

Luca Bottura The NET Team

"Validation
Results for
3-D Quench
Propagation"

Validation of the
3-D quench propagation code
SARUMAN

L. Bottura

&

Superconducting Magnets Group
of
ENEA C.R.E.-Frascati

Introduction

Which code ?

SARUMAN has:



3-D winding pack description

→ 1-D f.e. solution of heat conduction along the conductor

→ 2-D equivalent (thermal resistances) of heat conduction across the winding



1-D helium flow in equivalent channel

→ 1-D f.e. solution of mass, momentum, energy balances



Circuital Solution

→ Coupled analysis of external coils and power supplies



Hydraulic network

→ Coupled analysis of external piping and pumps

Introduction

Why a 3-D quench program ?

What is a 3-D program ?

large magnets

large cooling lengths

long times required for the longitudinal propagation

effect of transverse conduction becomes important



3-D code is taking into account the transverse conduction



comparable $V_{\text{long}}/V_{\text{trans}}$ ratio



3-D code is relevant for large magnets (e.g. fusion applications)



3-D code can be necessary for safety analysis studies

Introduction

Why coupled circuit and hydraulic networks?

coil systems

inductive coupling

common manifolding

operating current and
field evolution

boundary
p and T evolution



coupled code is modifying operating and boundary conditions according to the environment changes



coil systems



3-D code is relevant in the analysis of quench evolution and safety for large magnets and magnetic systems

Introduction

Fine, we have the 3-D code. And now ?

Option 1

How much do you believe it ?
issues of reliability, performance,
safety factors,...

Validation Studies

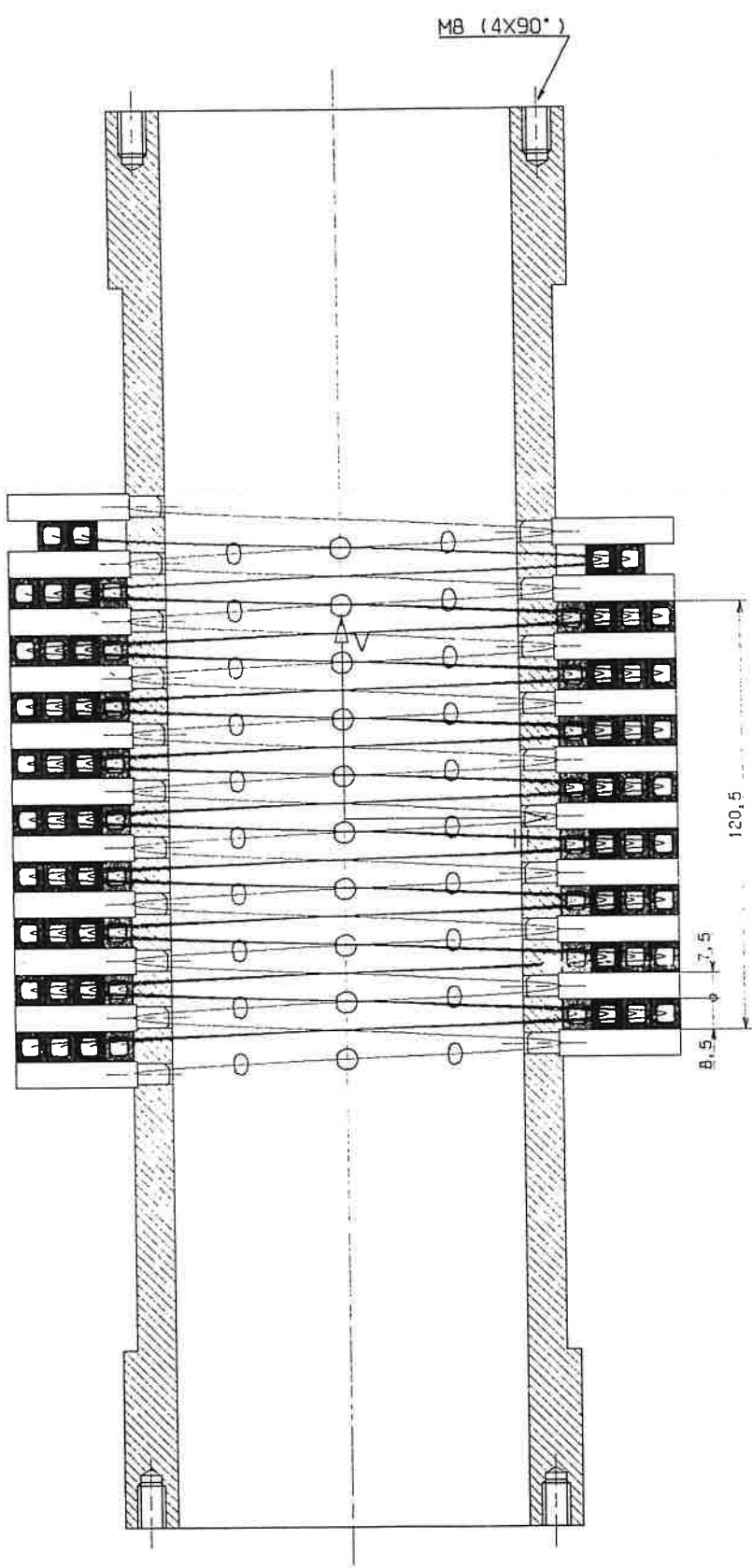
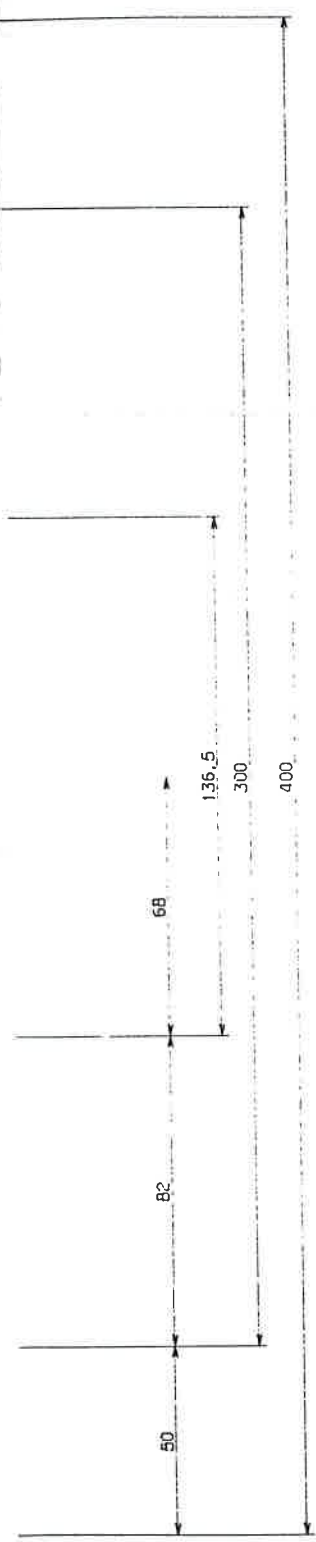
Code Improvements

Option 2

I need something to justify my salary
and invitations to workshops
fun, honor & glory

Validation Studies

Code Improvements



He
IN
He
OUT

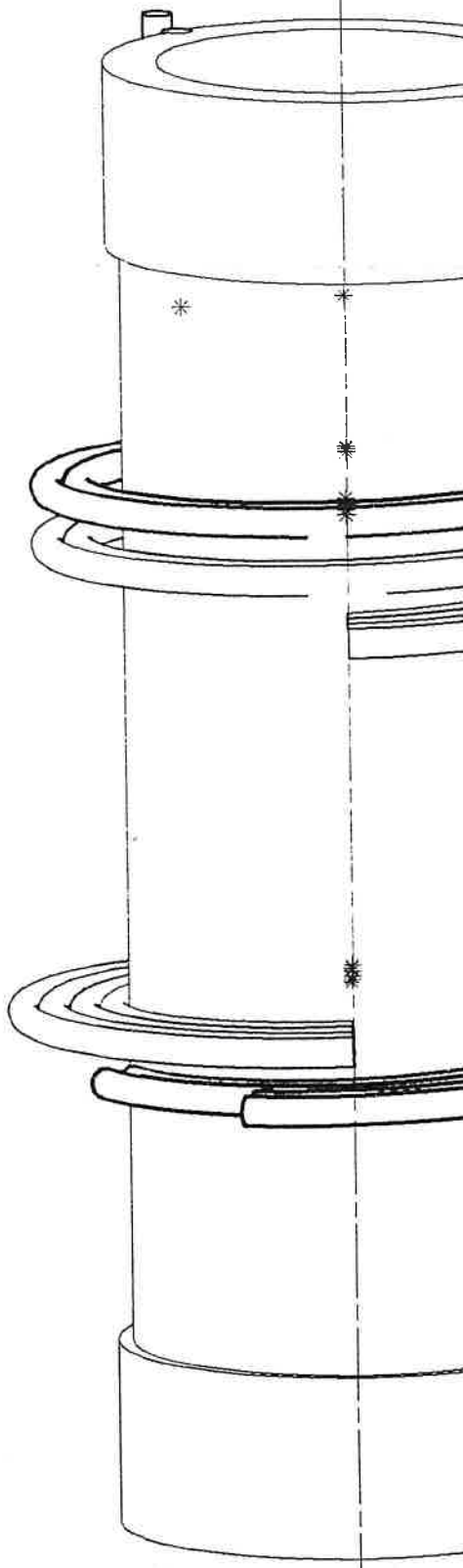
I+
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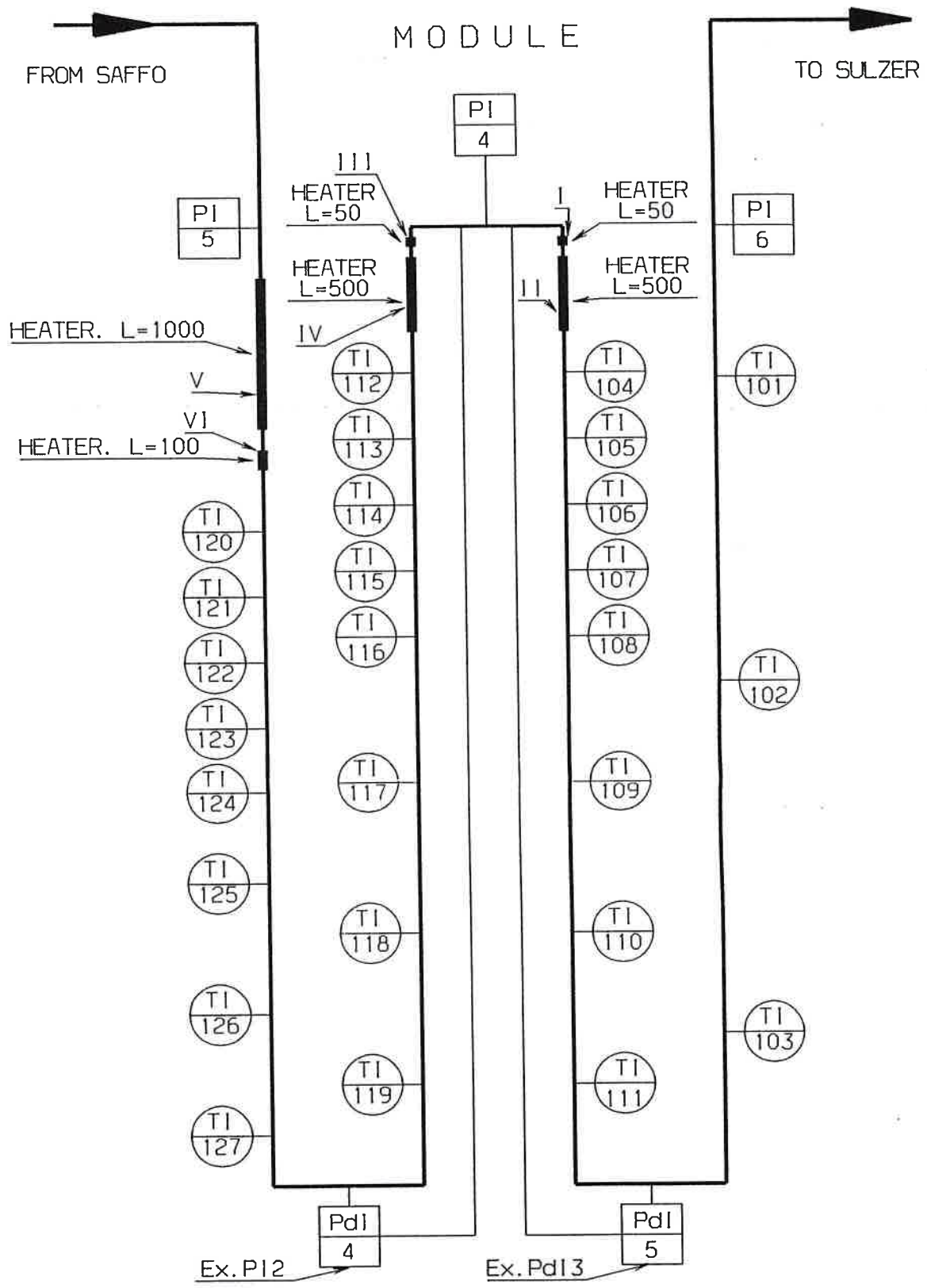
LAYER
1
2
3
4

EXTRA TURN FOR
CENTRAL HEATER

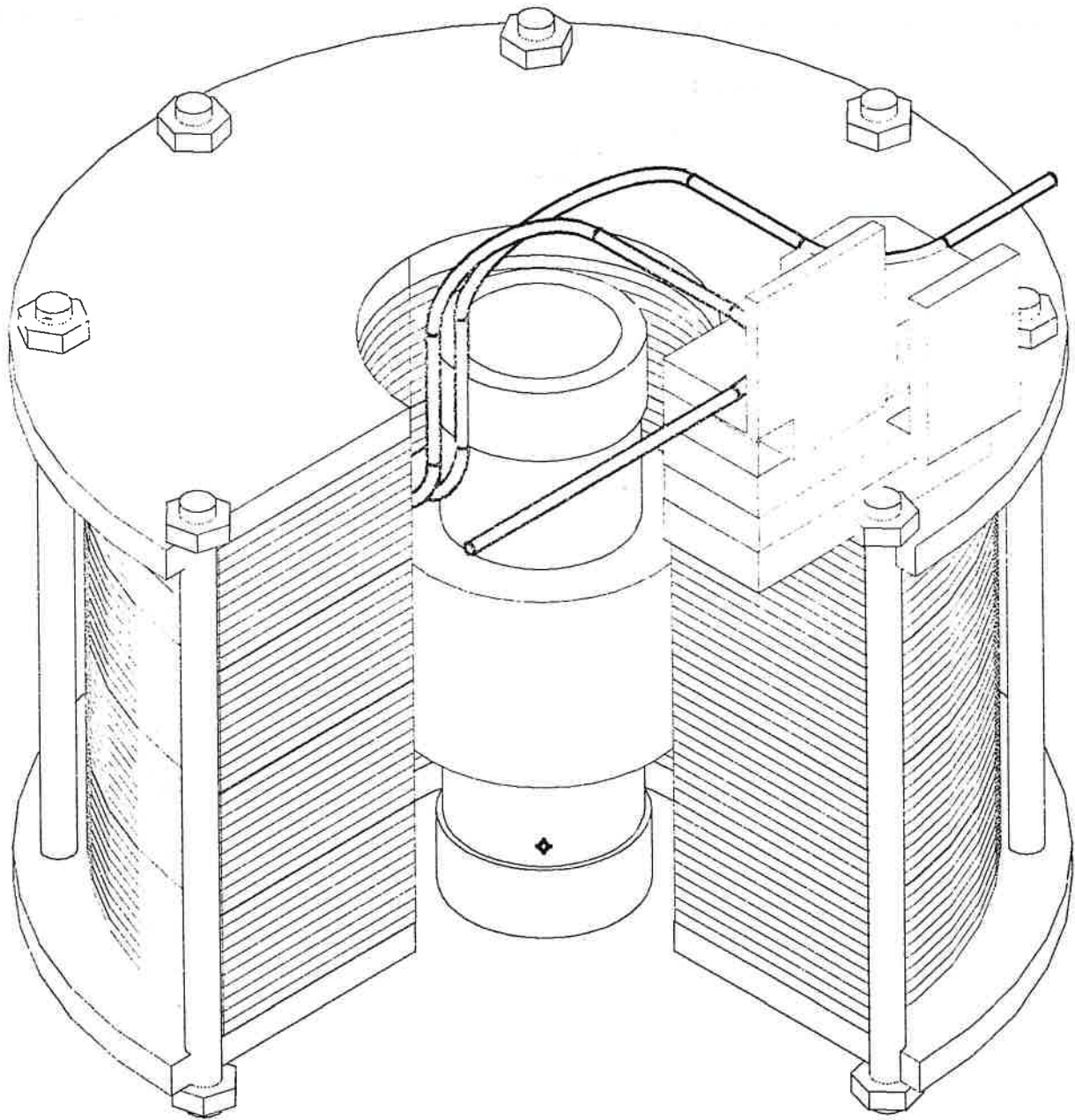
JOINT BETWEEN
LAYER 1 & 2
(OVER 247°)

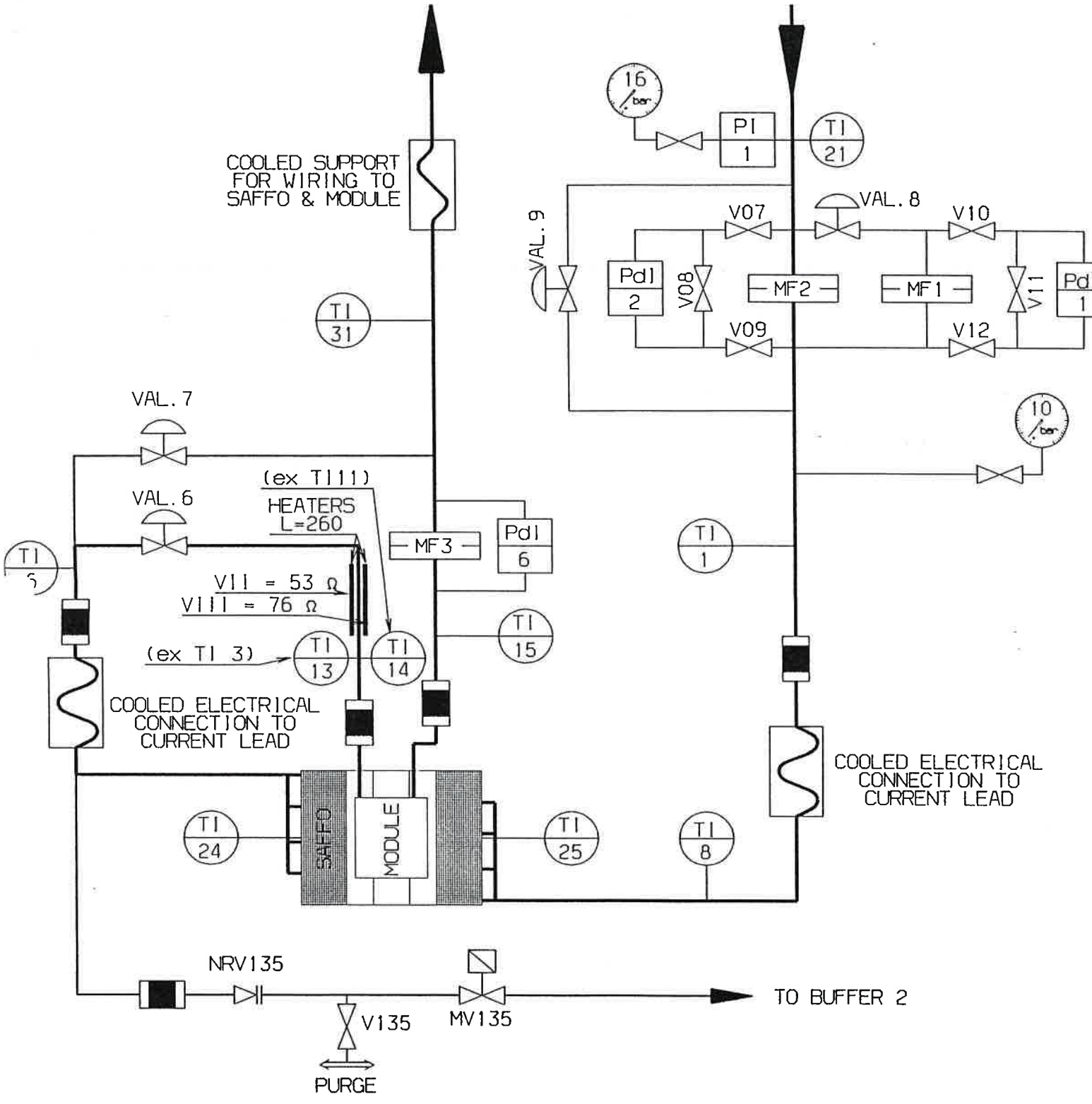
JOINT BETWEEN
LAYER 3 & 4
(OVER 199°)

