

CHATS 2002

IN-3

***HTS Magnets: Stability; Protection; Cryogenic;
Economics; Research Areas***

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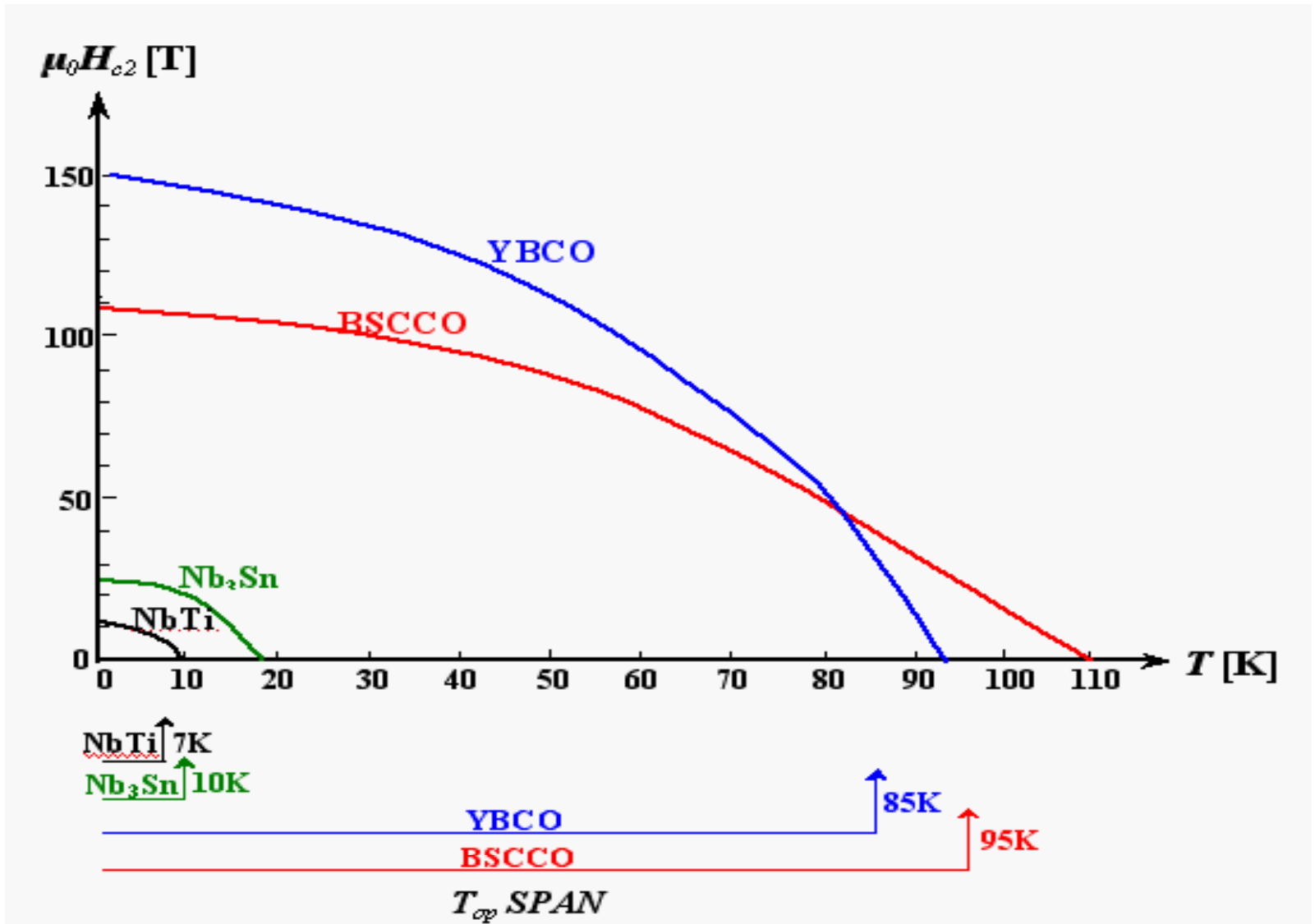
Forschungszentrum Karlsruhe

Karlsruhe, Germany

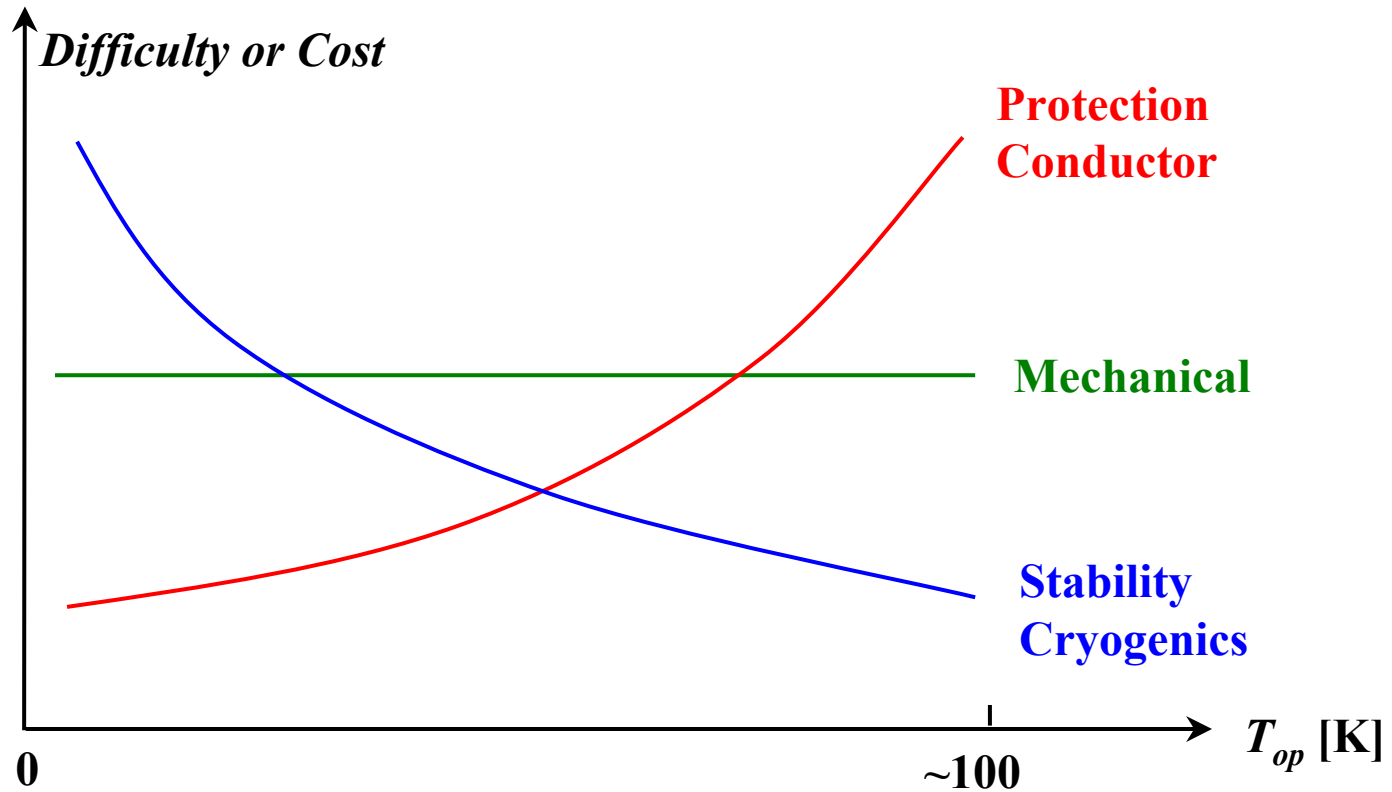
Outline

- **Introduction.**
 - ☆ **Range of T_{op} : LTS vs HTS.**
 - ☆ **Magnet issues.**
- **Stability.**
- **Protection.**
- **Cryogenics.**
- **Economics of large-scale HTS devices.**
- **Research areas.**
 - ☆ **Activities *at FBML*.**

Range of T_{op} : LTS vs HTS



Key Magnet Issues vs T_{op}



Stability: LTS vs HTS

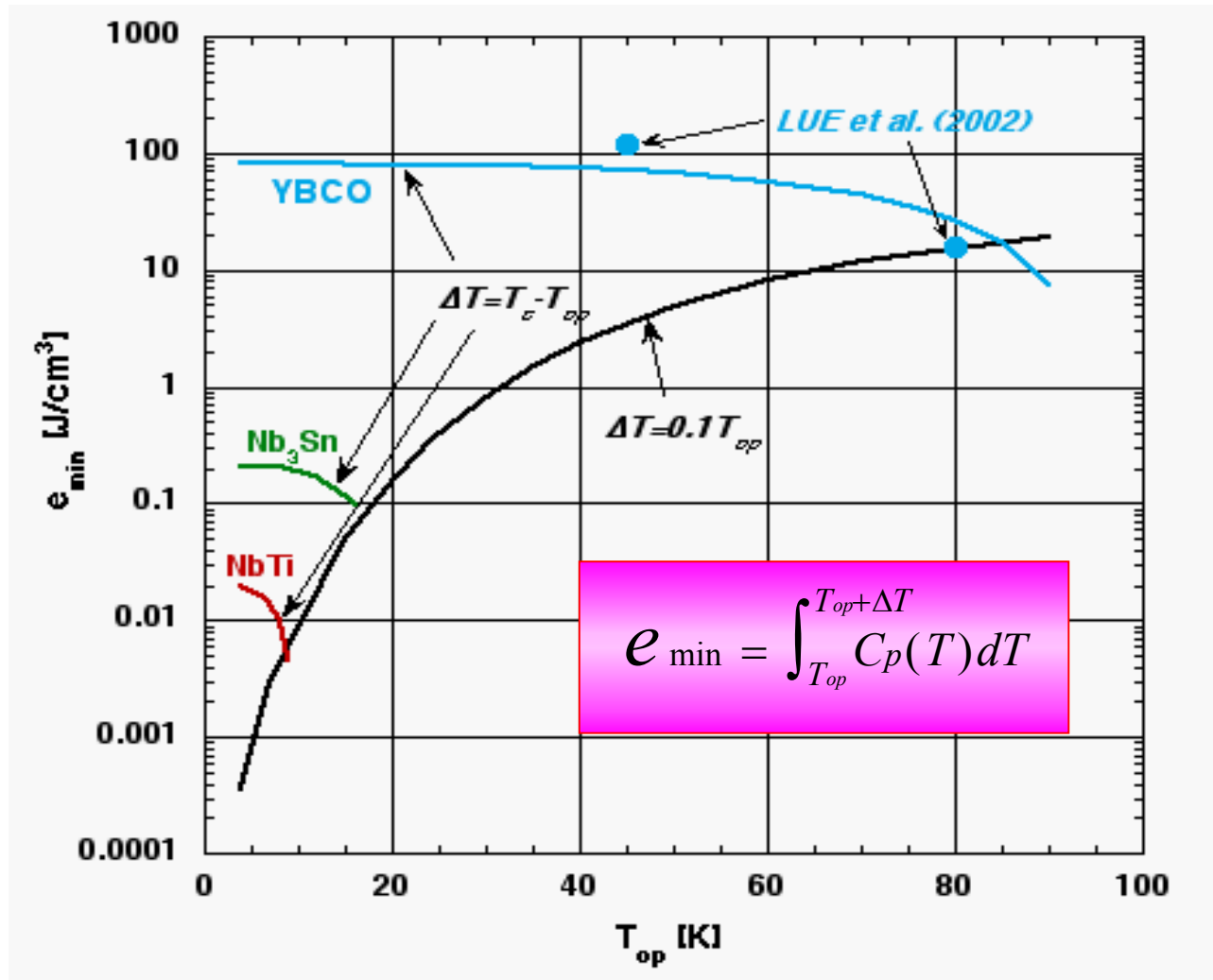
LTS: $dT_{op}/dt \approx 0$ ---permissible ΔT_{op} generally < 1 K.

- **Mechanical energy disturbance as small as $\sim 10\mu\text{J}$ may induce a quench.**

HTS: Permissible ΔT_{op} can exceed 10 K.

- **Immune against those disturbances that afflict high-performance (adiabatic) LTS magnets.**
- **May be vulnerable to fault-mode disturbances.**

Minimum Thermal Energy Density (C_p : copper; T_c : Superconductor)



Protection

Probable Causes of Quench in HTS Devices

- Malfunction, *e.g.*, cryogenics.
- Scheduled fault modes, *e.g.* FCL.
- **Non-issues: mechanical disturbances; AC losses.**

Key Areas

- Overheating.
- Arcing.
- Overstressing.

Protection (continued)

Magnet Self-Protecting if...

- NZP velocity “high:” $U_l > 1$ m/s.
- Magnet size ($a_2 - a_1$) “small:” $(a_2 - a_1)/U_l < \tau_j$.

Corollary: HTS devices not self-protecting.

- **Overheating: requires normal metal substrate.**
 - ☆ quench/recovery behavior;
 - ☆ detection of hot zones.
- **Arcing (internal): requires normal metal substrate.**
- **Overstressing: requires reinforcing substrate.**

Corollary: All three tend to reduce J_e .

NZP Velocity & Protection

LTS: In the range >1 m/s.

- “High” NZP velocities make LTS self-protecting.
- For multi-coil magnets---resistor shunting effective.

HTS: In the range 1-10 mm/s.

- “Low” NZP velocities make HTS **not self-protecting**.
- Active protection required---detection of a hot zone (though unlikely to be created) important.

NZP Velocity (Adiabatic Winding)

$$U_t = \frac{J_m}{C_{cd}} \sqrt{\frac{\rho_m k_i}{\Delta T}} \quad (J_m = 10^8 \text{ A/m}^2)$$

LTS (4.2 K): $C_{cd} \sim 10^3 \text{ J/m}^3 \text{ K}$; $\rho_m \sim 2 \times 10^{-10} \text{ } \Omega \text{ m}$;

$k_i \sim 0.2 \text{ W/m K}$; $\Delta T \sim 0.5 \text{ K} \rightarrow U_t \sim 1 \text{ m/s}$.

