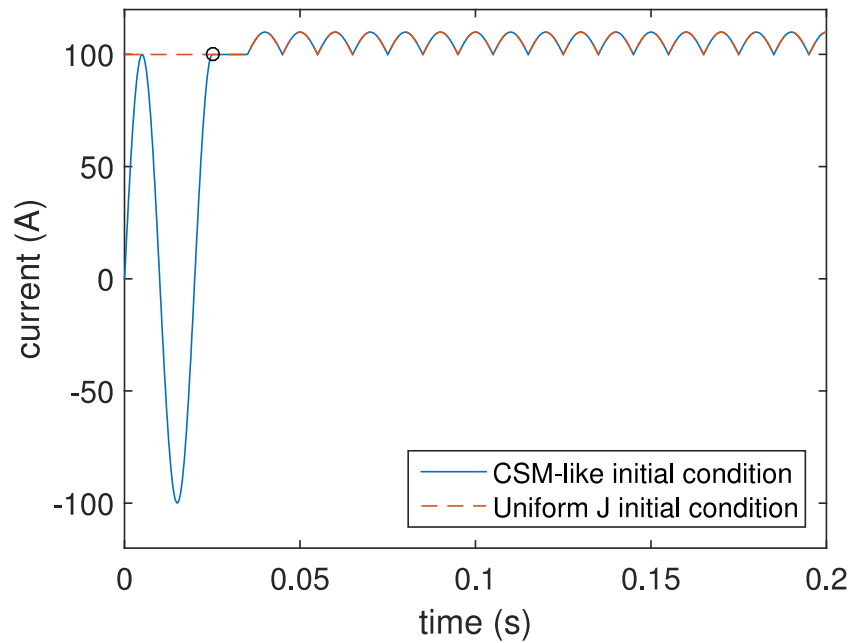
$$J(\mathbf{x}, t) = \frac{m d \dot{e}^x}{r \dot{e}^x} \int_{-a}^a \dot{H}_a(u, t) du + \int_{-a}^a J(u, t) \frac{1}{2\rho} \log|x - u| du + C(t)$$

## Integral equations for the current density in thin conductors and their solution by the finite-element method

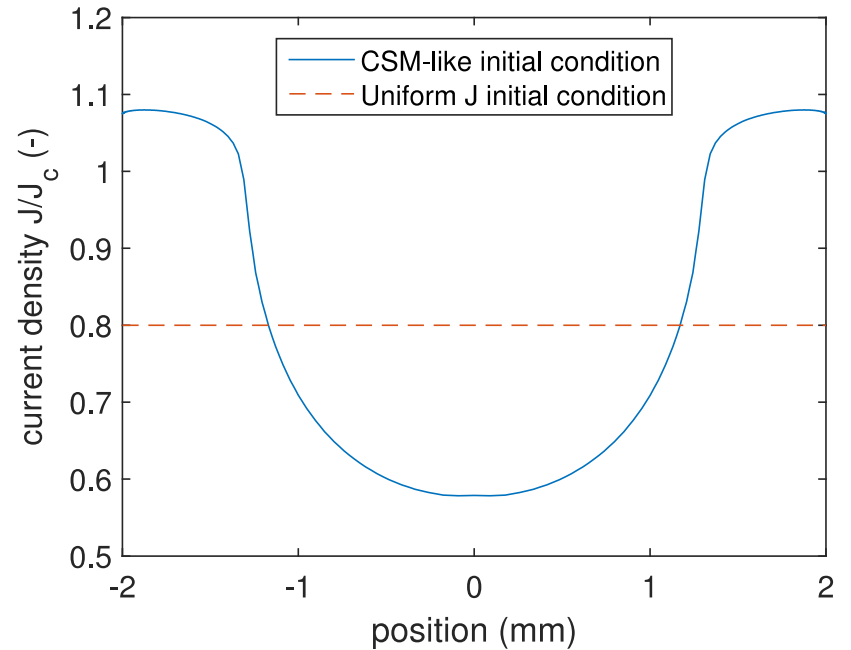
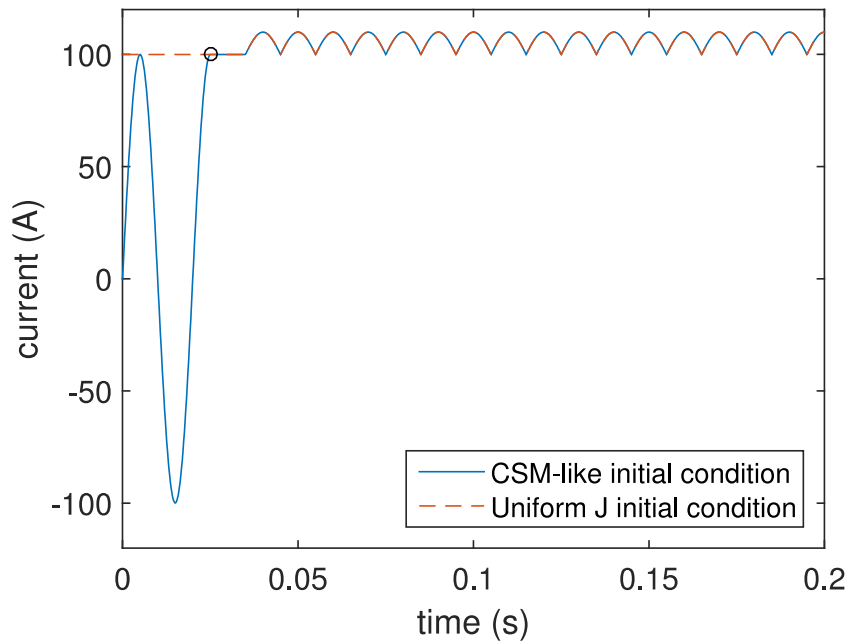
# IE and H-formulation model agree well.