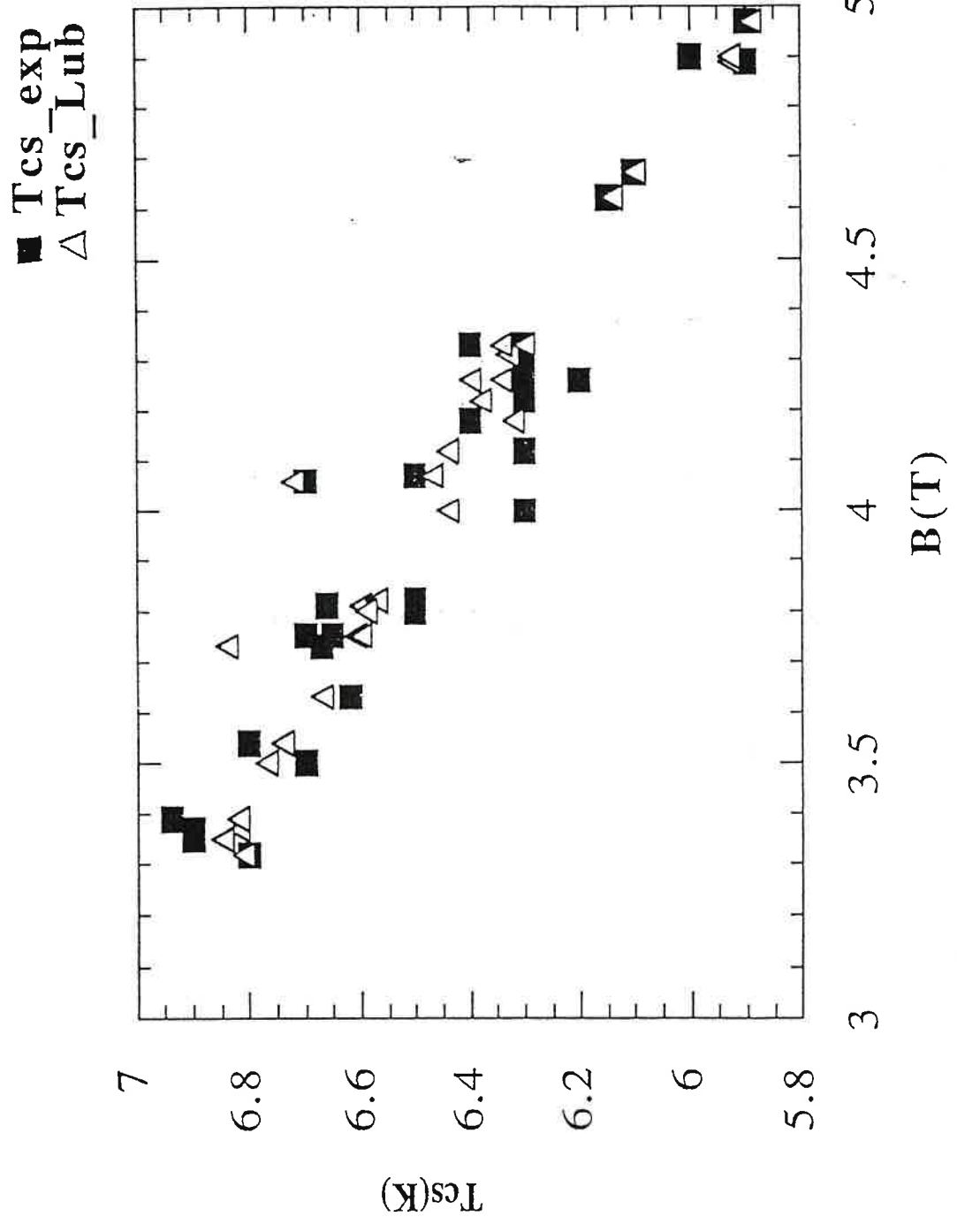




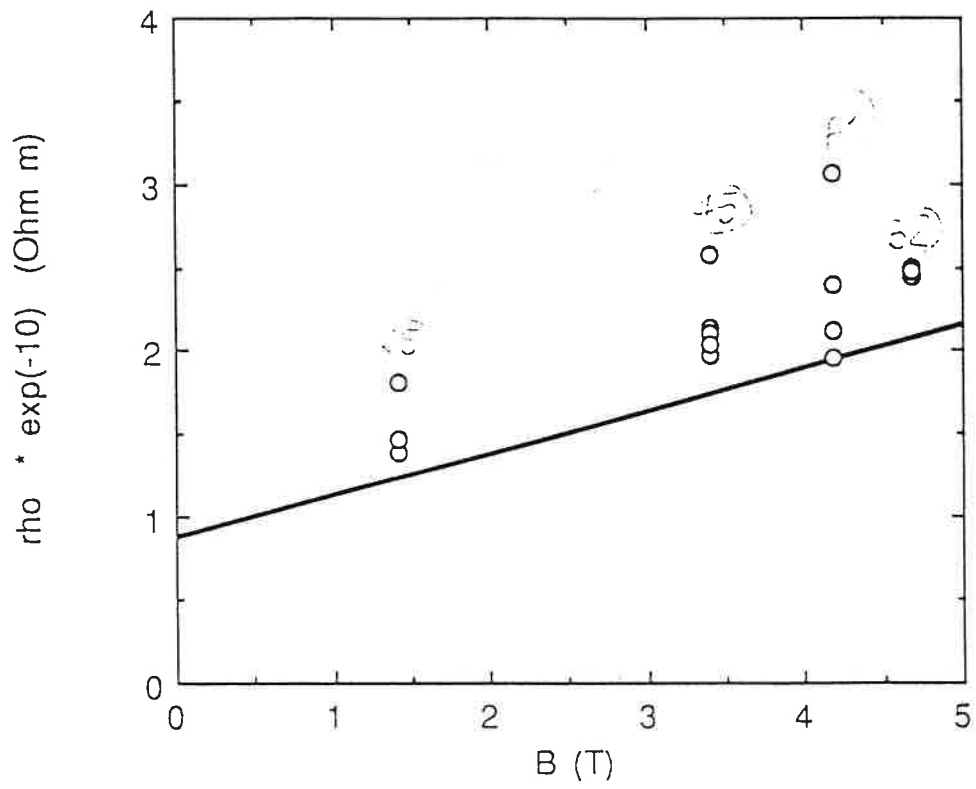
POS.	N PEZZI	DENOMINAZIONE E DIMENSIONI	MATERIALE	PIFEPIM, DISEGNO	NOTE
		ENEA		LABORATORIO SUPERCONDUTTIVITA' - CRE FRASCATI Via E. Fermi N 27	
MODIF.	INDICE		HYDRAULIC FLOWS SCHEME & LOCATION OF SENSORS IN SAFFO & MODULE		
	DATA				
FIRMA					
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		TOLL. GEOM.	SCALA	DATA	SOSTITUISCE
			DIS.	PROG.	SOSTITUITO



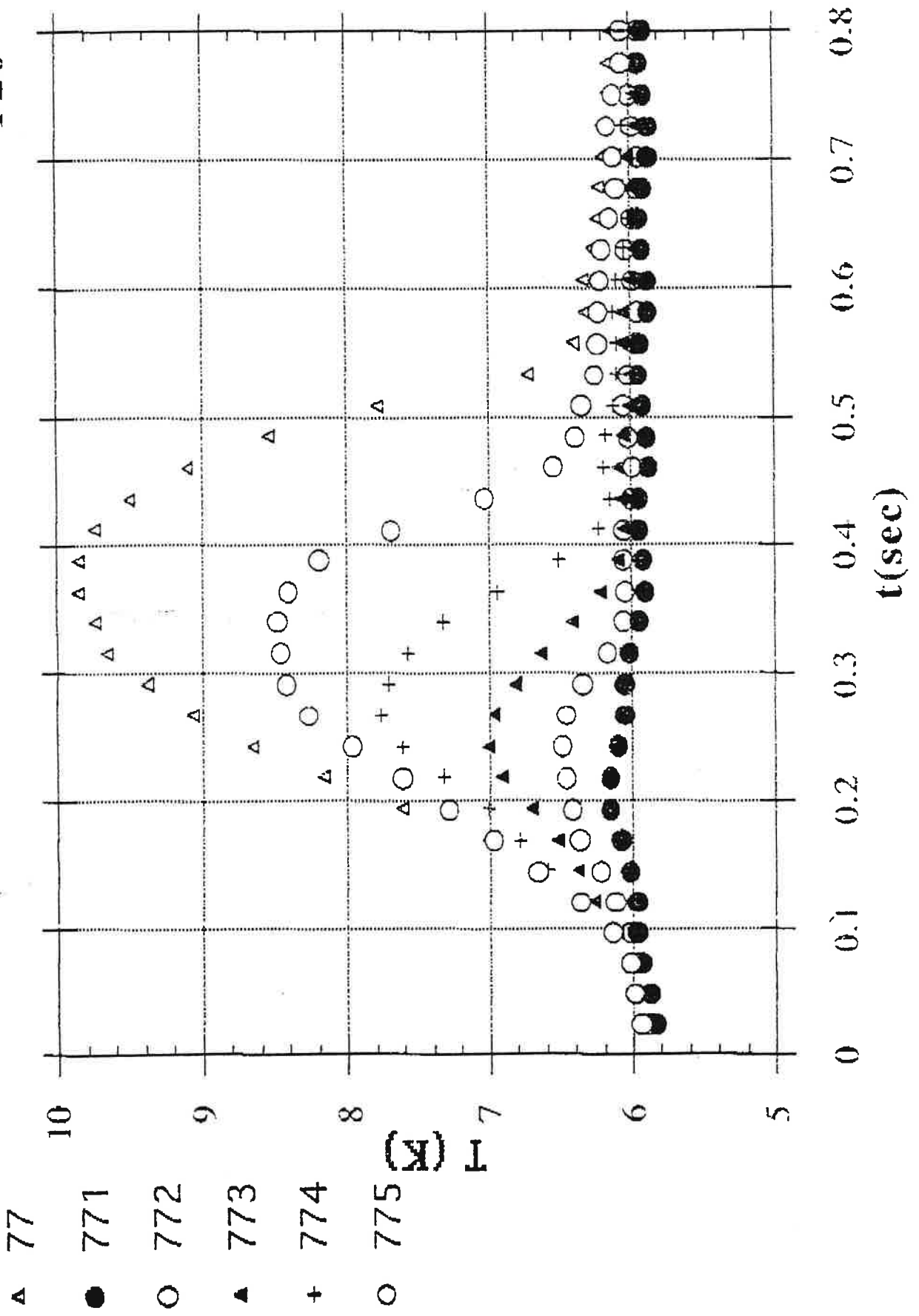




Fit to the copper resistivity

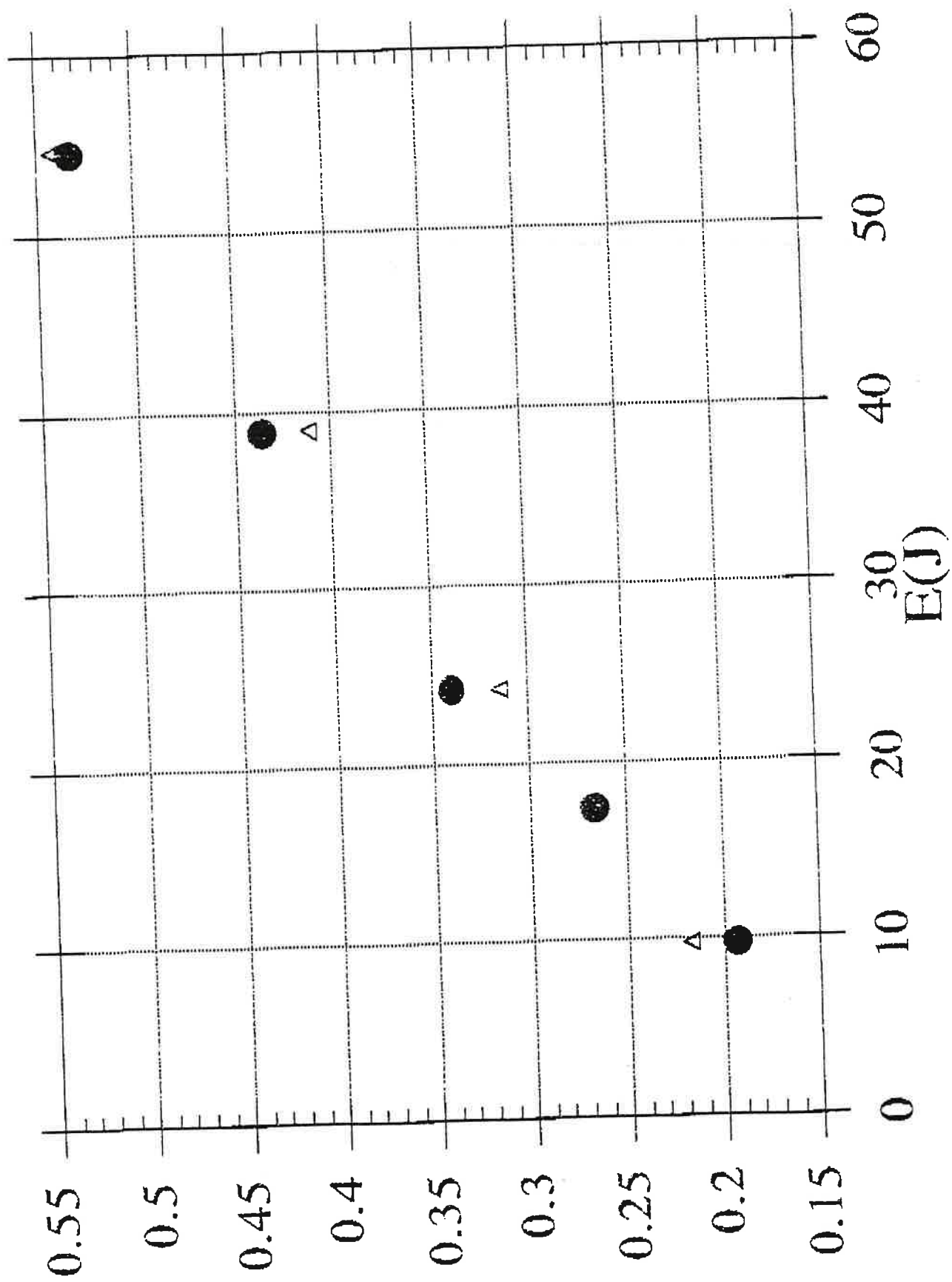


T20

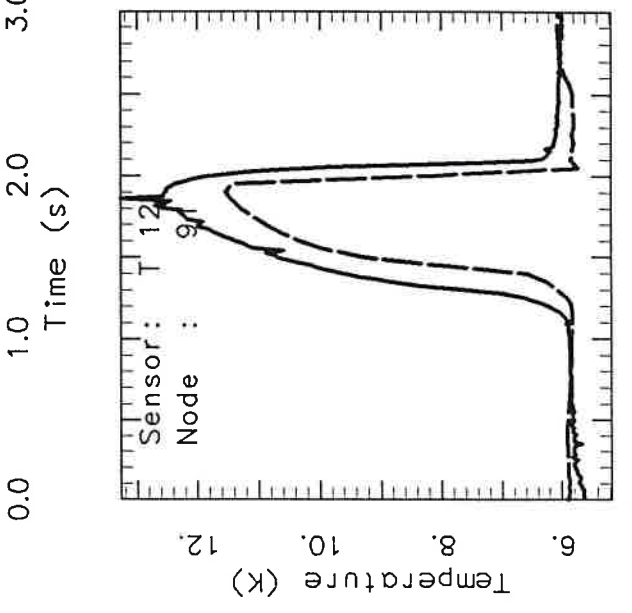
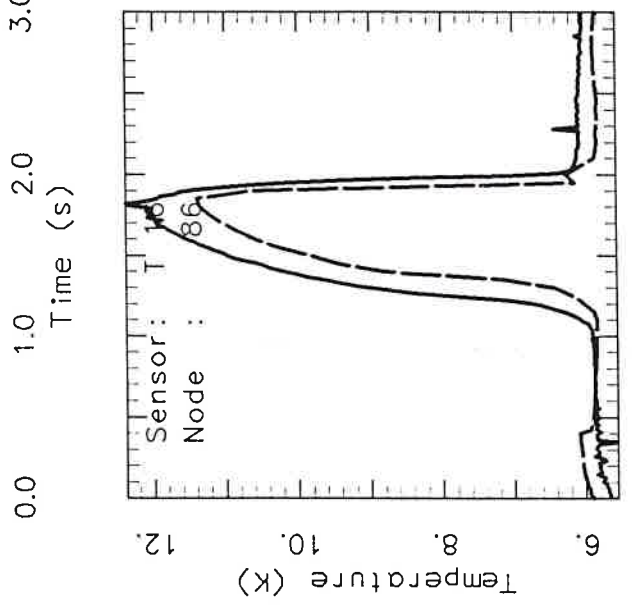
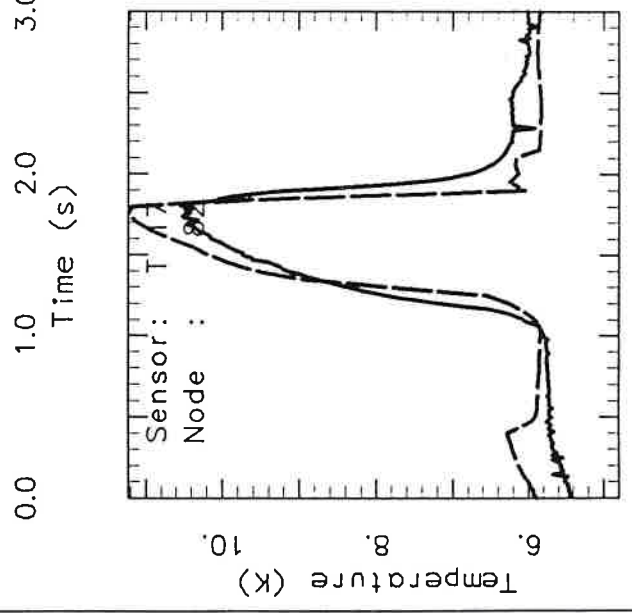
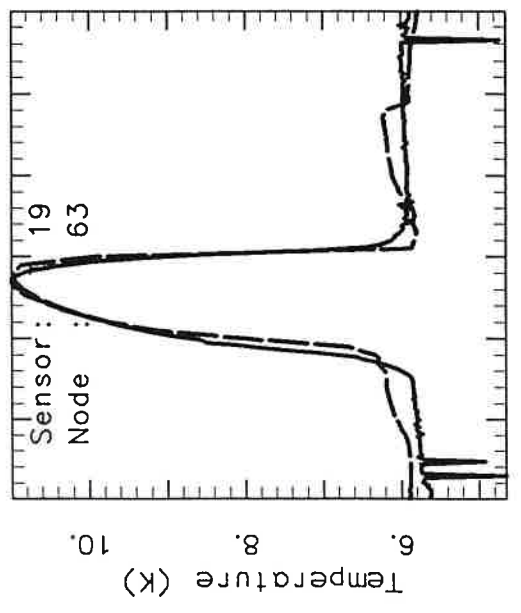
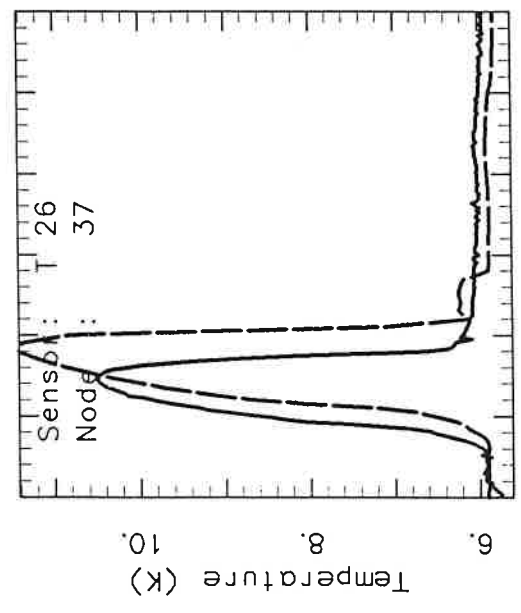
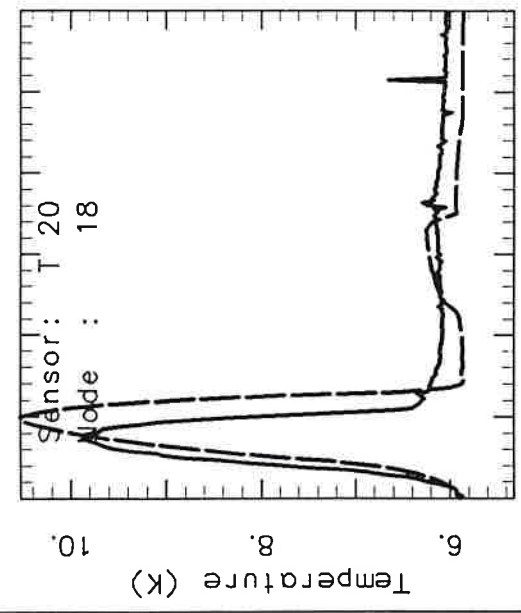


△ T20-delta_t(sec)

● T26-delta_t(sec)



SIM # 77. t_{in}=0.20 mm. TSS 3 m→it. Min htc. eff pulse. rho=1.65

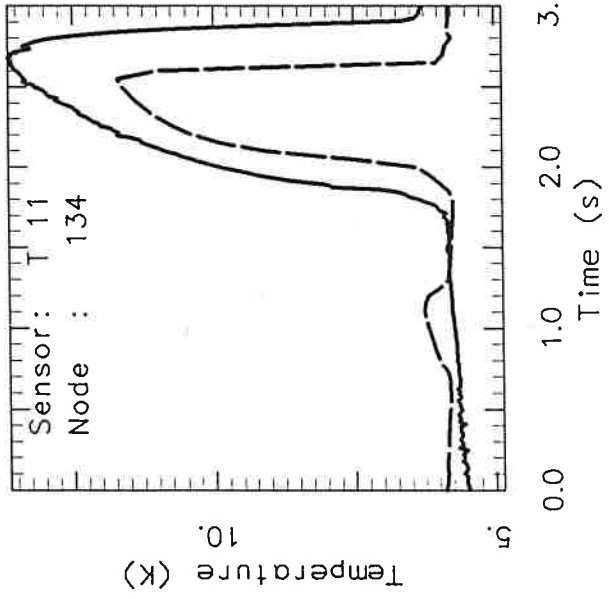
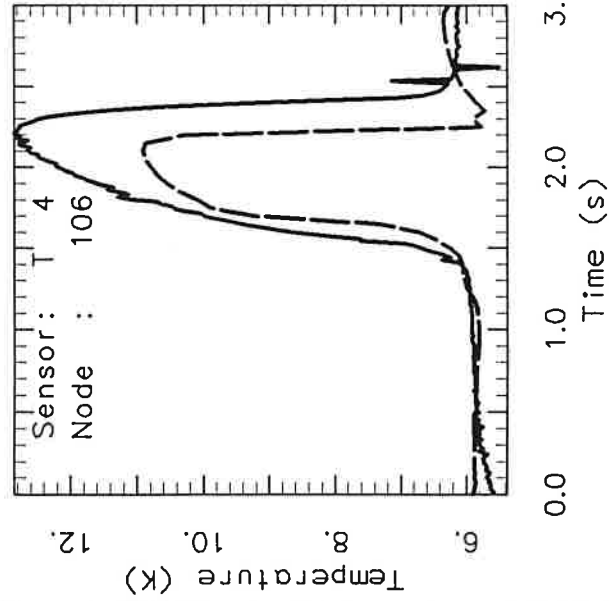


0.0 1.0 2.0 3.0
Time (s)