HTS (77 K): $C_{cd} \sim 2 \times 10^6 \text{ J/m}^3 \text{ K}$; $\rho_m \sim 2 \times 10^{-9} \text{ } \Omega \text{ m}$;

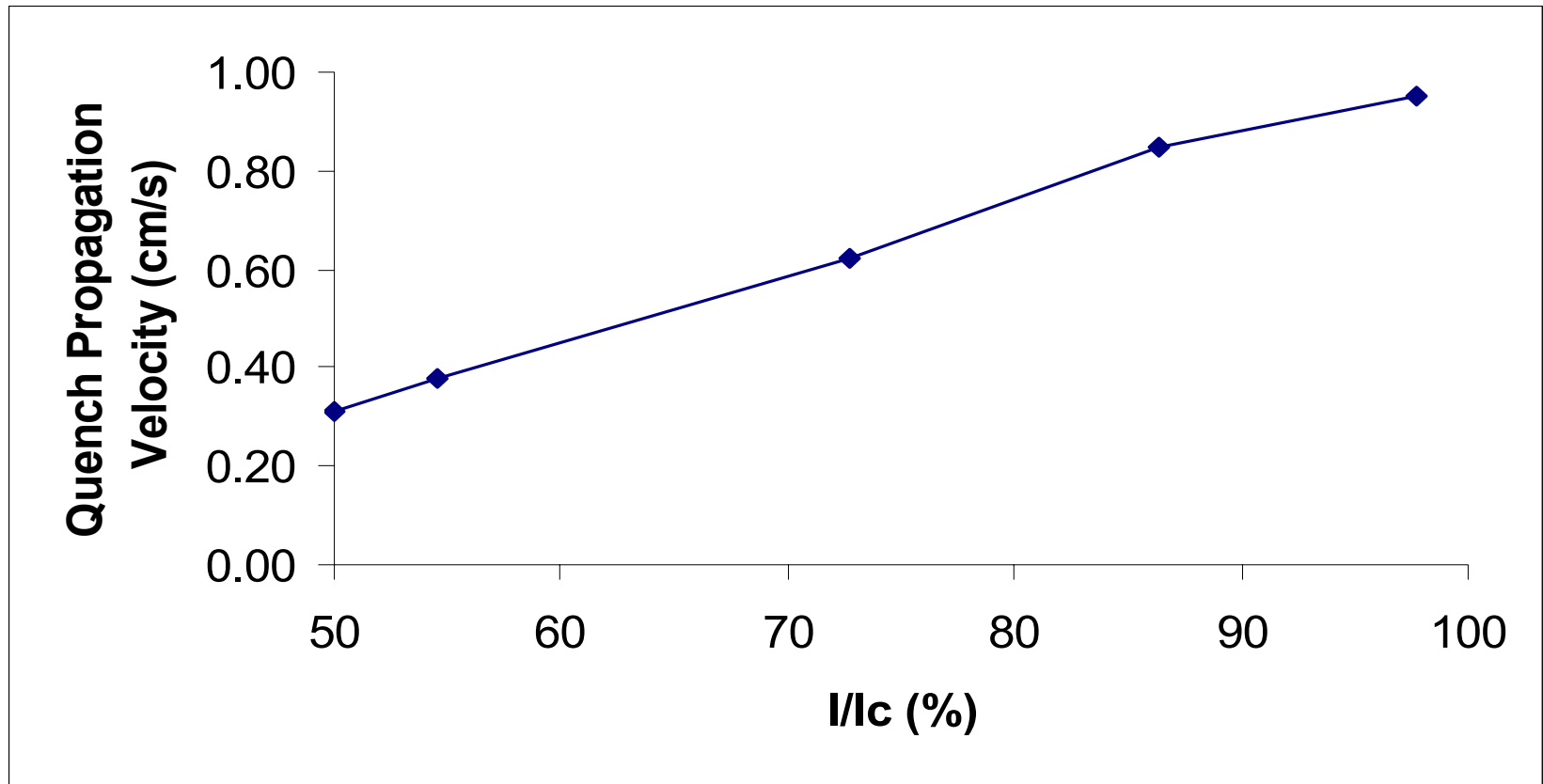
$k_i \sim 0.2 \text{ W/m K}$; $\Delta T \sim 10 \text{ K} \rightarrow U_t \sim 0.3 \text{ mm/s}$.

Schwartz: $J_m \sim 10^9 \text{ A/m}^2$; $C_{cd} \sim 2 \times 10^6 \text{ J/m}^3 \text{ K}$; $\rho_m \sim 2 \times 10^{-9} \text{ } \Omega \text{ m}$;

$k_m \sim 400 \text{ W/m K}$; $\Delta T \sim 20 \text{ K} \rightarrow U_l \sim 10 \text{ cm/s}$.

Quench Propagation Velocity vs I/I_c

(Schwartz, 2002)



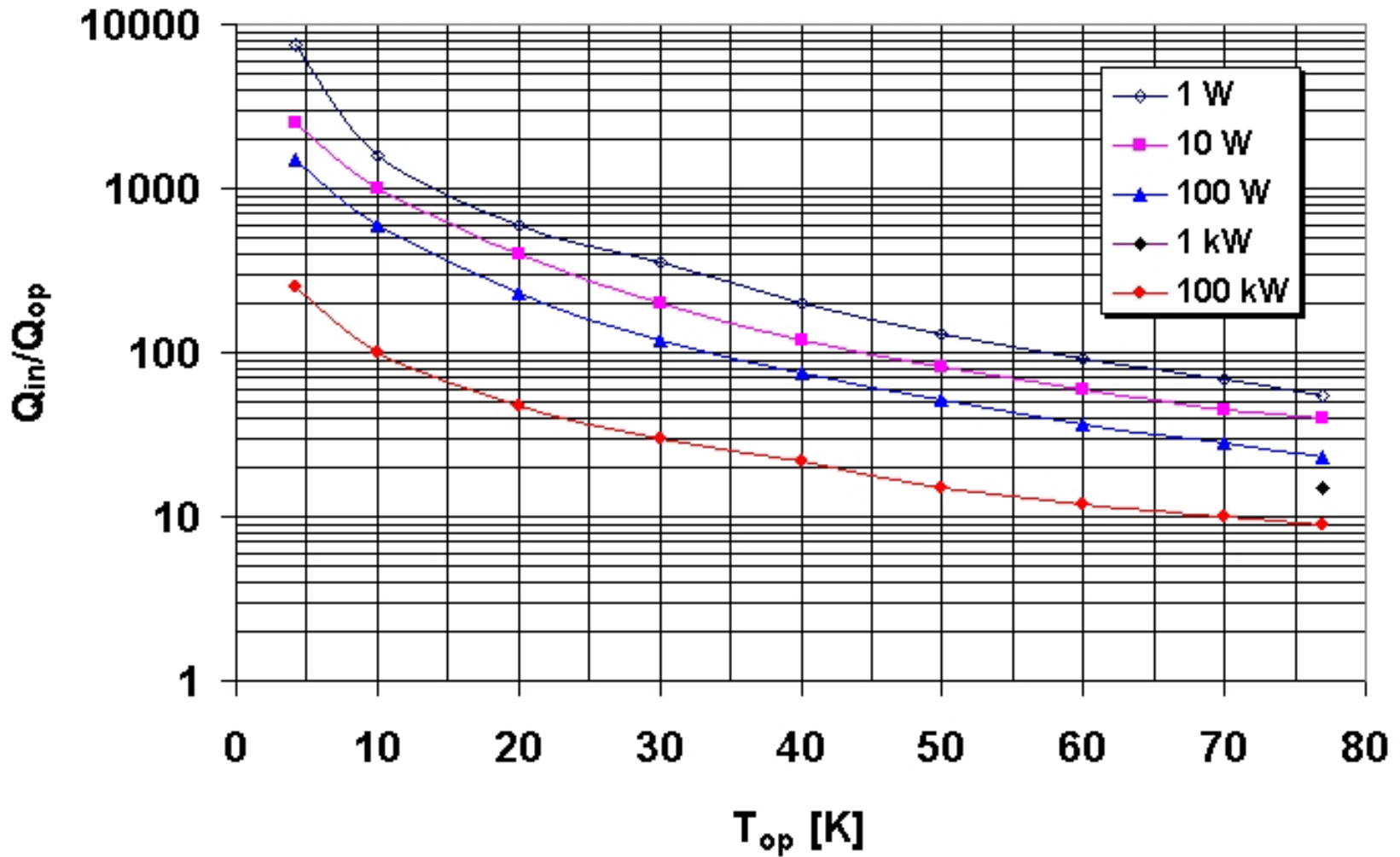
Cryogenics

- **Most devices operate at **RT**.**
motors; cameras; refrigerators; wrist watches;
CD players; pianos; airplanes; automobiles;
nuclear reactors---**note that some key components
operate above but generally not < RT.**
- **Prominent exceptions: superconducting &
cryogenic devices.**

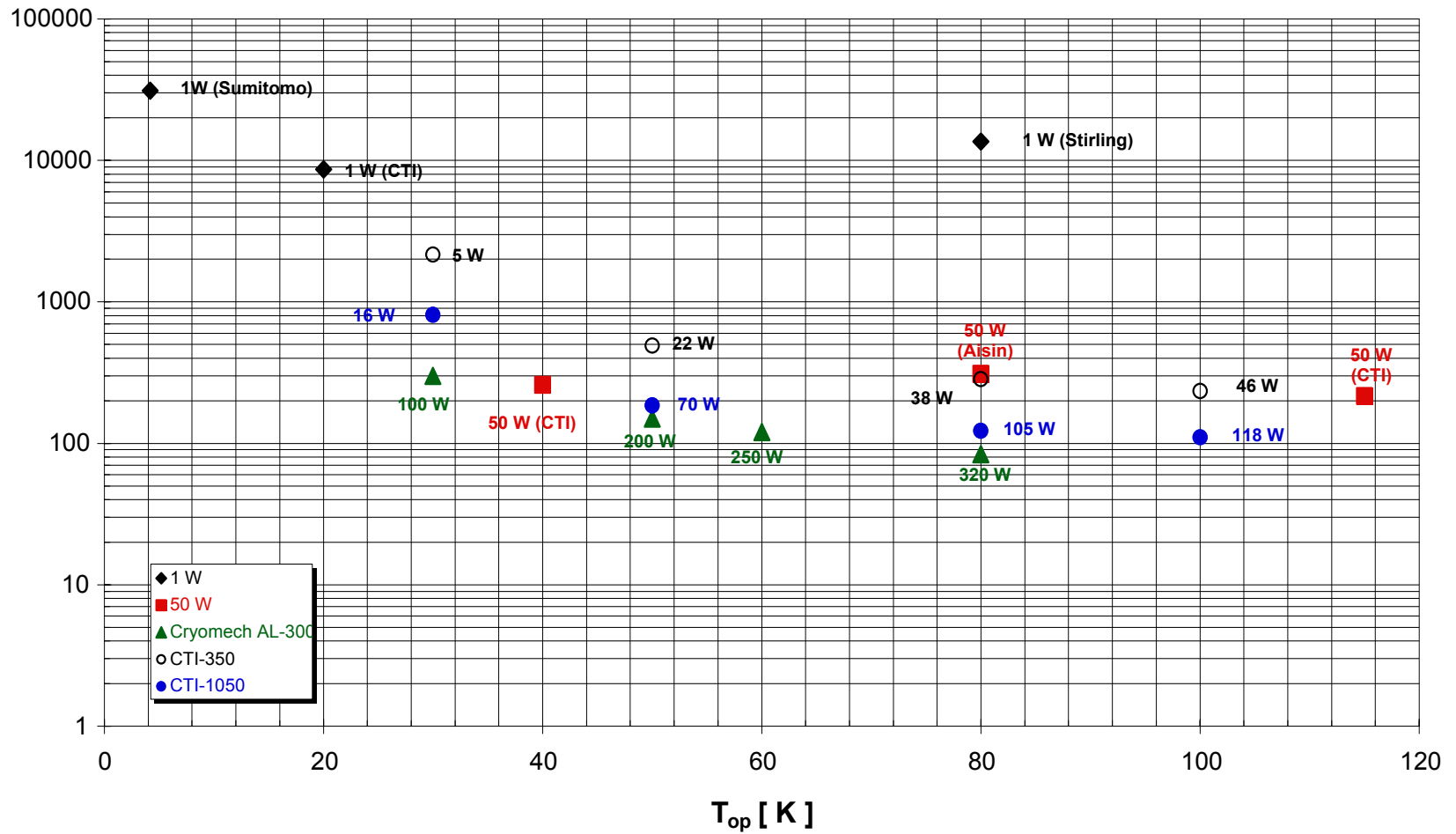
Operation at Cryogenic Temperature

- **Refrigeration and thermal insulation required.**
 - ☆ **Refrigeration power/cost---manageable.**
 - ☆ **Thermal insulation---fundamental hindrance.**
- *Needed: Quantum innovation in insulation technology
---- akin to Dewar's "Thermos" bottle.*

Refrigerator Performance vs. T_{op}



Refrigerator Capital Cost/Cooling Power vs T_{op}



Optimal T_{op} for Minimum Device Cost

Key Parameters

- **Conductor cost (T_{op} ; B ; Size).**
- **Refrigerator capital cost (T_{op} ; Capacity).**
- **Refrigerator operating cost (T_{op} ; Capacity).**
- **Stability/protection cost (T_{op} ; B ; Size)**
 - ☆ **normal metal (stability/peak voltage)**
→ reduced J_e → increased device cost.
 - ☆ **Cooling medium (high voltage): vapor, liquid, solid**
- **Mechanical integrity cost (J_e ; B ; Size).**

Economics of Large-Scale HTS Devices

Enabling vs Replacing Technology

<i>Technology</i>	<i>Performance</i>	<i>Competition</i>	<i>Criterion</i>
Enabling	Yes	No	Performance
Replacing	No	Yes	Cost

Large-Scale Superconducting Devices

Electricity

- **Fusion; SMES; Generator ; Cable; Transformer; FCT; Motor.**

Medicine

- **MRI.**

Research

- **HEP; NMR/MRI; High-*B* DC Magnets.**

Is Superconductivity Enabling?

<i>Technology</i>	<i>In General</i>	<i>Yes...only</i>
Fusion	Yes*	> 2050
SMES	Yes*	“Large” Wh
Cable	No	“Large” VA
Transformer	No	“Compact”
FCL	No	“Compact”
Motor/Generator	No	“Compact”

* *Not enabling* as a power converter or energy storage.

Is Superconductivity Enabling?

