
Experimental Study on the Influence of Inter-strand Current Distribution on Current Redistribution and Stability of Superconducting Cables

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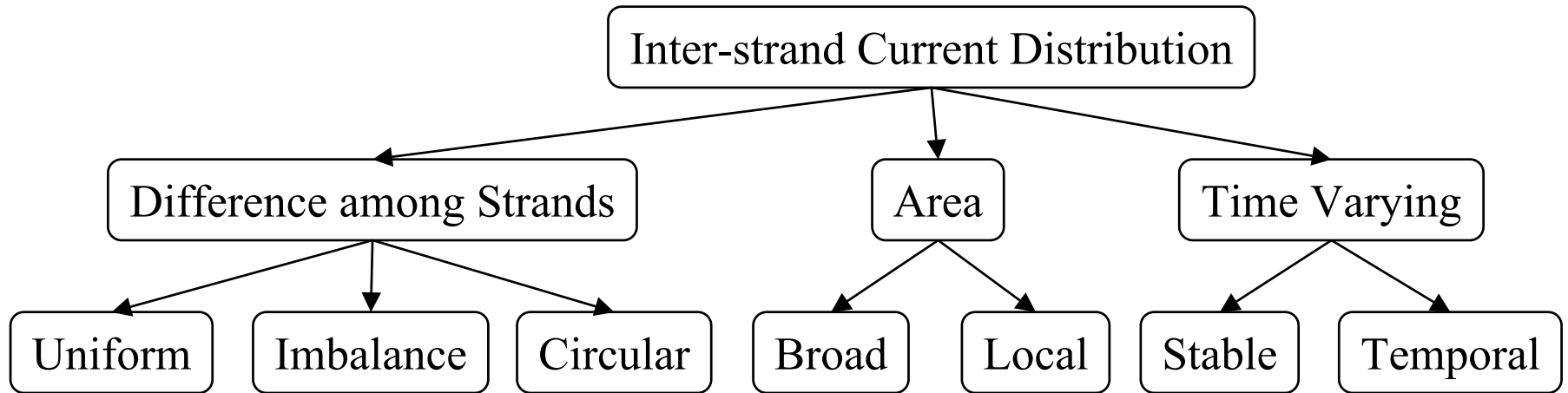
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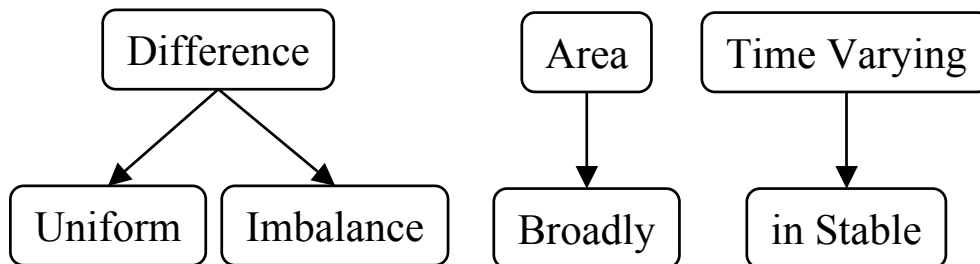
Introduction



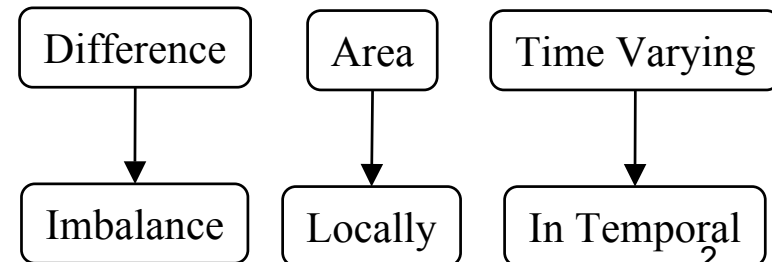
Inter-strand current distribution often affects the stability of superconducting cables with some phenomenon such as current redistribution.

Focus on the following case:

Initial :



After applying a disturbance :
during current redistribution process,



Objective

Problem :

Non-uniformity of inter-strand current distribution : often affects current redistribution and stability.

Larger cables (than triplex) : experimental researches are need.

Objective :

Experimental research on influence of inter-strand current distribution on current redistribution and stability.

Method :

Sample : eight-strand Rutherford cables with different strand surface; for simplicity.

Inter-strand current distribution: artificially controlled.

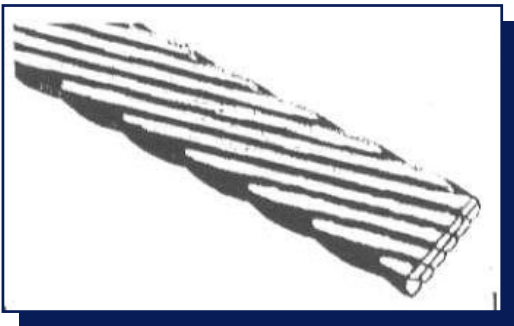
Current distribution : measured by Hall sensor sets.

Measured data :

Strand current and voltage,
Minimum Quench Energy (MQE).