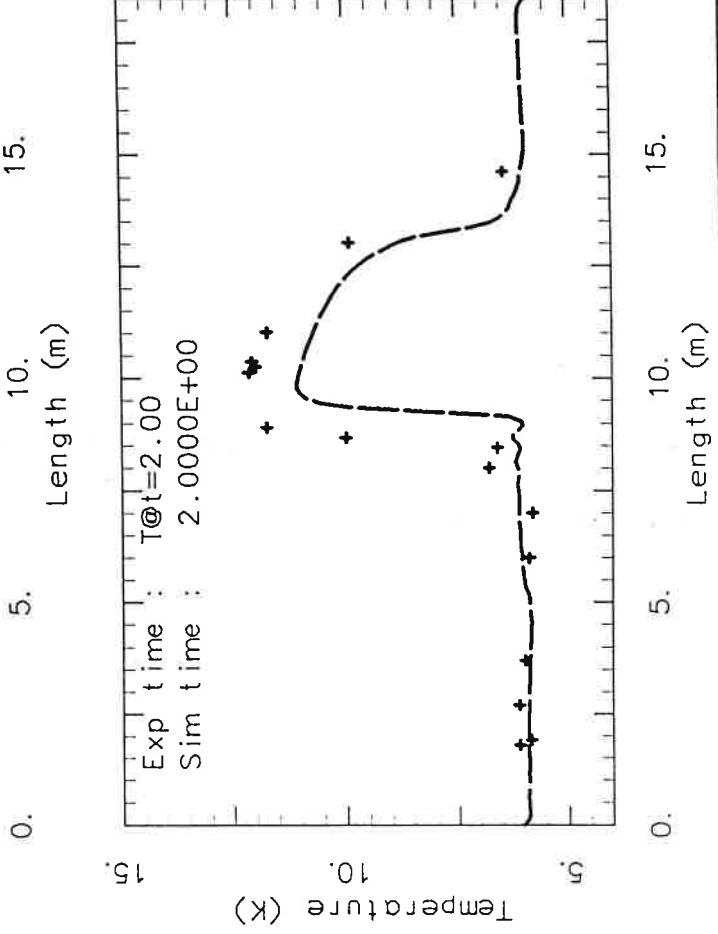
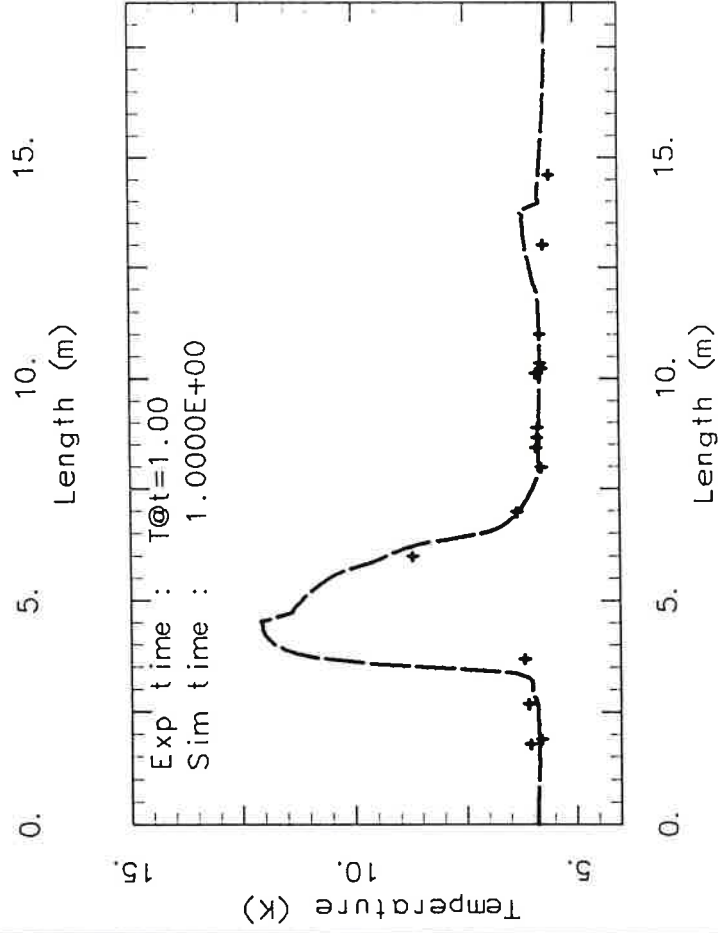
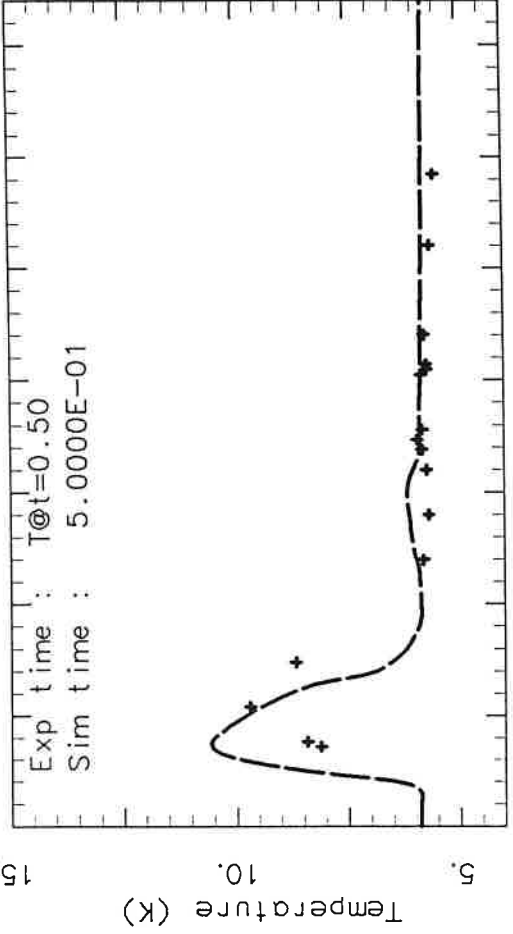
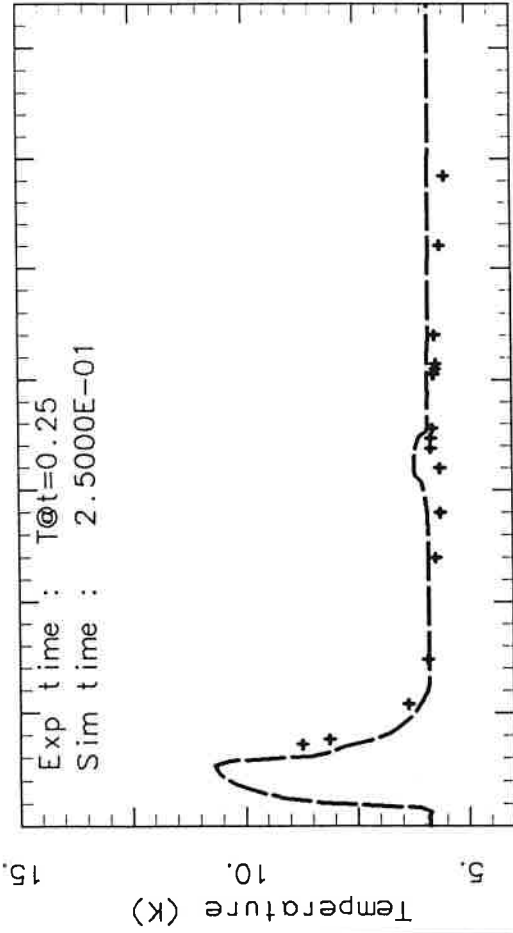
0.0 1.0 2.0 3.0
Time (s)

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Time (s)

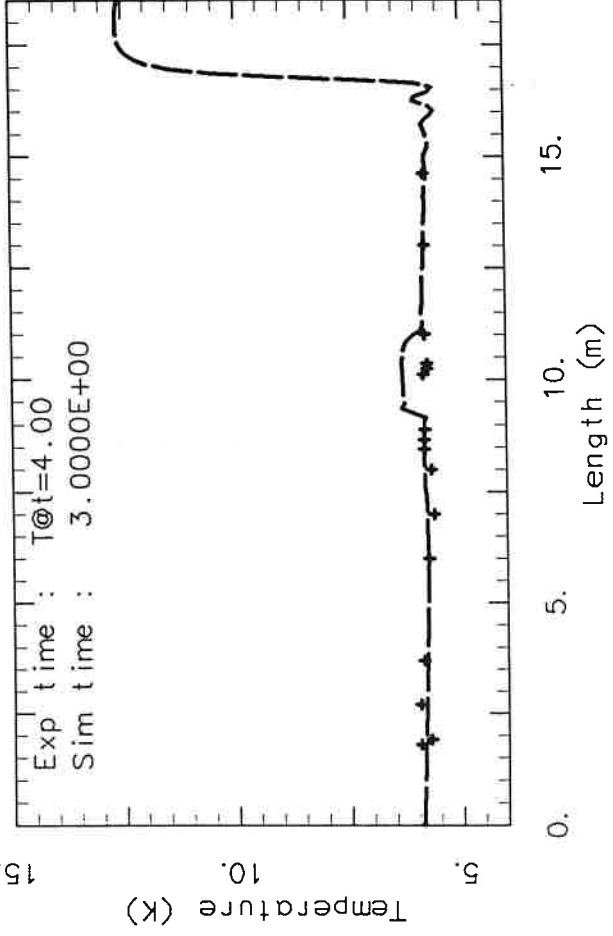
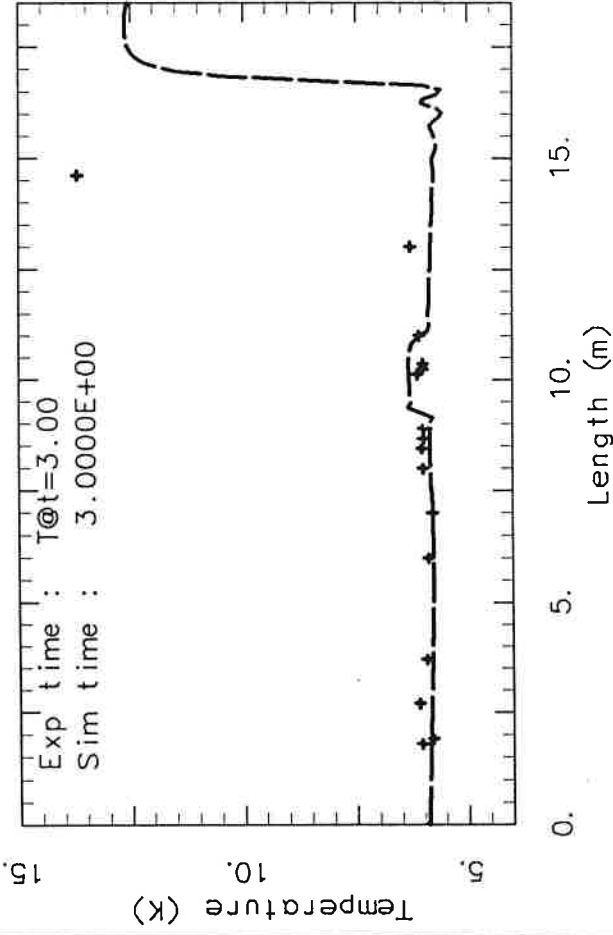
SIM # 77. t_{in}=0.20 mm. TSS 3 m_{it}. Min htc. eff pulse. rho=1.65



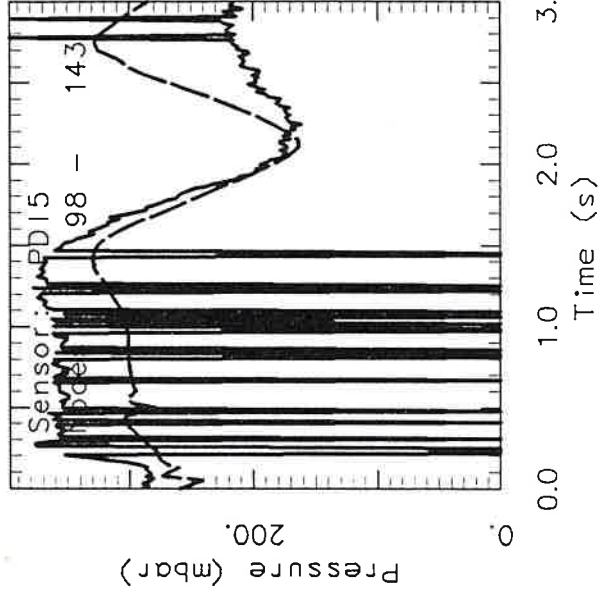
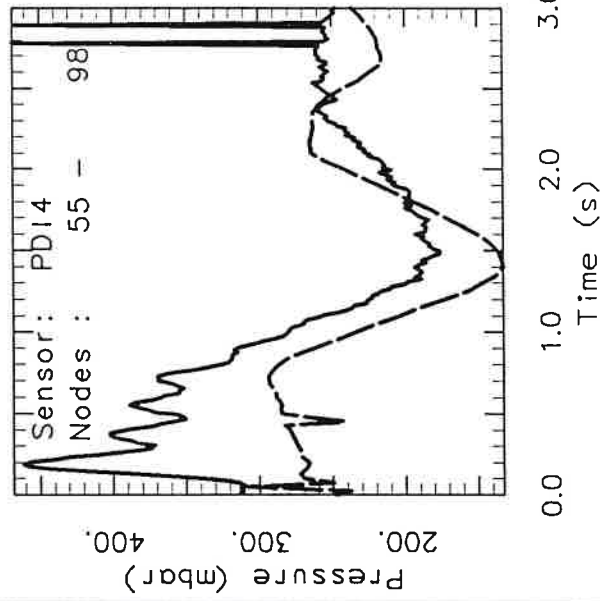
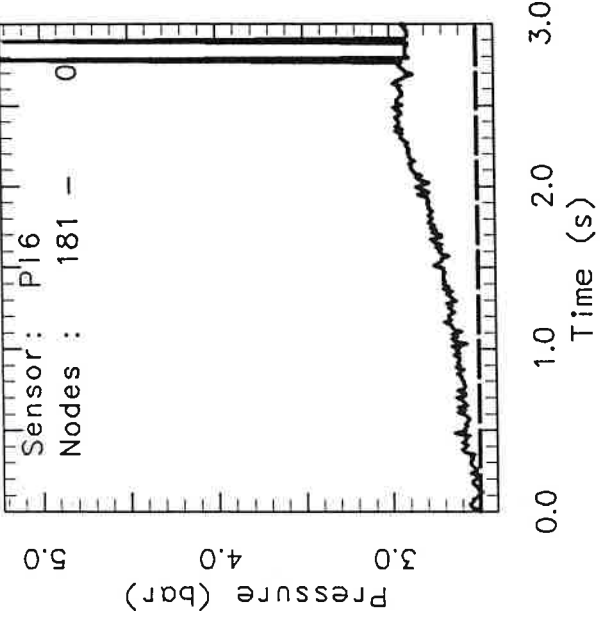
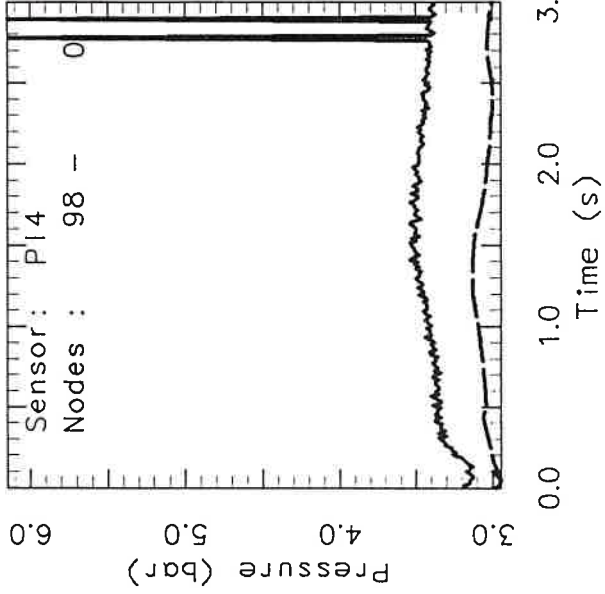
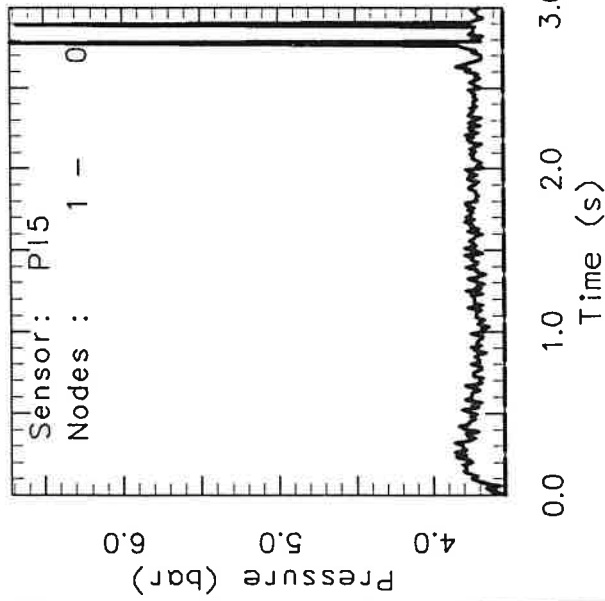
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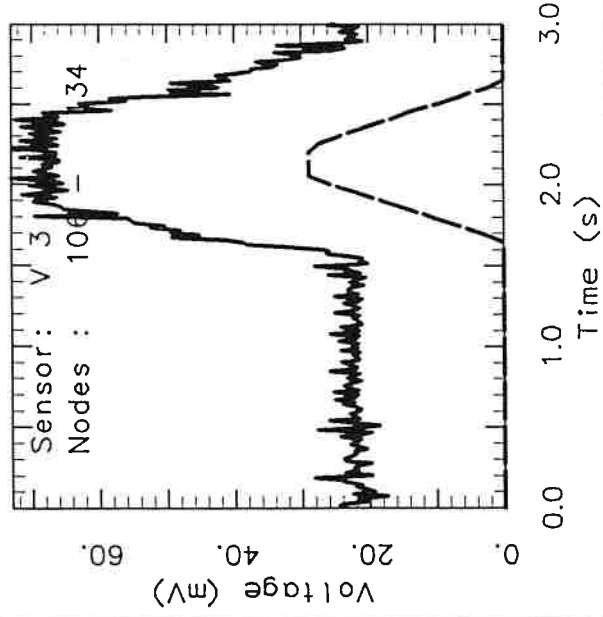
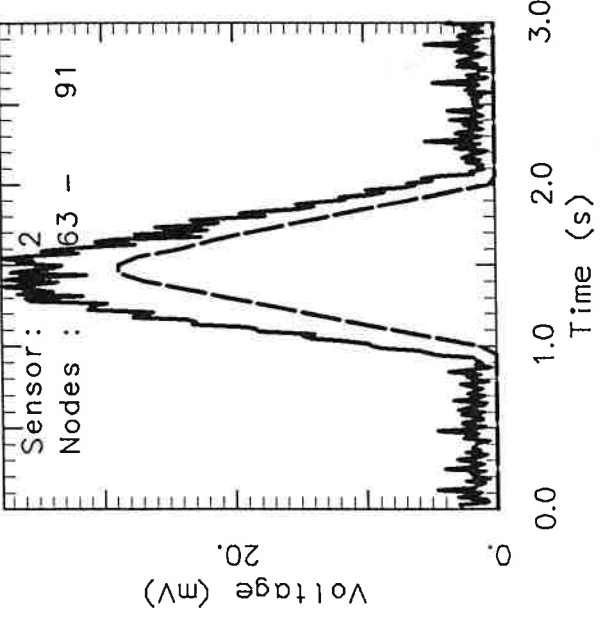
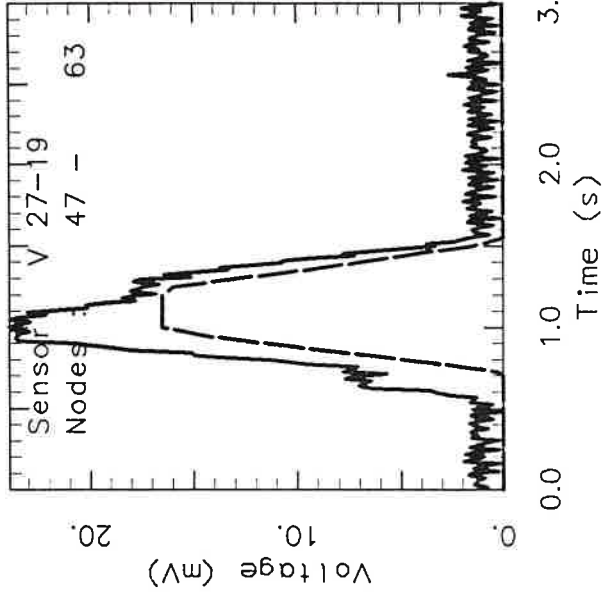
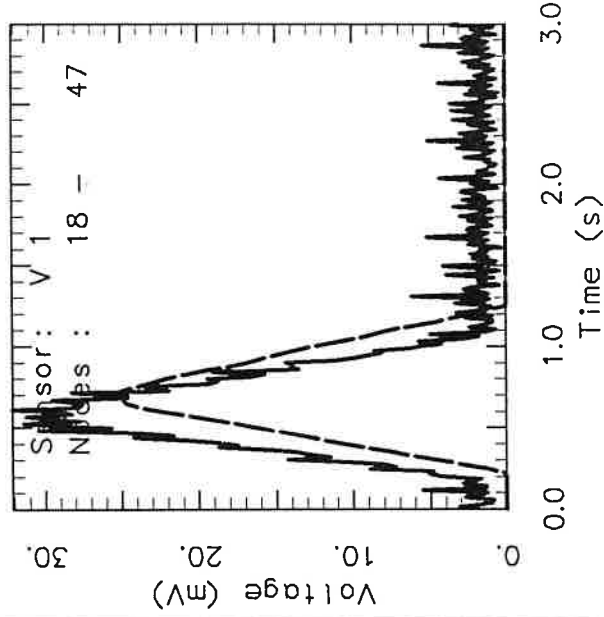
SIM # 77. t_{in}=0.20 nm. TSS 3 m→it. Min htc. eff pulse. rho=1.65



