

# Alternative Conductor Concept for SIS-100 at the IAF-GSI

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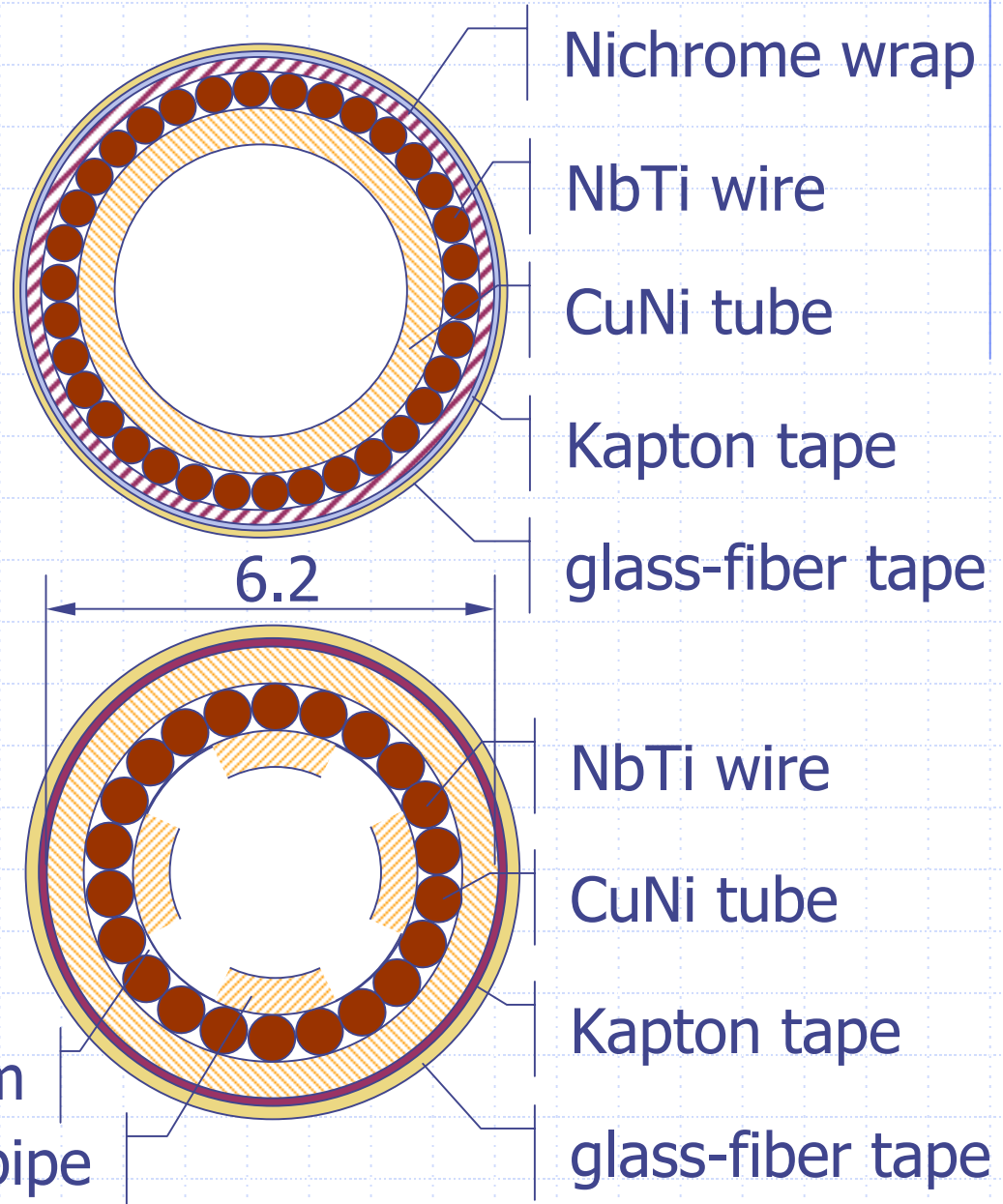
# Problem statement

- ◆ SIS-100 will be a pulsed machine with very heavy duty cycle
  - 2 T at 1 Hz, 4 T/s
  - $10^7$  operation cycles . Present design *may* require additional optimization.
- ◆ performance and reliability of SIS-100 will affect the whole complex
  - $10^7$  operation cycles
- ◆ Present design *may* require additional optimization