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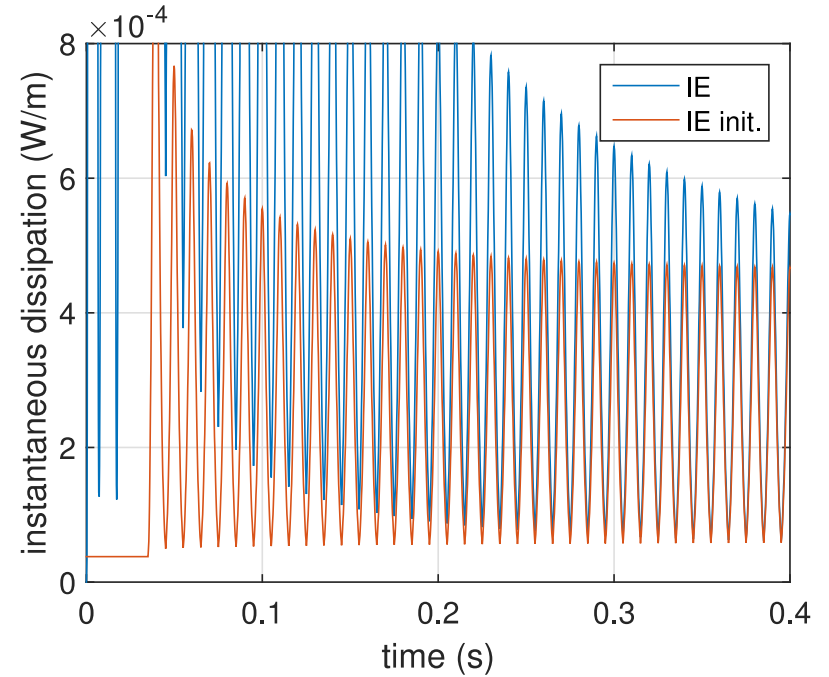
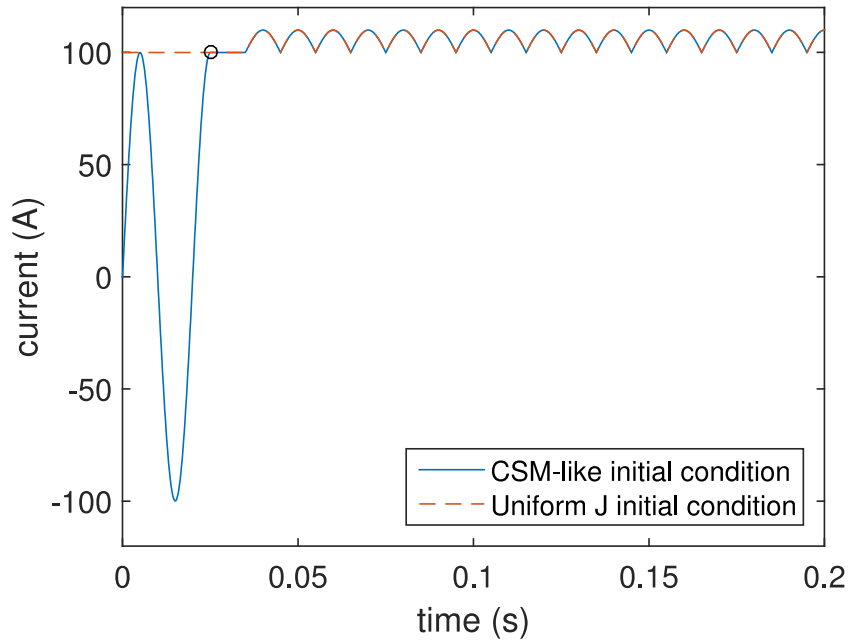