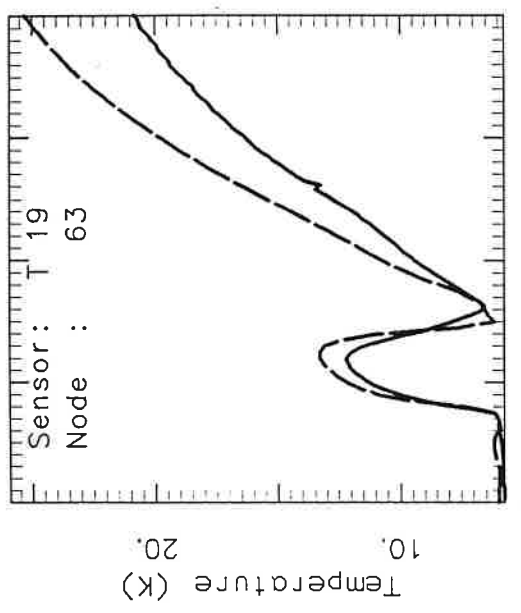
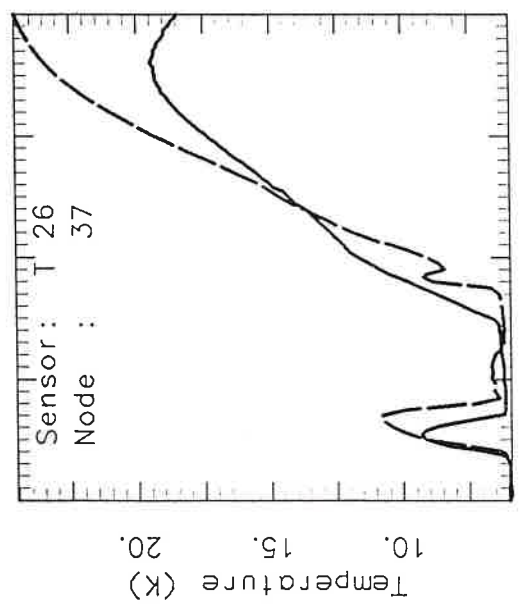
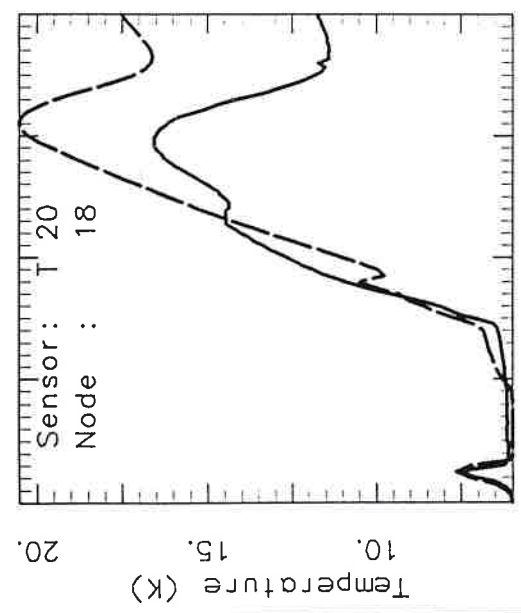
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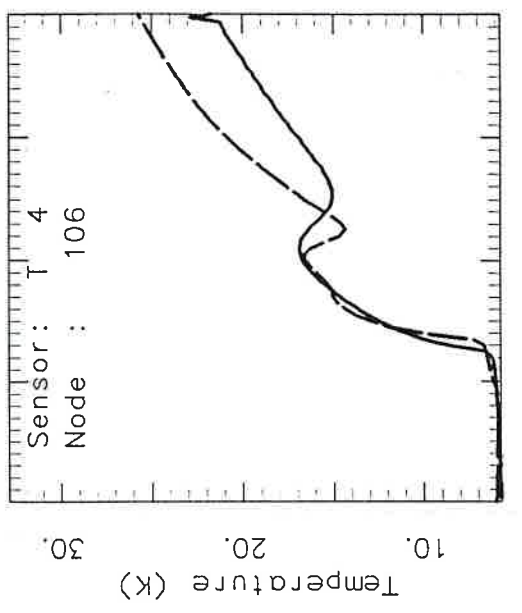
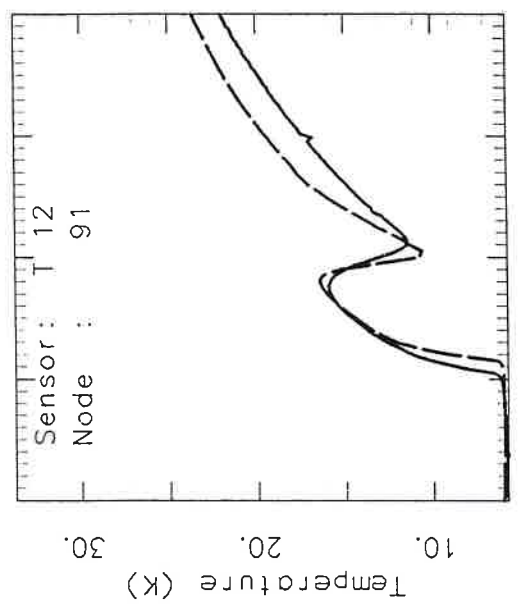
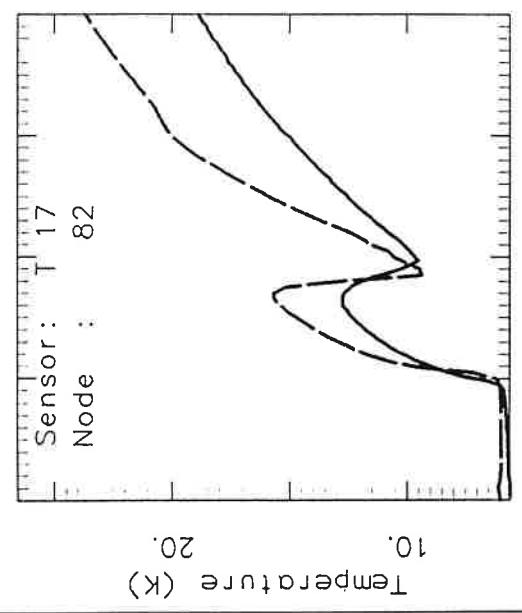
SIM # 48. 0.20 mm ins. TSS 3 mass it. min htc. 0.55*rho. no hyd net



Temperature (K)

Temperature (K)

Temperature (K)



Temperature (K)

Temperature (K)

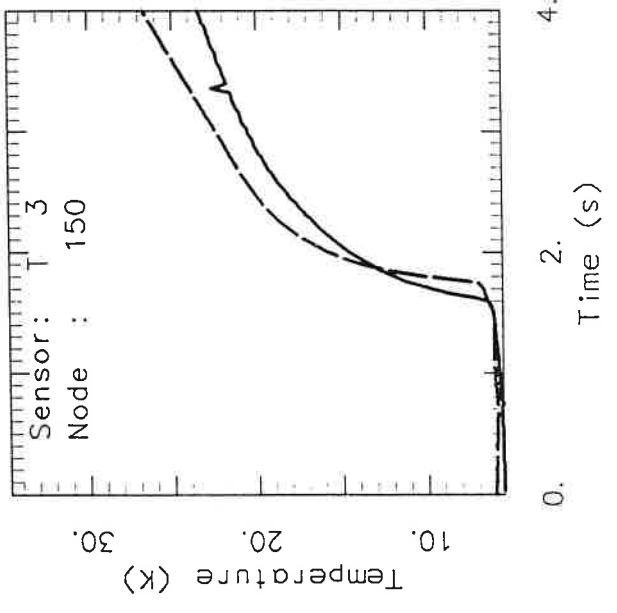
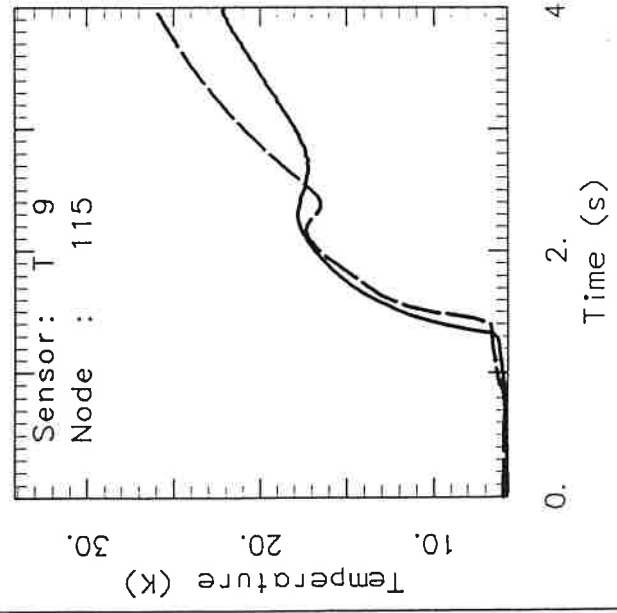
Temperature (K)

Time (s)

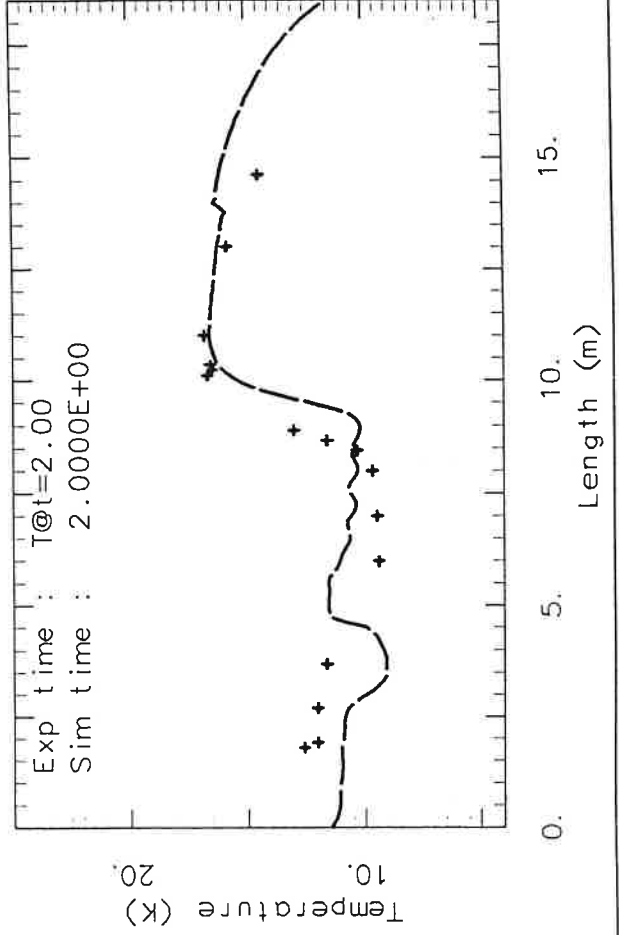
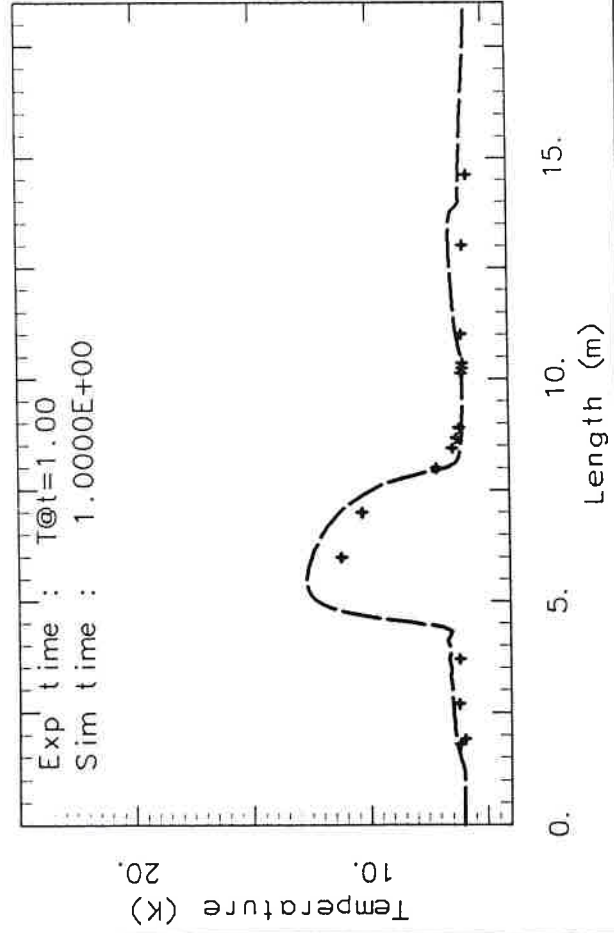
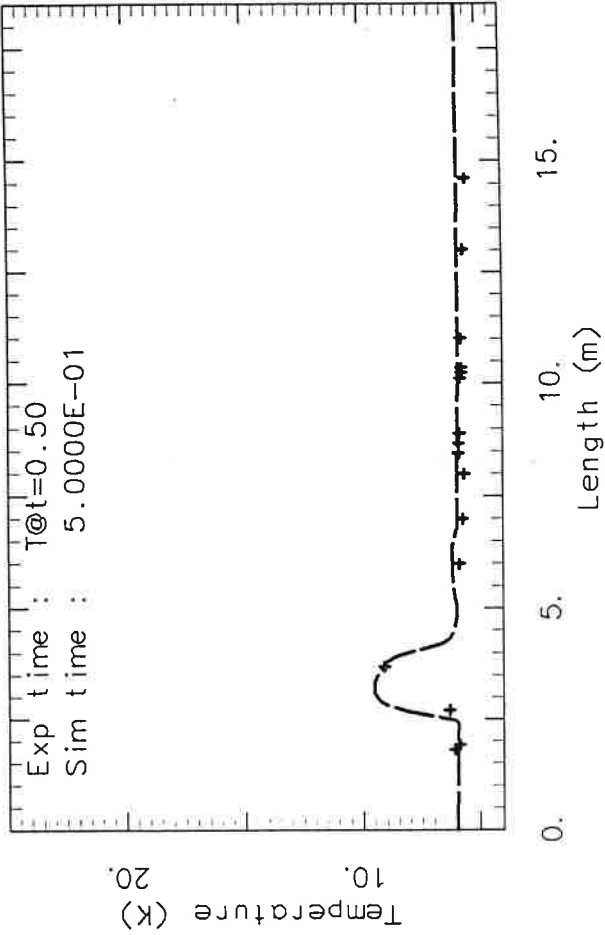
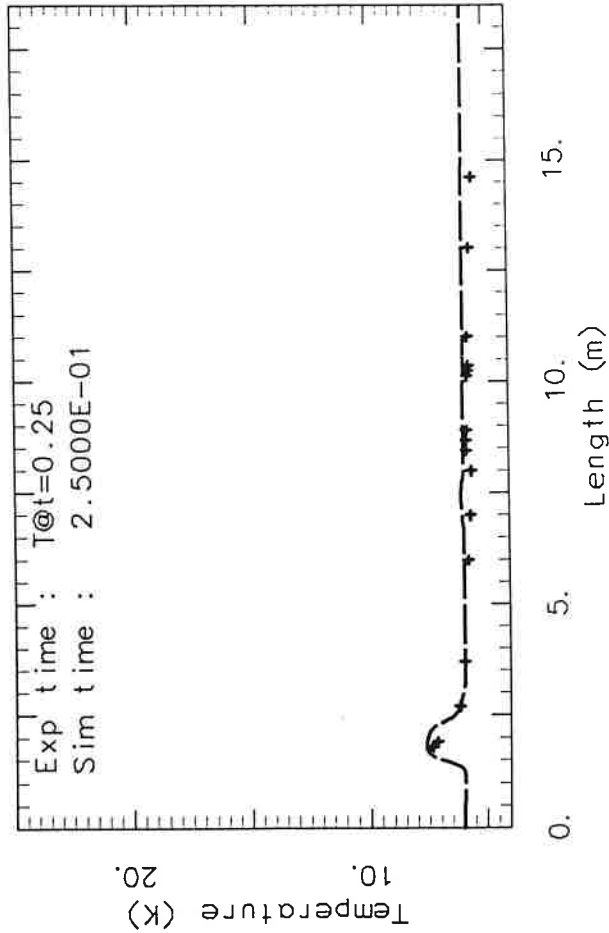
Time (s)

Time (s)

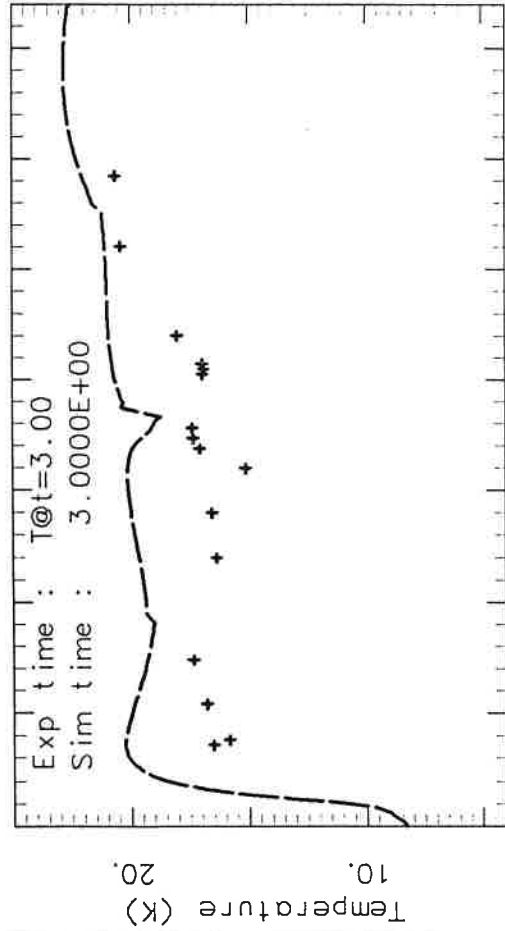
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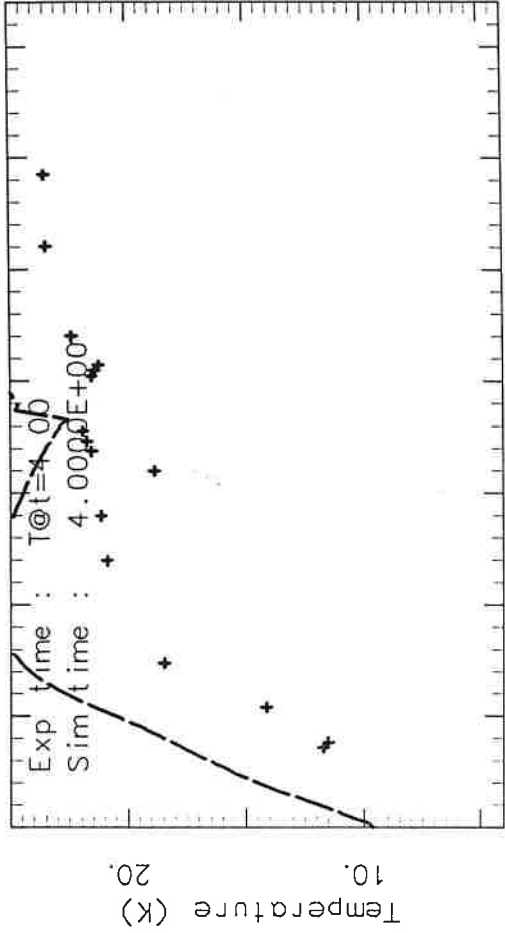


SIM # 48. 0.20 mm ins. TSS 3 mass it. min htc. 0.55*rho. no hyd net



0. 5. 10. 15.

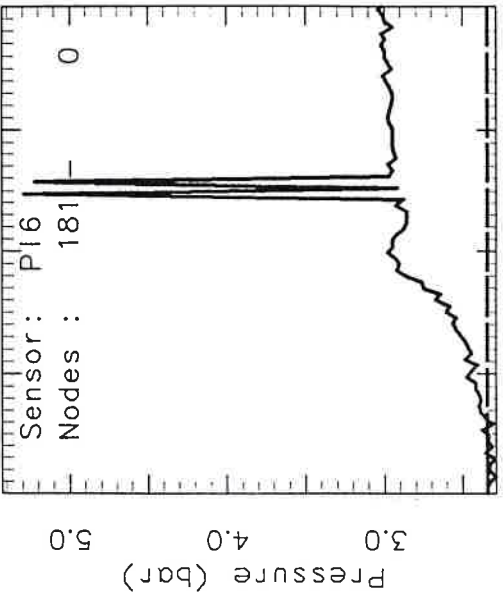
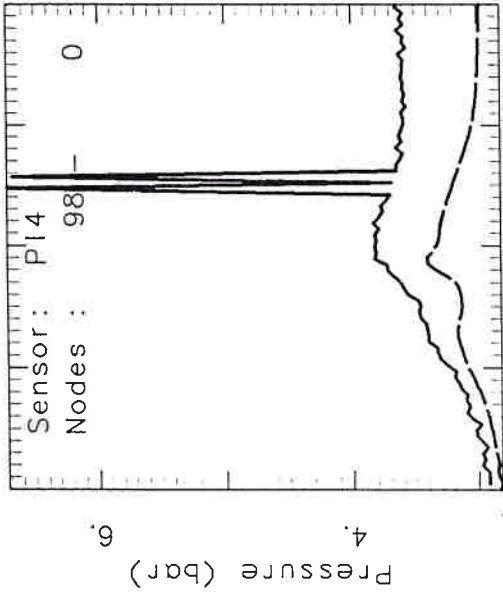
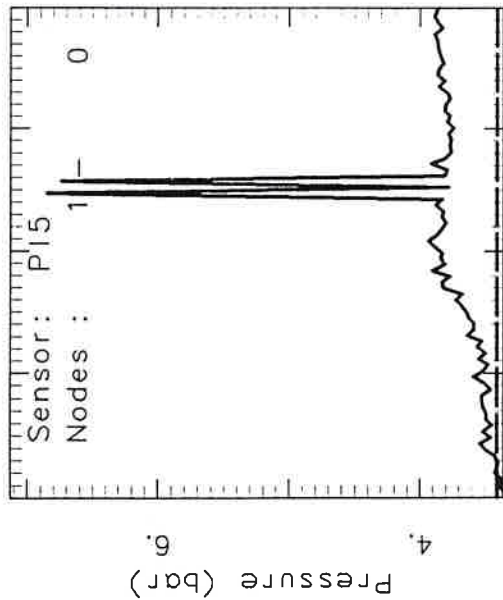
Length (m)



0. 5. 10. 15.