Specification of Samples

	Sample 1	Sample 2
Strand Surface	AgSn-plating	AgSn-Plating, Oxidized
Contact Resistance, side-by-side ($\mu\Omega\text{m}$)	0.04	4
Contact Resistance, one cross-over ($\mu\Omega$)	4	400
Number of Strands	8	8
Diameter (mm)	0.81	0.81
Twist Pitch (mm)	31	31
Thickness x Width (mm)	1.5 x 3.3	1.5 x 3.3
I_c (A) at 4.2 K, 4 T	435	435



Contact between Strands :

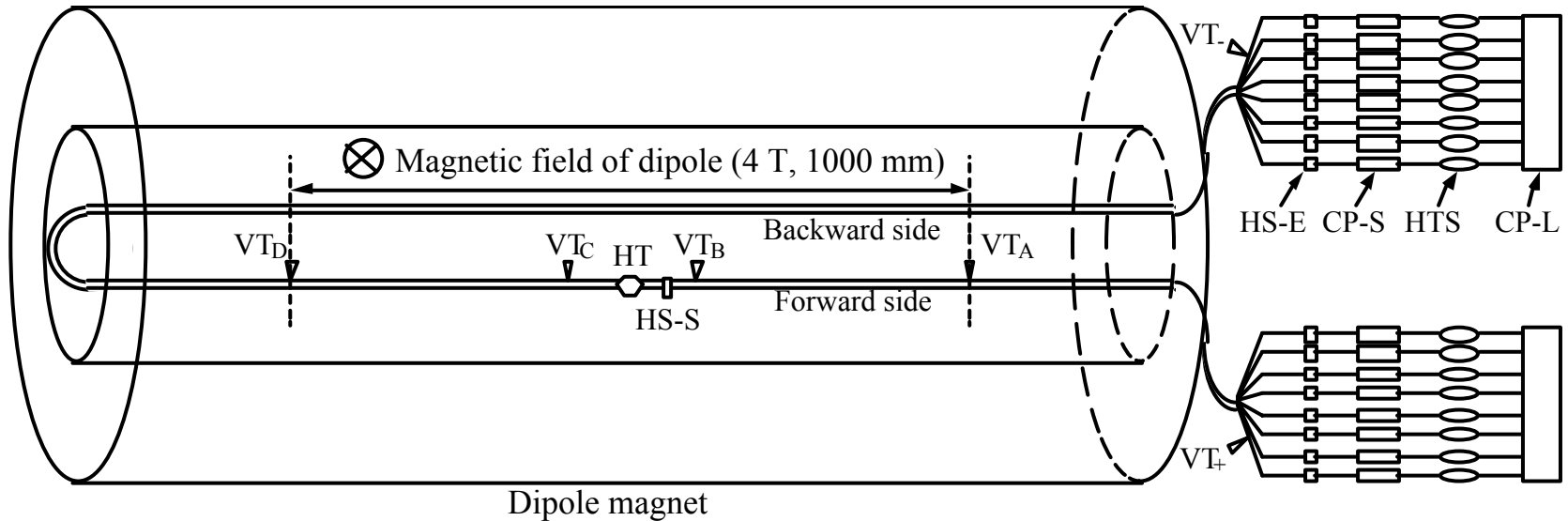
Sample 1 : Better .

Sample 2 : Worse.

The Other Characteristics :

Completely Same.

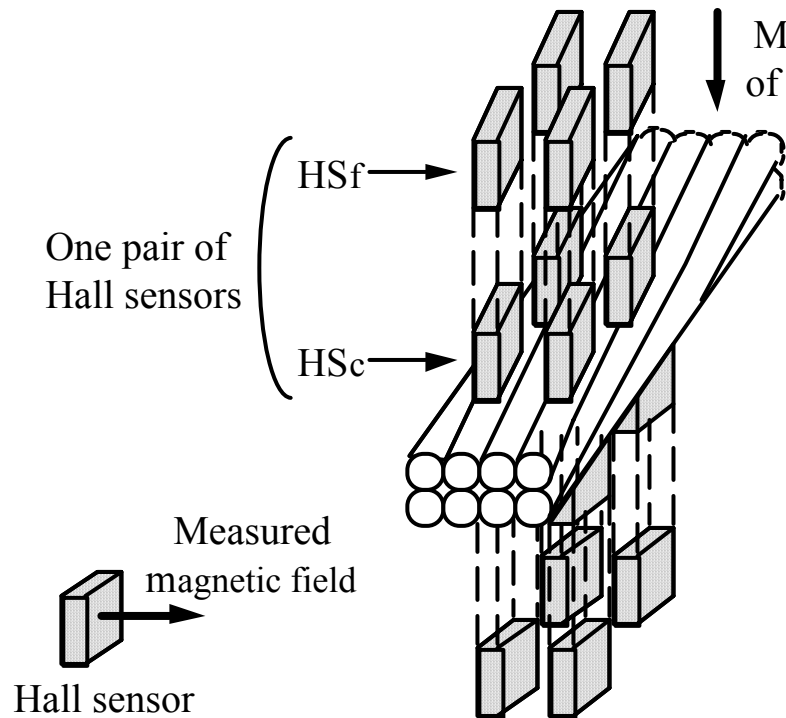
Arrangement : Sample, Heater, Hall Sensor, Voltage Tap, Copper Plate, and Magnet.



Sample :	3.6 m length, hairpin-shape (13 mm gap).
- Straight sections :	1m length, 4 T by a dipole magnet.
- Cable end :	All strands are separated.
Carbon Paste Heater, HT :	To input heat pulses to a strand.
Hall Sensor Sets :	Straight section (HS-S), both ends (HS-E).
Copper Plates :	Small one (CP-S) to each strand Large one (CP-L) to all strands.
Heater switches :	Resistive wire, between CP-S and CP-L (HTS). To control initial strand current distribution.

Hall Sensor Set

Hall Sensor Set at Straight Section, HS-S:



Magnetic field
of dipole magnet

Magnetic Field of Dipole Magnet (4 T) :
400 times larger than that of Strand Current.

Pair of Hall Sensors:

Two sensors measure same dipole field.

HS_c is close to a strand.

HS_f is far from the strand.

By electrical subtraction ($V_{HS_c} - V_{HS_f}$), dipole field is suppressed.

One set consists of eight pairs.