# IE allows imposing a $J$ distribution as initial condition.

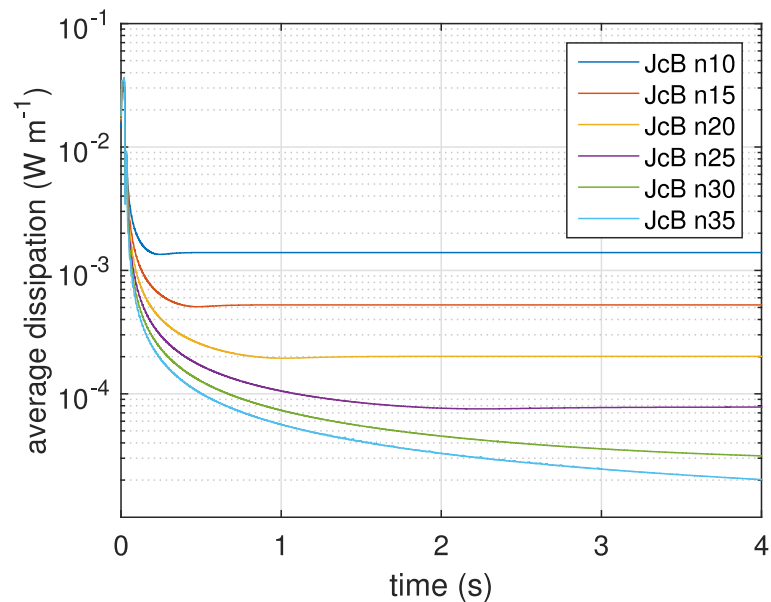
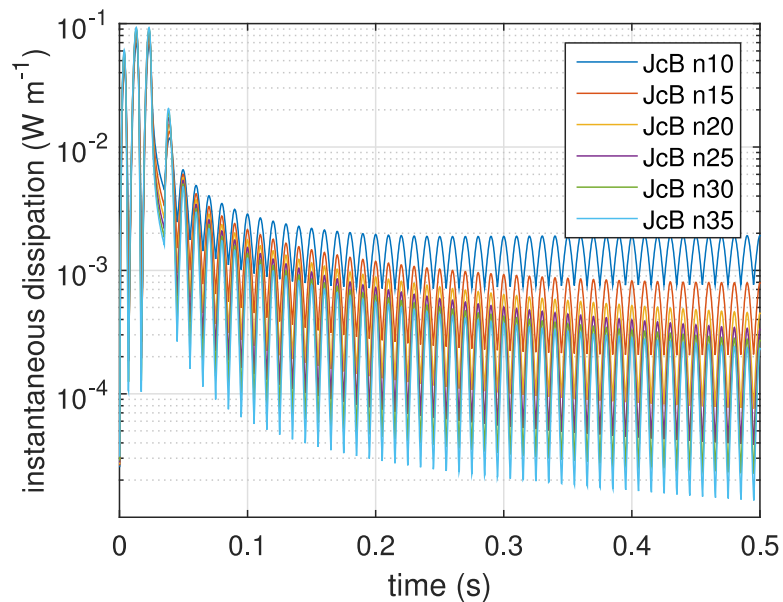
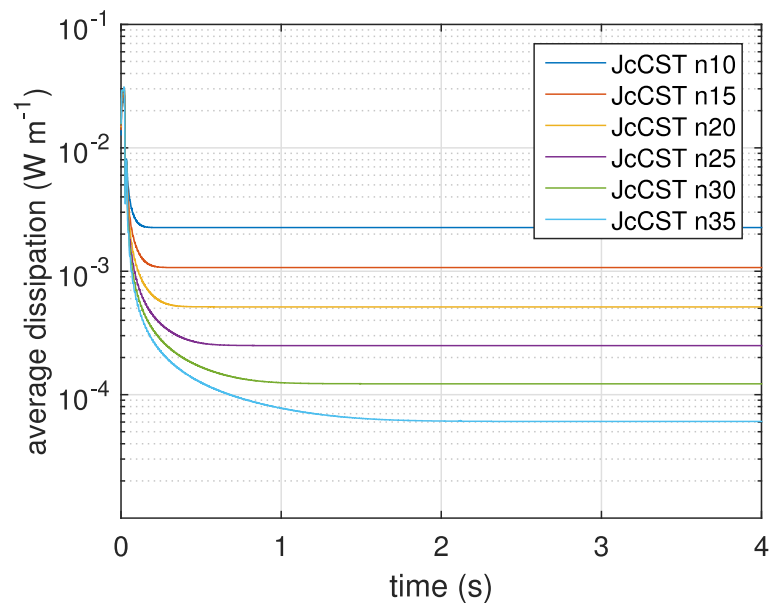
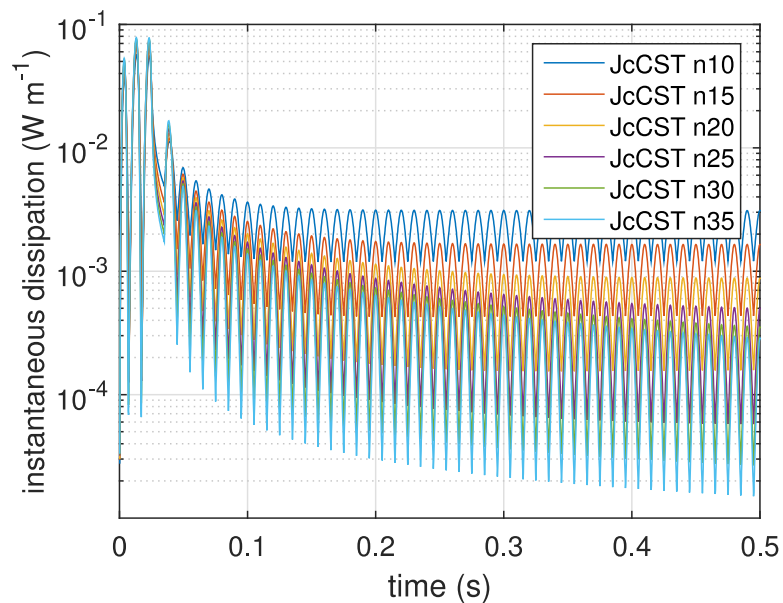