Length (m)

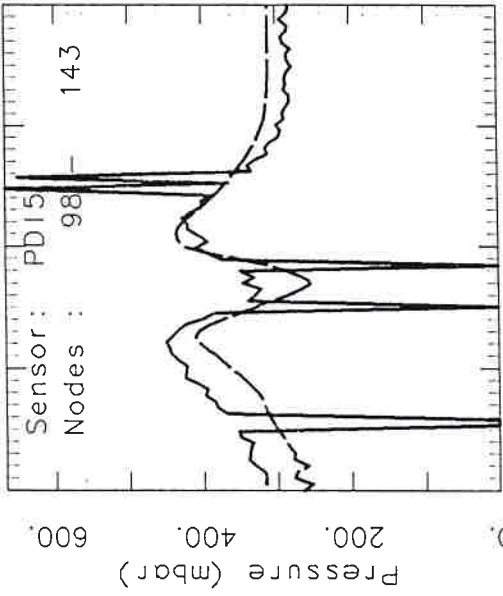
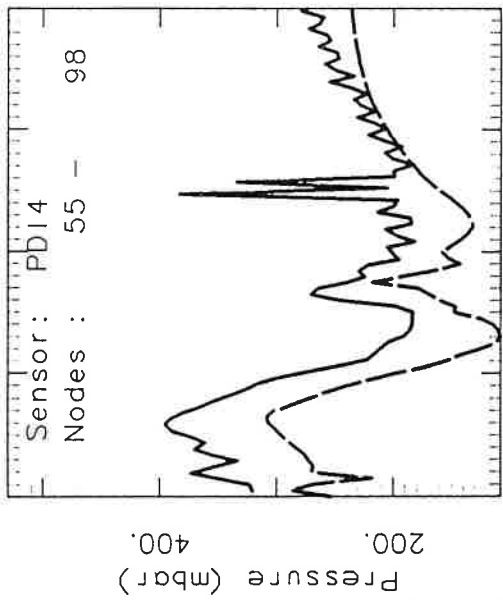
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0. 2. 4. Time (s)

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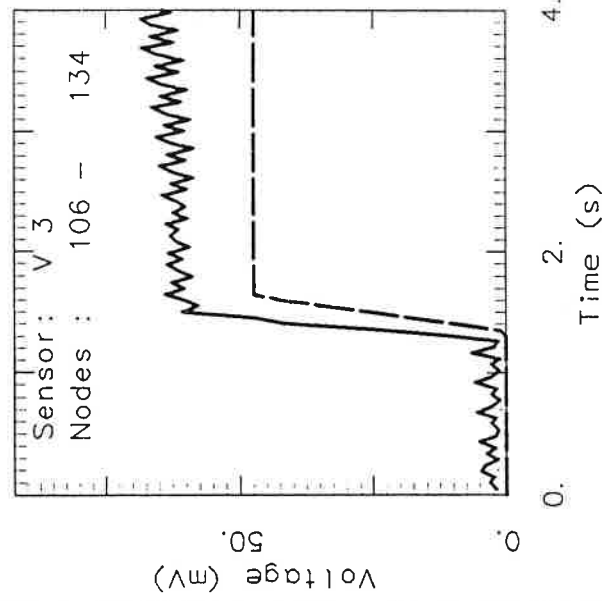
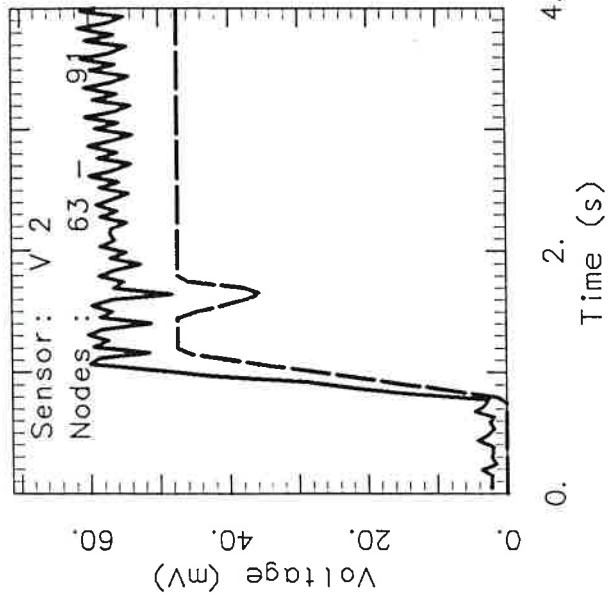
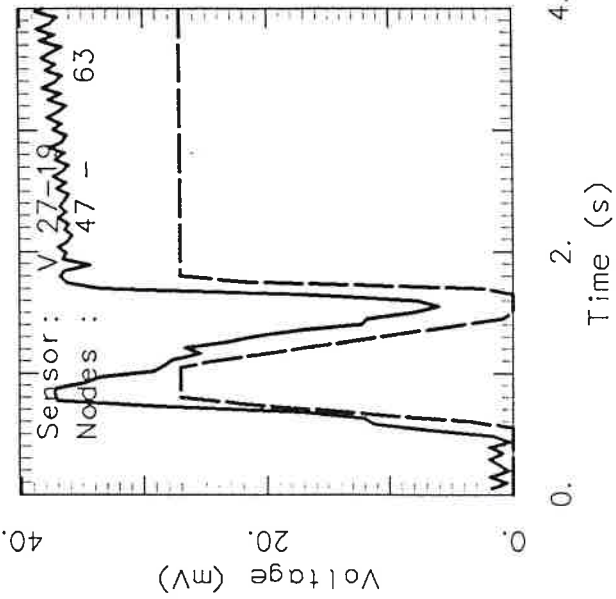
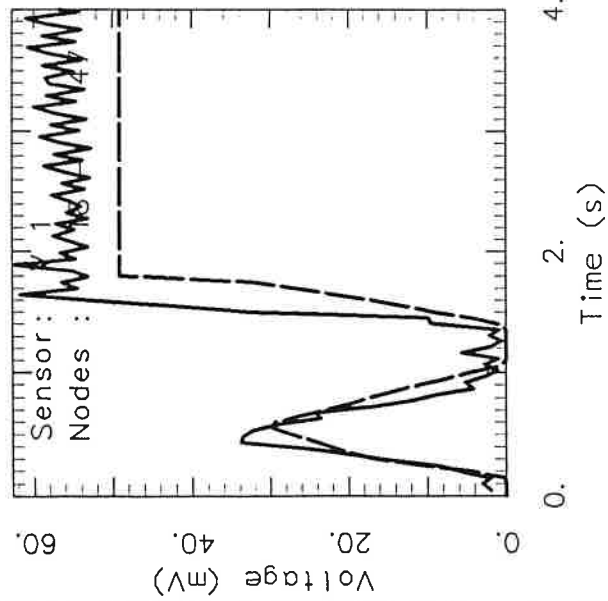


0. 2. 4. Time (s)

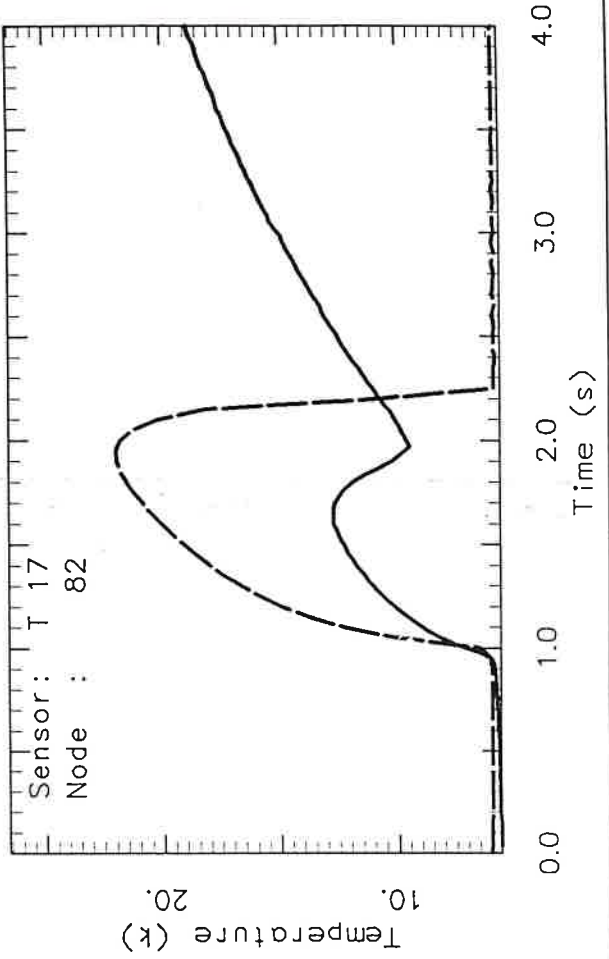
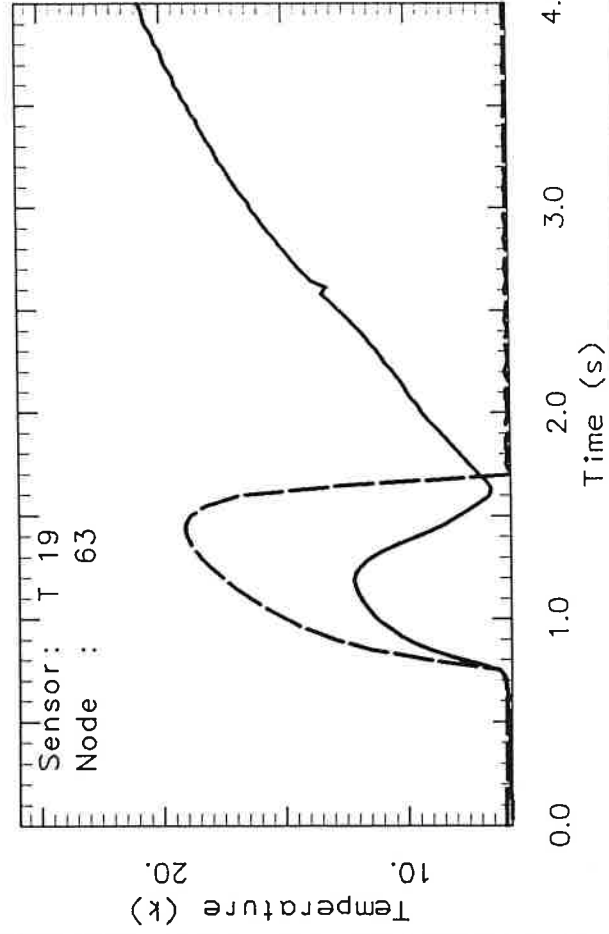
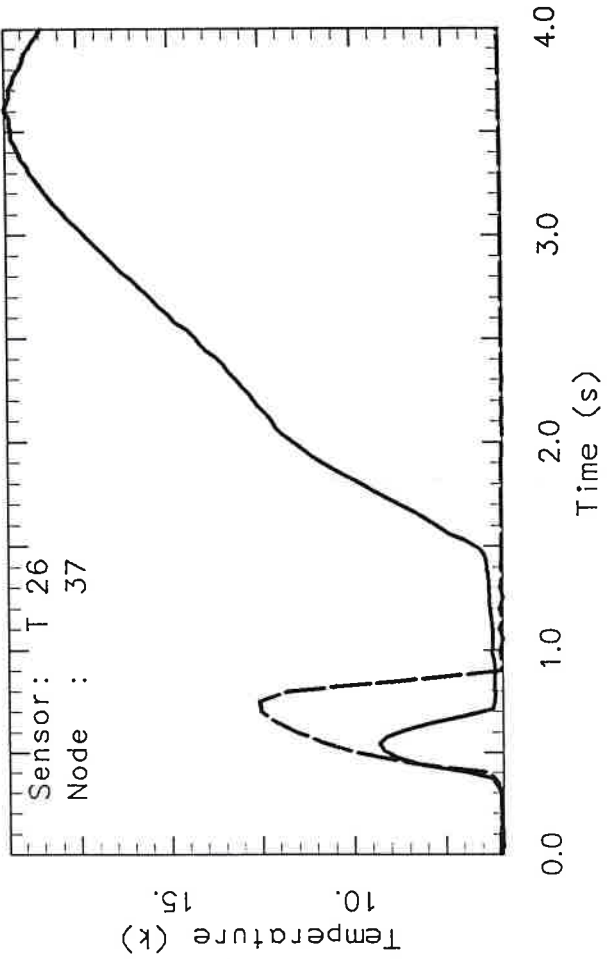
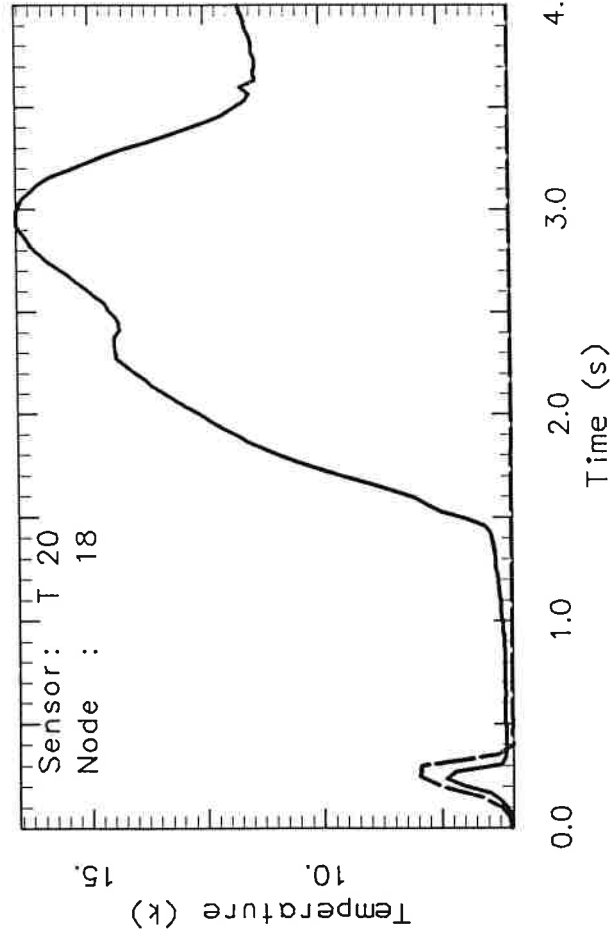
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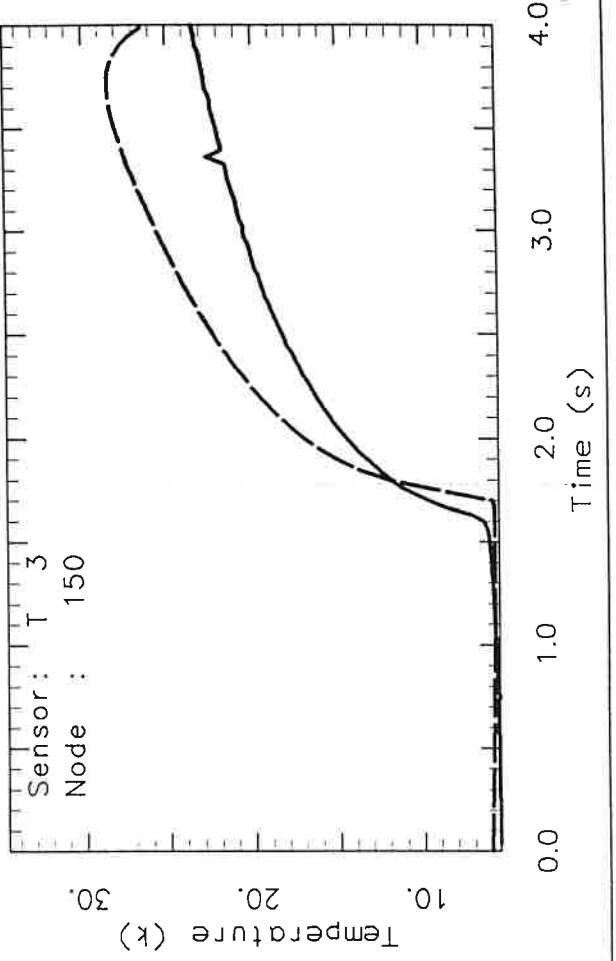
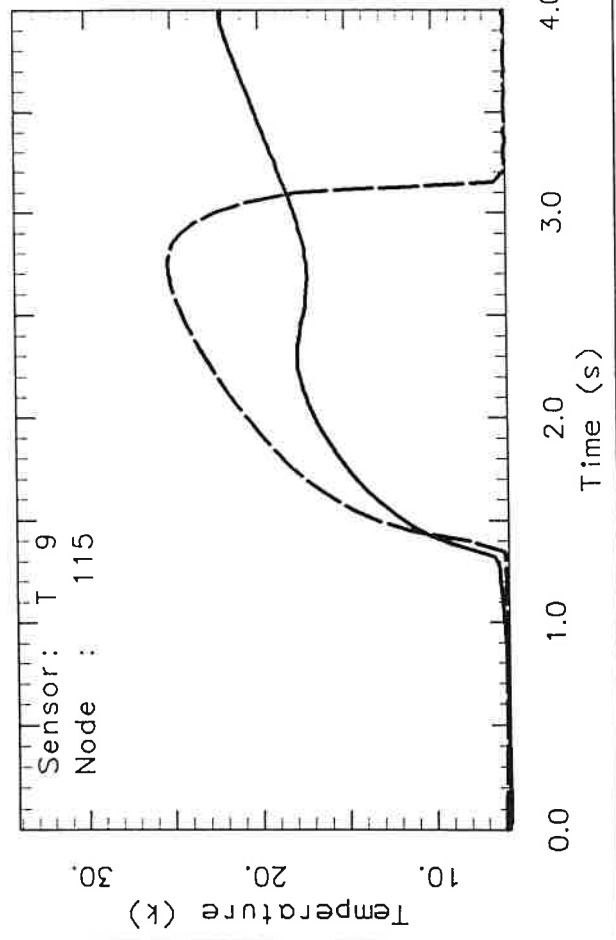
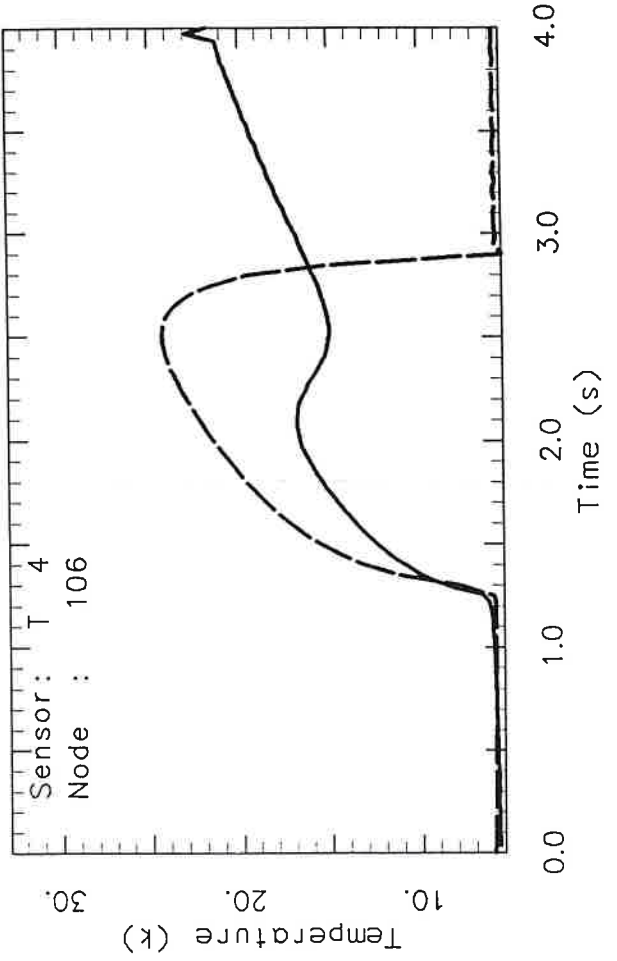
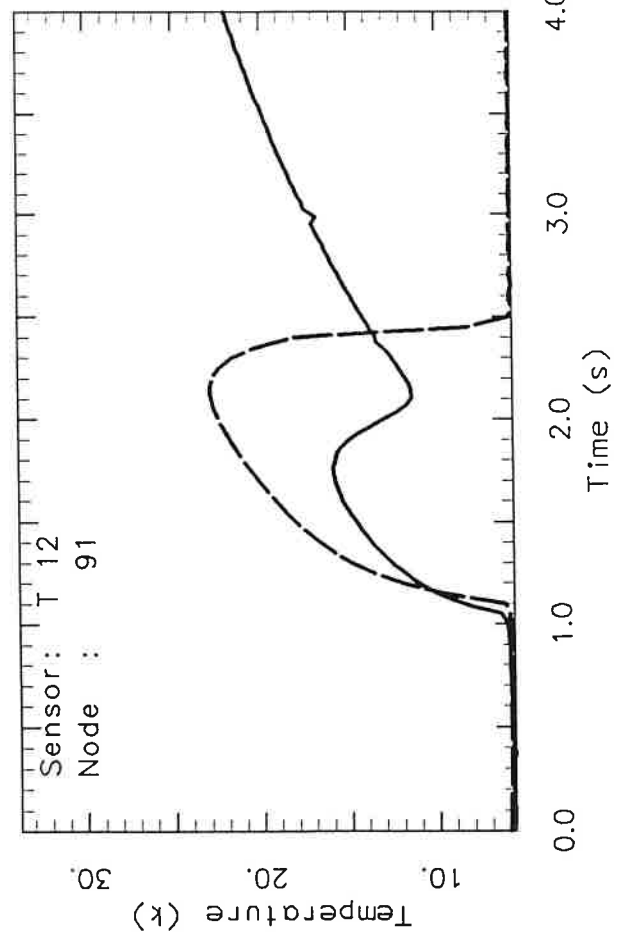
SIM # 48. 0.20 mm ins. TSS 3 mass it. min htc. 0.55*rho. no hyd net



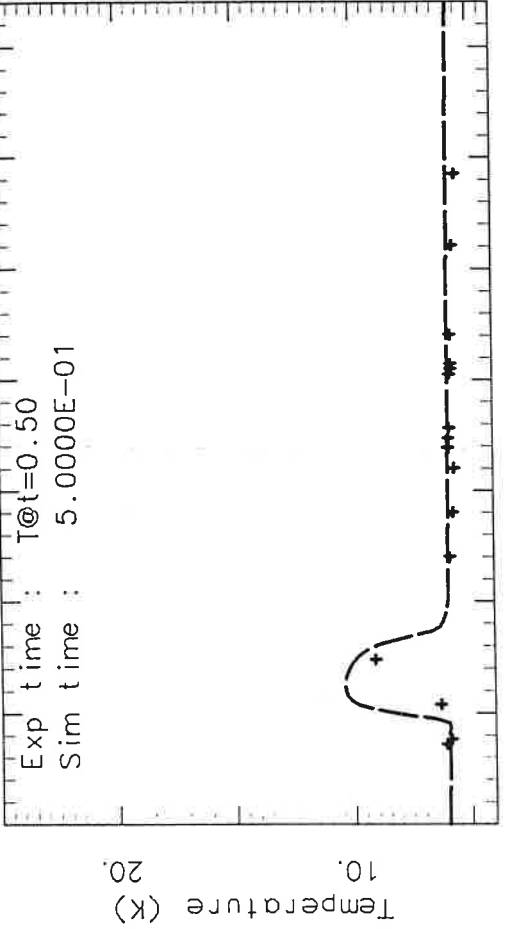
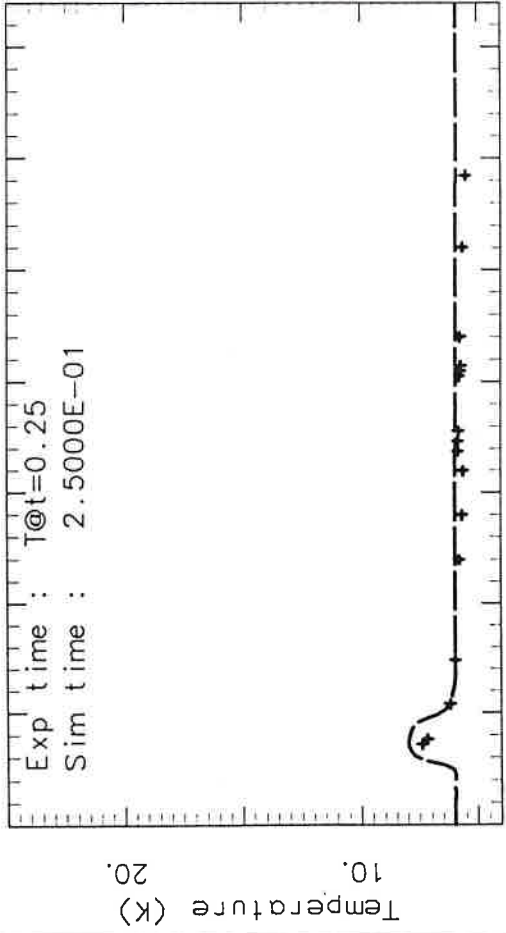
SIM # 48. TSS 3 mass it. min htc. 0.55*rho. no hyd net. 1-D RUN