(continued)

<i>Technology</i>	<i>In General</i>	<i>Yes...only</i>
MRI (medicine)	Yes	> 0.5 T
HEP	Yes	> ~1 TeV
NMR/MRI	Yes	> 2 T / > 0.5 T
High-<i>B</i> DC Magnet	Yes	> 2 T

Development Steps to Commercial Product

- **Step-by-step progression from small to large units.**
- **Continued development likely if the completed unit at each step serves the user.**
- **Desirable if the cost of each upgrade unit is *reasonable*, i.e. \$Ms rather than \$100Ms or \$Bs.**

Minimum Size Serviceable to the User

<i>Technology</i>	<i>Minimum Size</i>
Fusion	100-300 MW
SMES	0.1-1 GW h
Cable	0.5-1 GW; 1-2 km
Transformer	30 MVA
FCL	0.1-1 GVA
Motor/Generator	1 kHp / 300 MVA

Minimum Size Serviceable to the User
(continued)

<i>Technology</i>	<i>Minimum Size</i>
MRI (medicine)	> 0.3 T
HEP	> 1 TeV
NMR/MRI	> 2 T/ > 0.5 T
High-<i>B</i> DC Magnet	> 2 T

Fusion (& SMES)

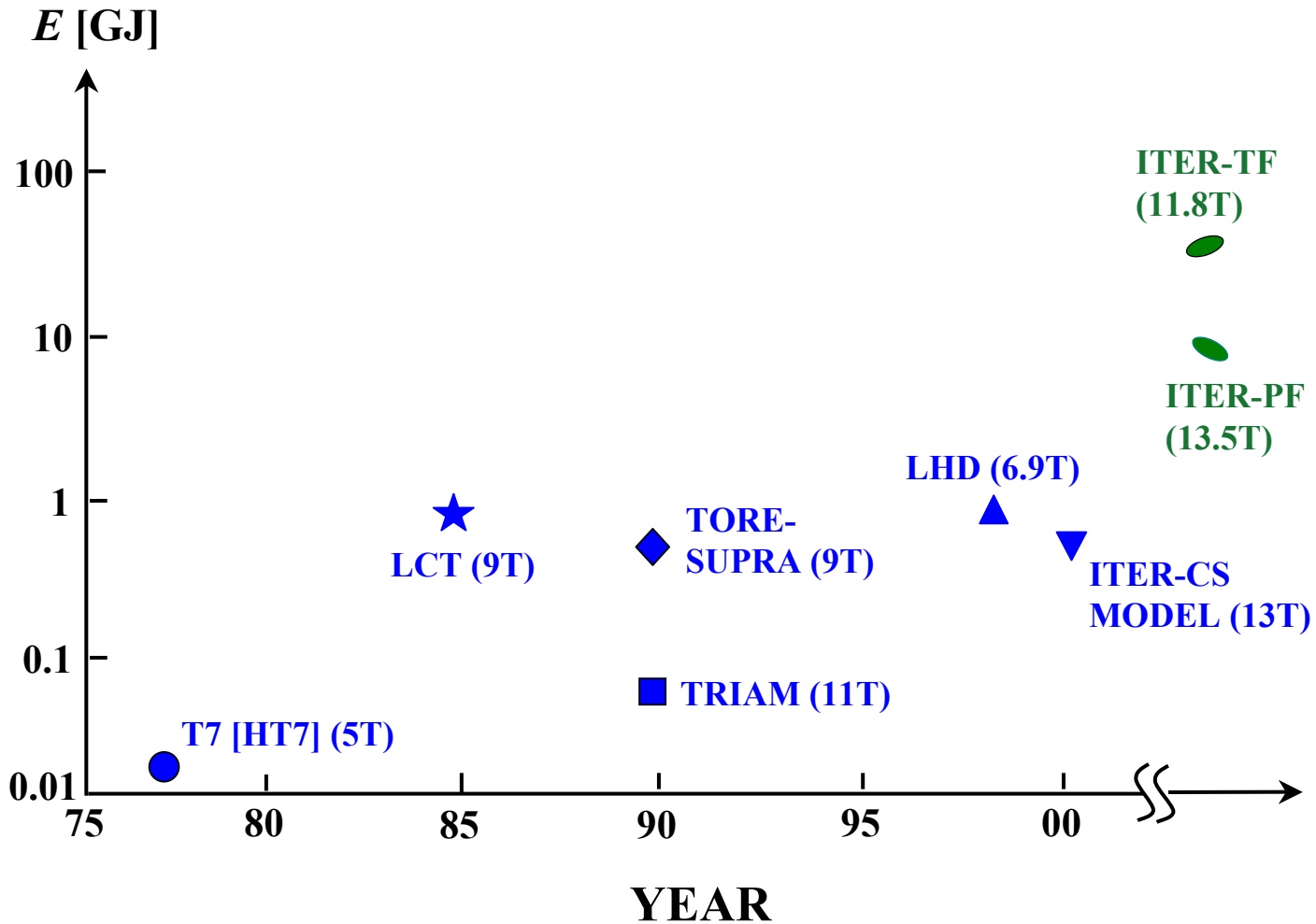
Disadvantages

- Unit must be huge, *i.e.*, **expensive**, to serve the user.
Even ITER (\$10B) still just a demonstration unit.
(Essentially the same with SMES.)

Prognosis

- May become a necessity, *i.e.*, an **enabling power converter**, after 2050. (SMES: ~2020 or later.)

Superconducting Tokamaks



Other Power Electric Devices

Conditions for Market Penetration

- “Promised” HTS, *i.e.*, **much less expensive and with “low” AC losses, must come through.**
- Cryogenics must become “invisible.”
 - ☆ **For most “large” devices, cost NOT an issue.**

HEP

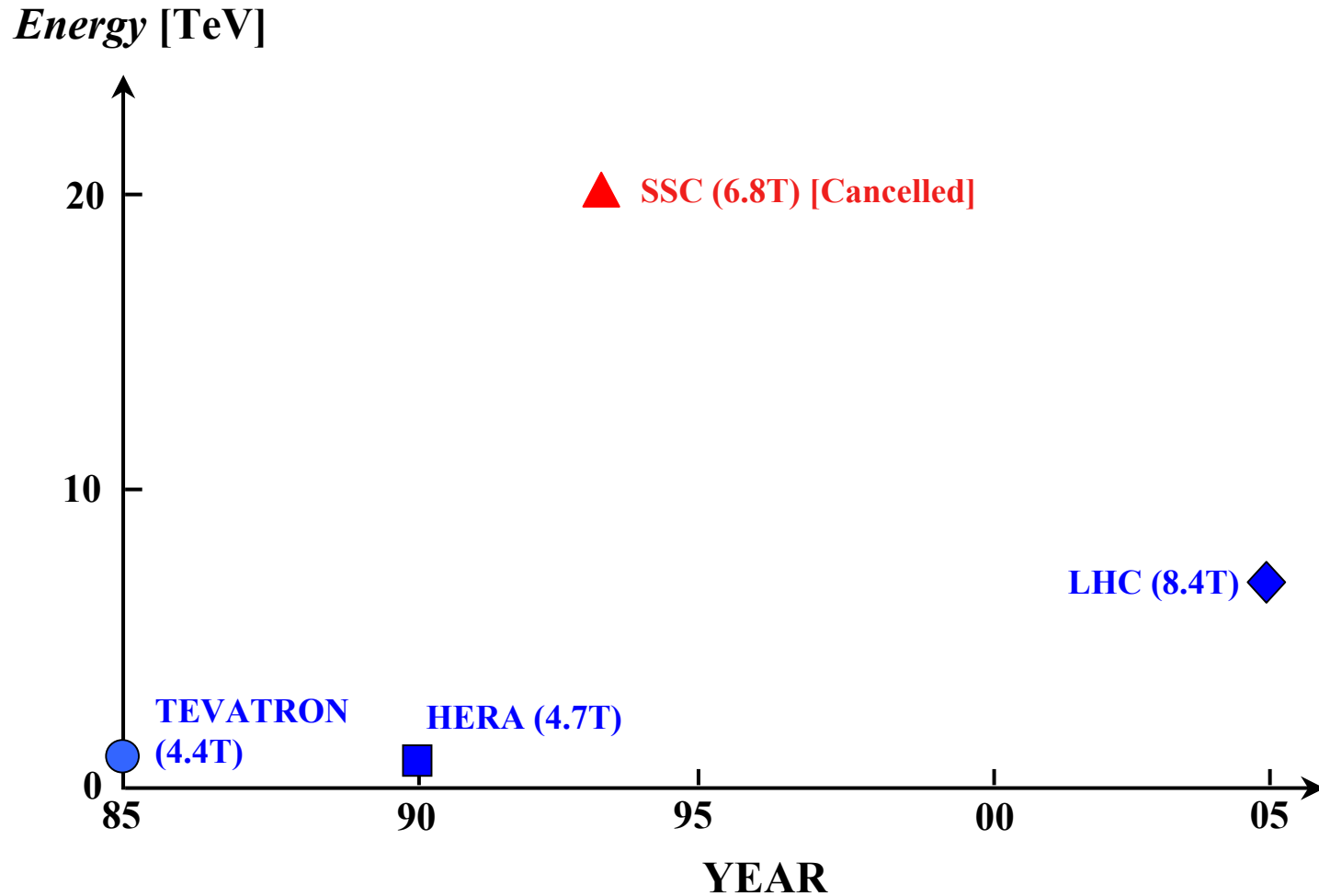
Reason for the SSC demise in 1993

- **Cost overrun, \$5B (1986) to ~\$15B (1993).**

“Smaller” Accelerators successful

- **Tevatron: $\pi D_{av}=6.3$ km (vs $\pi D_{av}=87$ km for SSC).**
- **LHC: $\pi D_{av}=27$ km.**

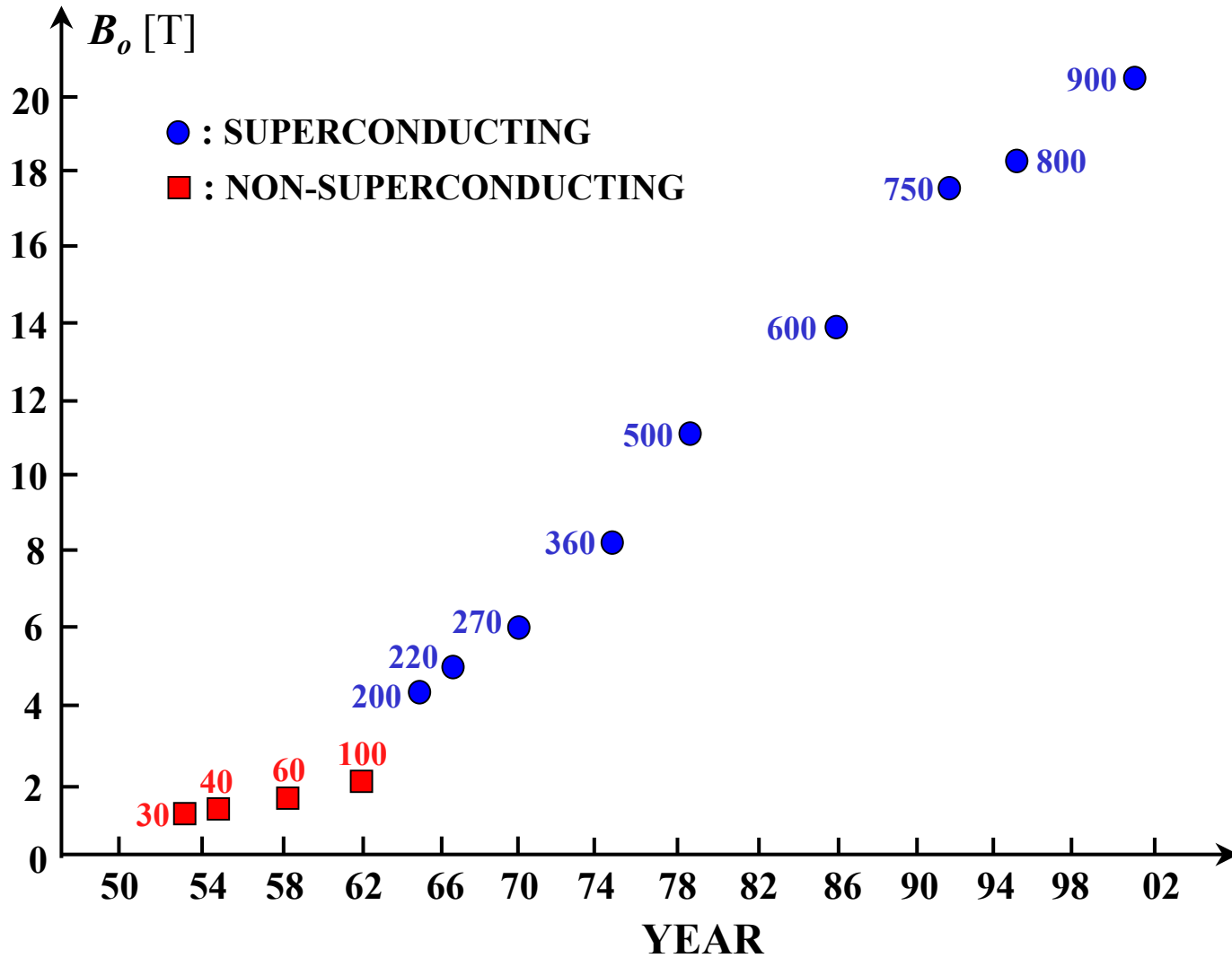
Superconducting Accelerators



NMR/MRI

- **Upward march, through step-by-step upgrading.**
- **Unit at each step serviceable to the user.**
- **Each upgrade \$Ms rather than \$100Ms to \$Bs.**

Progress of NMR



High-B DC Magnets

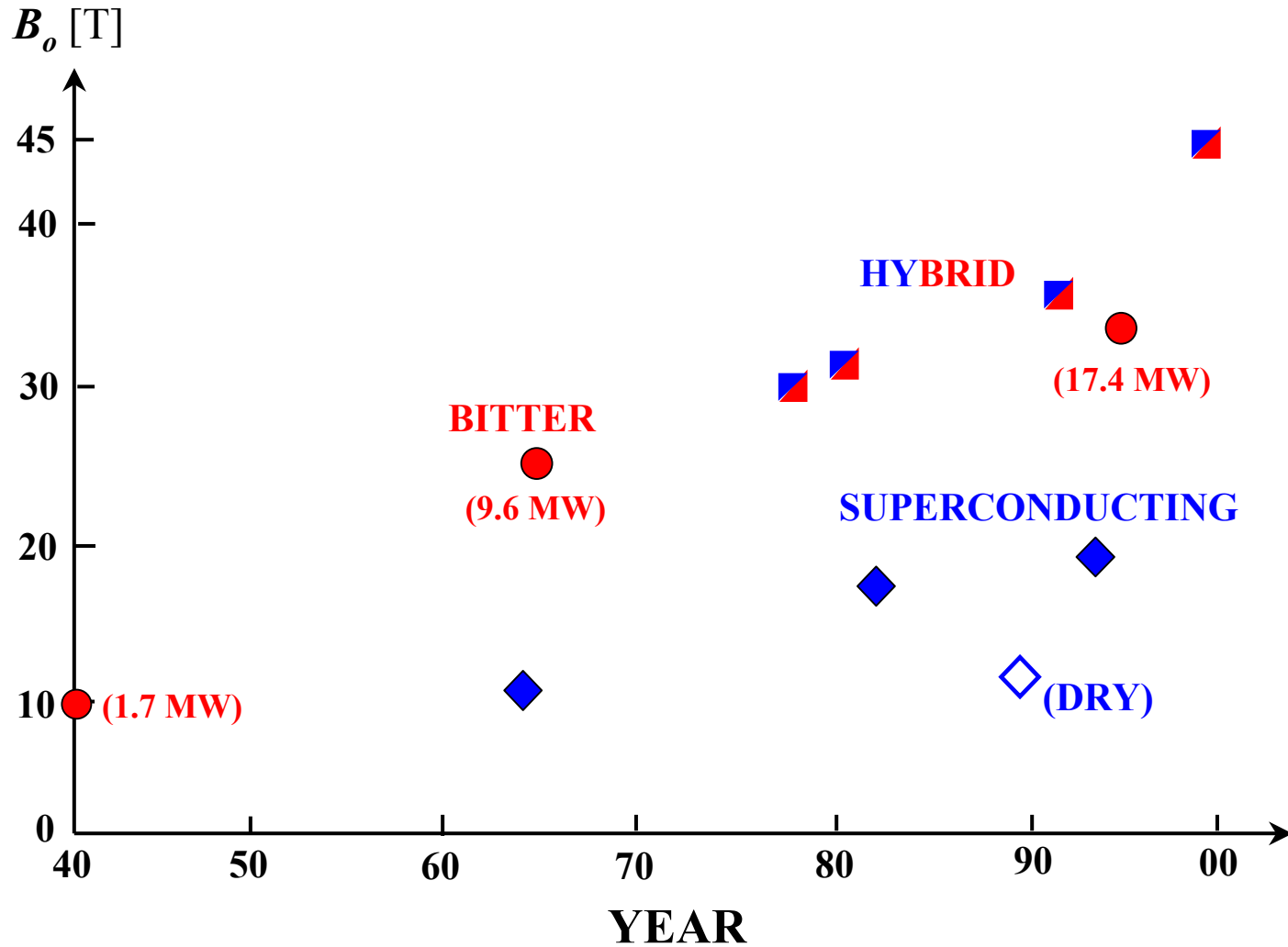
R&D Driven

- Started initially as “Bitter” magnets (>1930s).
- Superconducting magnets (>1960s)
- Hybrid magnets (>1970s).