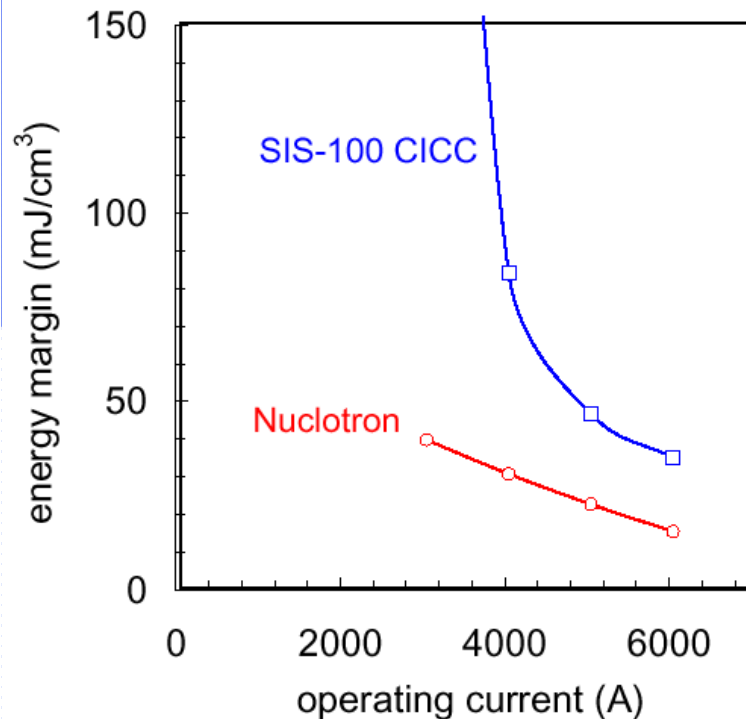
# A proposal

bring strands close to He  
provide a low-impedance cooling path  
use realistic strand data  
 $J_c = 5200 \text{ A/mm}^2$   
maintain operating conditions

helium  
perforated CuNi pipe



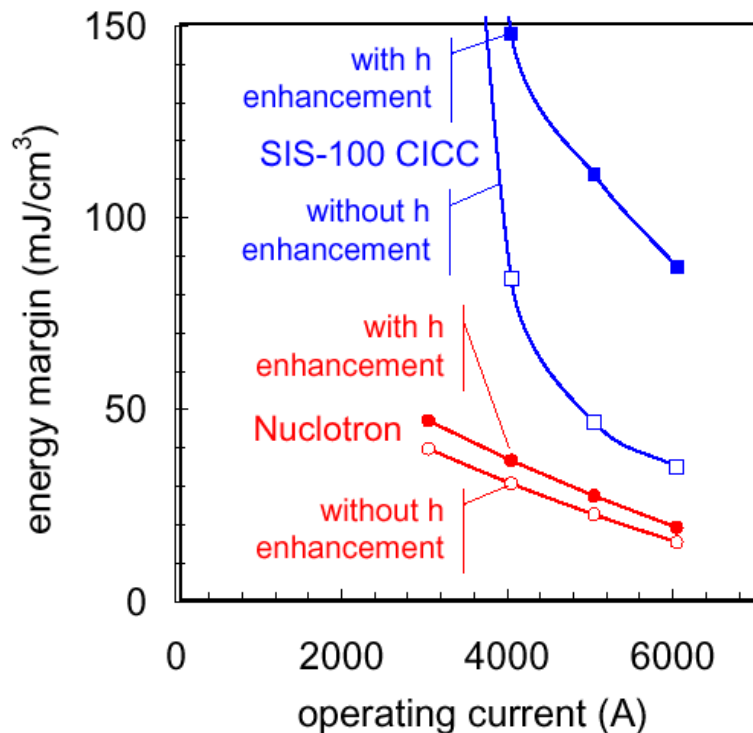
# Stability analysis (1/3)



- ◆ analysis of stability margin as a function of the operating current
  - simplified simulation
    - ◆ supercritical helium at 3 bar, 4.22 K
    - ◆ no transient heat transfer
    - ◆ 1 ms perturbation time