SIM # 48. TSS 3 mass it. min htc. 0.55*rho. no hyd net. 1-D RUN

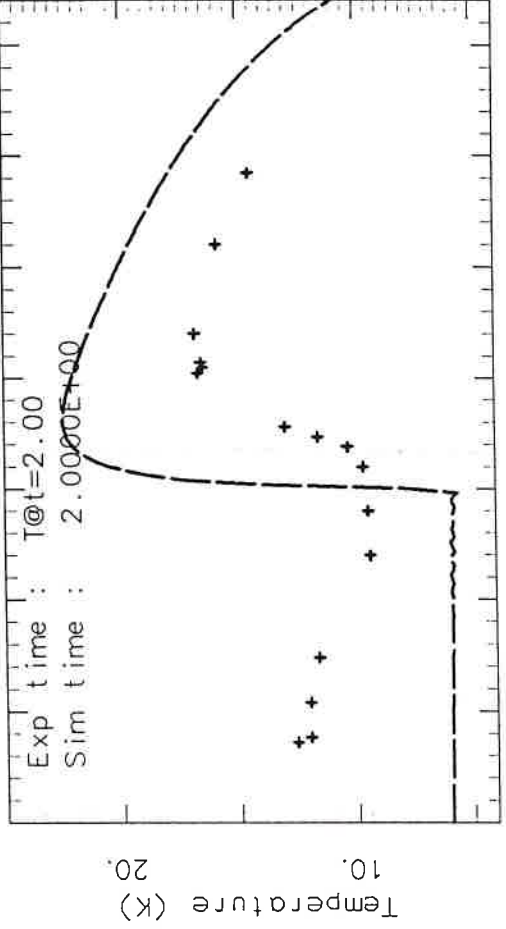
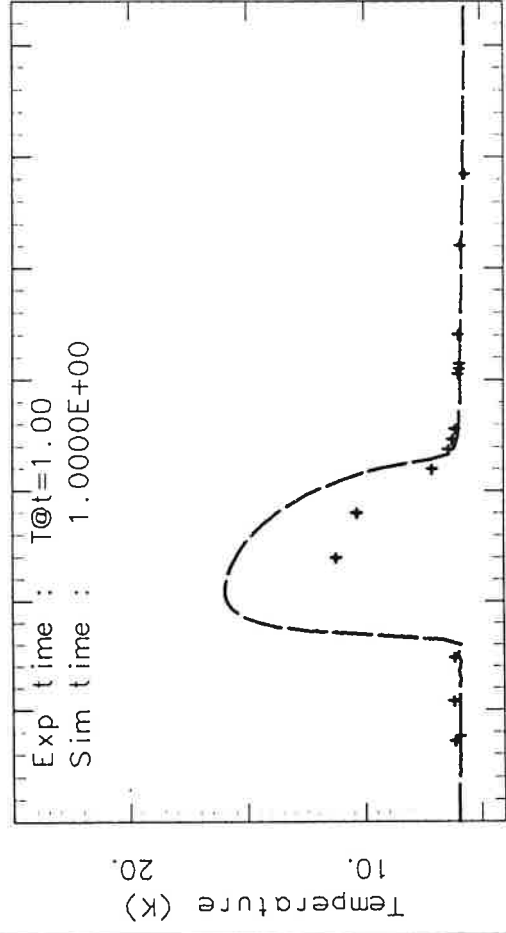


SIM # 48. TSS 3 mass it. min htc. 0.55*rho. no hyd net. 1-D RUN



Temperature (K)
Length (m)

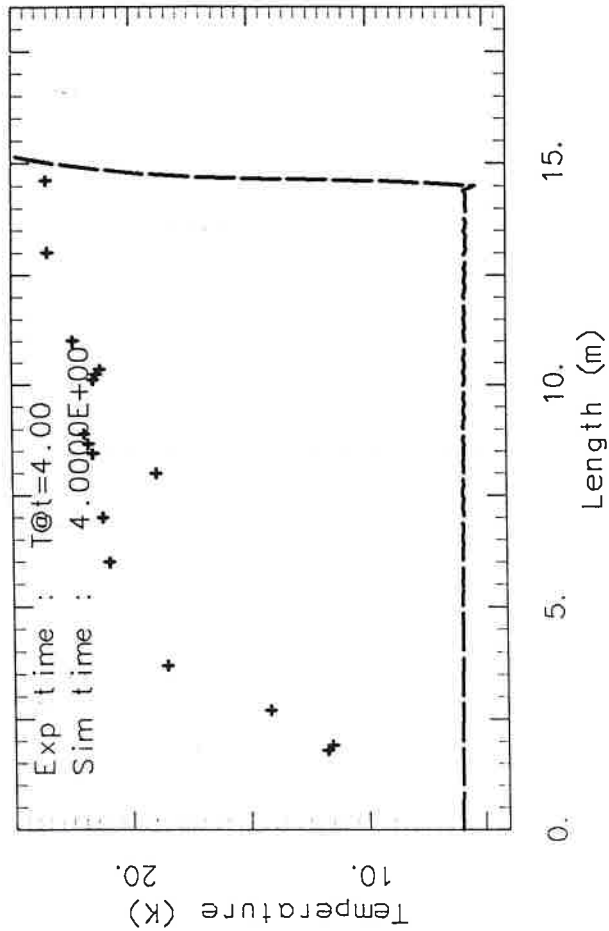
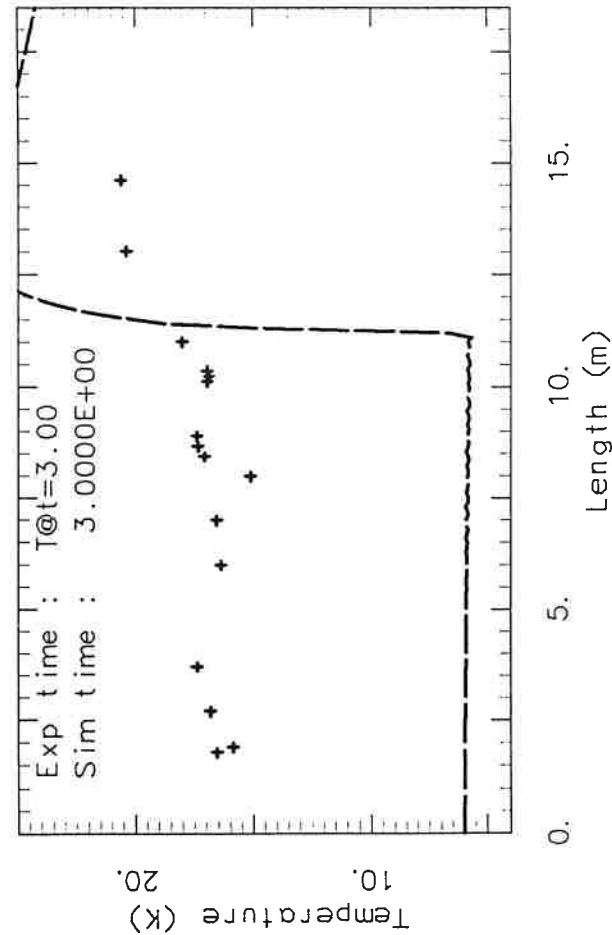
Temperature (K)
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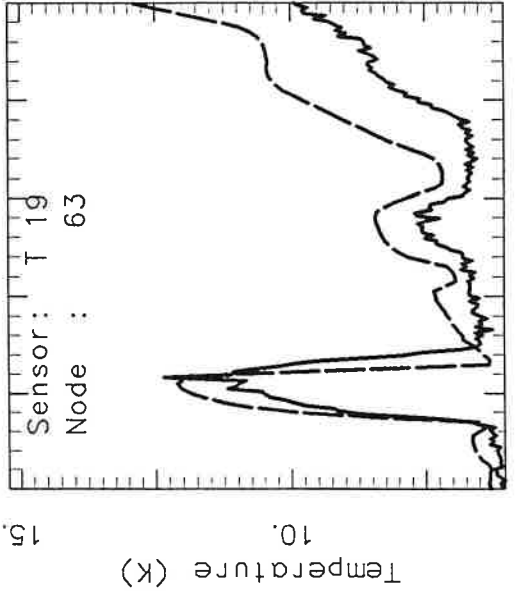
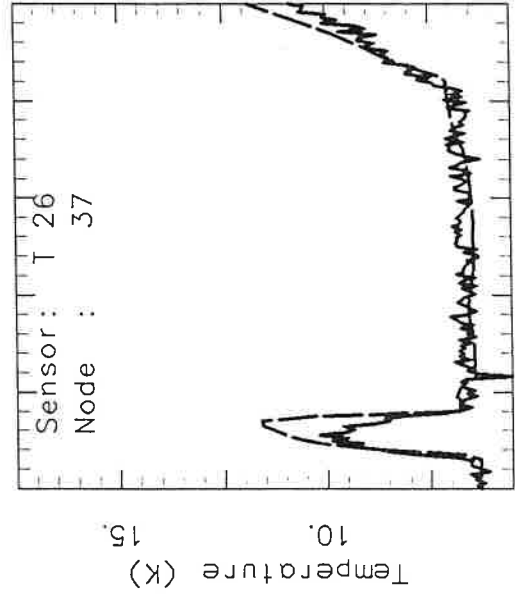
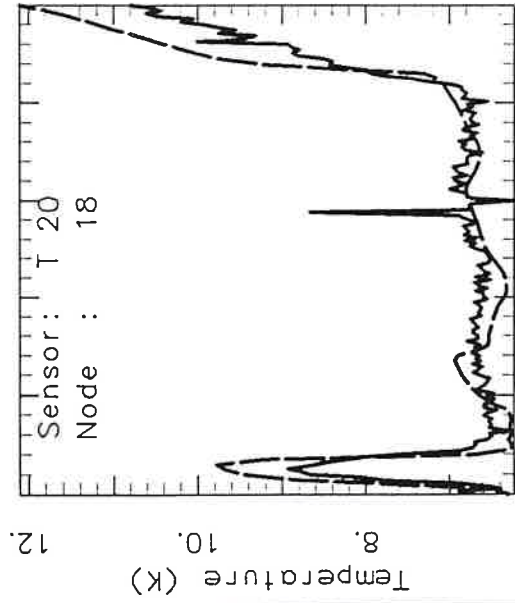
Temperature (K)
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SIM # 48. TSS 3 mass it. min htc. 0.55*rho. no hyd net. 1-D RUN



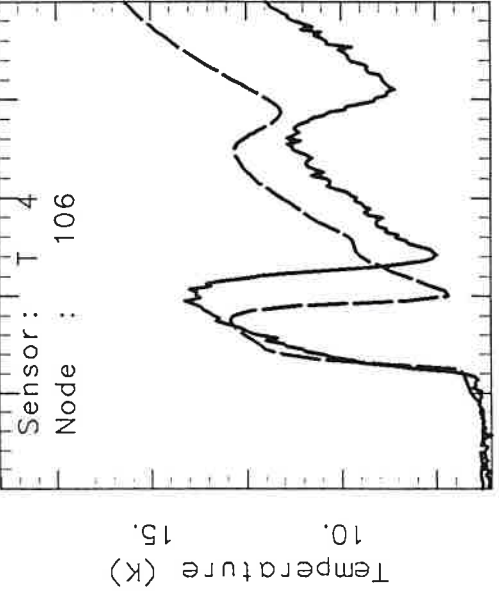
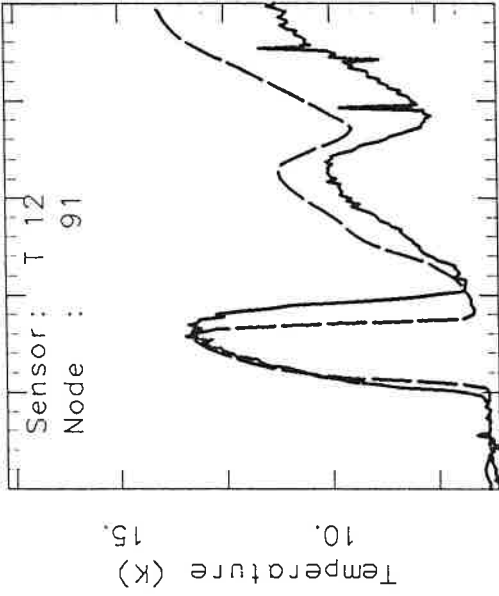
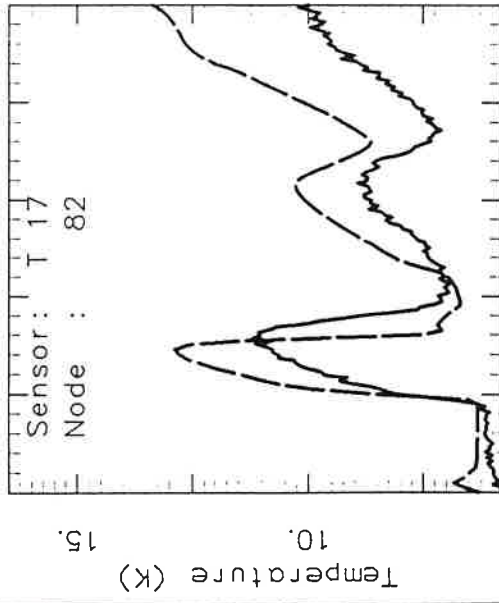
SIM # 45. t_{in}=0.20 mm. TSS 3 m→it. Min htc. rho=1.90e-10



0. 2. 4.
Time (s)

0. 2. 4.
Time (s)

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Time (s)

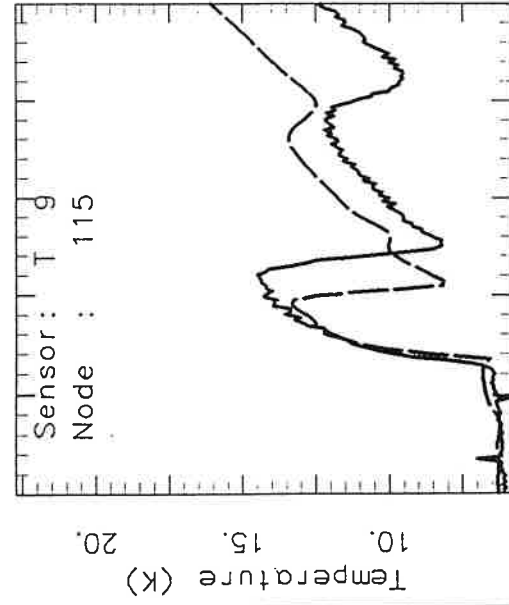


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Time (s)

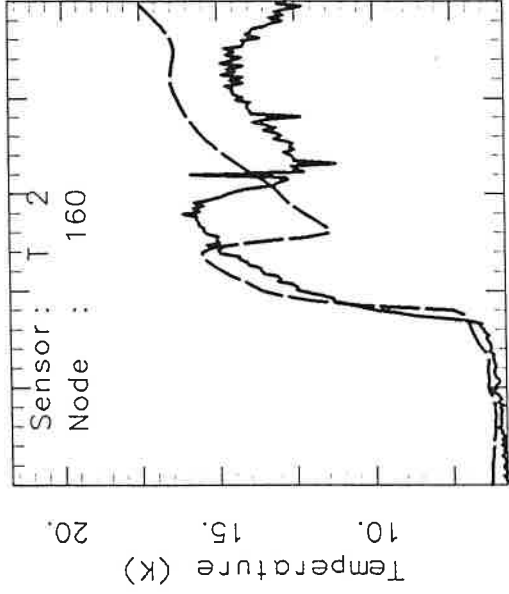
0. 2. 4.
Time (s)

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Time (s)

SIM # 45. t_{in}=0.20 nm. TSS 3 m_{it}. Min htc. rho=1.90e-10

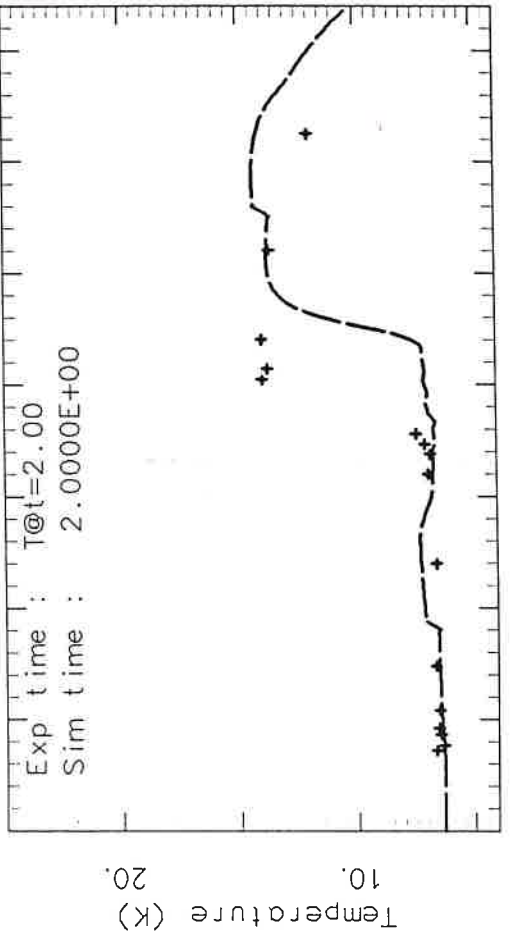
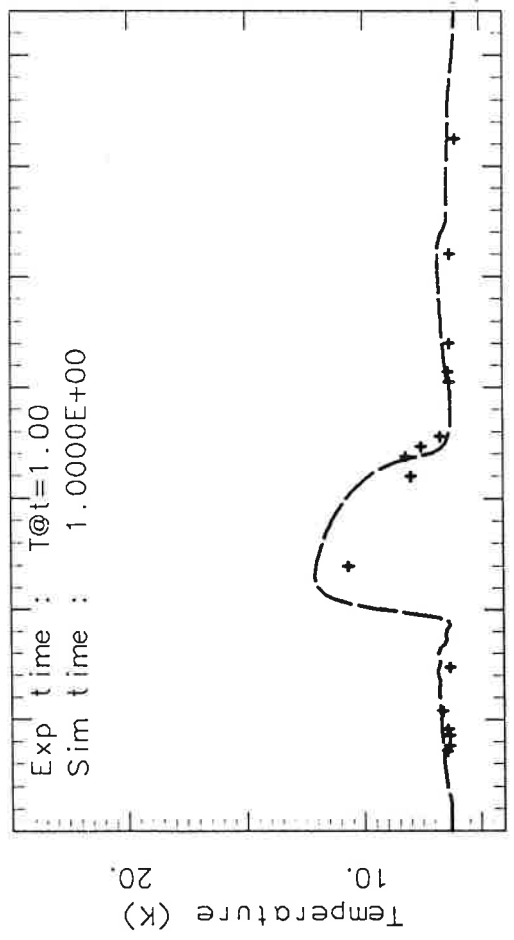
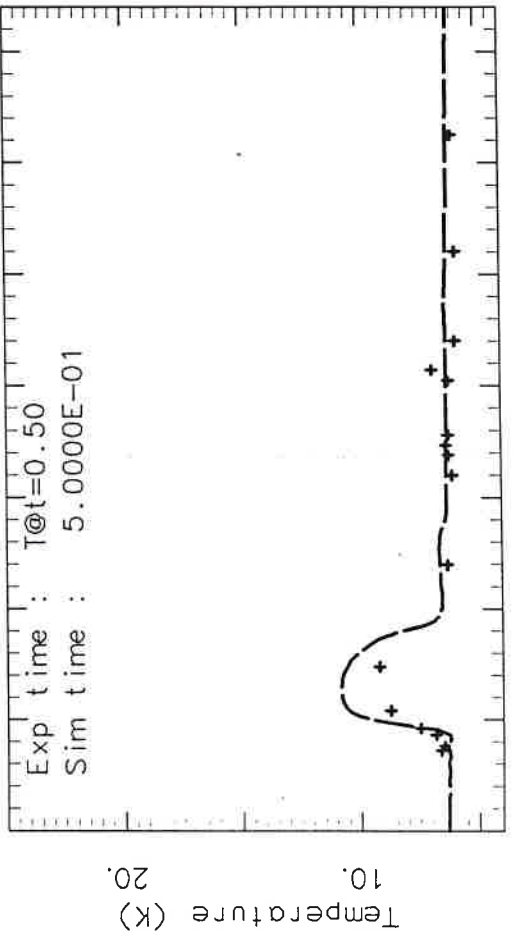
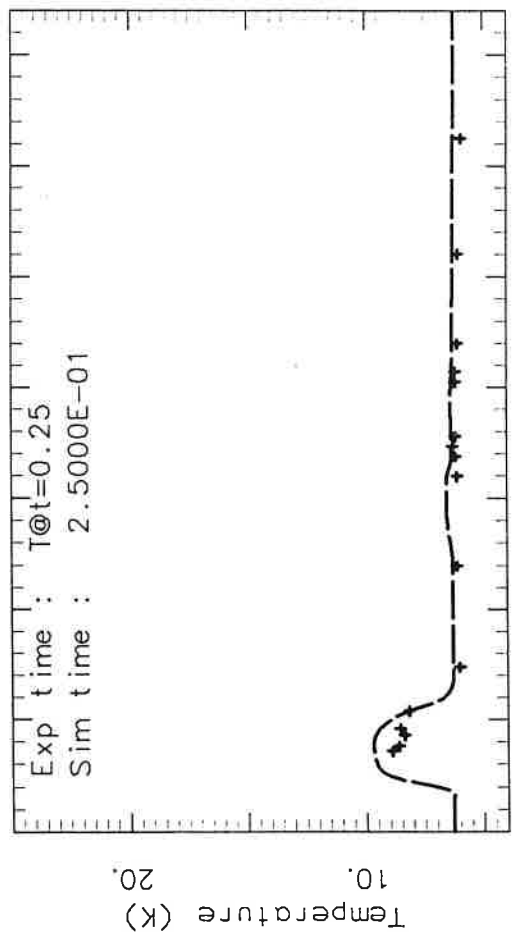


0. 2. 4.
Time (s)