Commercial

- Available starting in the 1970s.
- Now generally “dry,” up to ~10 T.

High-B DC Magnets



Activities: Past and Present

<i>Technology</i>	<i>1980s</i>	<i>1990s</i>	<i>2002</i>
Fusion	↗	↗	↗
Electrical Devices	→	↗	↗
MRI (medicine)	↗↗	↗↗	↗↗
HEP	↗	↗	↗
NMR/MRI	↗↗	↗↗	↗↗
High-<i>B</i> DC Magnet	↗↗	↗↗	↗↗

↗ : R&D; → : Dormant; ↗↗ : Commercial products

Research Areas in HTS Magnet Technology

Stability/Protection

- **Quench/recovery behavior of conductor subject to fault-mode type disturbances---includes e_{\min} ; NZP velocities.**
- **Detection of a localized hot zone.**

AC Losses

- **Measurement techniques.**
- **Reduction---through conductor fabrication?**

Current Activities at FBML

Stability/Protection

- **Response of YBCO tape to an over-current pulse:
LN2 bath and forced-flow cooling.**

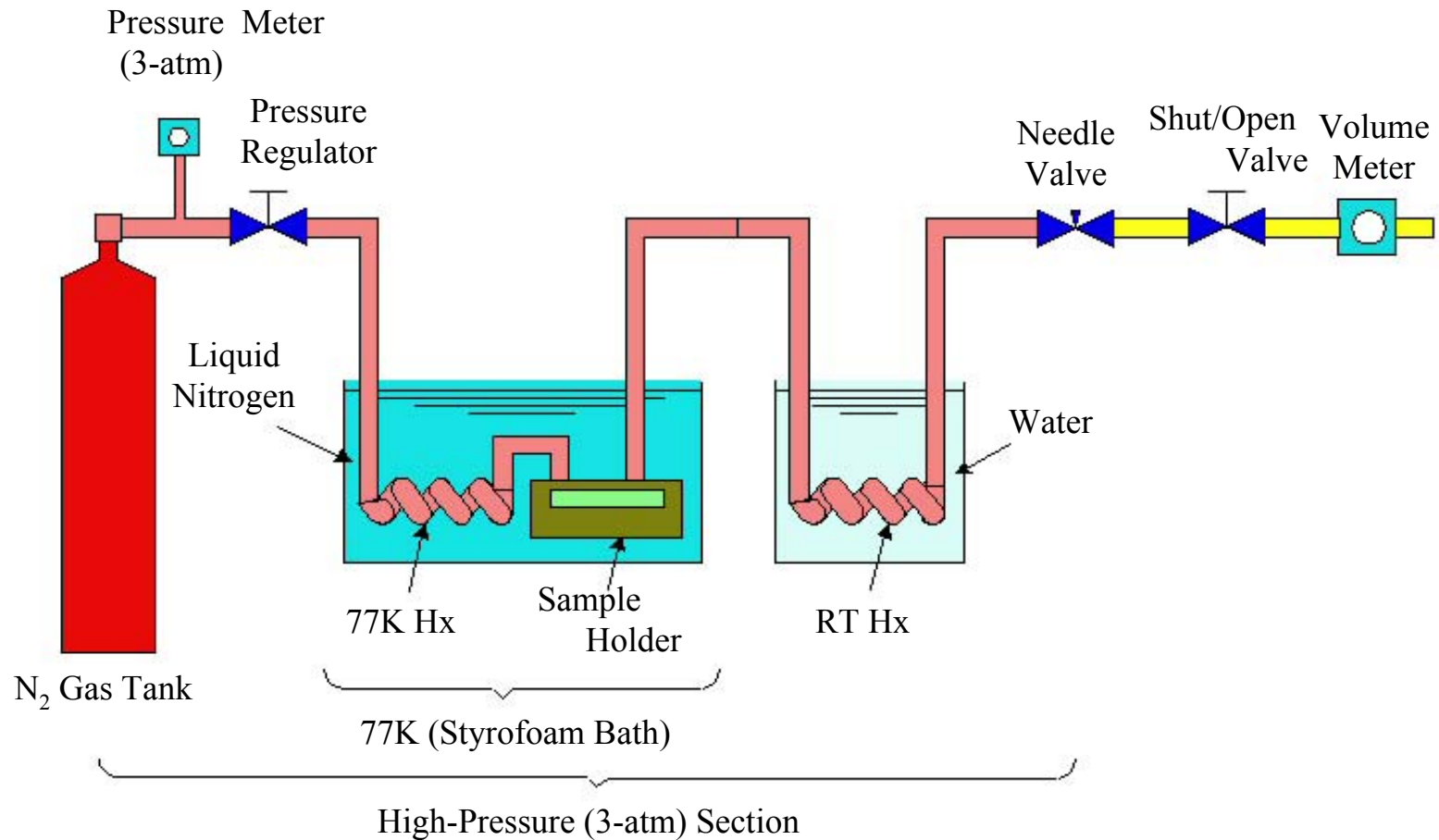
Detection of a Hot Zone

- **AE technique---new activity (08/02 →).**

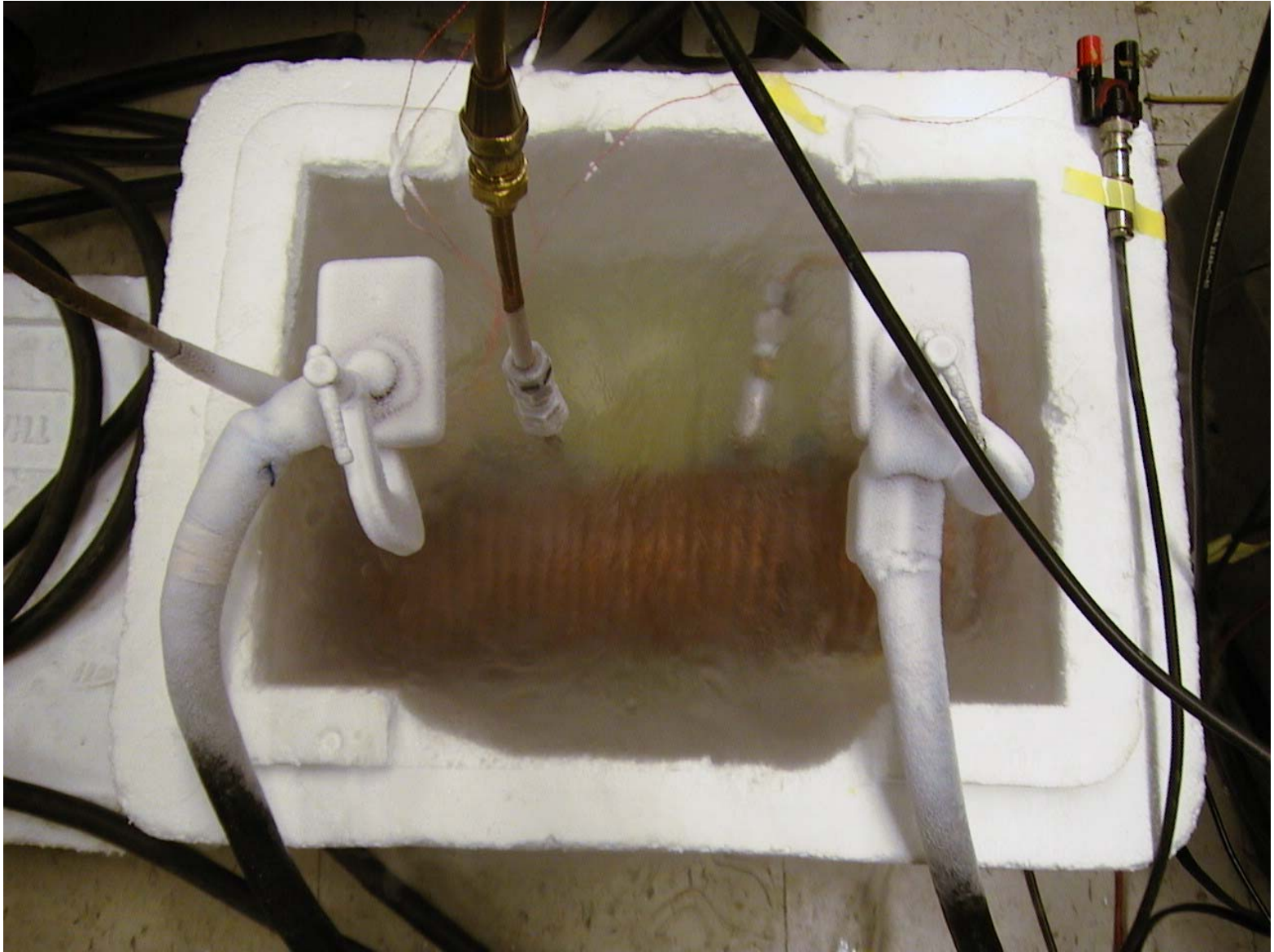
Quench/Recovery: Experiment & Simulation