clear gain in stability

# Stability analysis (2/3)



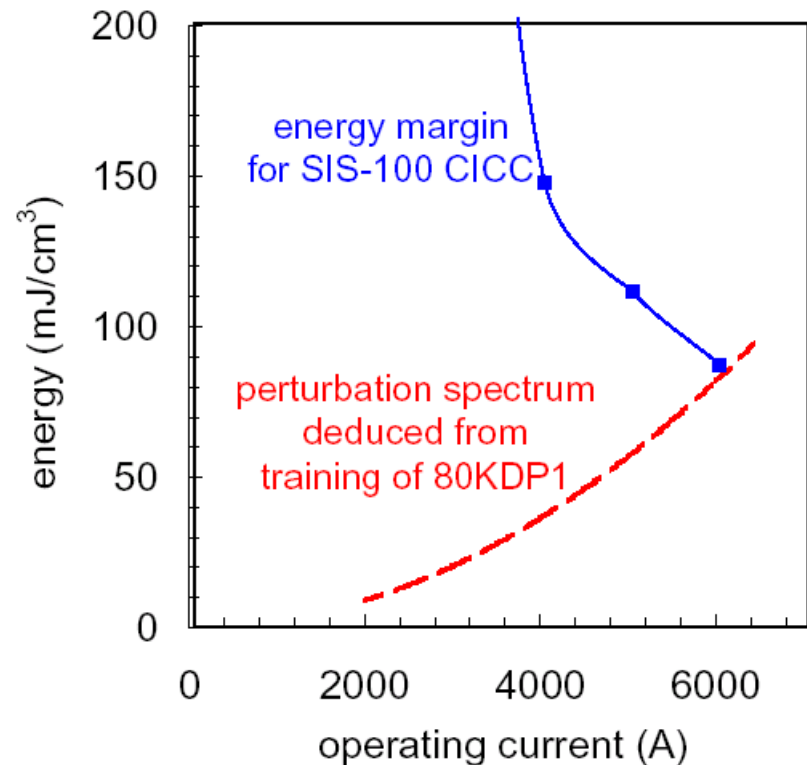
- ◆ effect of transient heat transfer important !
  - model as a boundary layer diffusion
    - ◆ supercritical helium at 3 bar, 4.22 K
    - ◆ 1 ms perturbation time
  - **gain in stability is exceptional:**
    - ◆ a factor 4.5 from 20 to 90 (mJ/cm<sup>3</sup>)

# Stability analysis (3/3)

- ◆ perturbation spectrum of the magnet:
  - first training quench of 80KDP1 at  $I_0=4$  kA
  - computed stability margin  $Q_0=36.4$  mJ/cm<sup>3</sup>
  - estimated energy spectrum:

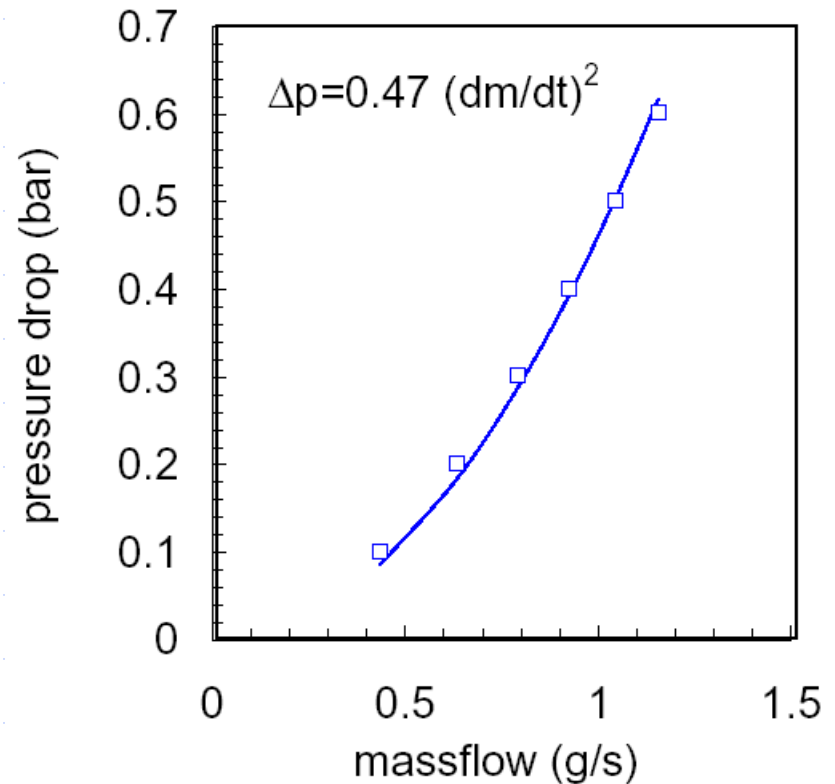
$$Q = Q_0 (I/I_0)^2$$

a SIS-100 CICC will have  
no training !