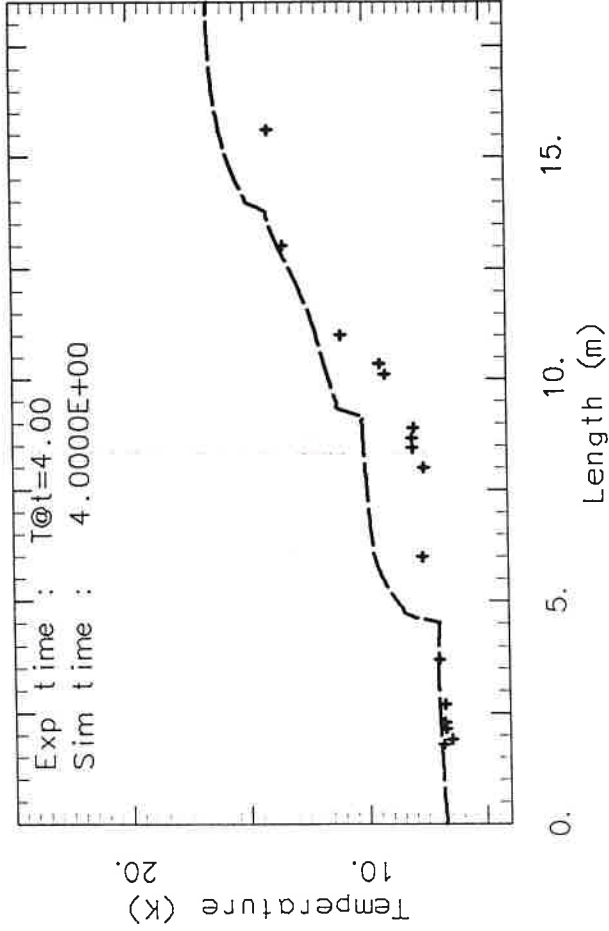
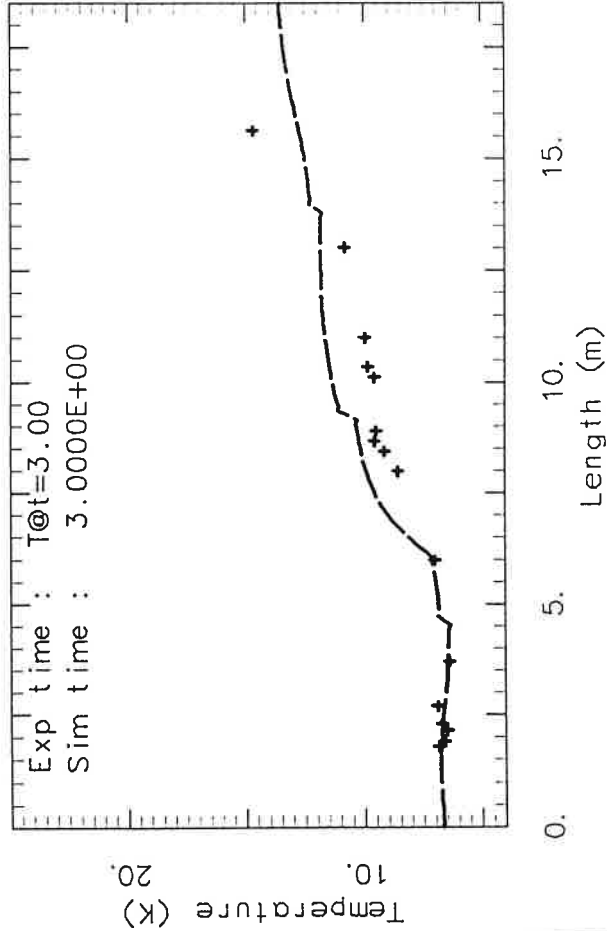


0. 2. 4.
Time (s)

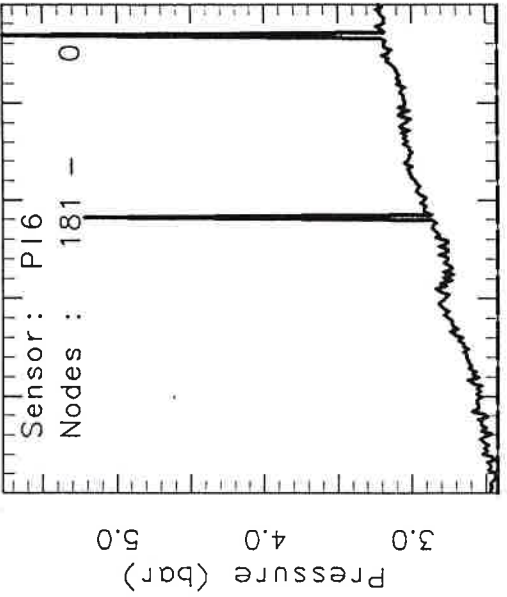
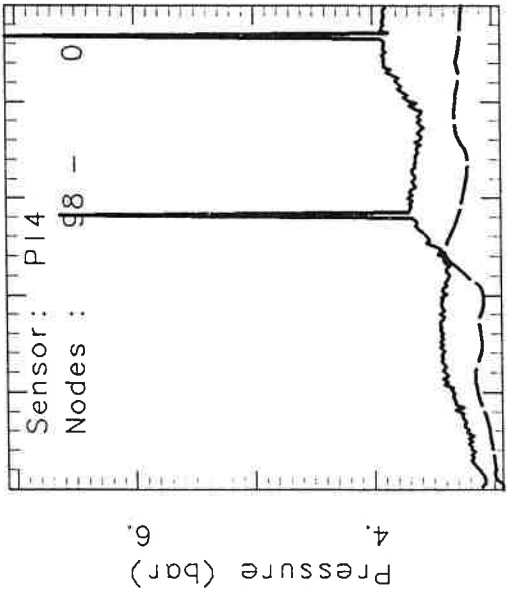
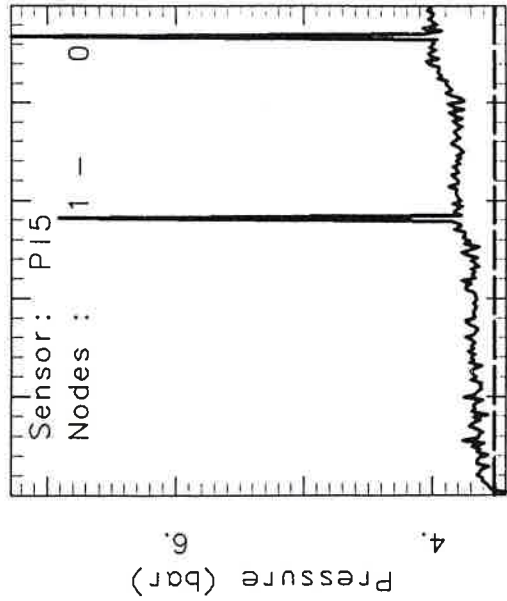
SIM # 45. t_{in}=0.20 mm. TSS 3 m_{it}. Min htc. rho=1.90e-10



SIM # 45. t_{in}=0.20 mm. TSS 3 m_{it}. Min htc. rho=1.90e-10



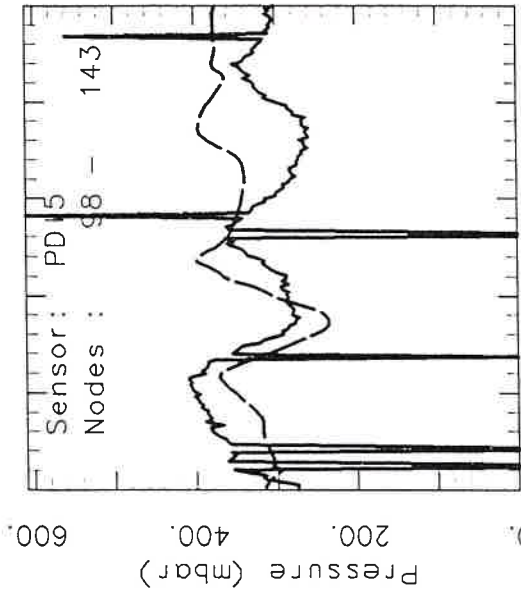
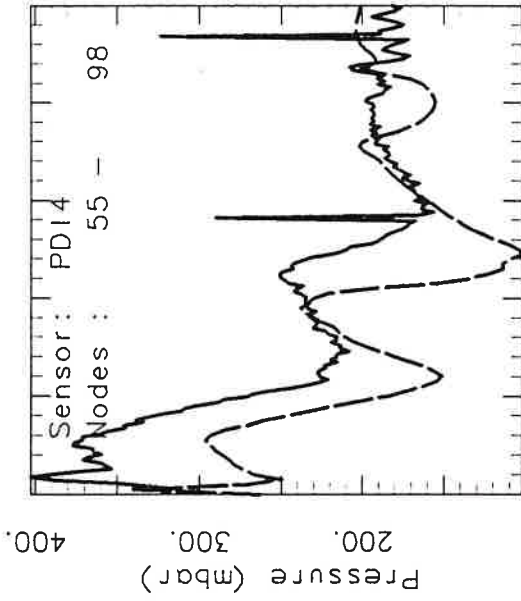
SIM # 45. t_{in}=0.20 mm. TSS 3 m→it. Min htc. rho=1.90e-10



Time (s)

Time (s)

Time (s)

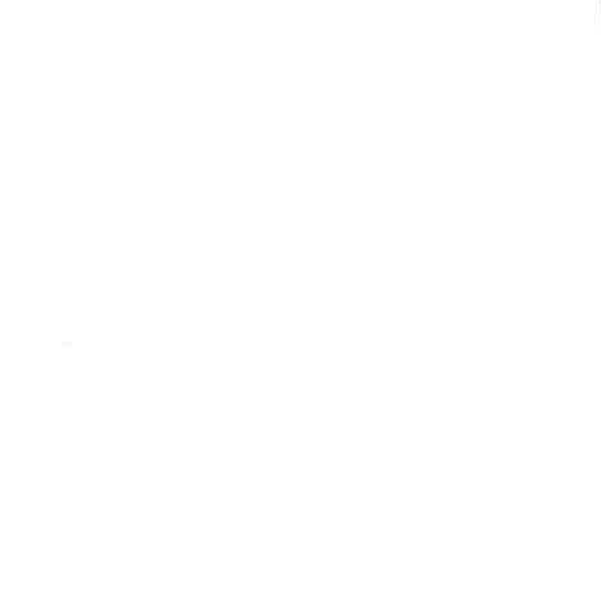
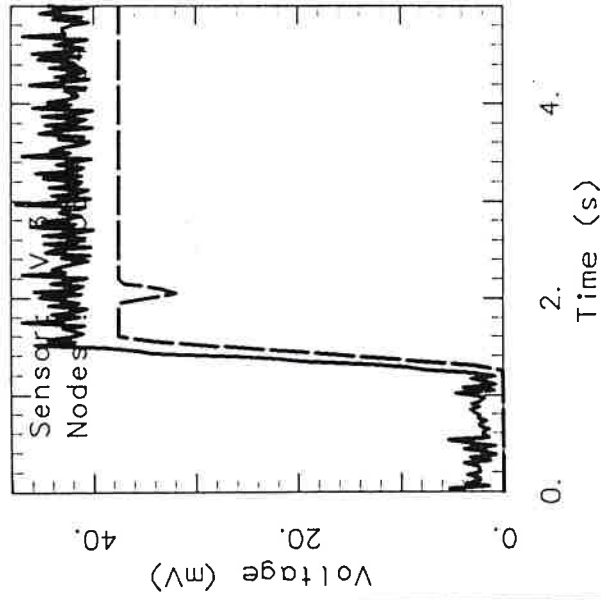
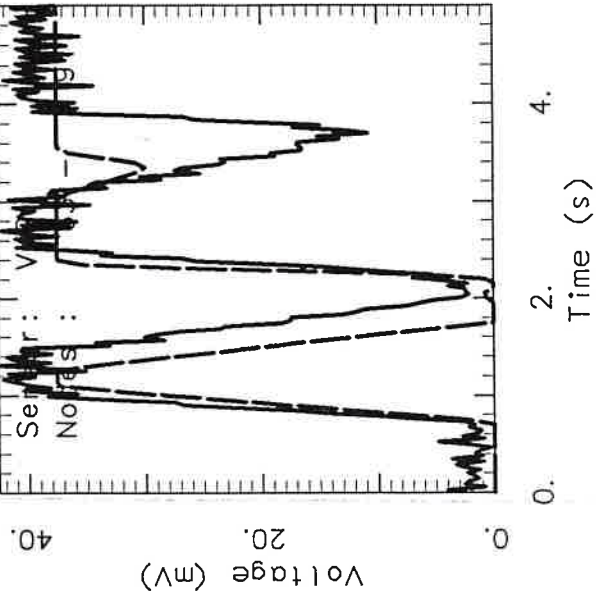
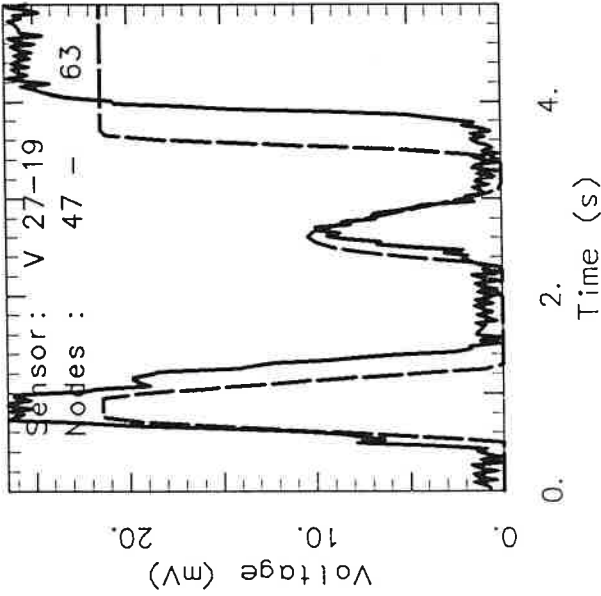
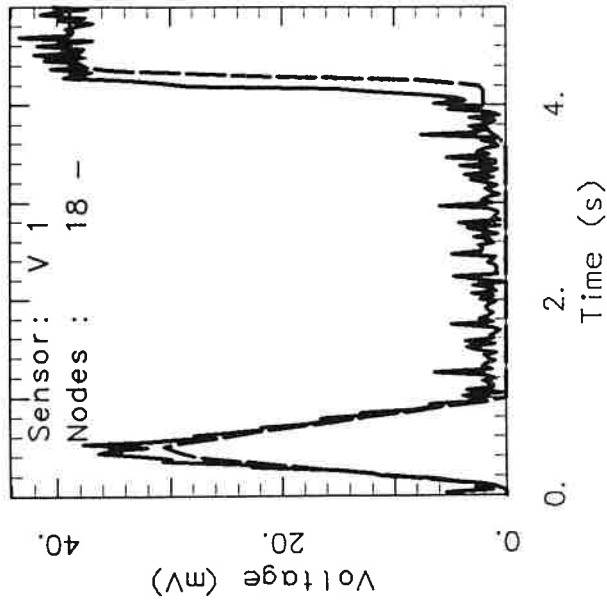


Time (s)

Time (s)

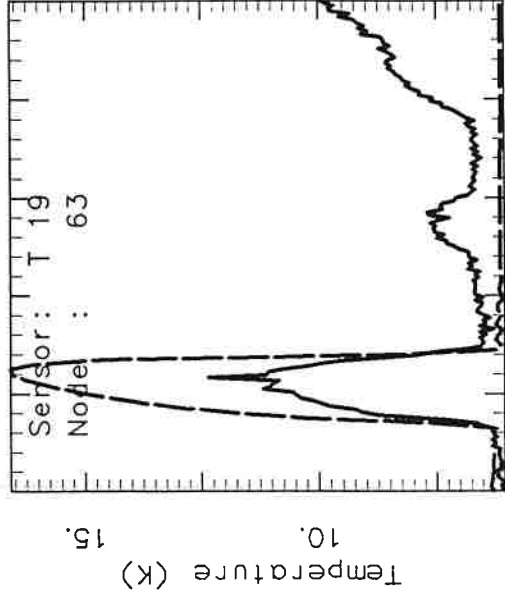
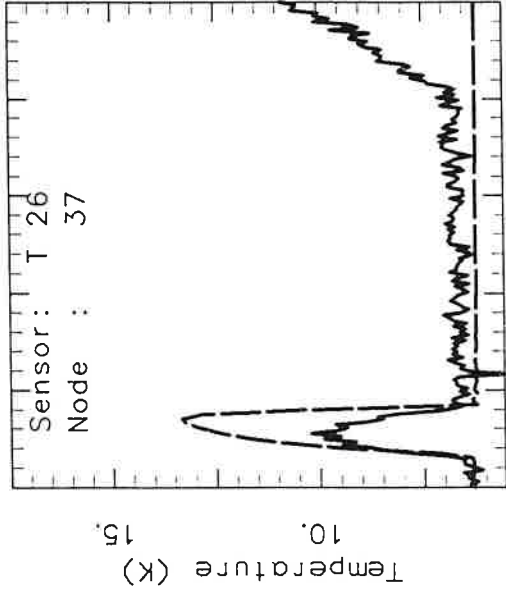
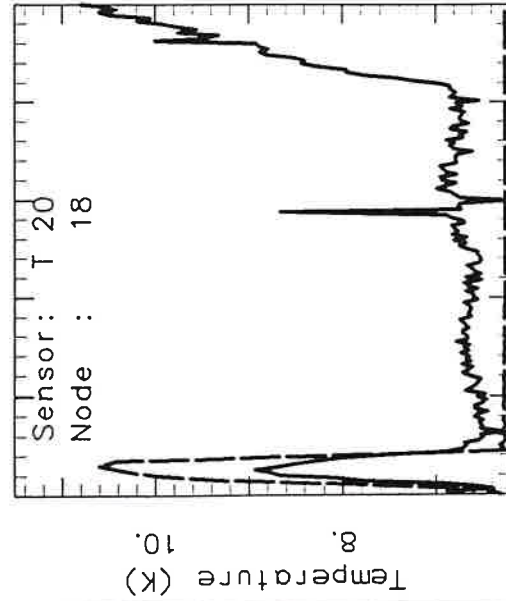
Time (s)

SIM # 45. t_{in}=0.20 mm. TSS 3 m_{it}. Min htc. rho=1.90e-10



SIM # 45. t_{in}=0.20 mm. TSS 3 m⁺it. Min htc. rho=1.8e-10. 1-D run

g



0. 2. 4. Time (s)

Temperature (K)

8.

10.

15.

0. 2. 4. Time (s)

Temperature (K)

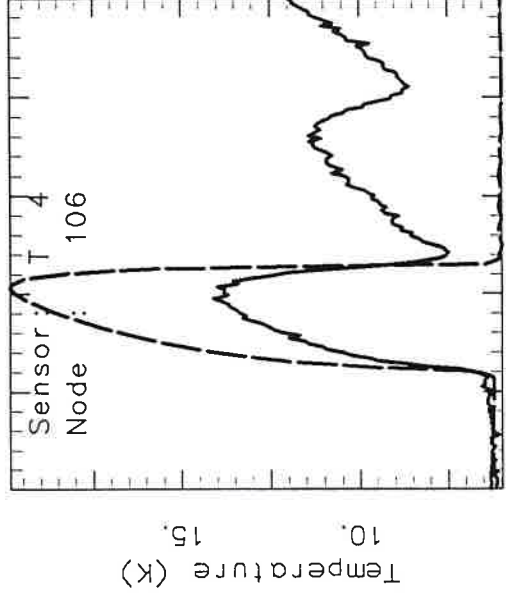
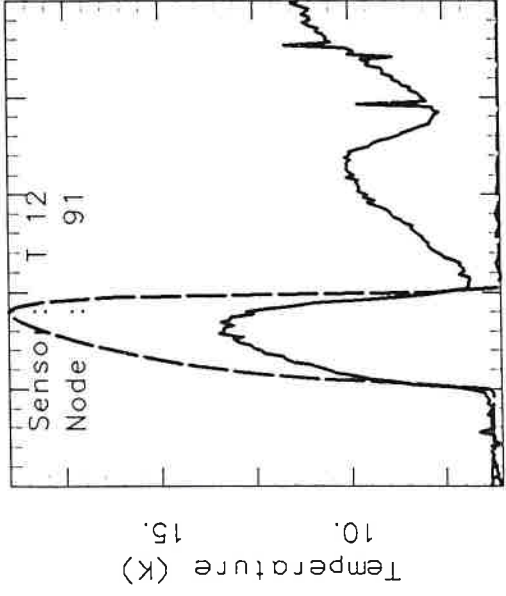
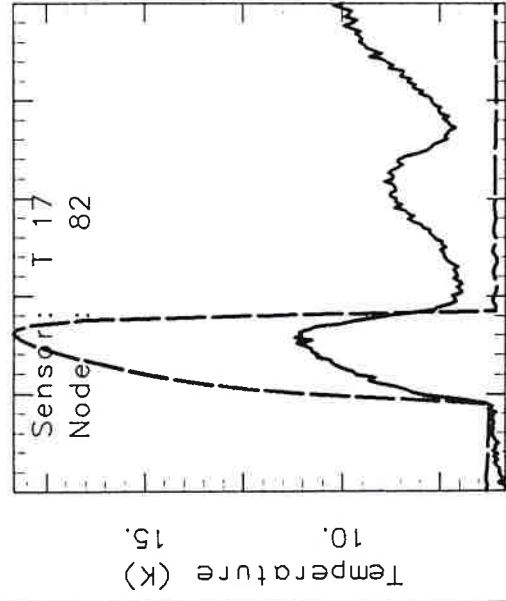
15.

17.

0. 2. 4. Time (s)

15.

17.



0. 2. 4. Time (s)

Temperature (K)

15.

17.

15.

0. 2. 4. Time (s)

Temperature (K)

15.

17.