- **Bath cooling @77 K.**
- **Forced-flow cooling @ 2-3 atm 80-81 K.**

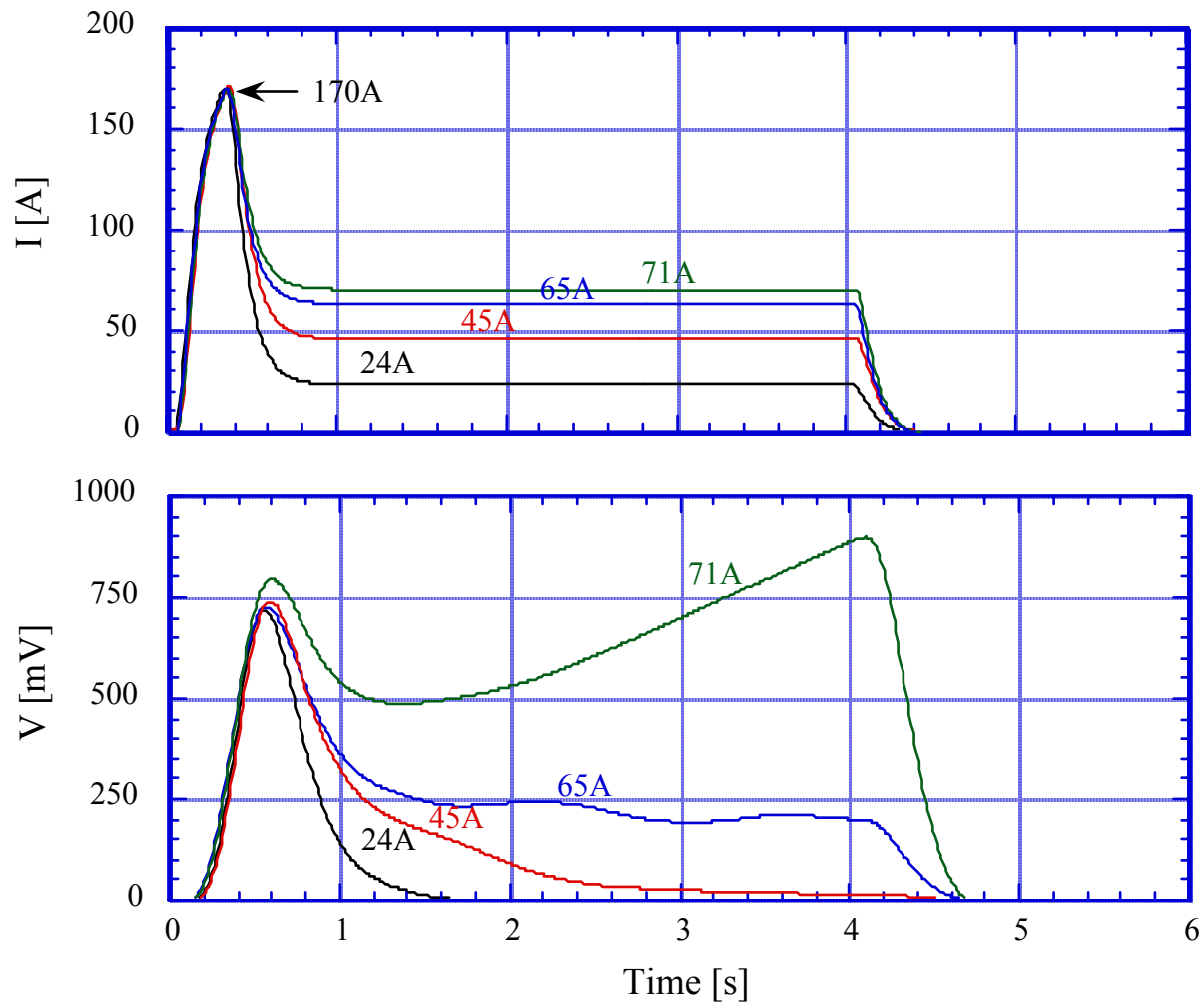
Forced-Flow Experimental Setup



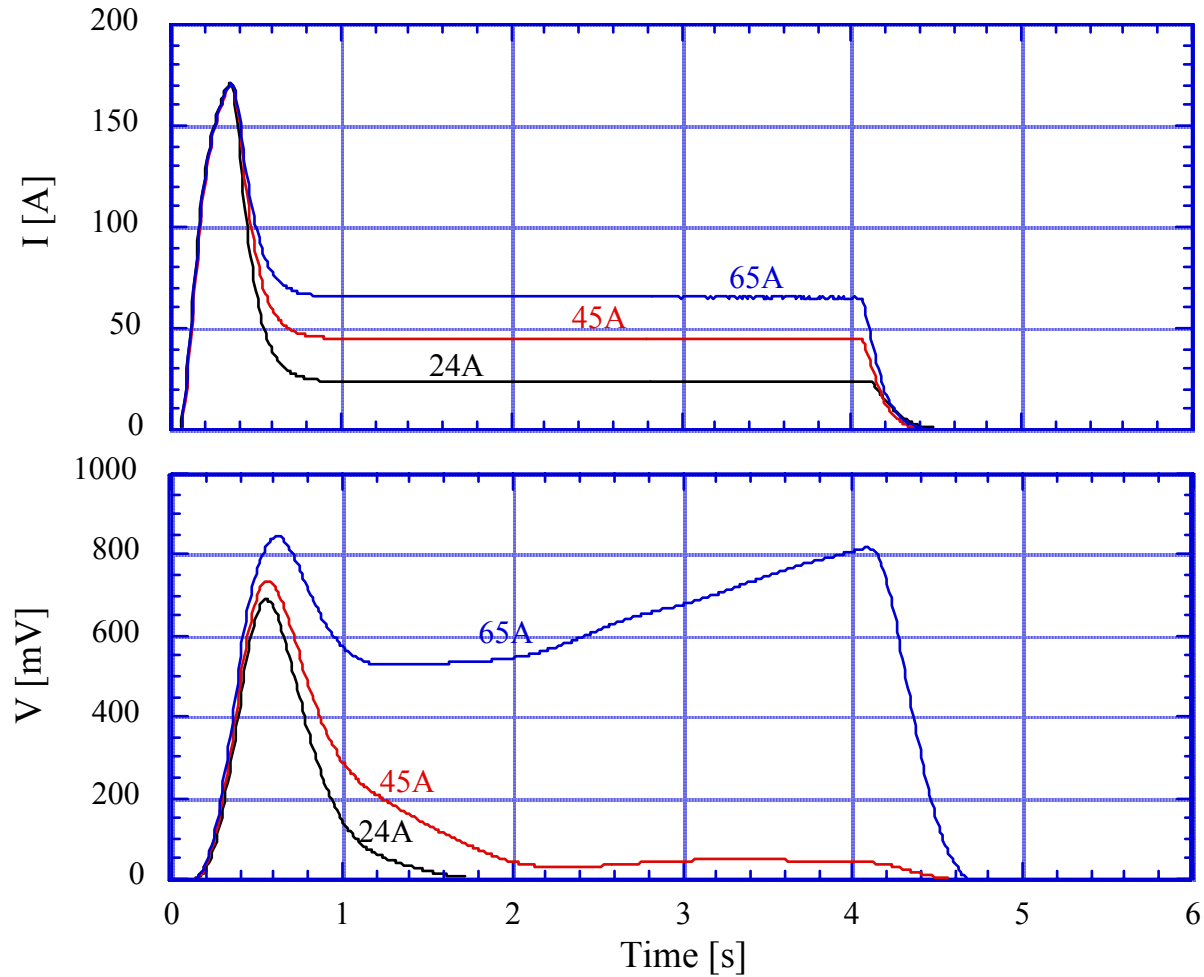




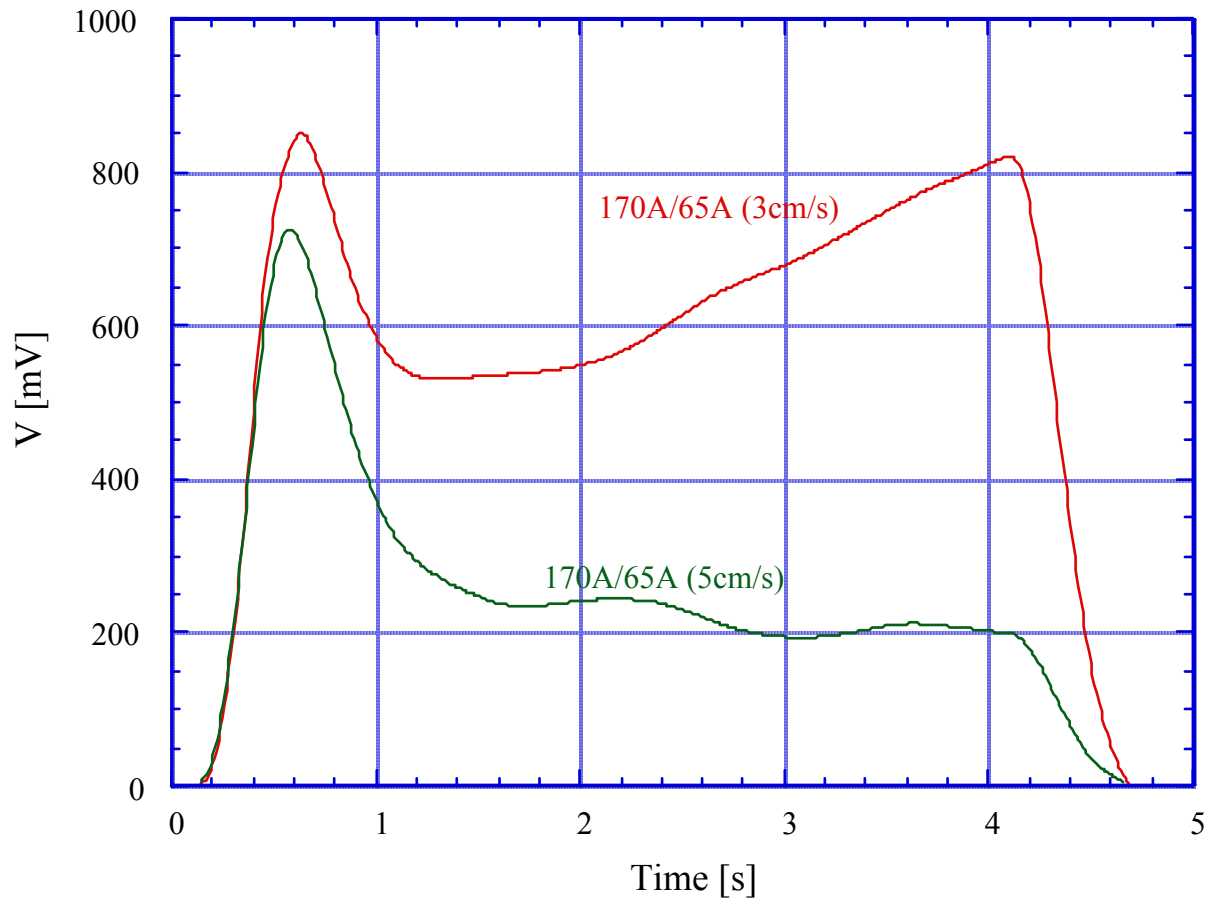
Sample 2: Forced-Flow (~ 81 K; 5 cm/s)



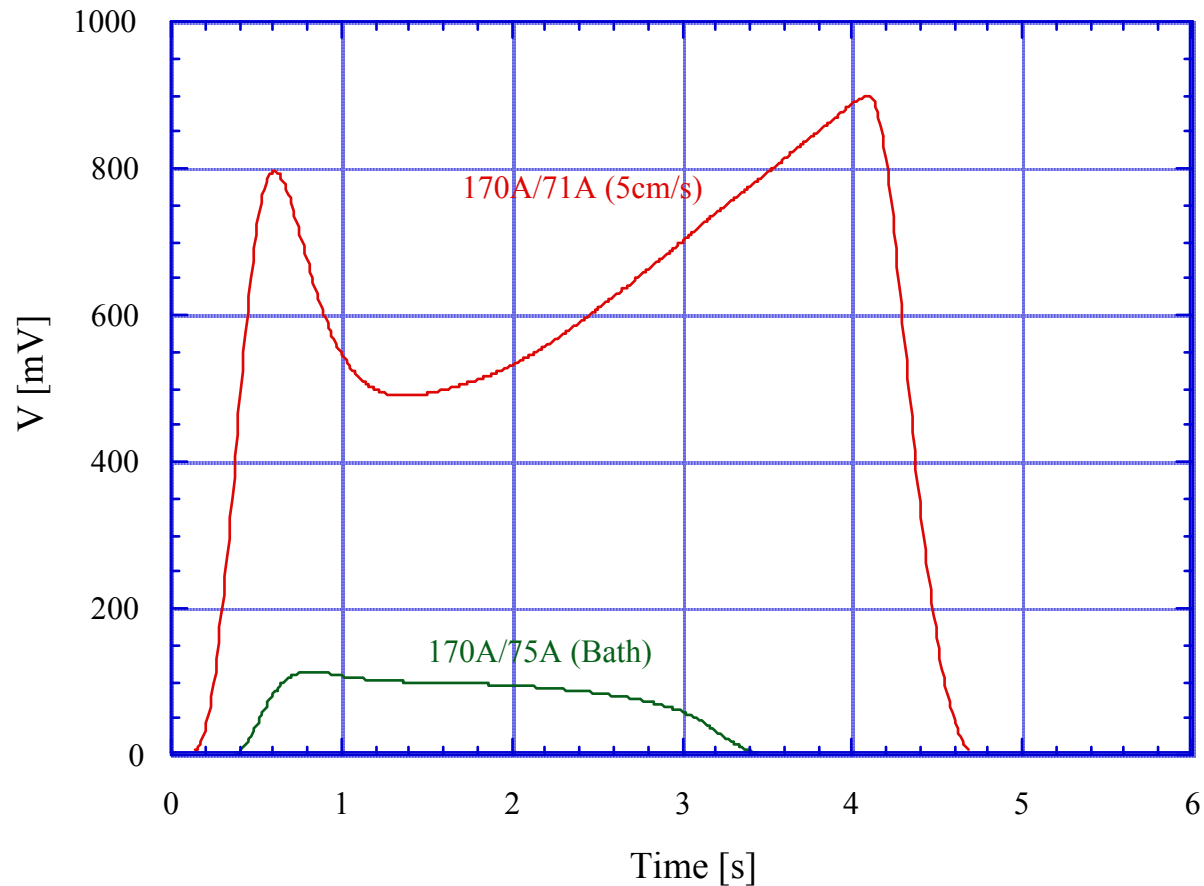
Sample 2: Forced-Flow (~ 81 K; 3 cm/s)



Sample 2: Forced-Flow (@81 K)



Sample 2: Forced-Flow (5 cm/s) & Bath



Simulation

$$Q = \dot{h} A_s \Delta T_w = \dot{h} A_s (T_w - T_f)$$

$$\dot{h} = \frac{kNu}{D}$$

Re \geq 3000, turbulent flow

$$Nu = 0.023 Re^{0.8} Pr^{0.3}$$

Re < 3000, laminar flow

$$Nu = 3.66 + \frac{0.0668 (D / L) Re Pr}{1 + 0.04 [(D / L) Re Pr]^{2/3}}$$

Nitrogen Properties at 2 bar (From Handbook of Cryogenic Engineering, I. G. Weisend II, 1998)				
T(K)	ρ (kg/m ³)	Cp(j/kg K)	μ (Pa s)	κ (W/m K)
83.0	779.9	2079	0.1228×10^{-3}	0.1247
84.0	8.628	1376	0.5791×10^{-5}	0.849×10^{-2}

1-D Power Flux Equation

$$\overline{\delta_{cd}C_{cd}(T)} \frac{\partial T}{\partial t} = \frac{\partial}{\partial x} \left[\overline{k_{cd}(T)} \frac{\partial T}{\partial x} \right] + g_j(T) + g_d(t, x) - q_{n2}(T)$$

$$\overline{\delta_{cd}C_{cd}(T)} = \delta_{ag}C_{ag}(T) + \delta_{sc}C_{sc}(T) + \delta_{ic}C_{ni}(T)$$

$$\overline{k_{cd}(T)} = \frac{\delta_{ag}k_{ag}(T) + \delta_{ic}k_{ic}(T)}{\delta_{ag} + \delta_{ic}}$$

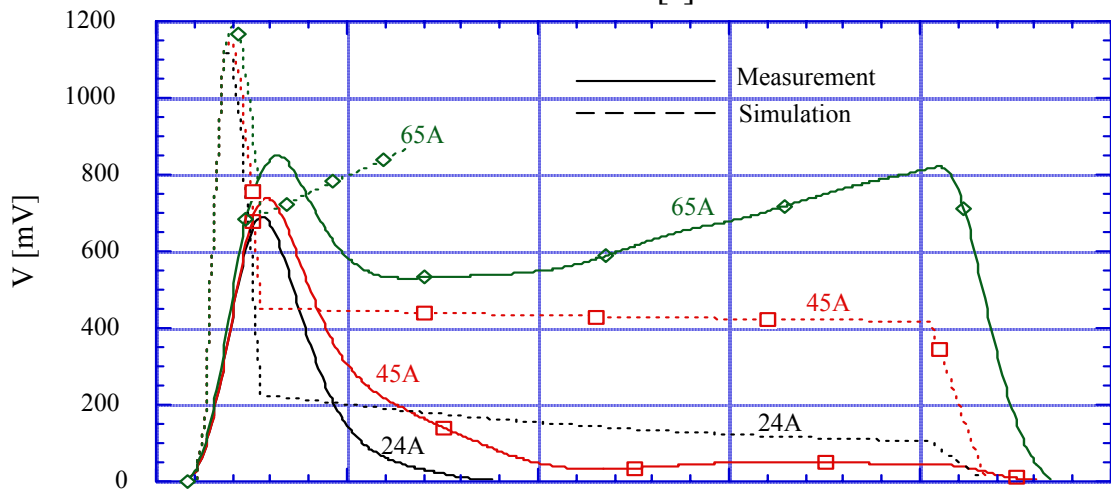
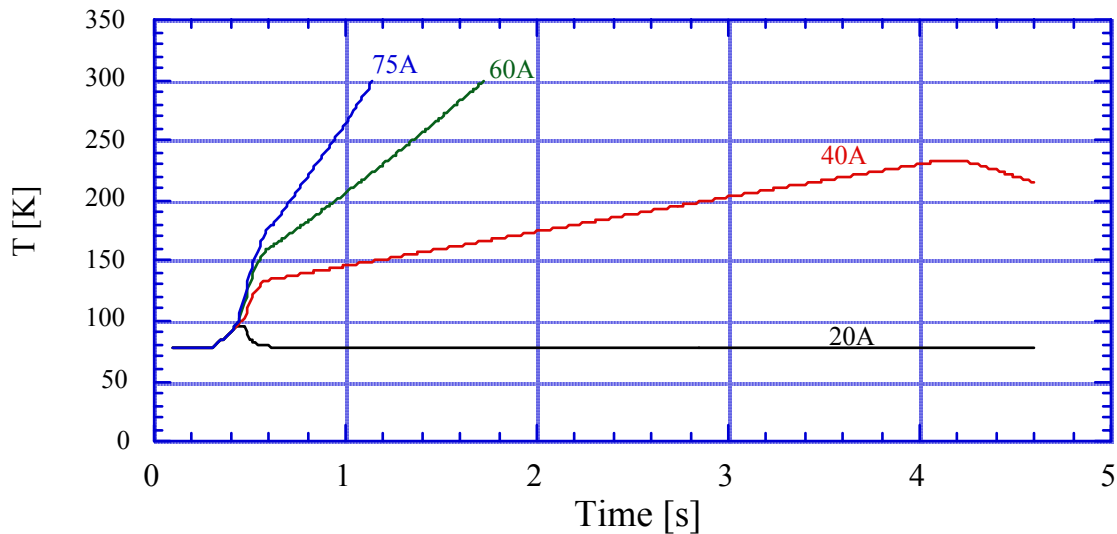
$$g_j(T) = 0 \quad [T_{op} \leq T \leq T_{cs}]$$

$$= \frac{1}{w^2} \left[\frac{\rho_{ag}(T)\rho_{ic}(T)}{\delta_{ic}\rho_{ag}(T) + \delta_{ag}\rho_{ic}(T)} \right] I_t [I_t - I_c(T)] \quad [T_{cs} \leq T \leq T_c]$$