Hall Sensor Set at End of Cable, HS-E:

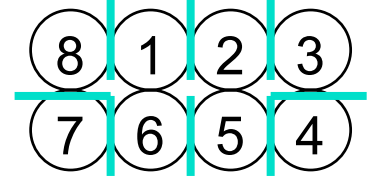
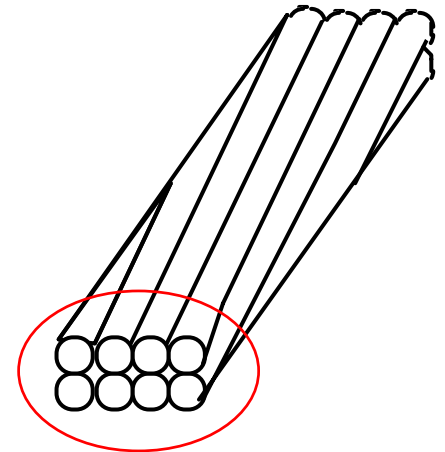
One Hall Sensor is attached on each strand.


Conditions

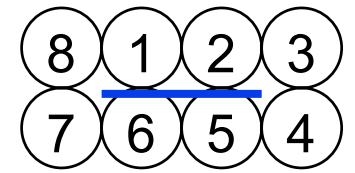
Cooling: 4.2 K, pool boiling LHe.
 External magnetic field: 4 T, dipole magnet.
 Transport current: 540 A to 3100 A.
 Heat pulse: 1ms width, to a strand.

Initial strand current distributions before applying a heat pulse:

Strand			
Current	v	v	-
Heat pulse	v	-	-

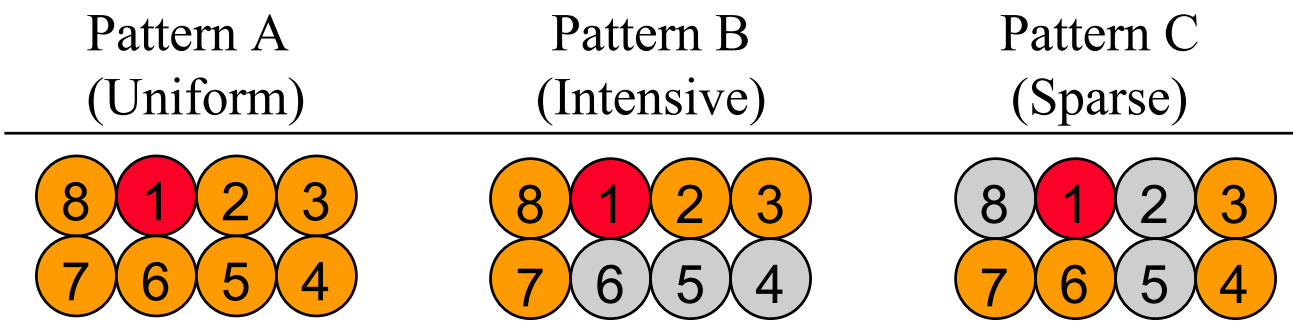


 Side-by-side contact



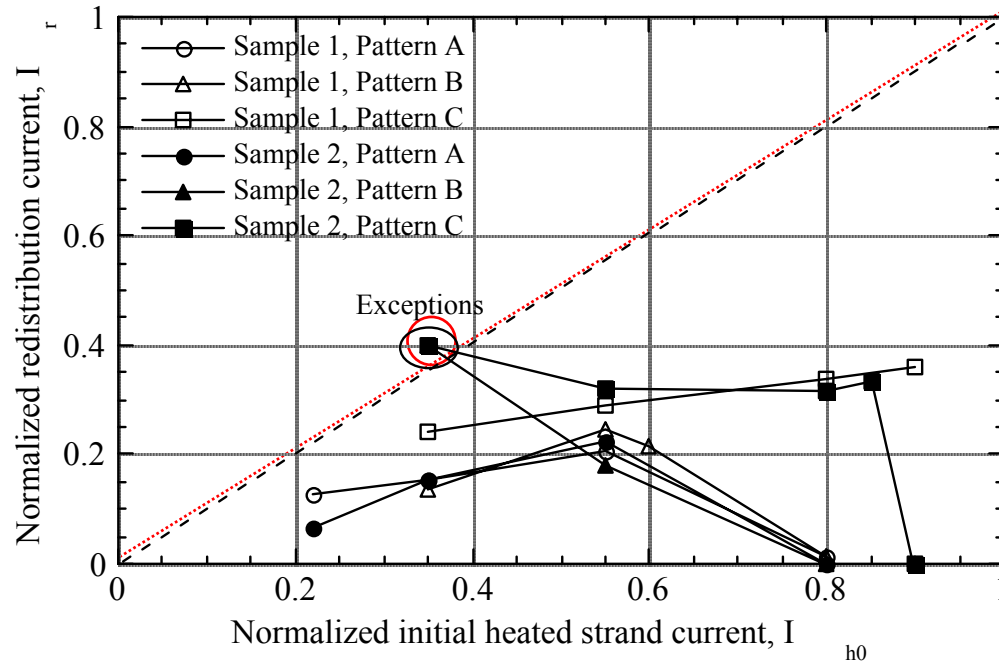
Cross-over contact

Neighbor : respect to side-by-side contact.



Measured values :

Redistribution Current during Recovery Process



Definition :

Redistribution Current, $I_r =$

Peak Value of Change of Heated Strand Current during Recovery Process.