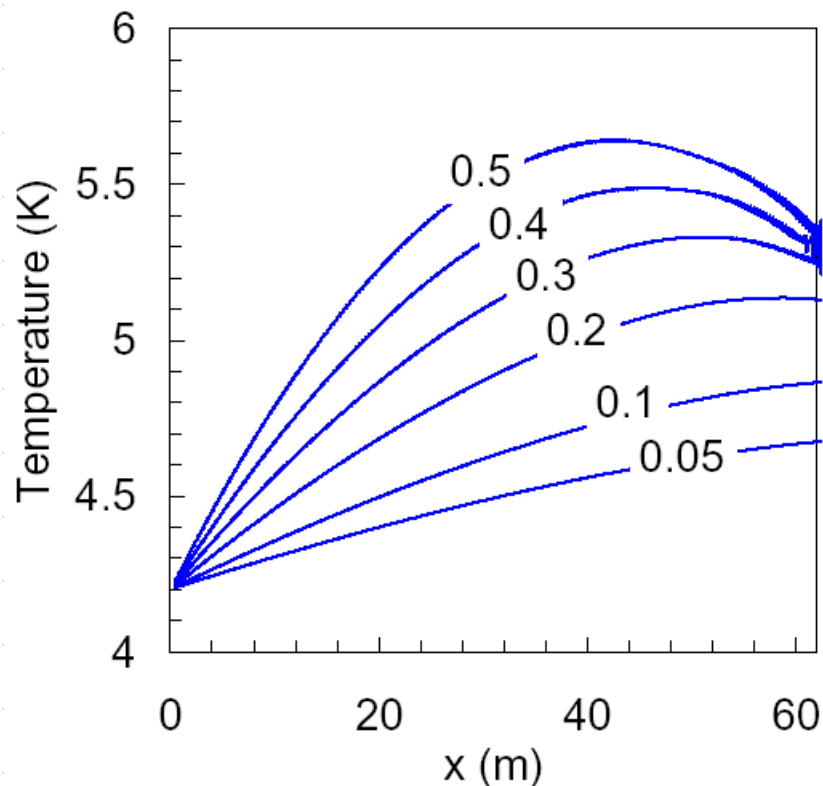
# Flow and cooling analysis (1/3)

- ◆ supercritical helium analysis:
  - $p_{in} = 3$  bar
  - $p_{out} = 2.4 \dots 2.9$  bar
- ◆ **modest pressure drop** for the short conductor length as envisaged
  - $L = 62$  m
- ◆ the helium flows mostly in the central hole:
  - hole: 99...98 %
  - bundle: 1...2 %



# Flow and cooling analysis (2/3)

$p_{in} = 5 \text{ bar}$   
 $p_{out} = 2.4 \text{ bar}$   
 $dm/dt = 2.5 \text{ g/s}$



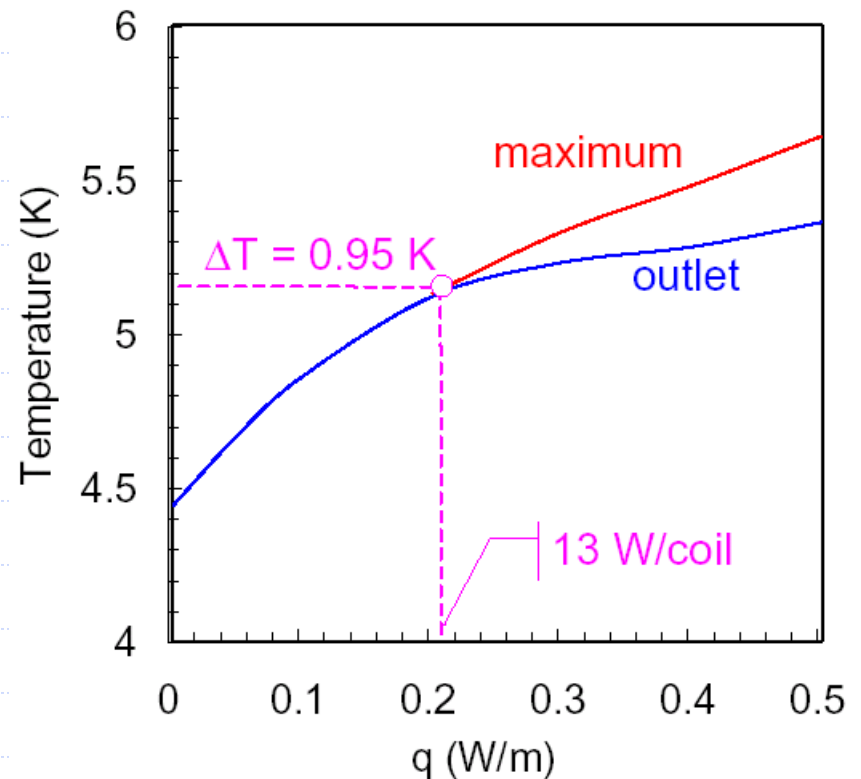
- ◆ maximum temperature is **inside the coil** for high heat load (above 13 W/coil) because of JT expansion along the cable