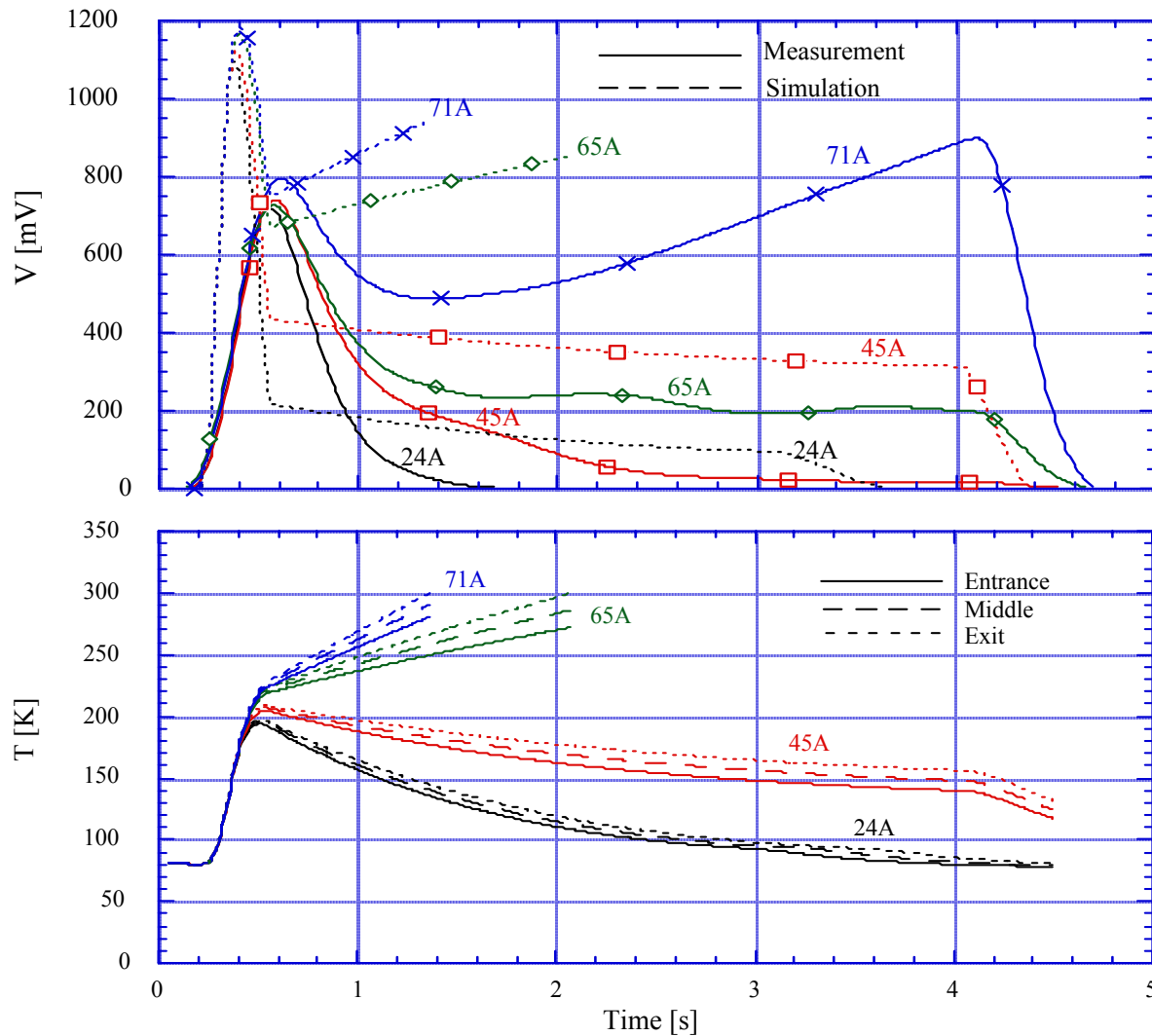
$$= \frac{1}{w^2} \left[\frac{\rho_{ag}(T)\rho_{ic}(T)}{\delta_{ic}\rho_{ag}(T) + \delta_{ag}\rho_{ic}(T)} \right] I_t^2 \quad [T \geq T_c]$$

$I_c(T)$: a linear function (100 A @77 K, sf; @ T_c =93 K).

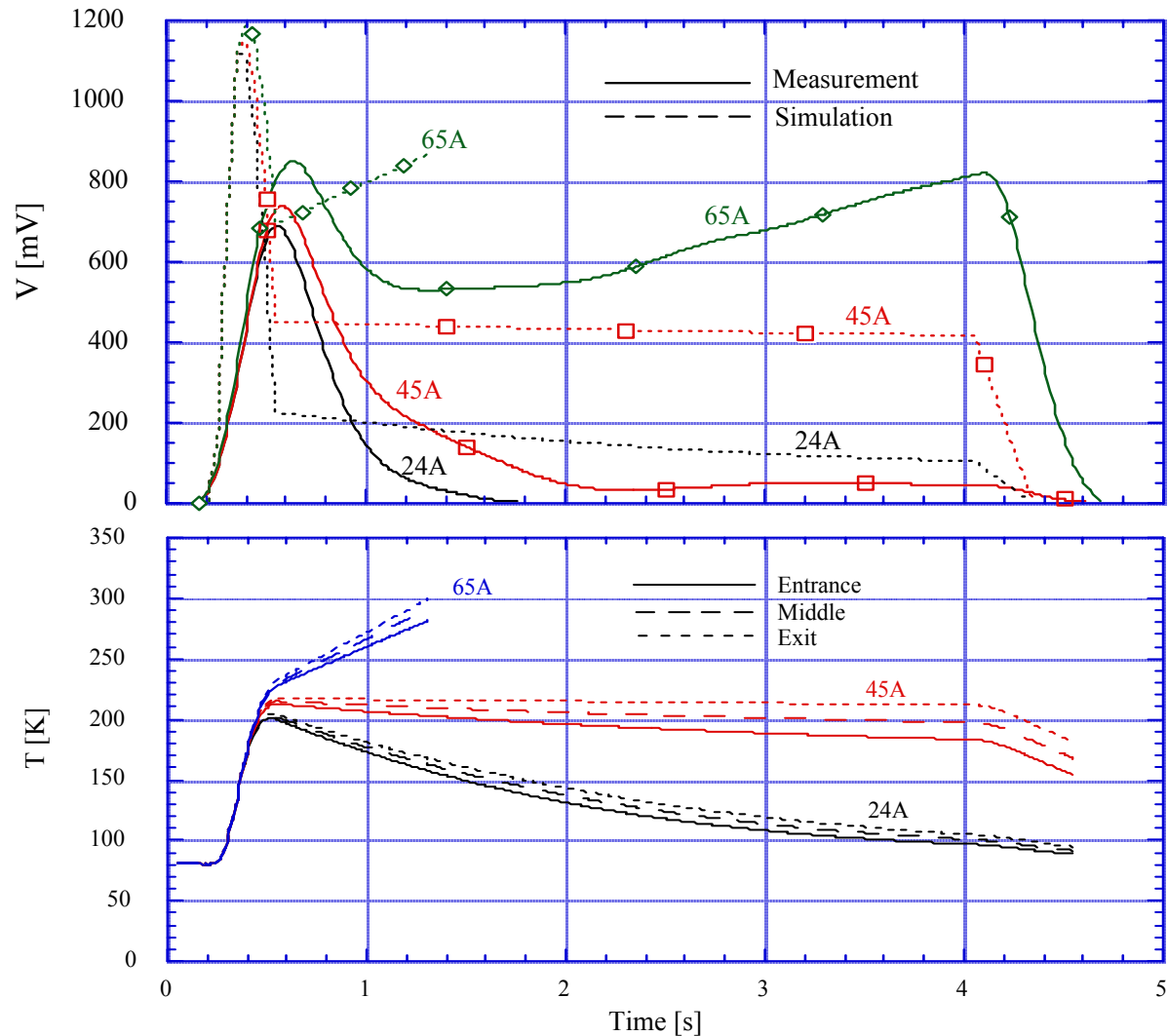
Sample 2: Bath @77 K & Simulation



Sample 2: Forced-Flow (5 cm/s) & Simulation



Sample 2: Forced-Flow (3 cm/s) & Simulation



Preliminary Conclusions

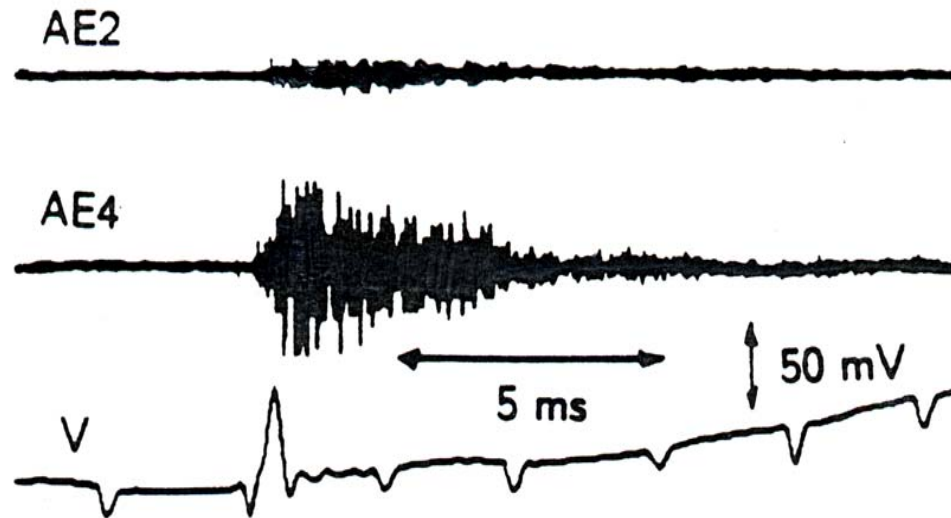
- **Forced cooling ($>3\text{cm/s}$) provides better cooling than bath.**
 - ☆ **Cooling improves with flow velocity.**
- **Simulation requires improvement.**

Detection of a Local Hot Zone with AE

- *AE (Acoustic Emission): Acoustic signals emitted by sudden mechanical events in a body being loaded (stressed) or unloaded.*
 - ☆ Stress can be of mechanical, magnetic, or **thermal**.
- Proven useful for high-performance (adiabatic) LTS magnets in distinguishing **mechanical-disturbance induced quench (AE)** from **I_c -induced quench (no AE)**.

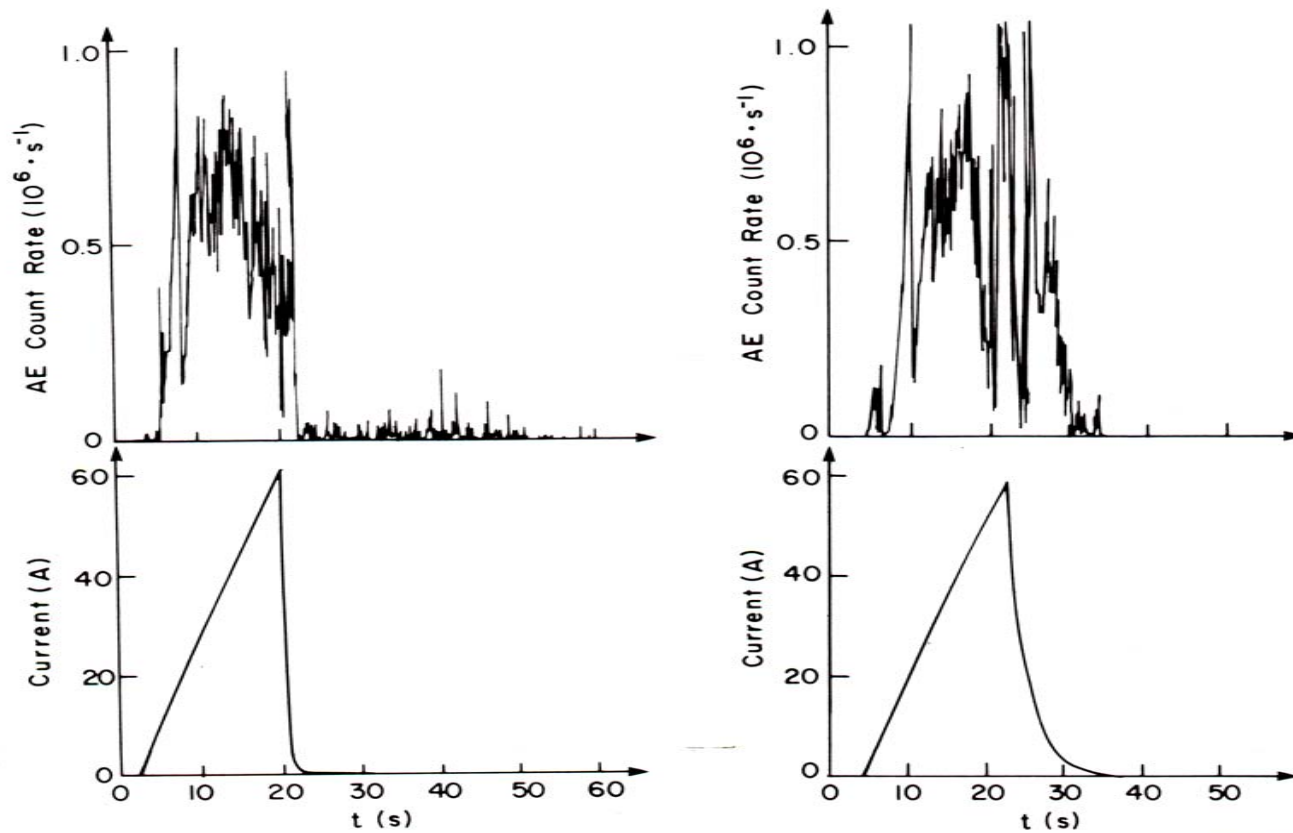
Early (1980s) Examples with LTS (4.2 K) Magnets