# This allows reaching the steady state more quickly.



# $n$ -value and $J_c(B)$ greatly influence the results.



## This is in contrast with 'conventional' AC simulations.

AC power loss ( $\text{Wm}^{-1}$ ) for different current amplitudes ( $I_a/I_c$ ) and n-values.

$I_a/I_c$	Norris	$n=10$	$n=25$	$n=35$
0.2	8.47E-05	1.28E-04	1.05E-04	1.00E-04
0.3	4.38E-04	5.69E-04	5.11E-04	4.95E-04
0.4	1.43E-03	1.66E-03	1.59E-03	1.56E-03
0.5	3.63E-03	3.83E-03	3.89E-03	3.75E-03
0.6	7.97E-03	7.66E-03	8.20E-03	8.24E-03
0.7	1.59E-02	1.39E-02	1.57E-02	1.59E-02
0.8	3.00E-02	2.36E-02	2.82E-02	2.90E-02
0.9	5.60E-02	3.81E-02	4.87E-02	5.10E-02
0.99	1.07E-01	5.67E-02	7.84E-02	8.45E-02

# Summary

- Current density dynamics investigated in detail
- Due to DC bias,  $-J_c$  not reached during cycle → one peak per cycle
- Integral equation method → Very fast, allows more comprehensive studies
- AC ripple loss not a concern in practical cables

But...

A few questions remain:

1. What is the  $J$  distribution associated to a purely DC current?
2. Is the power-law the correct constitutive equation to model AC ripples?
3. Can these small losses be measured experimentally?

Thank you for listening!