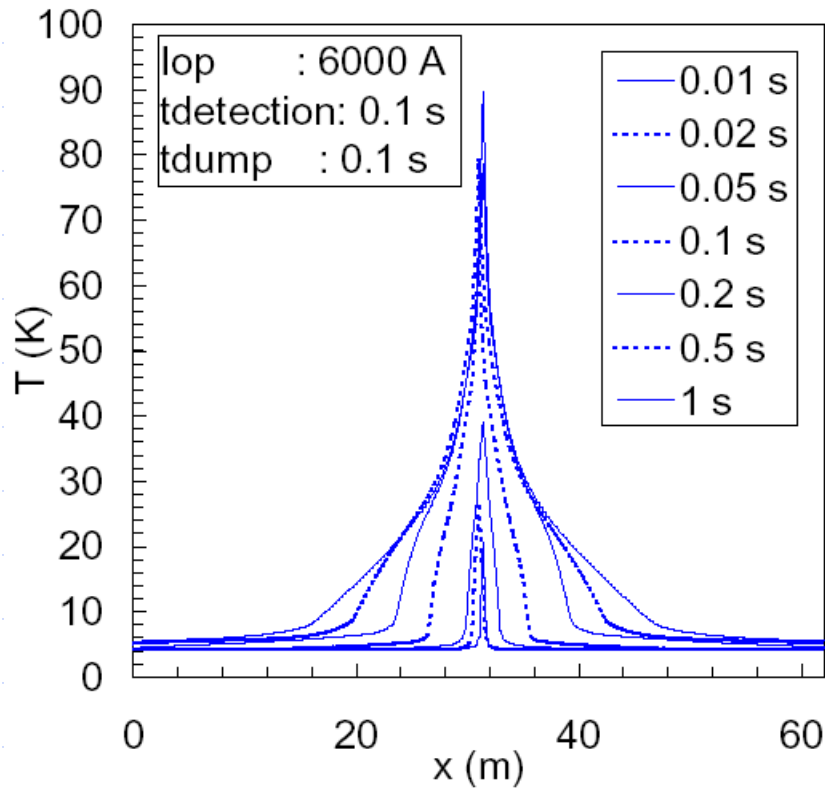
# Flow and cooling analysis (3/3)

- ◆ working conditions are acceptable **only if the heat load on the conductor is small (5...10 W)**
- ◆ increase flow, or decrease hydraulic impedance to accommodate higher heat loads

$$\begin{aligned}p_{\text{in}} &= 5 \text{ bar} \\ p_{\text{out}} &= 2.4 \text{ bar} \\ dm/dt &= 2.5 \text{ g/s}\end{aligned}$$