1. Conductor-Induced Quench in a Dipole

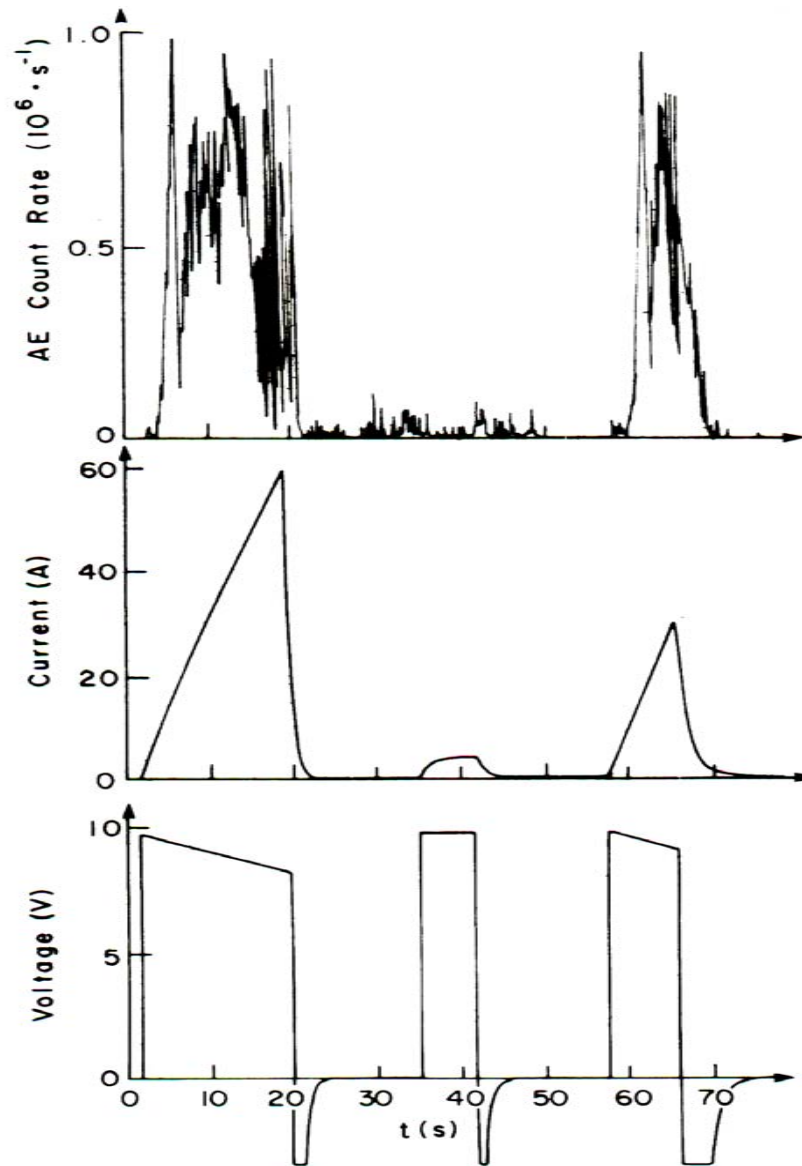


O. Tsukamoto, M.F. Steinhoff, Y. Iwasa (1981)

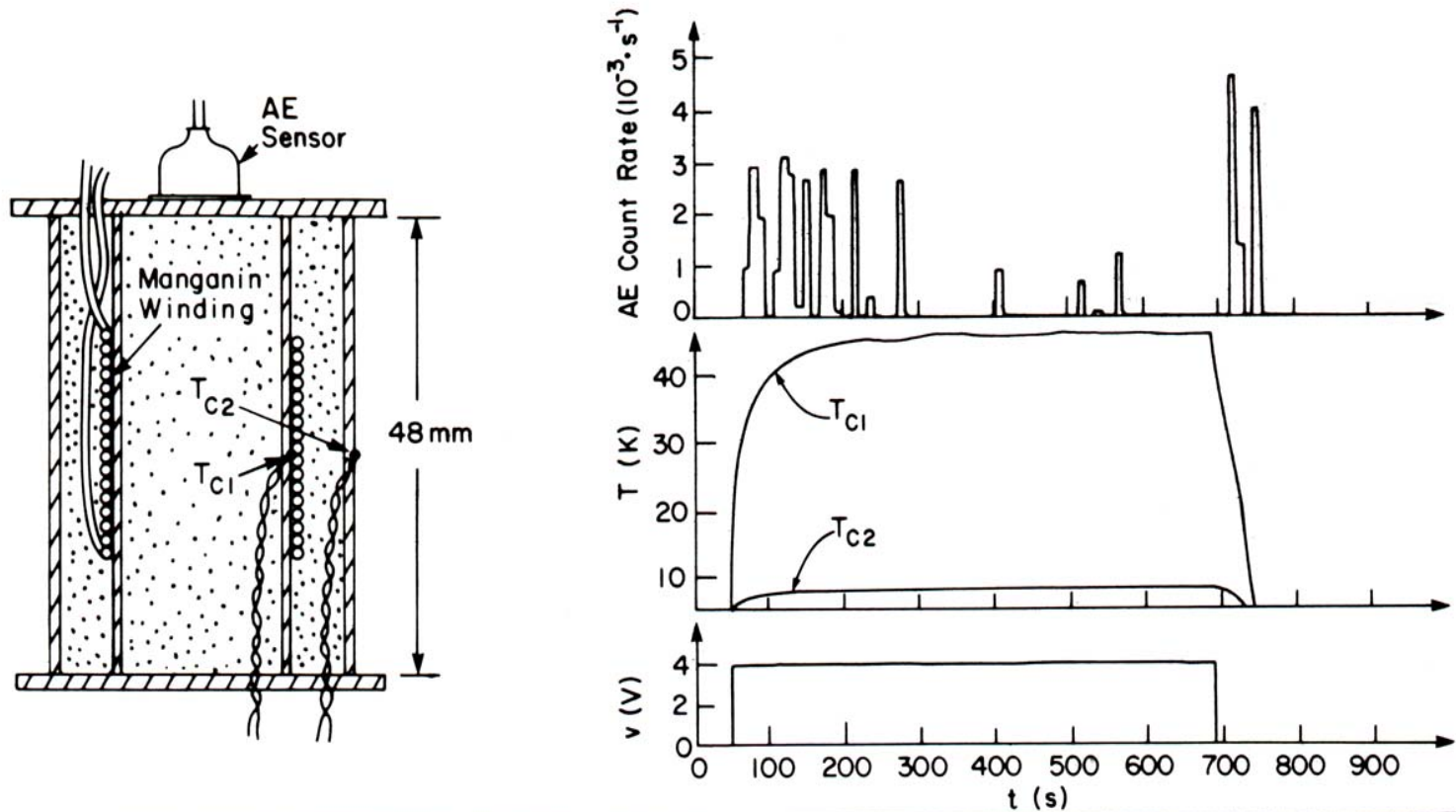
2. ΔT -Induced AE Signals: Magnet Discharge



O. Tsukamoto and Y. Iwasa (1984)



3. ΔT -Induced AE Signals: Heater

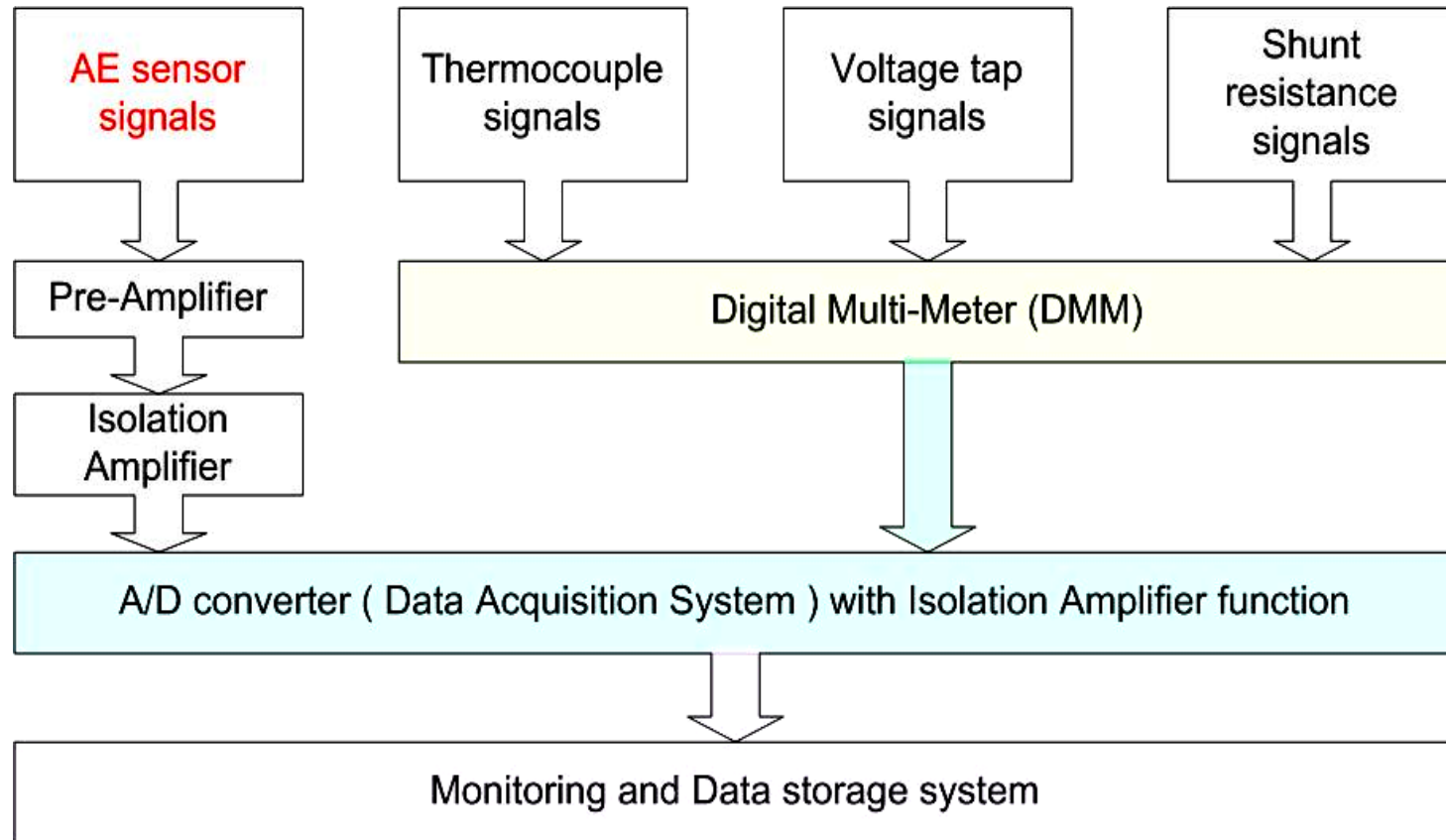


O. Tsukamoto and Y. Iwasa (1984)

Conclusions for LTS & Prospect for HTS

- Normal zone induced heating generates AE signals.
 - ☆ Thermal expansion small at 4.2 K---required $\Delta T \sim 40$ K.
- AE signals diminish as $\Delta T / \Delta t \rightarrow 0$.
- AE sensitivity increases with T_{op} .
 - ☆ AE technique more useful for HTS.

Signal Processing Block Diagram (2002)

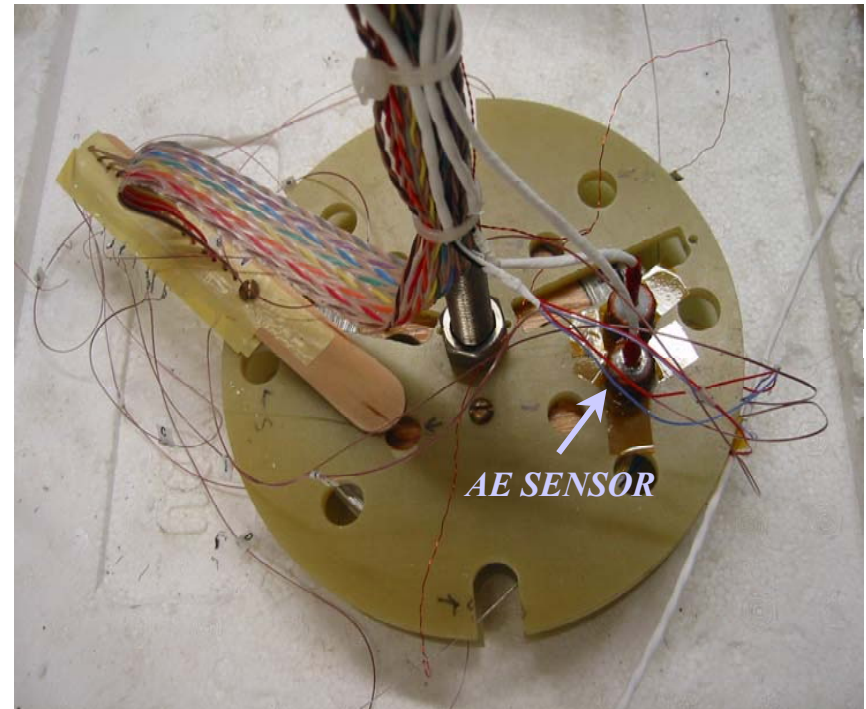


Double-Pancake Test Coil (Bi-2223)

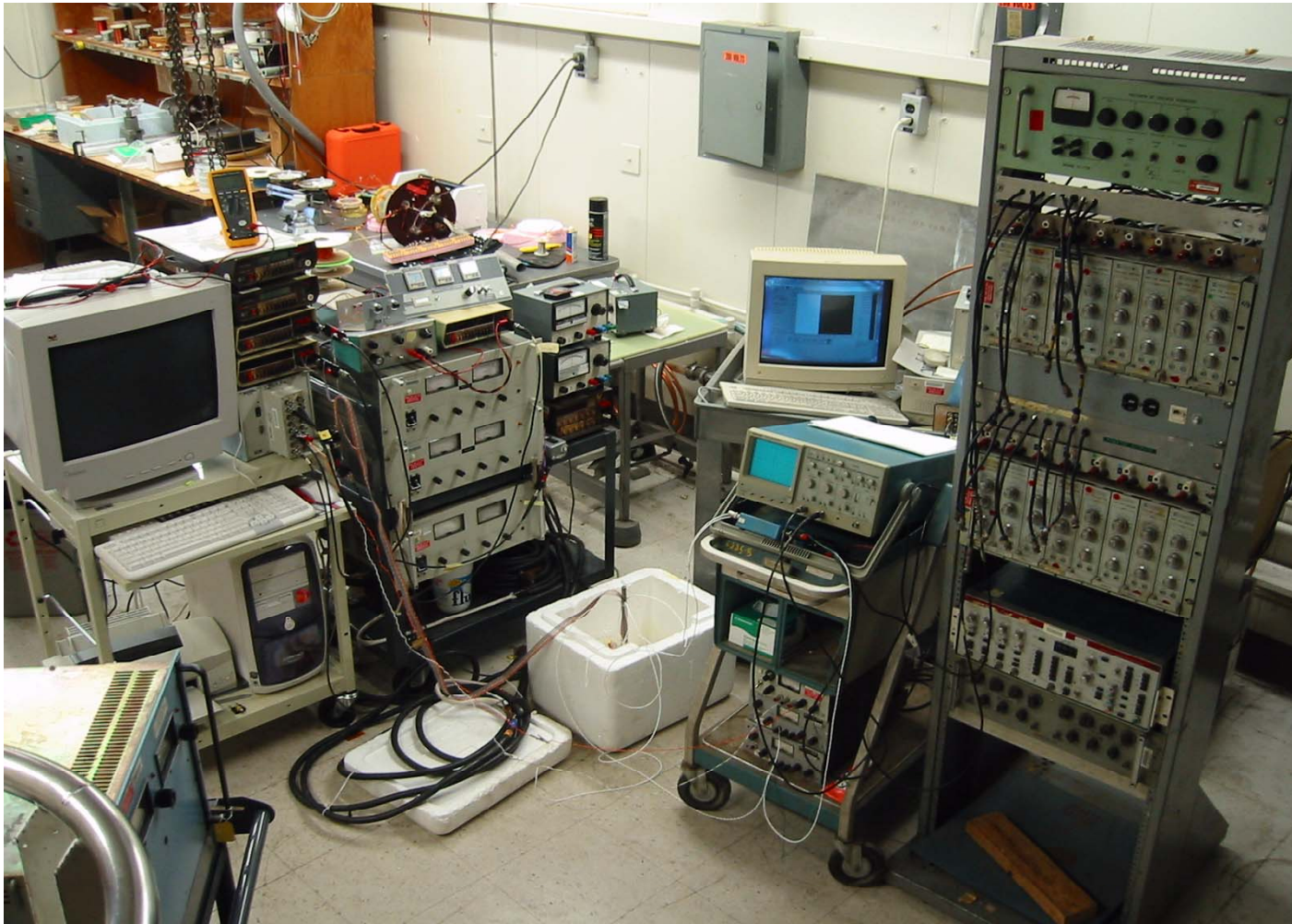
As Wound (o.d.: 12cm)