Dashed Line :

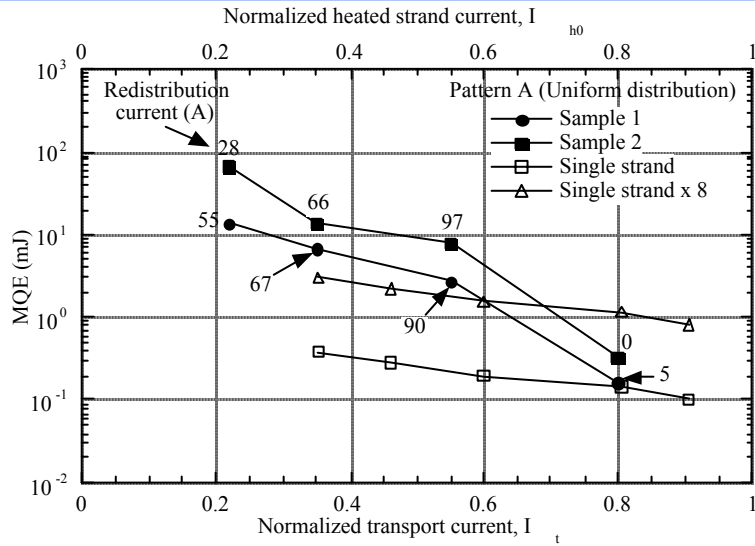
$I_{h0} \cdot I_r$ should $\leq I_{h0}$.

Exception :

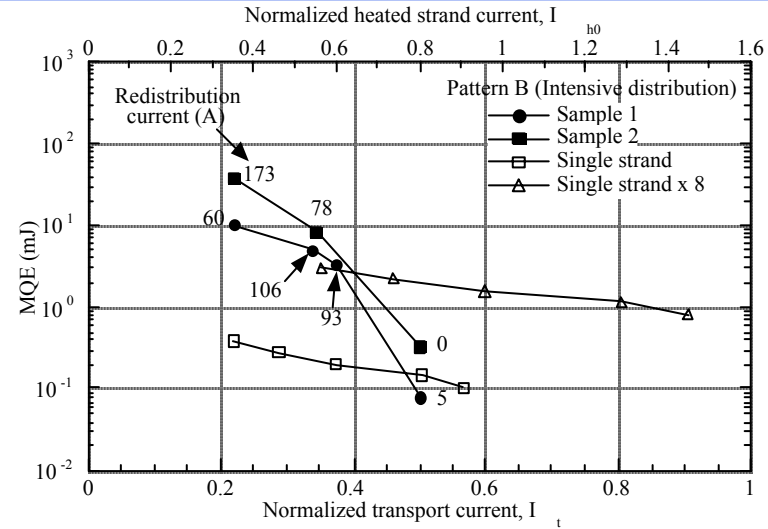
I_r of sample 2 where $I_{h0} = 0.35$ in the patter B and C.

Since they are on dashed line.

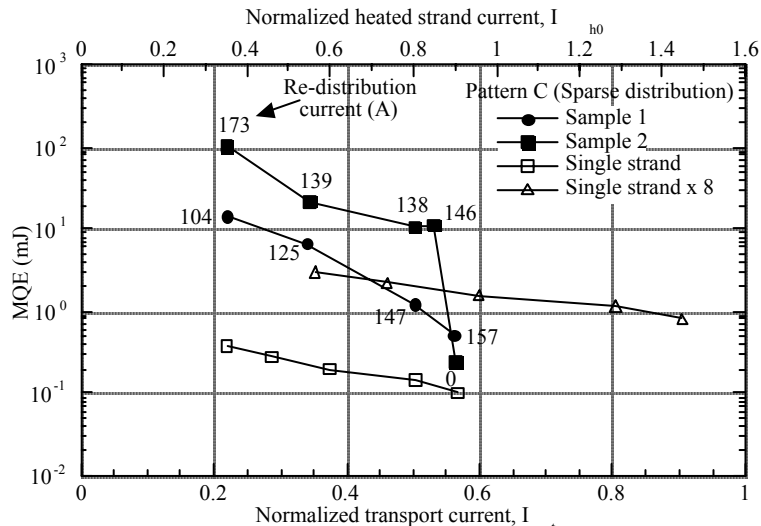
Measured values : MQE



Pattern A (Uniform)



Pattern B (Intensive)



Pattern C (Sparse)

Definition :

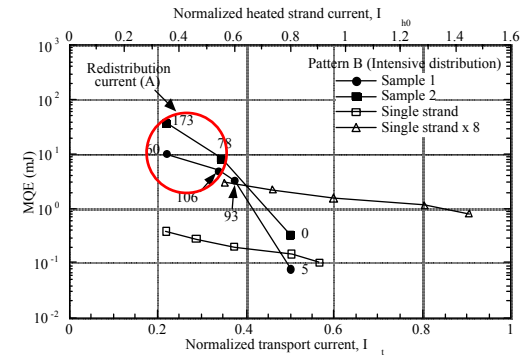
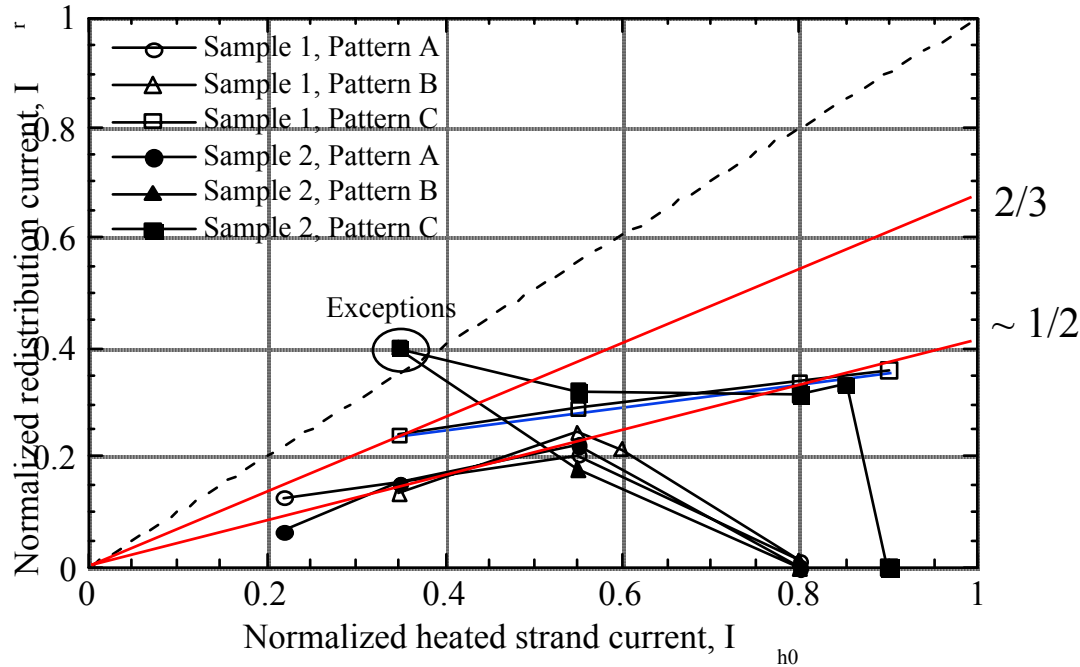
$$\text{MQE} = \frac{(\text{minimum heater energy for quench}) + (\text{maximum heater energy for recover})}{2}$$