# Quench analysis (1/3)

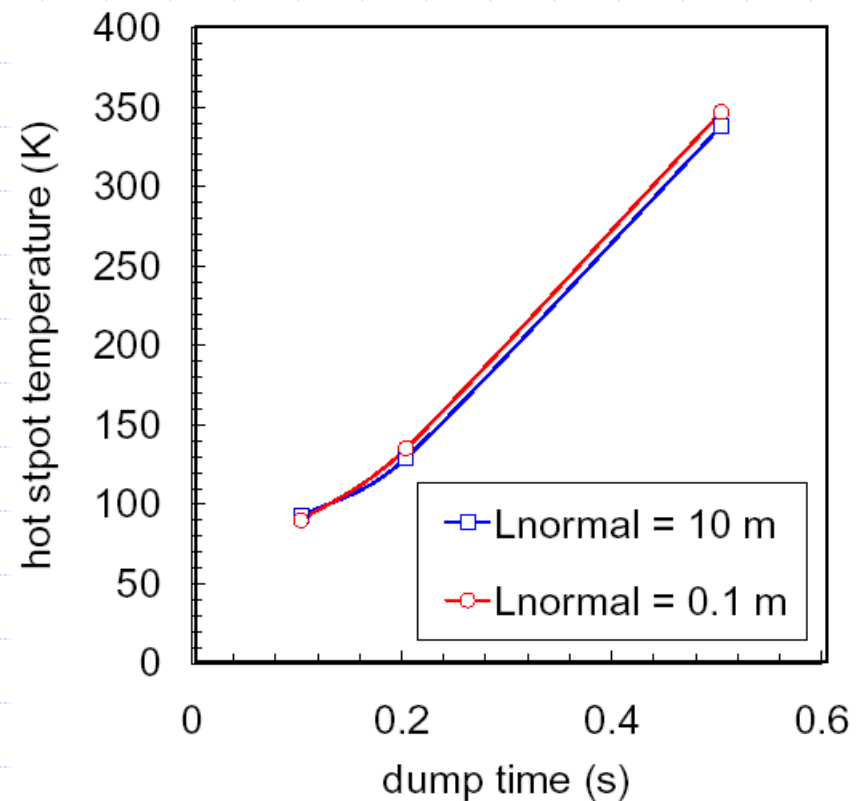


- ◆ quench propagation reaches THQB conditions
- ◆ average propagation speed in the time range 0 ... 0.5 s is approximately 20 m/s

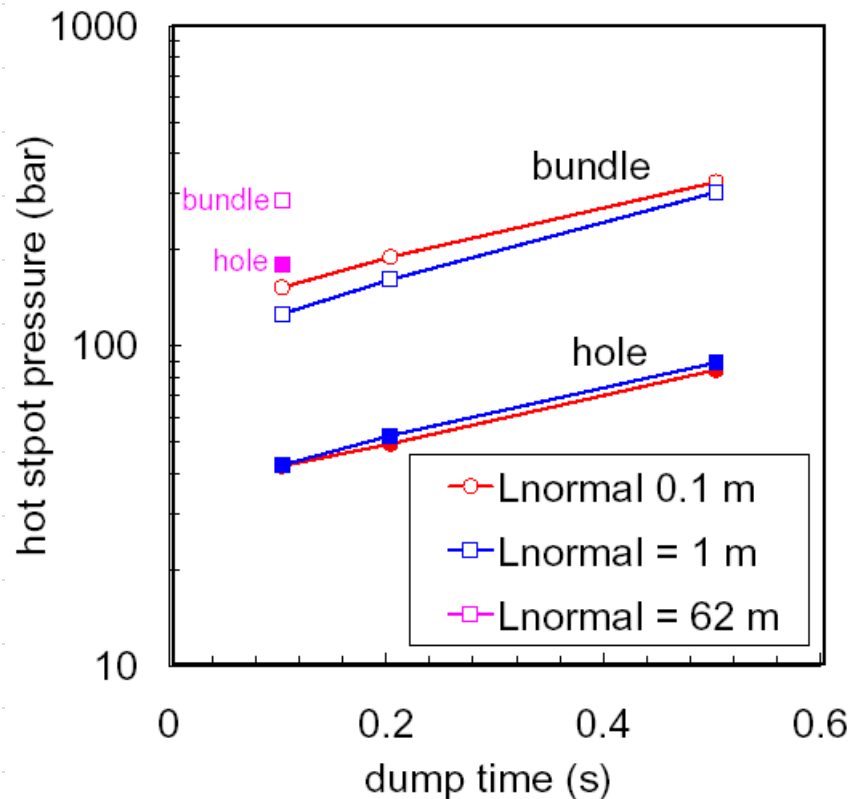
# Quench analysis (2/3)

◆ hot-spot temperature  
safely below 150 K if:

- detection within 0.1 s or faster
- dump with a 0.2 s time constant or faster



# Quench analysis (3/3)



◆ pressure increase is large (150 bar and more)

- poor hydraulic coupling of bundle and hole (small dimensions)
- can be improved by an increase of the effective transverse flow cross section

# Conclusions

- ◆ the CICC technology is **available and adapted to pulsed operation** (low loss, high stability)
- ◆ a CICC conductor for SIS-100 **appears to be feasible** using present technology
- ◆ first analysis show that:
  - ◆ stability greatly enhanced, a CICC SIS-100 **should have no training at all !**
  - ◆ pressure drop is acceptable
    - 1 g/s → 0.5 bar
    - 2.5 g/s → 2.4 bar
  - ◆ supercritical cooling **may be feasible**
    - $\Delta T < 1$  K for 13 W/coil if  $dm/dt = 2.5$  g/s
  - ◆ protection ( $T < 200$  K,  **$p < 150$  bar**) can be achieved with 0.1 s detection and 0.2 s dump time (approximately 60 V on a magnet) and can be improved with minor design changes