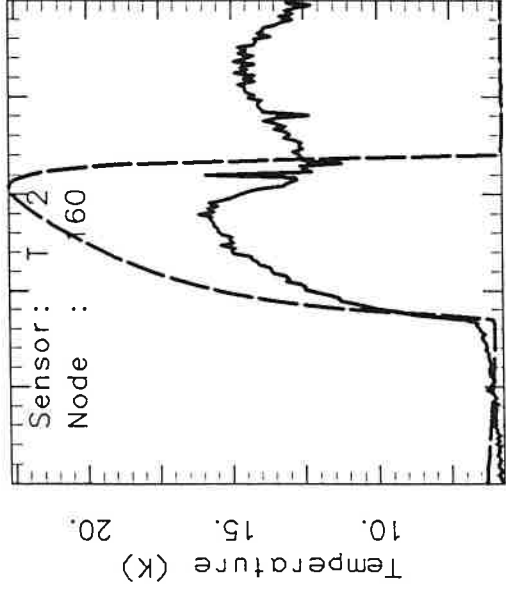
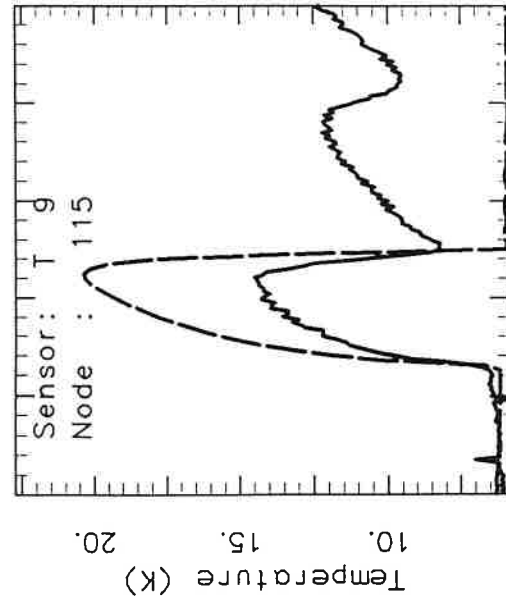
0. 2. 4. Time (s)

15.

17.

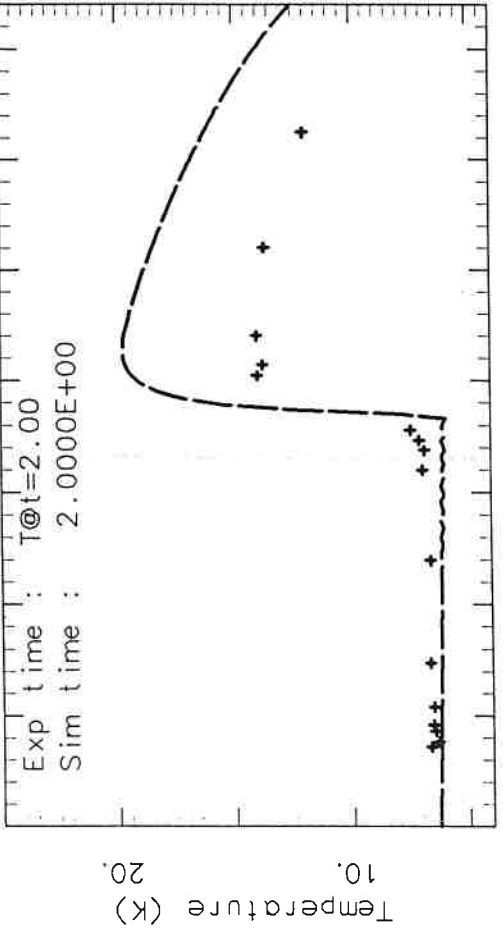
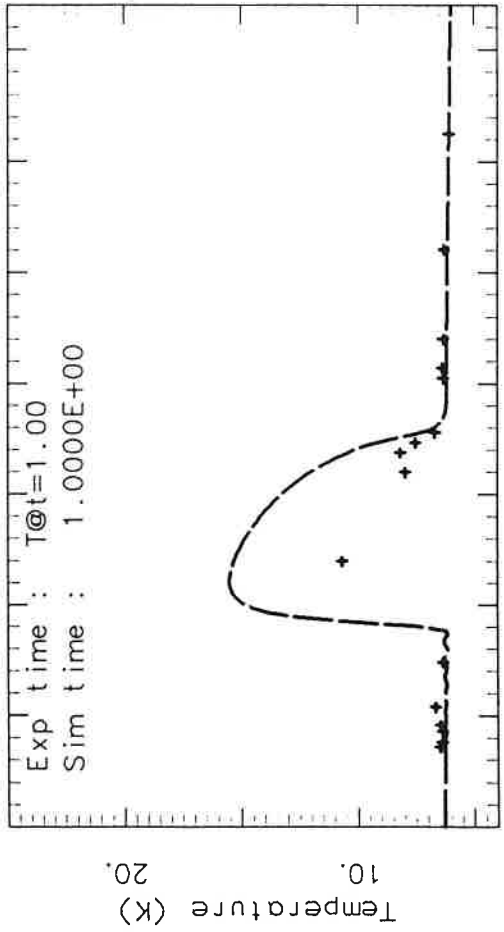
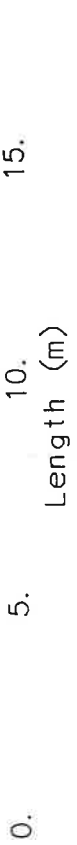
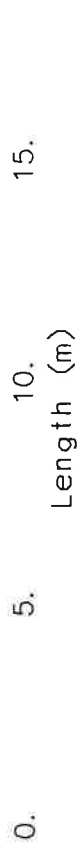
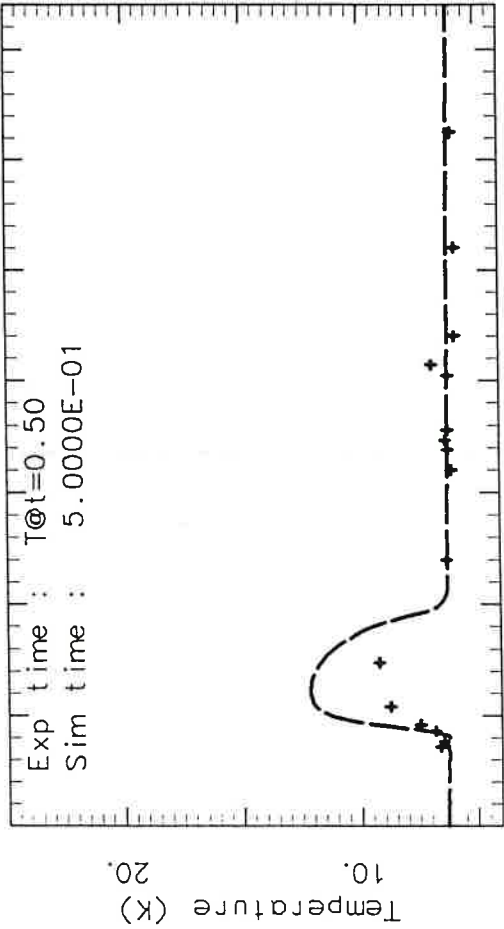
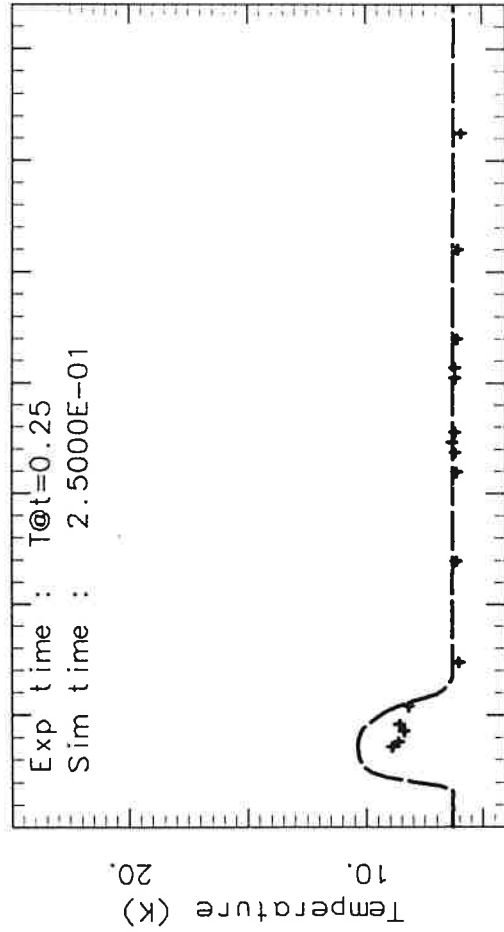
SIM # 45. $t_{in}=0.20$ mm. TSS 3 m+it. Min htc. rho=1.80e-10. 1-D run

g



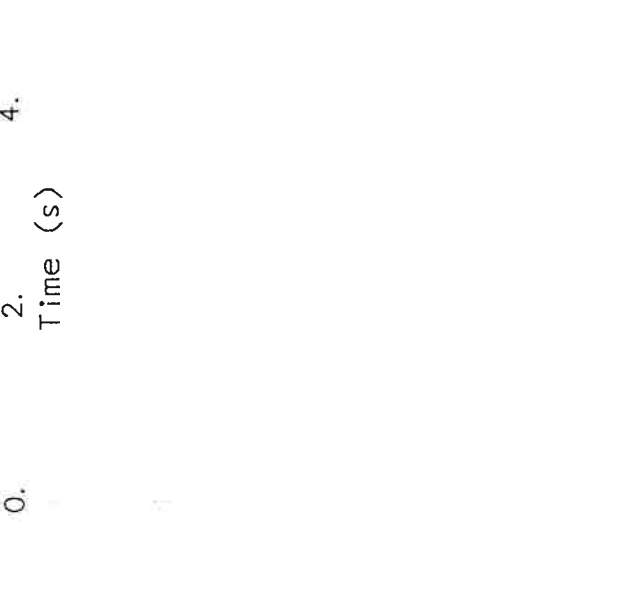
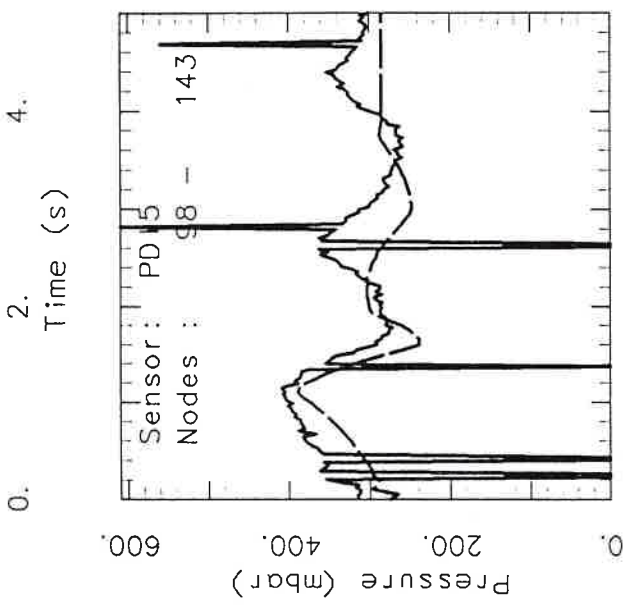
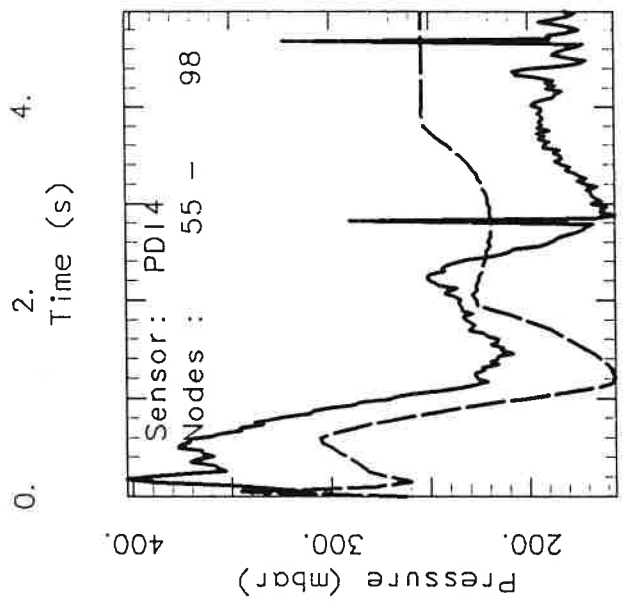
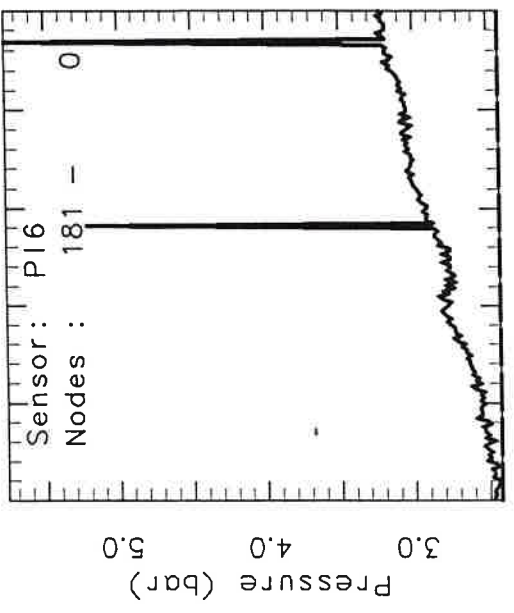
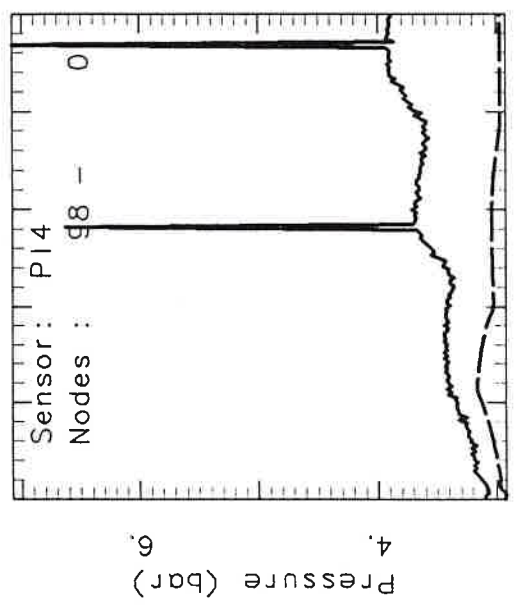
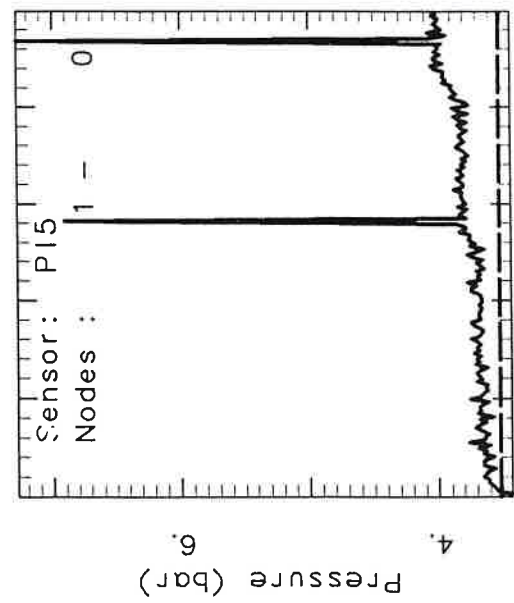
5

SIM # 45. t_{in}=0.20 mm. ISS 3 m_{it}. Min htc. rho=1.80e-10. 1-D run



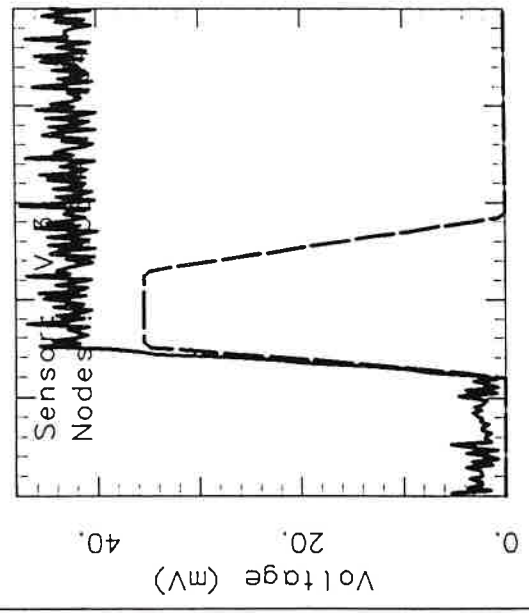
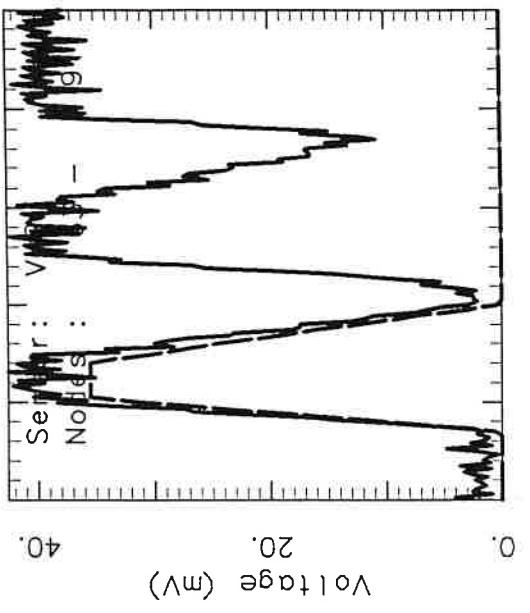
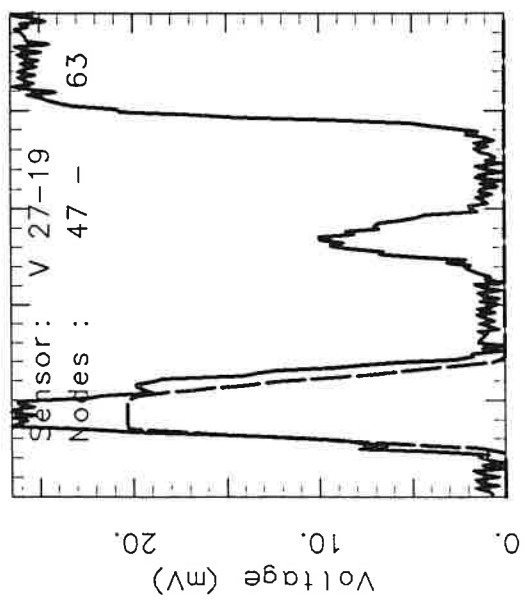
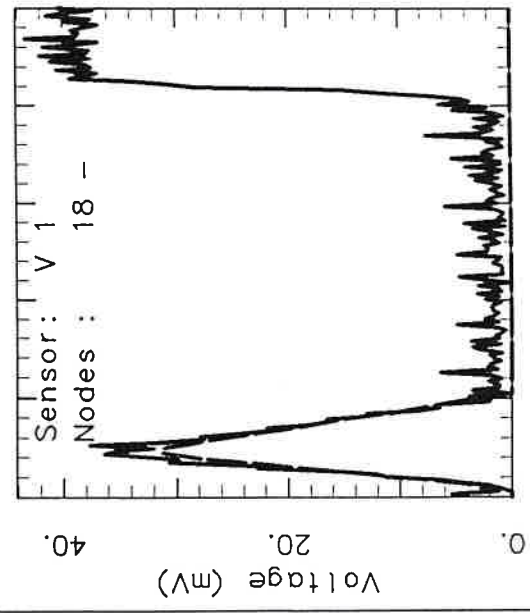
9

SIM # 45. t_{in}=0.20 mm. TSS 3 m_{it}. Min htc. rho=1.80e-10. 1-D run



SIM # 45. t_{in}=0.20 mm. TSS 3 m+it. Min htc. rho=1.80e-10. 1-D run

9



0. 2. 4. Time (s)

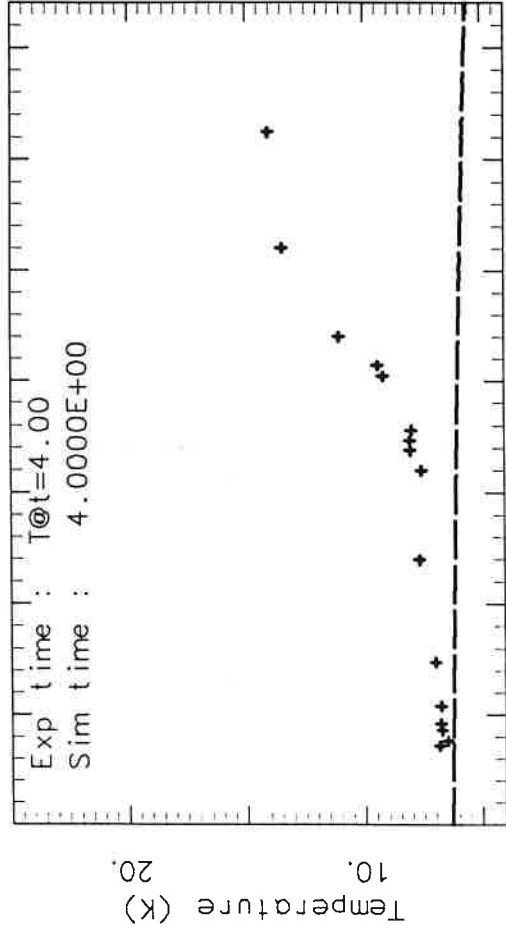
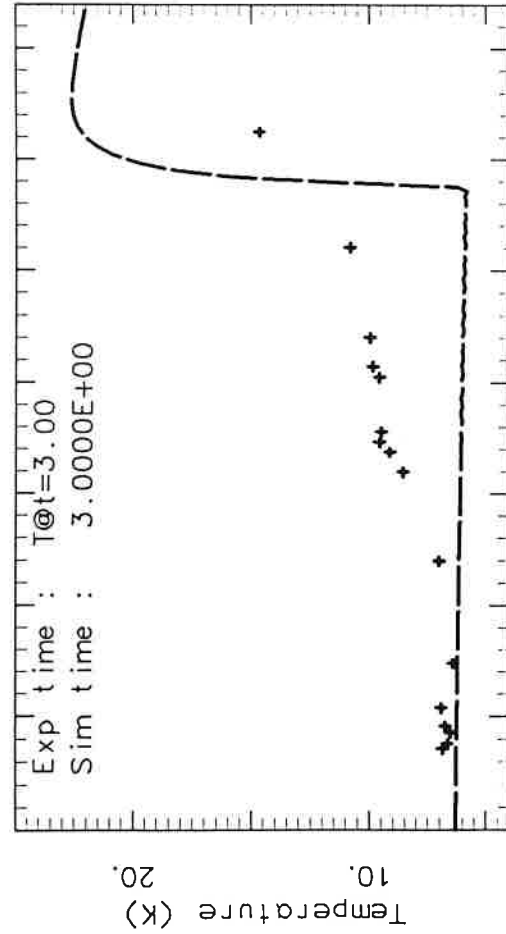
0. 2. 4. Time (s)

0. 2. 4. Time (s)

0. 2. 4. Time (s)

9

SIM # 45. t-in=0.20 mm. TSS 3 m-it. Min htc. rho=1.80e-10. 1-D run



Conclusion



A good amount of runs already performed (xxx CRAY-hrs)

⇒ nice looking curves

⇒ several things learned on the capabilities and limitations.

Influence of: conductor properties
boundary conditions

Choice of integrator

Higher confidence in the code

⇒ a nerve-consuming exercise highly recommended



Good inputs (experiments) are needed for good validation

⇒ *stimulating* way of designing experiments (so that data can be used)