Efficiency to input heat pulses :

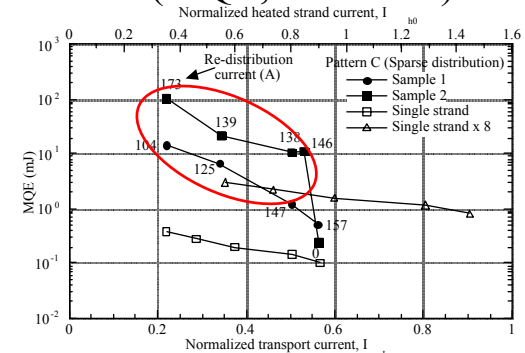
MQE of sample 2 was relatively larger, heater of sample 2 might have less efficiency. To watch tendency of profile is preferable.

Discussion:

Proportional Redistribution Current



(MQE, Pattern B)



(MQE, Pattern C)

Pattern A (Uniform distribution) :

Both samples had same profile.

When $I_{h0} \leq 0.55$, I_r was proportional to I_{h0} with ratio of 1:2 at each point.

Pattern B (Intensive distribution) without exception:

Both samples had almost same profiles as that of pattern A.

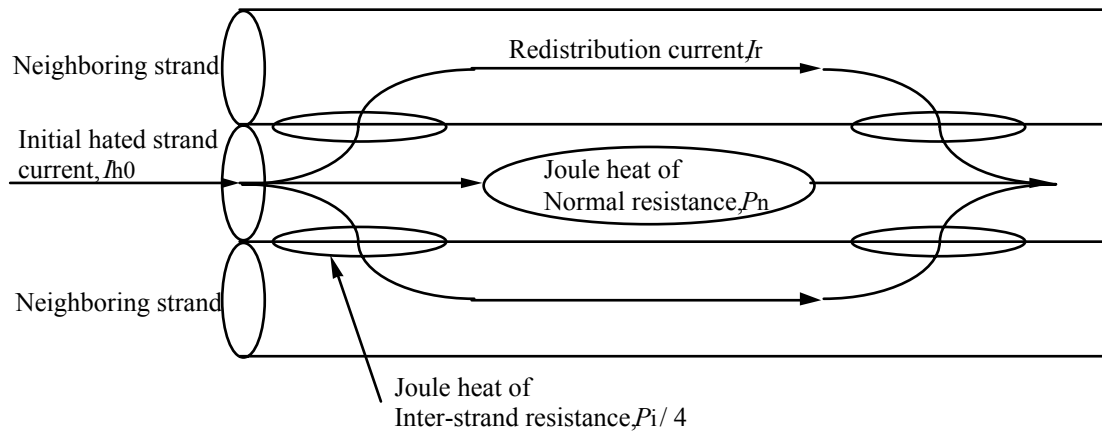
Pattern C (Sparse distribution) without exception :

Up to $I_{h0} \leq 0.8$, I_r was proportional to I_{h0} , within 1:2 and 2/3 at each point.

MQE was improved in the corresponding region.

Discussion:

Proportional Redistribution Current



When MQE was improved, I_r and the I_{h0} balanced with some ratio.

Joule heat in strand that transports current is most directive factor for the stability of the strand.

Pattern A and B:

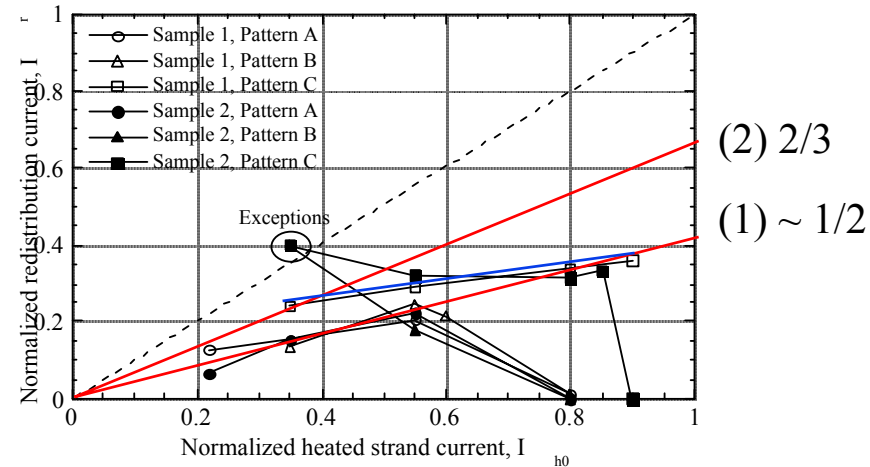
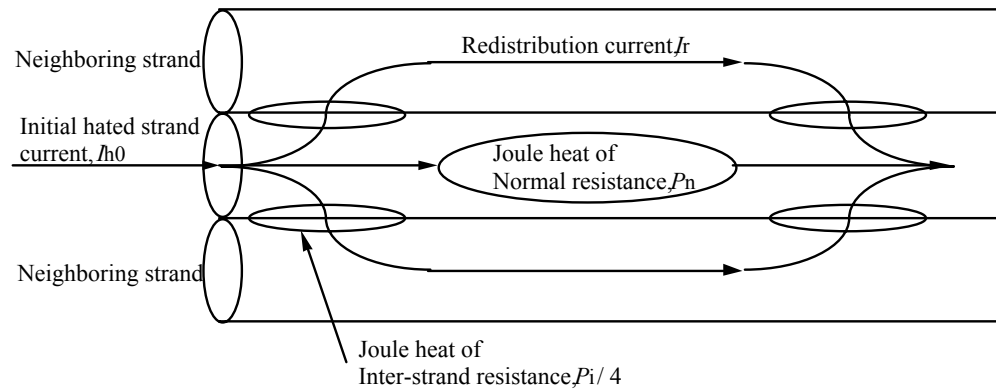
P_n and P_i are influential to stability.

Pattern C:

P_n and $1/2$ of P_i are influential when heat transferring from neighboring strands to other strands is neglected.

Discussion:

Proportional Redistribution Current



Influential Joule heats of these strands may balance to be equal by increasing or decreasing of I_r , so that heating of these strands becomes in minimum.

Pattern A and B :

$$P_n = P_i;$$

$$R_h (I_{h0} - I_r)^2 = R_i I_r^2$$

Voltage Drop :

$$R_h (I_{h0} - I_r) = R_i I_r$$

Then, $I_r : I_{h0} = 1:2 \dots (1)$

Pattern C :

$$P_n = P_i / 2$$

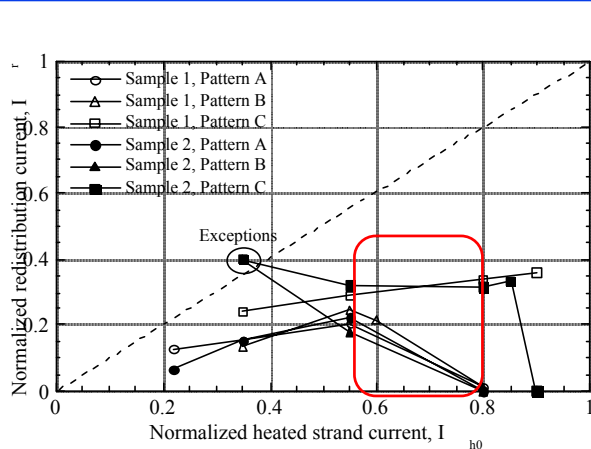
$$R_h (I_{h0} - I_r)^2 = R_i I_r^2 / 2$$

Then, $I_r : I_{h0} = 2:3 \dots (2)$

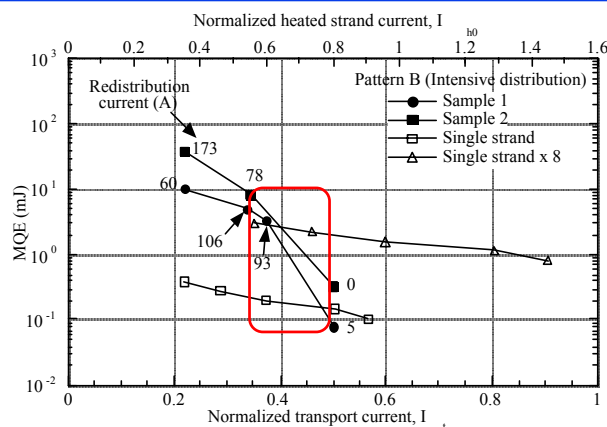
With increasing of I_{h0} , heat transferring from neighboring strands to others becomes influential.

Discussion:

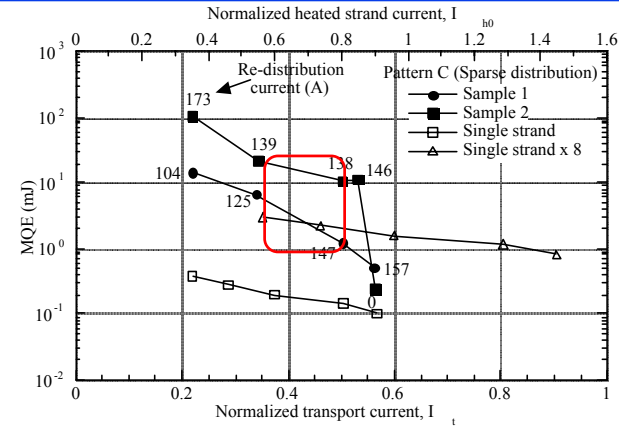
Decrease of Redistribution Current



Redistribution Current



MQE, Pattern B (Intensive)



MQE, Pattern C (Sparse)

When $I_{h0} > 0.55$,

Pattern A and B :

I_r decreased. MQE decreased to single strand stability region.

Pattern C :

I_r was still proportional to I_{h0} up to $I_{h0} = 0.8$. MQE was still higher.