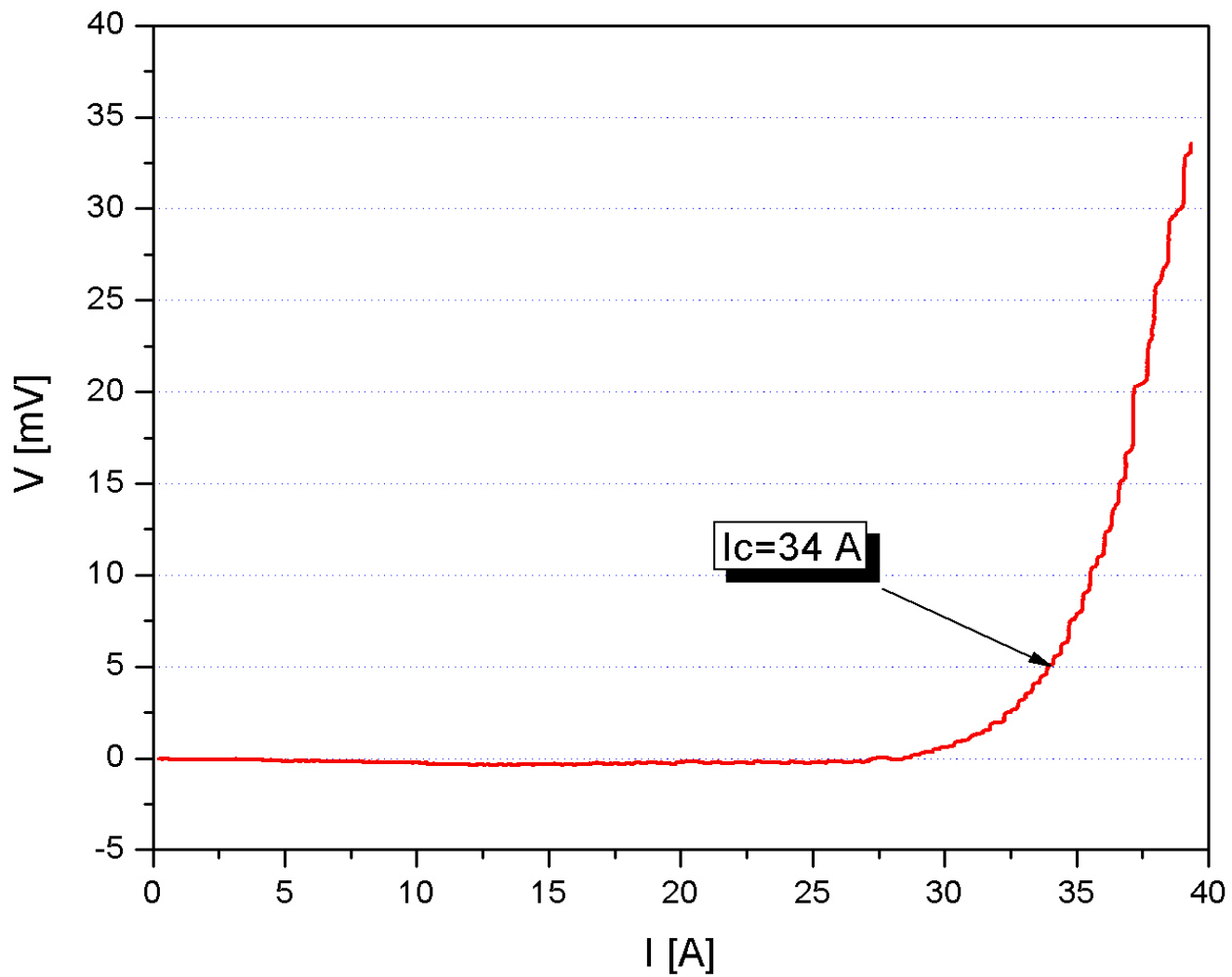
In a Sample holder



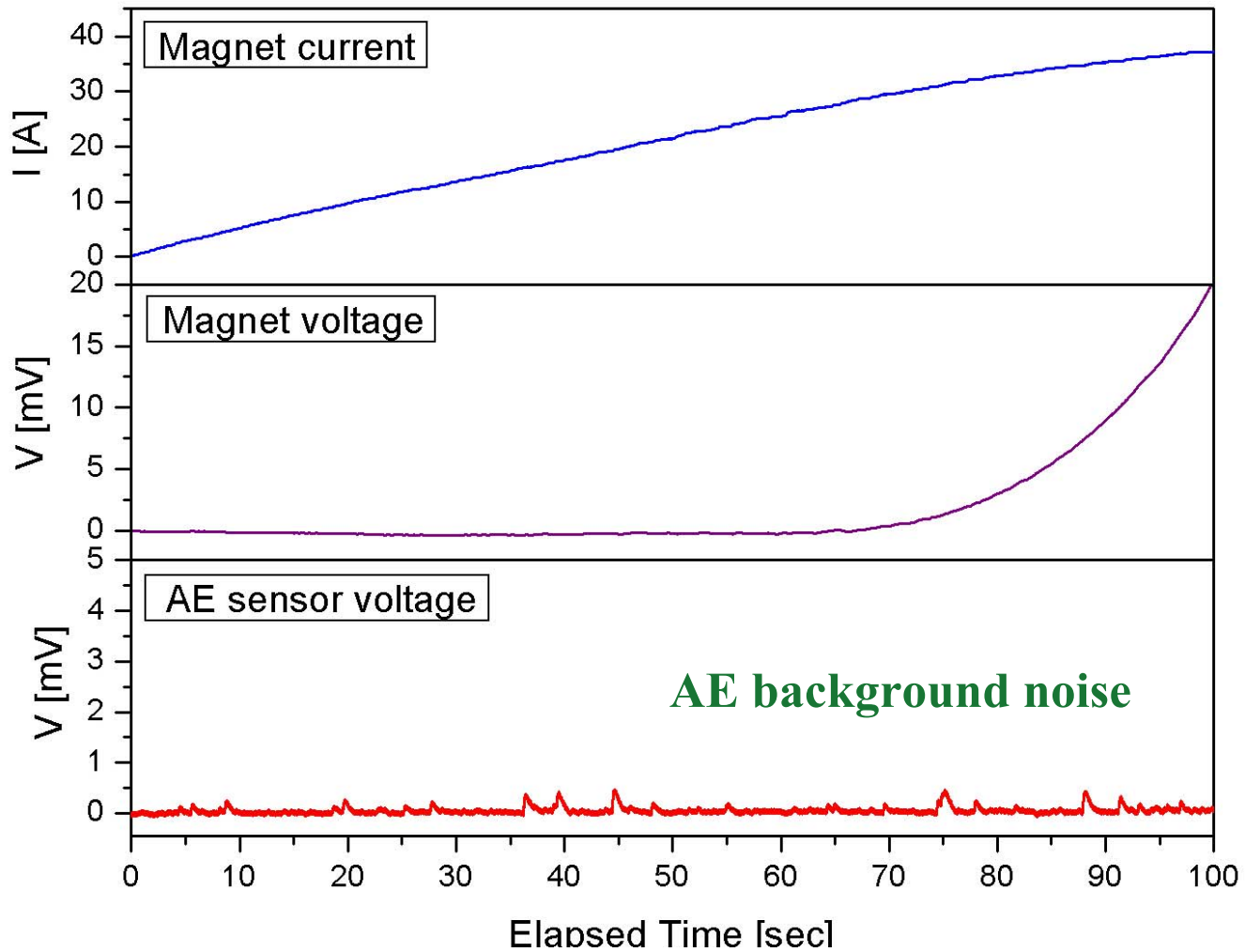
Experimental Setup



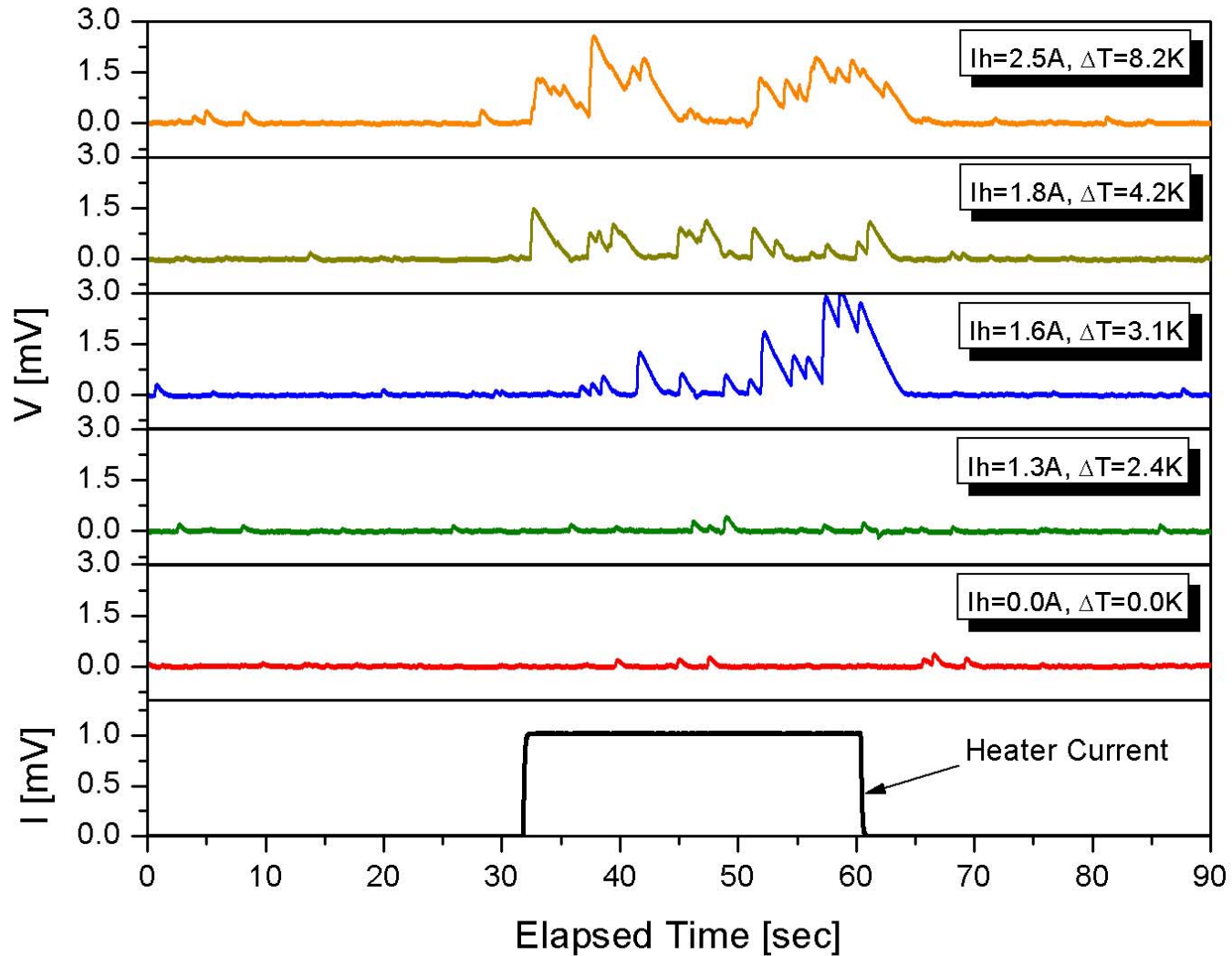
V(I) Plot @ 77 K



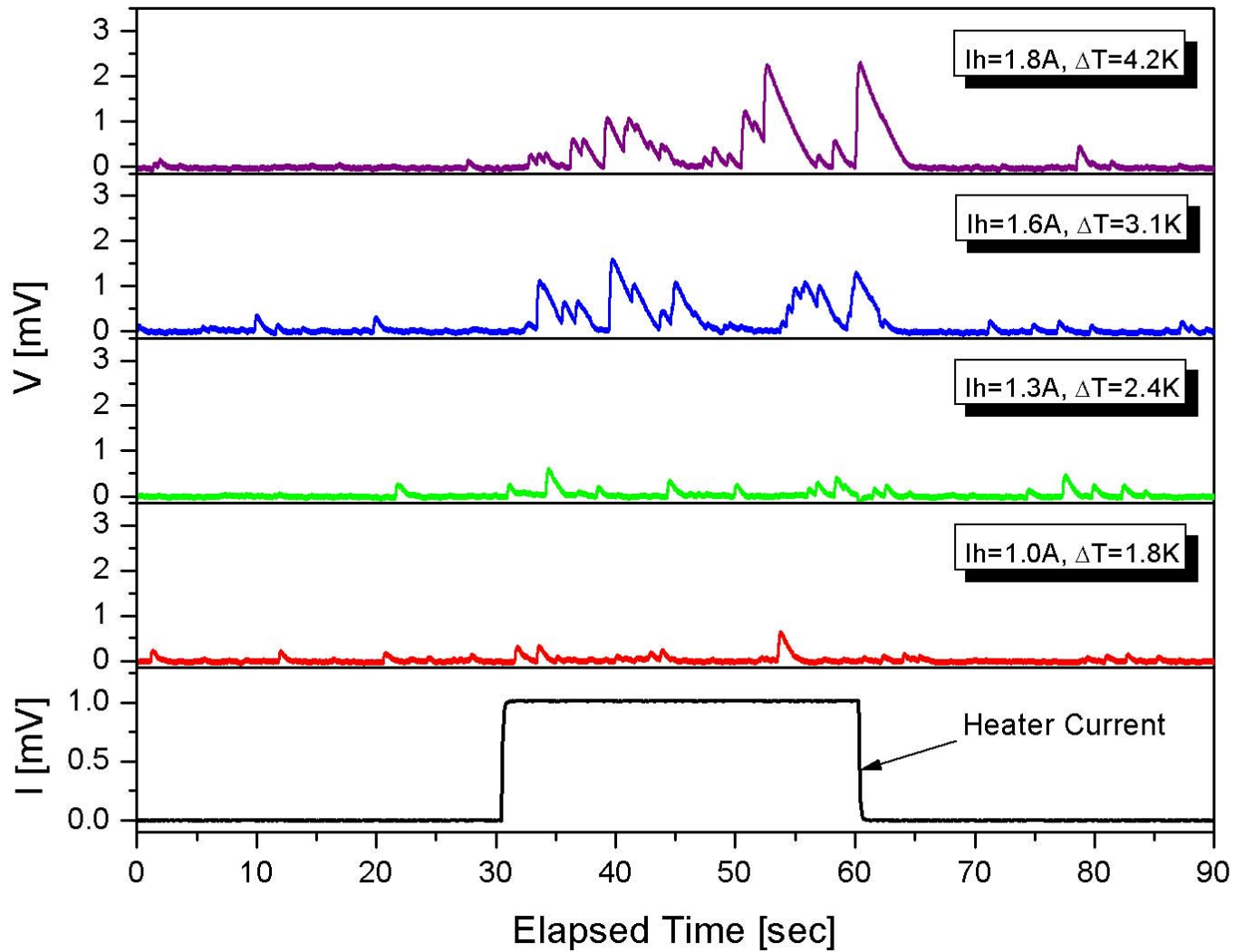
$I(t)$; $V(t)$; and $AE(t)$ Plots @ 77 K



Heating-Induced Data: $I_{op}=15 A$



Heating-Induced Data: $I_{op}=0 A$



Preliminary Conclusions on AE Experiment

- I_c transition does **not** generate AE signals.
 - ★ May generate AE signals if SC/Cu joint overheated.
- **Localized heating ($\Delta T \geq 4$ K) detectable with AE signals even with a test coil immersed in LN2.**
 - ★ ΔT sensitivity may be enhanced in “dry” coils.

Conclusions

HTS Magnet Technology

- **Stability:** **benign under routine conditions**, requires further **simulation/experimental study for fault-mode events**.
- **Protection:** **overheating ; arcing; overstressing key issues**---
HTS J_e likely no greater than LTS J_e .
- **Cryogenics:** **cost likely not an issue**; should become more
“invisible” with innovative insulation techniques.
- **Economics:** market penetration possible by being competitive
in **cost (replacing)** or **performance (enabling)**.
- **Research Areas:** **stability/protection; AC losses**.