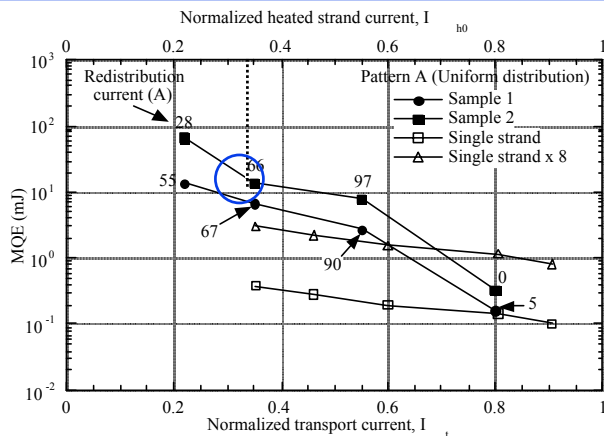
Strand stability region, a local heat pulse applying to a strand does not produce local normal zone in recovery process, or the cable quenches.

Initial condition: difference among pattern A, B and C : sparseness of distribution.

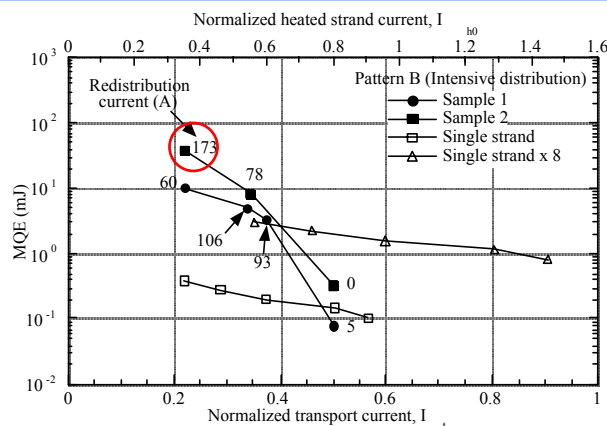
Chain reaction of changing to normal state is suppressed by sparse distribution. 13

Discussion:

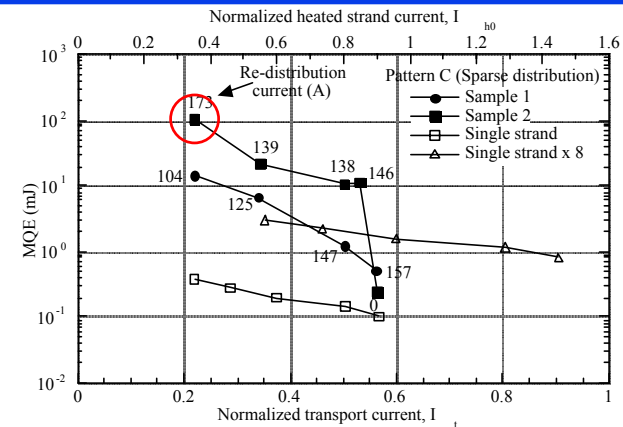
Exceptions of Redistribution Current



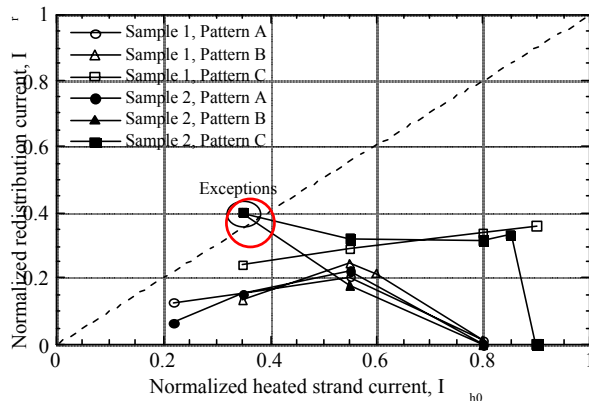
MQE, Pattern A (Uniform)



MQE, Pattern B (Intensive)



MQE, Pattern C (Sparse)



Exceptional Points:

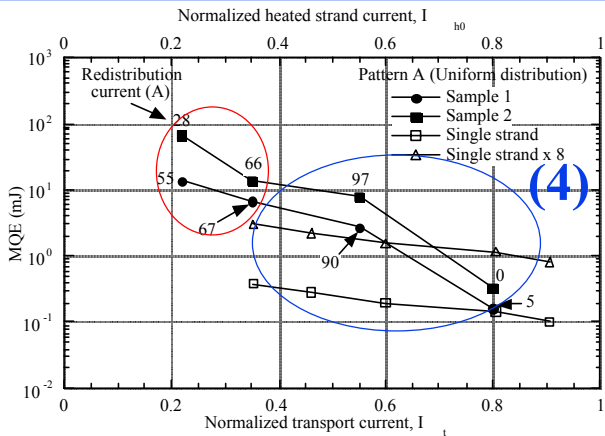
I_r of sample 2 at $I_{h0} = 0.35$ in the pattern B and C.

Corresponding MQE vs. I_{h0} :

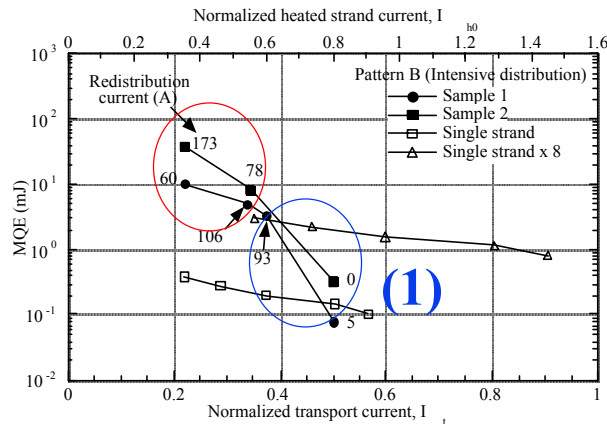
The highest.

Applied heat pulse was largest, and possibly heated strand might quench locally even so sample recovered after a moment, so that full of heated strand current transferred to other strands.

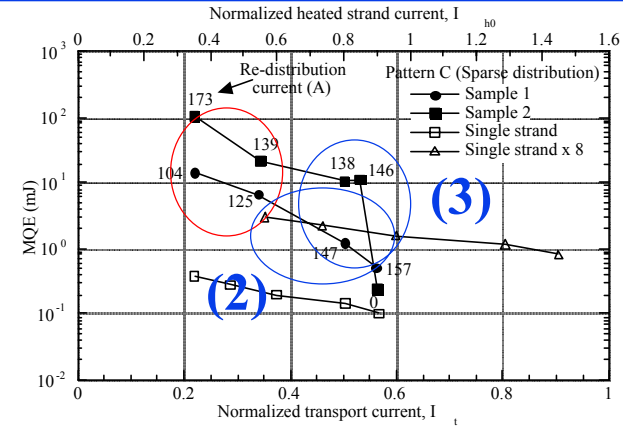
Discussion: Order of MQE



Pattern A (Uniform)



Pattern B (Intensive)



Pattern C (Sparse)

When $I_t \leq 0.35$: ○

Profiles of MQE were almost same.

Non-uniform current distribution didn't affect MQE in such transport current.

When $I_t > 0.35$: ○

MQE was improved as the following in ascending order:

- (1) Intensive (Worst)
 - (2) Sparse with Better Contact
 - (3) Sparse with Worse Contact
 - (4) Uniform (Best)
- ↓

Discussion:

Order of MQE

When $I_t > 0.35$:

MQE was improved as the following in ascending order:

- | | |
|--------------------------------|---------|
| (1) Intensive | (Worst) |
| (2) Sparse with Better Contact | |
| (3) Sparse with Worse Contact | |
| (4) Uniform | (Best) |
- 

Difference between (1) and (2) : Sparseness of distribution.

Sparse distribution might suppress chain reaction of changing to normal state.

Difference between (2) and (3) : Inter-strand contact.

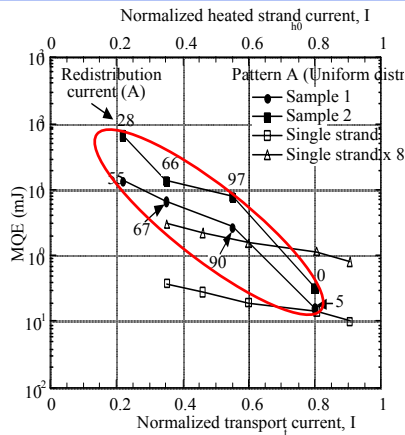
Larger inter-strand thermal conductivity might improve MQE.

Difference between (3) and (4) : Uniformity of distribution.

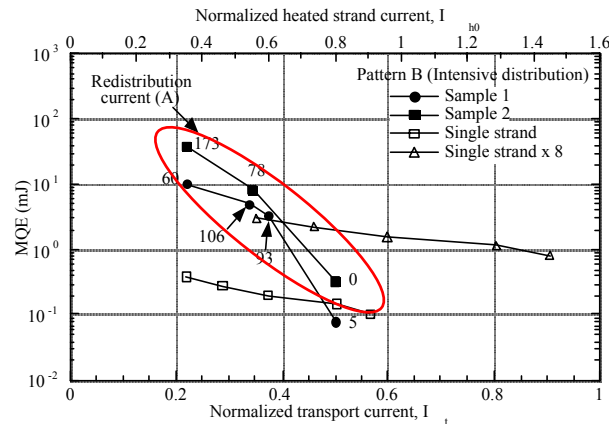
MQE of (3) did not decrease drastically when $I_t \leq 0.55$, which is corresponding to $I_{h0} \leq 0.8$.

Therefore when a cable has worse inter-strand contact and its inter-strand distribution is sparse by some reason, its MQE is significantly improved even so the inter-strand current distribution is not uniform.

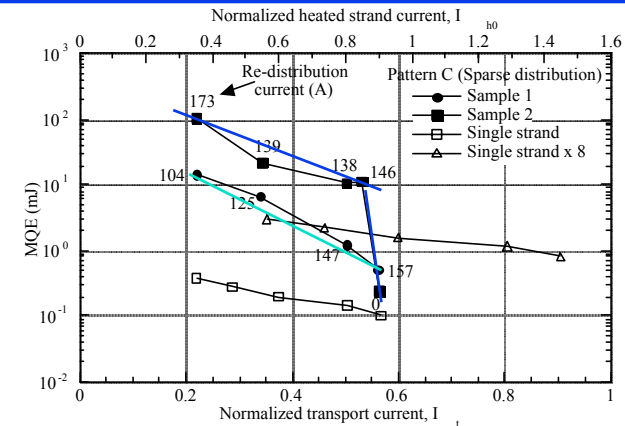
MQE vs. I_{h0}



Pattern A (Uniform)



Pattern B (Intensive)



Pattern C (Sparse)

In Uniform and Intensive Distribution:

Profiles of MQE vs I_{h0} were nearly same.

Strand without current didn't improve MQE much in intensive distribution.

In Sparse Distribution:

MQE vs. I_{h0} was better especially in the worse contact sample. —

Sparse distribution improved MQE, even so some strands transported much current than the others.

Conclusion

To examine the influence of inter-strand current distribution on current redistribution and MQE,

Two types of eight-strand Rutherford cables with different strand surfaces were tested.

Current Redistribution :

In uniform and intensive distribution:

Peak value of redistribution current during recovery process was proportional to heated strand current when cable transported smaller current.

In sparse distribution :

Proportional redistribution current was observed up to larger transport current.

Possible reasons :

Sparseness of initial strand current distribution
and Balance of Joule heat in strands that transports current.

MQE

In sparse current distribution:

Worse contact cable was significantly improved , even so sparse distribution is one of non-uniform distributions.